

Argonne National Laboratory

**RESULTS OBTAINED FROM THE FRICKE
DIFFUSION KINETICS CODE**

by

**Erwin H. Bareiss, Cynthia Chamot,
and Hugo Fricke**

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ABSTRACT

The Diffusion Kinetics codes described by the authors in ANL-6556 were used to study hypothetical reactions of free radicals produced by passing α rays and γ rays through aqueous solutions. Tables and graphs of results are given for about 200 cases run on the IBM 704 with various parameter combinations. Intermediate as well as final concentrations are given for some γ -ray cases.

INTRODUCTION

The IBM 704 Diffusion Kinetics codes⁽¹⁾ were used for over 200 cases to study from two to four primary reactions involving free radicals, and also a secondary reaction. Cases were run to determine values of various parameters, giving results, R_1 and R_2 , consistent with those obtained experimentally for water and for water:iodine:iodide systems. Other parameters were varied to study their effects. In this report, results are tabulated and a large number of graphs are included to illustrate various effects. Also, some results of the previous Avidac codes⁽²⁾ are included for comparison.

Complete output was normally obtained; so reactions of interest may be traced over all space up to the time they were removed from the machine. Although most α -ray cases ($\epsilon = 1$ for cylindrical symmetry) were run until the reaction was complete, some of the first cases were not allowed to finish, but those reactions can be followed part way to $T = 0.001$. Complete output is available for several γ -ray cases ($\epsilon = 2$ for spherical symmetry) which were run to completion. However, it was profitable to stop many of these cases at $T = 0.1$, since final concentrations of reaction products could be obtained by extrapolation.

The actual reactions being considered were: $H + H = H_2$; $H + OH = H_2O$; and $OH + OH = H_2O_2$ in all three codes; and $H + I = H^+ + I^-$ and $OH + I^- = OH^- + I$ in code B only; and a secondary reaction, $OH + H_2O_2 = H_2O + HO_2$ in code C only.

For the machine codes, $H = X_1$, $OH = X_2$, $I = X_3$, $I^- = X_4$, and $H_2O_2 = X_4^*$. The amounts of reaction products formed are F_{11} for H_2 , F_{12} for H_2O , F_{22} for H_2O_2 , F_{13} for H^+ , F_{24} for OH^- , and F_{24}^* for HO_2 .

The physical interpretations of the symbols are given in Table I. It should be noted that these are all dimensionless parameters. For further information, see Ref. 1.

Table I

SYMBOLS AND THEIR PHYSICAL MEANINGS

Input Parameters	
Symbol	Definition
β	A measure of the initial scatter of X_1 relative to X_2 .
$\theta_i = D_i/D_1$	The diffusion rate for X_i relative to that of X_1 .
$E = E_R$	A measure of the initial concentration of X_1 . It should be noted that E_M referred to in references 2 and 3 would be $2E_R$.
ϵ	This is 1 for cylindrical symmetry (α rays) and 2 for spherical symmetry (γ rays).
γ_i	Ratio of the initial concentrations of the solutes to the concentration of X_1 at the origin.
$\kappa_{ij} = k_{ij}/k_{11}$	The rate of reaction for X_i combining with X_j relative to that of X_1 with X_1 .
Problem Parameters	
Symbol	Definition
B_i	A measure of the initial concentrations of the solutes, X_3 , and X_4 , incorporated into γ_i for input data.
F_{ij}	Transformed fractional amounts of reaction products formed (or of free radicals remaining if $j=0$).
R	Position in transformed space, going from 1 at the center of the initial free radical concentrations, to 0 far away.
T	Transformed time, going from 1 at time of initial free radical formation, to 0 as real time t increases to ∞ .
$U_i(R, T)$	Transformed concentrations of reactants X_i at various points in space at time T .
Experimentally Determined Quantities (at $T = 0$)	
Symbol	Definition
R_1	$F_{22}/F_{11} = 1.62$ for γ rays with no solute present.
R_2	$(F_{10} + F_{20})/(F_{11} + F_{22}) = 2.40$ for γ rays with no solute present.

Note: The subscripts i and j refer to the reactants X_1 , X_2 , X_3 , or X_4 . The ij combinations are limited to 11, 12, 13, 22, and 24.

SECTION ONE: FINAL RESULTS FOR α -RAY CASES
(CYLINDRICAL GEOMETRY)

Table II gives certain standard parameter values which were common to several cases.

Table III gives some parameter combinations for which the computations were not completed, so that only intermediate results are available.

Table IV gives results for some cases based on Standard I.

Table V gives parameter combinations for cases based on Standard II, with six different values of E. It should be noted that for the smaller values of E, smaller values of B must be used to facilitate the normalizations of curves to $B = 0$.

Tables VI to XI give the final results for the cases in Table V.

Figures 1-22 are graphs of final F_{ij} vs. B and normalized F_{ii} vs. B_{i+2} for each value of E in Table V.

Table II

VALUES OF PARAMETERS FOR STANDARD α -RAY CASES

B_3 and B_4 vary.	ϵ	β	D_2/D_1	D_4/D_1 D_3/D_1	k_{12}/k_{11}	k_{24}/k_{11} k_{13}/k_{11}	k_{22}/k_{11}
STANDARD I	1	1	0.4545	0.15	2	2*	1
STANDARD II	1	1	0.25	0.15	2	2*	0.55

*It should be noted that for 2-radical cases only, k_{13}/k_{11} and k_{24}/k_{11} are set equal to zero.

Table III

PARAMETERS FOR PRELIMINARY α -RAY ($\epsilon = 1$) CASES
WITH TWO RADICALS ONLY (CODE A)

Case No.	β	E	D_2/D_1	k_{12}/k_{11}	k_{22}/k_{11}	
1-1	1	1.8	0.333	2	1	
1-2	1	1.8	0.50	2	1	
1-3	1	1.8	0.667	2	1	
1-4	1	1.8	1.0	2	1	
1-5	1	2.5	0.333	2	1	
1-6	1	2.5	0.50	2	1	
1-7	1	2.5	0.667	2	1	
1-8	1	2.5	1.0	2	1	
26	1	1.97	0.4545	2	1	Standard I

These cases were not computed all the way. Cases No. 1-1 to 1-8 were stopped at $T = 0.001$, when F_{10} and F_{20} were still near 0.05, and No. 26 was run until $T = 10^{-16}$, at which time F_{10} still exceeded 0.01.

Table IV

PARAMETERS AND FINAL RESULTS OF SOME FOUR-COMPONENT CASES
BASED ON STANDARD I WITH $E = 1.97$ AND $\epsilon = 1$ (FOR α RAYS)

Case No.	B_3	B_4	F_{11}	F_{12}	F_{13}	F_{22}	F_{24}
126	10^{-5}	10^{-5}	0.4565	0.4711	0.0724	0.5070	0.0219
127	10^{-3}	10^{-5}	0.4332	0.4567	0.1101	0.5034	0.0399
128	10^{-1}	10^{-5}	0.3312	0.3759	0.2929	0.4653	0.1588
129	1	10^{-5}	0.1788	0.2372	0.5840	0.4086	0.3542
130	10	10^{-5}	0.0404	0.0697	0.8899	0.3621	0.5682
126	10^{-5}	10^{-5}	0.4565	0.4711	0.0724	0.5070	0.0219
132	10^{-5}	10^{-3}	0.4540	0.4566	0.0894	0.4896	0.0538
133	10^{-5}	10^{-1}	0.4240	0.3778	0.1962	0.3778	0.2443
134	10^{-5}	1	0.3789	0.2387	0.3824	0.1951	0.5662
135	10^{-5}	10	0.3426	0.0699	0.5875	0.0413	0.8888

Table V

CASE NUMBERS OF α -RAY CASES WITH STANDARD II PARAMETERS AND SIX VALUES OF E FOR WHICH B_3 AND B_4 VARY

$E = 5.305$		B_4						
		10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
B_3	10	580			525			
	1	581			526			
	0.1				527			
	10^{-3}	582			528			
	10^{-5}	520	521	522	523	524		
	10^{-7}							
	10^{-10}							

$E = 0.675$		B_4						
		10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
B_3	10	585			555			
	1	586			556			
	0.1				557			
	10^{-3}	587			558			
	10^{-5}	550	551	552	553	554	517	
	10^{-7}							
	10^{-10}							
	10^{-15}							515A

$E = 2.48$		B_4						
		10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
B_3	10	505			535			
	1	506			536			
	0.1				537			
	10^{-3}	507			538			
	10^{-5}	508	532	533	534	509		
	10^{-7}							
	10^{-10}							

$E = 0.3535$		B_4						
		10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
B_3	10	500			565			
	1	501			566			
	0.1				567			
	10^{-3}	502			568			
	10^{-5}	503	561	562	563	564	519	
	10^{-7}							
	10^{-10}							
	10^{-15}							529

$E = 1.29$		B_4						
		10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
B_3	10							
	1							
	0.1							
	10^{-3}							
	10^{-5}							
	10^{-7}							
	10^{-10}							

$E = 0.1875$		B_4						
		10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
B_3	10	590			575			
	1	591			576			
	0.1				577			
	10^{-3}	592			578			
	10^{-5}	572	573	574	595	579		
	10^{-7}							
	10^{-10}							
	10^{-15}							512

Table VI

RESULTS FOR STANDARD II AND $E_R = 5.305$ ($E_M = 10.61$)

Case No.	520	521	522	523	524
$B_3 = 10^{-5}$ $B_4 =$	10	1	0.1	10^{-3}	10^{-5}
F_{11}	0.35475	0.38508	0.40787	0.41951	0.42131
F_{12}	0.14213	0.36699	0.48859	0.53667	0.54404
F_{13}	0.5031	0.2479	0.1035	0.0438	0.0347
F_{22}	0.05295	0.21260	0.36252	0.43966	0.45048
F_{24}	0.8049	0.4204	0.1489	0.0237	0.0055

Case No.	525	526	527	528	524
$B_4 = 10^{-5}$ $B_3 =$	10	1	10^{-1}	10^{-3}	10^{-5}
F_{11}	0.08592	0.26192	0.37117	0.41371	0.42131
F_{12}	0.14327	0.36144	0.48488	0.53603	0.54404
F_{13}	0.7708	0.3766	0.1440	0.0503	0.0347
F_{22}	0.28252	0.35229	0.41697	0.44714	0.45048
F_{24}	0.5742	0.2863	0.0982	0.0168	0.0055

Case No.	580	581	582	583	524
$B_3 = B_4 =$	10	1	10^{-1}	10^{-3}	10^{-5}
F_{11}	0.08785	0.26150	0.36887	0.41355	0.42131
F_{12}	0.09246	0.30574	0.46292	0.53402	0.54404
F_{13}	0.8197	0.4328	0.1682	0.0524	0.0347
F_{22}	0.05369	0.20501	0.35512	0.43907	0.45048
F_{24}	0.8539	0.4893	0.1820	0.0269	0.0055

Table VII

RESULTS FOR STANDARD II AND $E_R = 2.48$ ($E_M = 4.96$)

Case No.	530	531	532	533	534
$B_3 = 10^{-5}$ $B_4 =$	10	1	0.1	10^{-3}	10^{-5}
F_{11}	0.34104	0.36493	0.39316	0.41169	0.41284
F_{12}	0.08548	0.28650	0.44167	0.51852	0.53033
F_{13}	0.5735	0.3486	0.1652	0.0698	0.0568
F_{22}	0.02886	0.14926	0.31906	0.43293	0.44942
F_{24}	0.8857	0.5642	0.2393	0.0486	0.0203

Case No.	535	536	537	538	534
$B_4 = 10^{-5}$ $B_3 =$	10	1	0.1	10^{-3}	10^{-5}
F_{11}	0.04871	0.19602	0.32785	0.39924	0.41284
F_{12}	0.08620	0.28473	0.43688	0.51771	0.53033
F_{13}	0.8651	0.5193	0.2353	0.0831	0.0568
F_{22}	0.27090	0.33118	0.40221	0.44568	0.44942
F_{24}	0.6429	0.3841	0.1609	0.0366	0.0203

Case No.	505	506	507	508	534	509
$B_3 = B_4 =$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}
F_{11}	0.04862	0.19410	0.32542	0.39883	0.41284	0.41849
F_{12}	0.05036	0.22234	0.40597	0.51379	0.53033	0.53569
F_{13}	0.9010	0.5836	0.2686	0.0874	0.0568	0.0458
F_{22}	0.02874	0.14500	0.31140	0.43202	0.44942	0.45400
F_{24}	0.9209	0.6327	0.2826	0.0542	0.0203	0.0103

Table VIII

RESULTS FOR STANDARD II AND $E_R = 1.29$ ($E_M = 2.58$)

Case No.	540	541	542	543	544	539	539A
$B_3 = 10^{-5}$ $B_4 =$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
F_{11}	0.32624	0.34420	0.37382	0.39781	0.39950	0.39971	0.39971
F_{12}	0.05056	0.21258	0.38402	0.49168	0.51141	0.51345	0.51347
F_{13}	0.6232	0.4432	0.2422	0.1105	0.0891	0.0868	0.0868
F_{22}	0.01601	0.10080	0.26972	0.42124	0.44738	0.45388	0.4555
F_{24}	0.9334	0.6866	0.3463	0.0871	0.0412	0.0327	0.0310

Table IX

RESULTS FOR STANDARD II AND $E_R = 0.675$ ($E_M = 1.35$)

Case No.	550	551	552	553	554	589	516
$B_3 \times 10^{-5}$ $B_4 \times$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
F11	0.30916	0.32088	0.34703	0.37357	0.37578		0.37599
F12	0.02862	0.14513	0.31251	0.45098	0.48198		0.48523
F13	0.6622	0.5540	0.3405	0.1755	0.1422		0.1388
F22	0.00869	0.06321	0.21220	0.39945	0.44012		0.45411
F24	0.9627	0.7917	0.4753	0.1496	0.0779		0.0607

Case No.	555	556	557	558	554	559	517
$B_4 \times 10^{-5}$ $B_3 \times$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
F11	0.01508	0.08864	0.21464	0.33913	0.37578		0.40493
F12	0.02874	0.14462	0.30713	0.44916	0.48198		0.48540
F13	0.9562	0.7667	0.4782	0.2117	0.1422		0.1097
F22	0.253	0.29279	0.36365	0.43152	0.44012		0.44039
F24	0.7183	0.5626	0.3292	0.1193	0.0779		0.0742

Case No.	585	586	587	588	554	584	515	515A
$B_3 + B_4 \times$	10	1	10^{-1}	10^{-3}	10^{-5}	10^{-7}	10^{-10}	10^{-15}
F11	0.01508	0.08831	0.21340	0.33863	0.37578		0.40664	0.41845
F12	0.01542	0.09873	0.26614	0.44017	0.48198		0.50865	0.51636
F13	0.9695	0.8130	0.5205	0.2212	0.1422		0.0847	0.0652
F22	0.00868	0.06245	0.20730	0.39793	0.44012		0.46086	0.46532
F24	0.9759	0.8388	0.5266	0.1619	0.0779		0.0305	0.0183

Table X

RESULTS FOR STANDARD II AND $E_R = 0.3535$ ($E_M = 0.707$)

Case No.	560	561	562	563	564	504	518
$B_3 \times 10^{-5}$ $B_4 \times$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
F11	0.28622	0.29286	0.31130	0.33540	0.33788		0.33807
F12	0.01569	0.09153	0.23386	0.39338	0.43833		0.44321
F13	0.6981	0.6156	0.4548	0.2712	0.2238		0.2187
F22	0.00864	0.03724	0.15283	0.36163	0.42189		0.44632
F24	0.9797	0.8712	0.6133	0.2450	0.1398		0.1105

Case No.	565	566	567	568	564	569	519
$B_4 \times 10^{-5}$ $B_3 \times$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}
F11	0.00810	0.05315	0.15280	0.28750	0.33788		0.38250
F12	0.01573	0.09126	0.22971	0.39111	0.43833		0.44359
F13	0.9762	0.8556	0.6175	0.3214	0.2238		0.1739
F22	0.24639	0.27445	0.33569	0.41043	0.42189		0.42225
F24	0.379	0.6343	0.4346	0.1985	0.1398		0.1342

Case No.	500	501	502	503	564	513	514	529
$B_4 \times B_3 \times$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}	10^{-15}
F11	0.00810	0.05306	0.15215	0.28708	0.33788		0.38495	0.40411
F12	0.00826	0.05892	0.19047	0.37904	0.43833		0.48157	0.49513
F13	0.9836	0.8880	0.6574	0.3339	0.2238		0.1335	0.1008
F22	0.00864	0.03698	0.14996	0.35999	0.42189		0.45748	0.46596
F24	0.9871	0.9041	0.6596	0.2610	0.1398		0.0610	0.0389

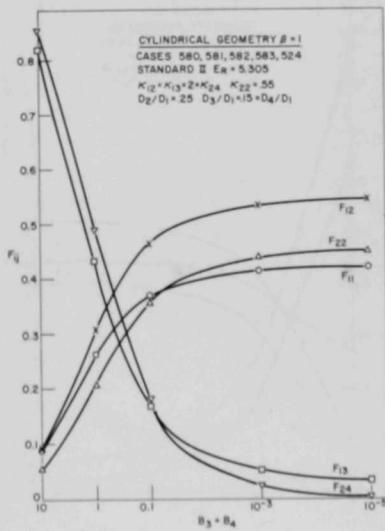
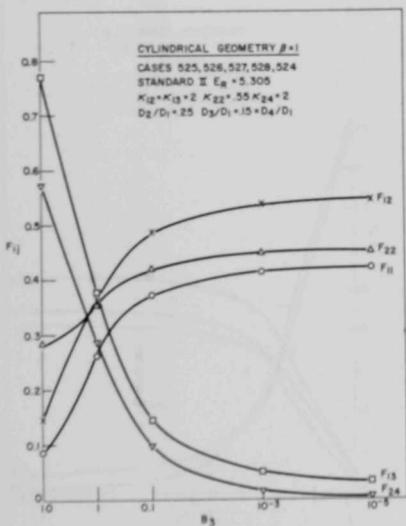
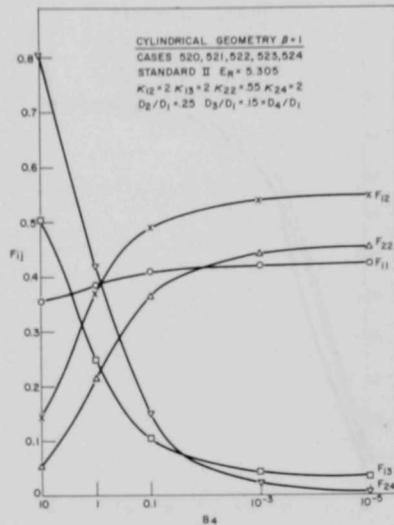
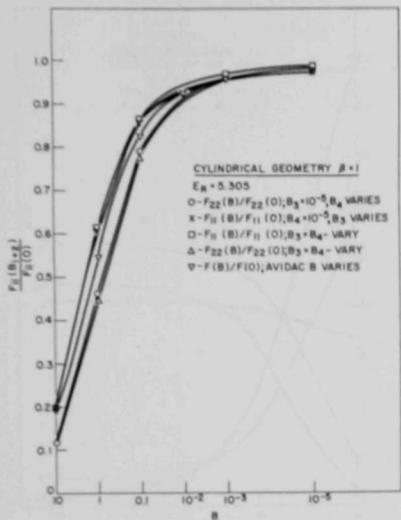
Table XI

RESULTS FOR STANDARD II AND ER = 0.1875 (EM = 0.375)

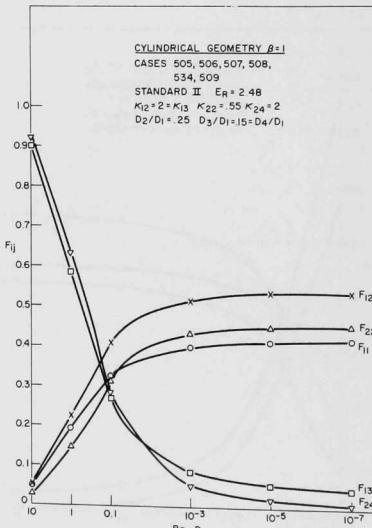
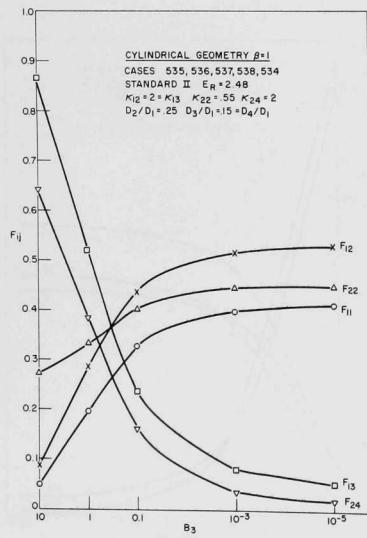
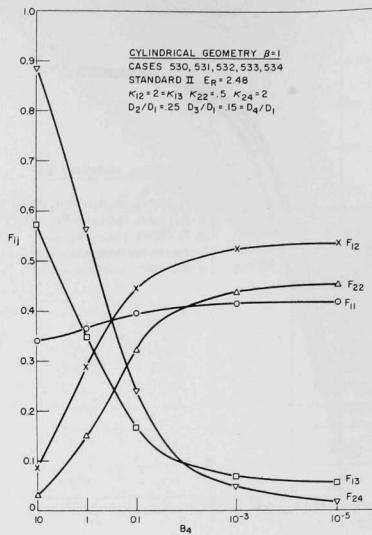
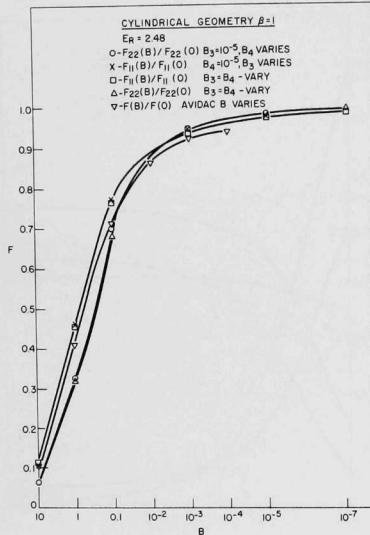
Case No.	570	571	572	573	574	595	596	597
$B_3 = 10^{-5}$ $B_4 =$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}	10^{-15}
F_{11}	0.25275	0.25595	0.26637	0.28365	0.28590	0.28597		0.28605
F_{12}	0.00853	0.05458	0.16093	0.32126	0.37912	0.38558		0.38579
F_{13}	0.7387	0.6895	0.5727	0.3951	0.3350	0.3285		0.3282
F_{22}	0.00249	0.02118	0.10130	0.30567	0.38629	0.4156		0.43026
F_{24}	0.9890	0.9242	0.7378	0.3731	0.2346	0.1988		0.1840

Case No.	575	576	577	578	574	594	598	599
$B_4 = 10^{-5}$ $B_3 =$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}	10^{-15}
F_{11}	0.00436	0.03055	0.10035	0.22601	0.28590			0.36987
F_{12}	0.00854	0.05447	0.15836	0.31895	0.37912			0.38638
F_{13}	0.9871	0.9150	0.7413	0.4550	0.3350			0.2438
F_{22}	0.23493	0.25395	0.30141	0.37313	0.38629			0.38672
F_{24}	0.7565	0.6916	0.5402	0.3079	0.2346			0.2269

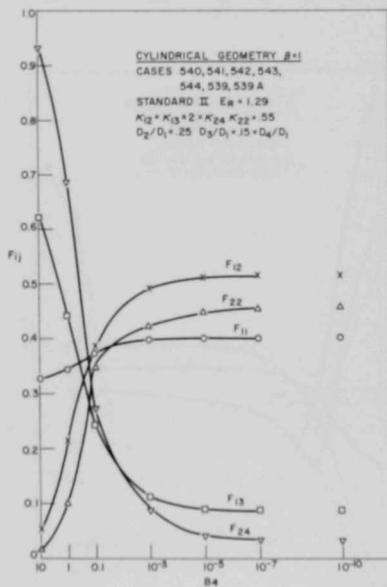
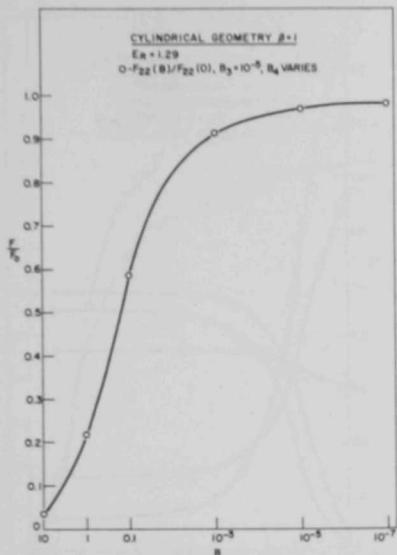
Case No.	590	591	592	593	574		579	512
$B_3 = B_4 =$	10	1	0.1	10^{-3}	10^{-5}		10^{-10}	10^{-15}
F_{11}	0.00436	0.03053	0.10010	0.22572	0.28590		0.3497	0.3779
F_{12}	0.00444	0.03377	0.12582	0.30462	0.37912		0.4432	0.4655
F_{13}	0.9912	0.9357	0.7741	0.4697	0.3350		0.2071	0.1566
F_{22}	0.00249	0.02110	0.09993	0.30421	0.38629		0.4437	0.4574
F_{24}	0.9931	0.9451	0.7743	0.3912	0.2346		0.1131	0.0771



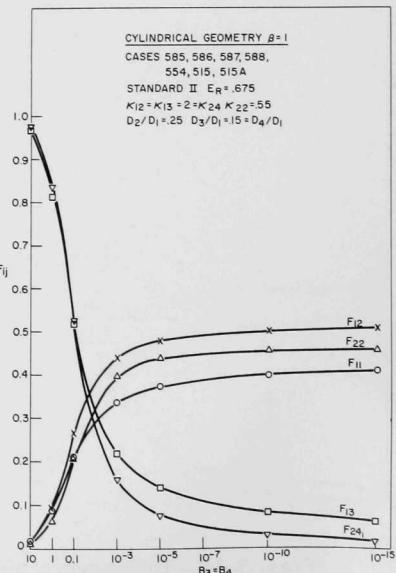
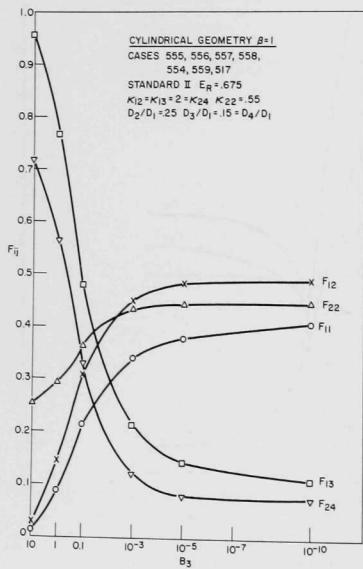
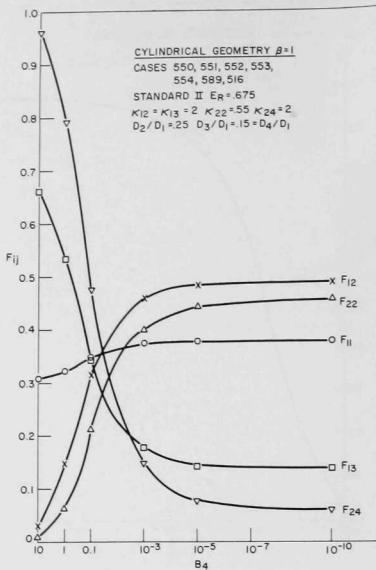
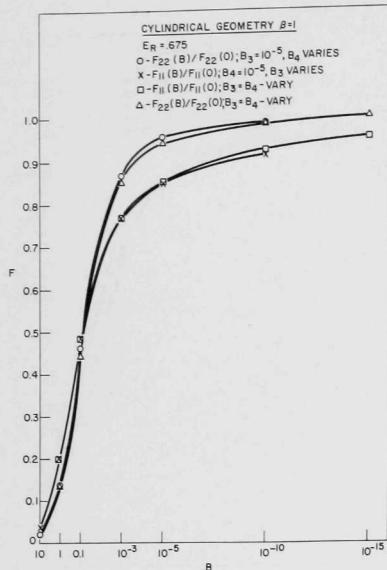
Figs. 1-4. Dependence of Normalized Recombination Fractions on B_i ($E = 5.305$)



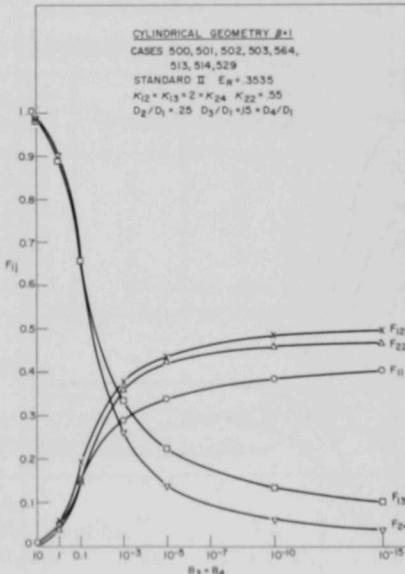
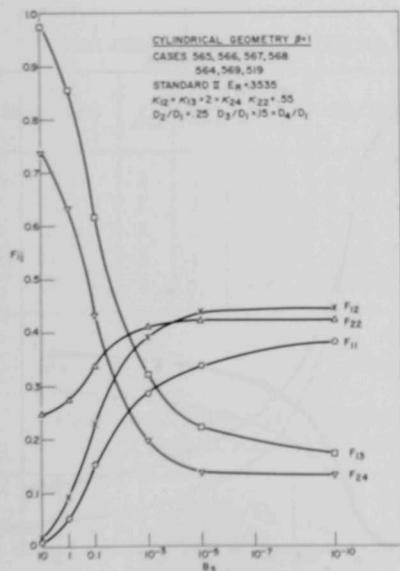
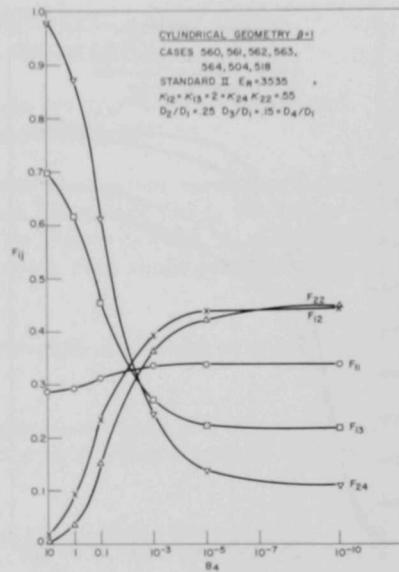
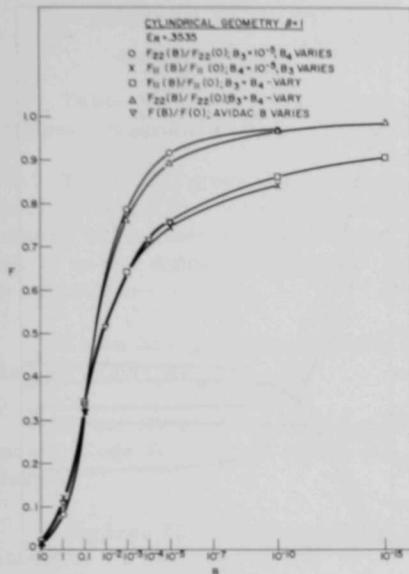
Figs. 5-8. Dependence of Normalized Recombination Fractions on B_i ($E = 2.48$)



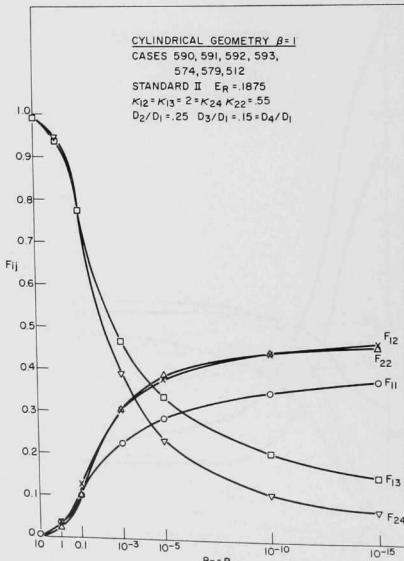
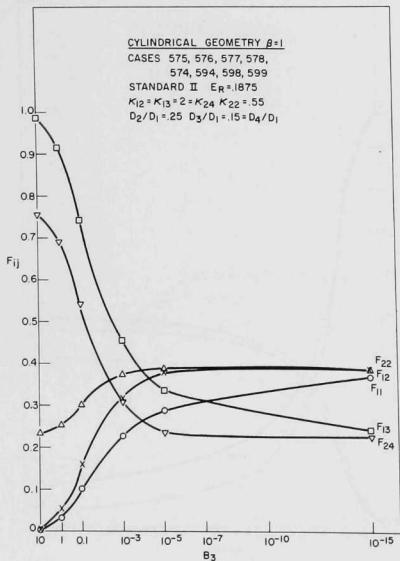
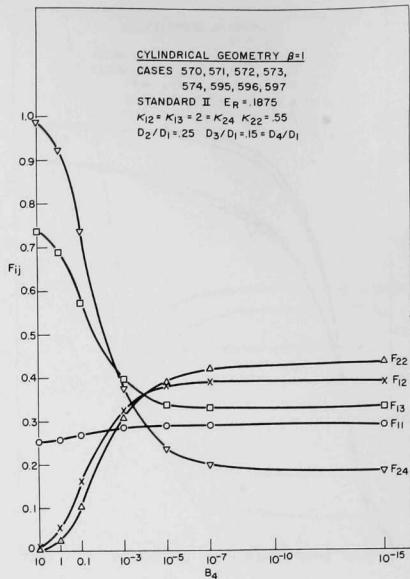
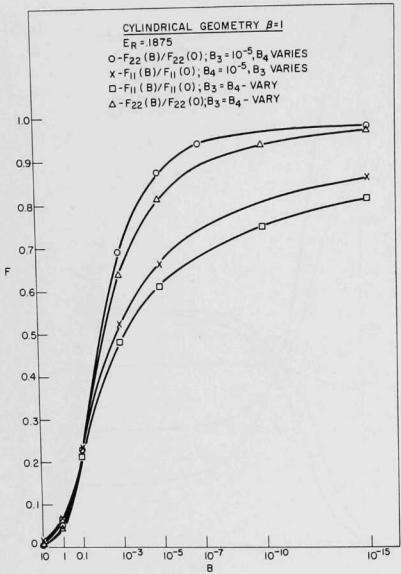
Figs. 9-10. Dependence of Normalized Recombination Fractions on B_i ($E = 1.29$)



Figs. 11-14. Dependence of Normalized Recombination Fractions on B_i ($E = 0.675$)



Figs. 15-18. Dependence of Normalized Recombination Fractions on B_i ($E = 0.3535$)



Figs. 19-22. Dependence of Normalized Recombination Fractions on B_i ($E = 0.1875$)

SECTION TWO: FINAL RESULTS FOR γ -RAY CASES
(SPHERICAL GEOMETRY)

Table XII gives the standard values for five sets of parameter combinations which were investigated most thoroughly.

Table XIII gives values of parameters used for some preliminary spherical cases limited to one radical and one solute (Code B). Comparisons were made with previous runs by Flanders (Ref. 2) and Phillips (Ref. 3) on the Avidac and George, with codes that could accommodate only two reactions.

Table XIV gives parameters and results for cases with two radicals only (Code A).

Table XV gives results for the spherical cases run with four components (Code B), most of which are based on the five standard sets of values.

Figures 23-35 are graphs of final F_{ij} vs B for the cases in Table XV.

Table XII

VALUES OF PARAMETERS FOR STANDARD γ -RAY CASES

Standard	ϵ	β	E	D_2/D_1	D_4/D_1 D_3/D_1	k_{12}/k_{11}	k_{24}/k_{11} k_{13}/k_{11}	k_{22}/k_{11}
I	2	1	0.87	0.4545	0.15	2	2	1
II	2	1	0.87	0.25	0.15	2	2	0.55
III	2	1	0.91	0.25	0.15	4	2	0.60
IV	2	1	0.87	0.25	0.15	1	2	0.55
V	2	1	0.87	0.125	0.15	2	2	0.30

Table XIII

PARAMETERS AND RESULTS FOR CASES WITH ONLY ONE RADICAL (WITH AND WITHOUT A SOLUTE)

Case	ϵ	β	E	D_4/D_1 D_2/D_1	D_3/D_1	k_{24}/k_{11} k_{22}/k_{11} k_{12}/k_{11}	k_{13}/k_{11}	T_f	F_{11}	F_{13} or F_{10}
DP	2	1	2.5	0	1	0	1	0.17	0.1505	0.8495
DAF	2	1	2.5	0	0	0	0	0.05	0.430	0.570

Table XIV

SPHERICAL CASES WITH TWO COMPONENTS ONLY

β	Case No.	E	D ₂ /D ₁	k ₁₂ /k ₁₁	k ₂₂ /k ₁₁	F ₁₁	F ₁₂	F ₂₂	F ₁₀	F ₂₀	R ₁	R ₂
1	2-1	1.8	0.3333	2	1	0.2477	0.2999	0.4238	0.4525	0.2764	1.711	1.086
1	2-2	1.8	0.5	2	1	0.2503	0.2939	0.3697	0.4558	0.3365	1.477	1.278
1	2-3	1.8	0.6667	2	1	0.2539	0.2858	0.3302	0.4603	0.3840	1.300	1.445
1	2-4	1.8	1	2	1	0.2615	0.2615	0.2615	0.4771	0.4771	1.000	1.825
1	2-5	2.5	0.3333	2	1	0.2810	0.3317	0.4485	0.3873	0.2198	1.596	0.832
1	2-6	2.5	0.5	2	1	0.2846	0.3279	0.4016	0.3876	0.2705	1.411	0.959
1	2-7	2.5	0.6667	2	1	0.2886	0.3208	0.3649	0.3907	0.3143	1.265	1.079
1	2-8	2.5	1	2	1	0.2972	0.2972	0.2972	0.4056	0.4056	1.000	1.365
1	2-9	3.2	0.3333	2	1	0.3053	0.3543	0.4641	0.3404	0.1816	1.520	0.678
1	2-10	3.2	0.5	2	1	0.3089	0.3513	0.4221	0.3398	0.2267	1.366	0.775
1	2-11	3.2	0.6667	2	1	0.3131	0.3448	0.3879	0.3420	0.2672	1.239	0.869
1	2-12	3.2	1	2	1	0.3224	0.3224	0.3224	0.3552	0.3552	1.000	1.102
1	1	1.25	0.3333	2	1	0.2094	0.2604	0.3861	0.5302	0.3535	1.844	1.484
1	2	1.25	0.5	2	1	0.2114	0.2535	0.3285	0.5352	0.4180	1.554	1.766
1	3	1.25	0.6667	2	1	0.2144	0.2441	0.2875	0.5410	0.4678	1.341	2.010
1	4	1.25	1	2	1	0.2201	0.2201	0.2201	0.5599	0.5599	1.000	2.544
1	5	0.6	0.333	2	1	0.1365	0.1803	0.2948	0.6832	0.5249	2.160	2.801
1	6	0.6	0.5	2	1	0.1381	0.1714	0.2334	0.6905	0.5952	1.690	3.461
1	7	0.6	0.6667	2	1	0.1398	0.1623	0.1948	0.6979	0.6429	1.393	4.007
1	8	0.6	1	2	1	0.1423	0.1423	0.1423	0.7154	0.7154	1.000	5.027
1	10	0.8	0.45	2	1	0.1651	0.2053	0.2857	0.6296	0.5090	1.731	2.526
1	11	0.8	0.5	2	1	0.1658	0.2026	0.2701	0.6317	0.5273	1.629	2.659
1	251	0.87	0.4545	1.5	0.5	0.1812	0.1854	0.1943	0.6335	0.6204	1.072	3.340
2	252	0.87	0.4545	2	1	0.1659	0.2060	0.4384	0.6281	0.3556	2.642	1.628
1	253	0.87	0.4545	2	1	0.1737	0.2145	0.2951	0.6118	0.4904	1.699	2.351
2	254	0.87	0.25	1.3	0.3	0.1746	0.1860	0.2280	0.6394	0.5859	1.306	3.043
1	255	0.87	0.4545	2	1	0.1708	0.2236	0.3904	0.6056	0.3860	2.286	1.767
1	256	0.87	0.25	1.75	0.75	0.1776	0.2007	0.2511	0.6217	0.5482	1.413	2.729
1	257	0.87	0.25	2	0.55	0.1670	0.2412	0.2735	0.5918	0.4853	1.637	2.445
1	258	1.10	0.25	1.25	0.25	0.2102	0.2081	0.2004	0.5817	0.5915	0.953	2.857
1	259	0.75	0.25	3.125	1	0.1388	0.2871	0.3289	0.5741	0.3840	2.370	2.048
1	260	0.8	0.25	1	0.5	0.1814	0.1344	0.2874	0.6842	0.5782	1.584	2.693
1	261	0.8	0.25	2	0.5	0.1589	0.2331	0.2476	0.6080	0.5193	1.558	2.773
1	262	0.8	0.25	4	0.5	0.1282	0.3697	0.1938	0.5021	0.4365	1.512	2.915
1	263	0.89	0.25	2	0.53	0.1690	0.2450	0.2265	0.5860	0.4856	1.594	2.444
1	264	0.87	0.125	2	0.55	0.1651	0.2434	0.3264	0.5915	0.3810	2.274	1.798
1	265	0.87	0.25	1	0.55	0.1918	0.1397	0.3844	0.6685	0.5417	1.661	2.371
1	266	0.435	0.25	2	0.55	0.1073	0.1602	0.1416	0.7325	0.6456	1.810	4.902
1	267	0.87	0.25	2	0.275	0.1649	0.2558	0.0883	0.5793	0.5784	1.006	3.501
1	268	0.87	0.25	4	0.55	0.1337	0.3802	0.0759	0.4861	0.4107	1.564	2.615
1	269	0.87	0.5	2	0.55	0.1711	0.2265	0.1843	0.6024	0.5893	1.077	3.353
1	270	1.74	0.25	2	0.55	0.2340	0.3264	0.3426	0.4397	0.3310	1.465	1.337
1	271	0.91	0.25	4	0.6	0.1370	0.3844	0.2293	0.4787	0.3864	1.674	2.362
1	272	0.87	0.125	1	0.55	0.1879	0.1416	0.4381	0.6706	0.4203	2.332	1.743
1	273	0.435	0.25	1	0.55	0.1175	0.0883	0.2154	0.7942	0.6963	1.834	4.477
1	274	0.87	0.25	0.5	0.55	0.2075	0.0759	0.3473	0.7166	0.5768	1.674	2.331
1	275	0.87	0.25	1	0.275	0.1902	0.1499	0.1968	0.6599	0.6533	1.035	3.394
1	276	1.74	0.25	1	0.55	0.2827	0.1990	0.4192	0.5183	0.3818	1.483	1.282
1	279	0.75	0.125	2	0.275	0.1496	0.2414	0.2341	0.6090	0.5245	1.565	2.954
1	280	0.87	0.125	2	0.30	0.1629	0.2592	0.2633	0.5780	0.4775	1.616	2.476
0.5	281	0.87	0.25	2	0.275	0.275						
2	282	0.87	0.25	2	0.275	0.1531	0.2622	0.2808	0.5847	0.4571	1.834	2.401
1	283	0.87	0.25	2	1.10	0.1712	0.2199	0.4096	0.6089	0.3705	2.392	1.686
0.5	284	0.87	0.25	2	0.55							
2	285	0.87	0.25	2	0.55	0.1586	0.2335	0.4157	0.6079	0.3508	2.621	1.669

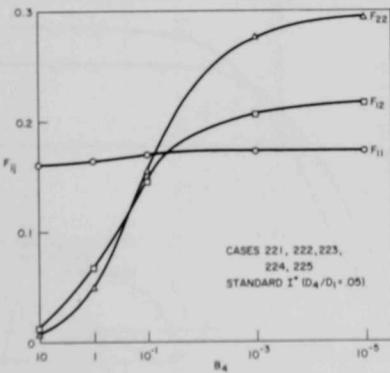
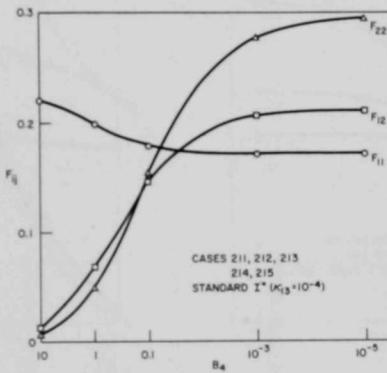
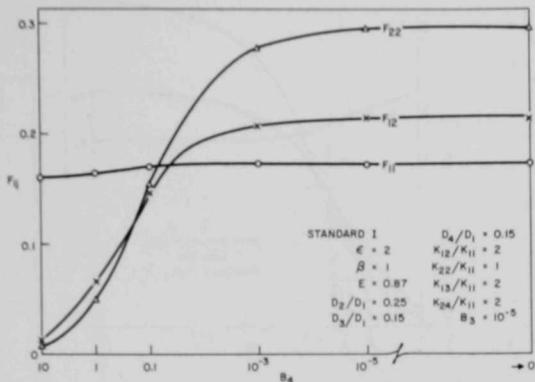
Table XII
RESULTS FOR 4-COMPONENT γ -RAY CASES

Case No.	Deviation from Standard I			B_3 or B_4 Variable B	Calculated Concentrations & Corrected				
	E	D	Constant B		F ₁₁	F ₁₂	F ₂₂	F ₁₃	F ₂₄
{101 102 103 104 109}	0.8	$D_2/D_1 = 0.4$	$B_4 \times 10^{-5}$	$B_3 \times 10^{-5}$	0.1629	0.2067	0.3031	0.6404	0.4902
				10^{-3}	0.1557	0.1997	0.3026	0.6447	0.4977
				10^{-1}	0.0989	0.1382	0.2879	0.7629	0.5738
				1	0.0385	0.0626	0.2624	0.8990	0.6750
				10	0.0062	0.0120	0.2452	0.9818	0.7428
				$B_4 \times 10^{-5}$	$B_3 \geq 10^{-5}$	0.1720	0.2134	0.2950	0.6146
{105 106 107 108 110}	0.1	$D_2/D_1 = 1.0$	$B_3 \geq 10^{-5}$	$B_4 \geq 10^{-5}$	0.1642	0.2059	0.2946	0.6299	0.4995
				$\geq 10^{-3}$	0.1032	0.1415	0.2806	0.7553	0.5778
				$\geq 10^{-1}$	0.0394	0.0634	0.2567	0.8972	0.6798
				1	0.0064	0.0121	0.2414	0.9815	0.7464
				≥ 10	-	0.0118	0.0064	-	0.9818
{116 117 118 119 120}	-	$D_2/D_1 = 1.0$	$B_3 \geq 10^{-5}$	$B_4 \geq 10^{-5}$	0.1794	0.1794	0.1794	0.6412	0.6412
				$\geq 10^{-3}$	0.1793	0.1735	0.1708	0.6417	0.6557
				$\geq 10^{-1}$	0.1755	0.1226	0.1056	0.7018	0.7718
				1	0.1675	0.0579	0.0396	0.7745	0.9025
				≥ 10	-	0.0118	0.0064	-	0.9818
{105 122 123 124 125}	-	$D_2/D_1 = 1.0$	$B_3 \geq 10^{-5}$	$B_4 \geq 10^{-5}$	0.1720	0.2134	0.2950	0.6146	0.4916
				$\geq 10^{-3}$	0.1719	0.2061	0.2768	0.6219	0.5171
				$\geq 10^{-1}$	0.1693	0.1428	0.1507	0.6878	0.7065
				1	0.1640	0.0639	0.0470	0.7720	0.8891
				≥ 10	0.1607	0.0121	0.0066	0.8271	0.9812
Standard I Case									
{141 142 143 144 145}	$E = 0.87$ $D_2 = 0.4545$	$K_{12} \cdot 2$ $K_{13} \cdot 2$ $K_{22} \cdot 1$ $K_{24} \cdot 2$	$B_3 = 10^{-5}$	$B_4 = 10^{-5}$	0.1720	0.2135	0.2951	0.6145	0.4915
				10^{-3}	0.1720	0.2065	0.2776	0.6216	0.5160
				10^{-1}	0.1695	0.1452	0.1547	0.6853	0.7000
				1	0.1642	0.0668	0.0498	0.7690	0.8834
				10	0.1603	0.0129	0.0070	0.8267	0.9800
	K	E	D	$B_3 = 10^{-5}$ Variable B_4					
{151 152 153 154 155}	$K_{13} \cdot 10^{-2}$		$D_2/D_1 = 0.4545$	10^{-5}	0.1718	0.2132	0.2947	0.6150	0.4921
				10^{-3}	0.1720	0.2063	0.2772	0.6217	0.5164
				10^{-1}	0.1792	0.1470	0.1547	0.6738	0.6984
				1	0.1987	0.0681	0.0497	0.7331	0.8822
				10	0.2185	0.0130	0.0070	0.7685	0.9800
{203 202 201}			$D_2/D_1 = 0.4545$	10^{-5}	0.1720	0.2135	0.2951	0.6145	0.4914
				10^{-1}	0.1709	0.1454	0.1547	0.6837	0.6998
				10	0.1663	0.0129	0.0070	0.8207	0.9800
{208 207 206}			$D_2/D_1 = 0.4545$	10^{-5}	0.1720	0.2135	0.2951	0.6145	0.4914
				10^{-1}	0.1695	0.1448	0.1541	0.6856	0.7011
				10	0.1603	0.0129	0.0070	0.8267	0.9800
{211 212 213 214 215}	$K_{13} \cdot 10^{-4}$		$D_2/D_1 = 0$	10^{-5}	0.1720	0.2135	0.2951	0.6145	0.4914
				10^{-3}	0.1722	0.2066	0.2776	0.6211	0.5158
				10^{-1}	0.1795	0.1471	0.1548	0.6733	0.6980
				1	0.1993	0.0682	0.0498	0.7325	0.8820
				10	0.2197	0.0133	0.0072	0.7670	0.9796
216	$K_{13} \cdot 10^{-2}$		$D_2/D_1 = 0$	10	-	0.0132	0.0072	-	-
{221 222 223 224 225}			$D_2/D_1 = 0.05$	10^{-5}	0.1720	0.2135	0.2951	0.6145	0.4915
				10^{-3}	0.1728*	0.2063*	0.2760*	0.6208*	0.5177*
				10^{-1}	0.1695	0.1453	0.1550	0.6851	0.6997
				1	0.1642	0.0668	0.0498	0.7690	0.8833
				10	0.1603	0.0129	0.0070	0.8267	0.9800
{231 232 233 234 235}	$K_{24} \cdot 0.02$		$D_2/D_1 = 0$	10^{-5}	0.1720	0.2135	0.2951	0.6145	0.4915
				10^{-3}	0.1720	0.2063	0.2770	0.6217	0.5167
				10^{-1}	0.1694	0.1431	0.1507	0.6875	0.7061
				1	0.1641	0.0654	0.0485	0.7704	0.8861
				10	0.1603	0.0128	0.0070	0.8268	0.9802

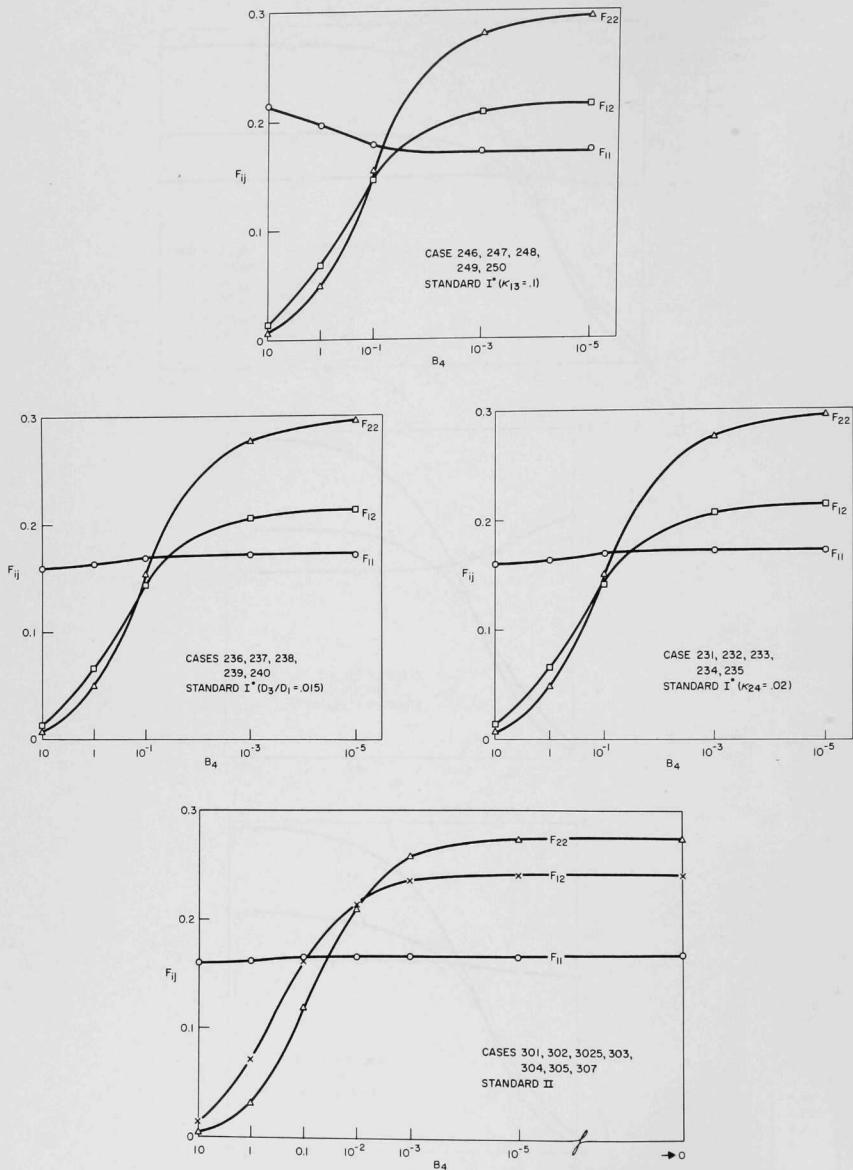
Table XV (Cont'd.)

Case No.	Deviation from Standard I			$B_3 = 10^{-5}$ Variable B_4	Calculated Concentrations & Corrected					
	K	E	D		F ₁₁	F ₁₂	F ₂₂	F ₁₃	F ₂₄	
{236 237 238 239 240}			$D_3/D_1 = 0.015$	10^{-5} 10^{-3} 10^{-1} 1 10	0.1720 0.1720 0.1690 0.1633 0.1591	0.2135 0.2064 0.1450 0.0667 0.0129	0.2951 0.2776 0.1547 0.0498 0.0070	0.6145 0.6216 0.6859 0.7699 0.8280	0.4914 0.5160 0.7003 0.8835 0.9800	
{246 247 248 249 250}	$K_{13} = 0.1$			10^{-5} 10^{-3} 10^{-1} 1 10	0.1720 0.1722 0.1789 0.1969 0.2149	0.2135 0.2066 0.1470 0.0681 0.0130	0.2951 0.2776 0.1548 0.0498 0.0070	0.6145 0.6211 0.6740 0.7350 0.7720	0.4914 0.5158 0.6981 0.8820 0.9799	
	D_2/D_1	K_{12}	K_{22}	E	B	Extrapolated Concentrations and By Difference				
Std. II 301 302 3025 303 304 305	0.25	2	0.55	0.87	$B_3 = 10^{-5}$ $B_4 = 10^{-5}$ 10^{-3} 10^{-2} 0.1 1 10	0.1667 0.1666 0.1663 0.1650 0.1620 0.1600	0.2405 0.2356 0.2141 0.1617 0.0712 0.0132	0.2731 0.2575 0.2092 0.1196 0.0312 0.0040	0.5928 0.5978 0.6196 0.6733 0.7668 0.8268	0.4864 0.5169 0.5767 0.7187 0.8976 0.9829
Std. III 311 312 3125 313 314 315	0.25	4	0.60	0.91	$B_3 = 10^{-5}$ $B_4 = 10^{-5}$ 10^{-3} 10^{-2} 0.1 1 10	0.1368 0.1374 0.1404 0.1500	0.3769 0.3480 0.2743 0.1324	0.2170 0.1799 0.1080 0.0317	0.4864 0.5146 0.5853 0.7176	0.4061 0.4721 0.6177 0.8359
Std. IV 316 317 3175 318 319 320	0.25	1	0.55	0.87	$B_3 = 10^{-5}$ $B_4 = 10^{-5}$ 10^{-3} 10^{-2} 0.1 1 10	0.1912 0.1899 0.1841 0.1711	0.1361 0.1225 0.0902 0.0377	0.2993 0.2406 0.1345 0.0331	0.6727 0.6876 0.7357 0.7912	0.5646 0.6365 0.7753 0.9292
Std. V 306 307 3075 308 309 310	0.125	2	0.30	0.87	$B_3 = 10^{-5}$ $B_4 = 10^{-5}$ 10^{-3} 10^{-2} 0.1 1 10	0.1625 0.1625 0.1624 0.1616 0.1603 0.1597	0.2585 0.2539 0.2313 0.1862 0.0902 0.0133	0.2657 0.2470 0.1862 0.0902 0.0187 0.0022	0.5790 0.5836 0.6063 0.6645 0.7655 0.8270	0.4759 0.4991 0.5825 0.7359 0.9070 0.9875
Std. II* 301 321 322 323 324 325	0.25	2	0.55	0.87	$B_3 = B_4$ $B_4 = 10^{-5}$ 10^{-3} 10^{-2} 0.1 1 10	0.1667 0.1610 0.1435 0.1032 0.0412 0.0068	0.2405 0.2313 0.2018 0.1361 0.0472 0.0070	0.2731 0.2571 0.2081 0.1180 0.0310 0.0040	0.5928 0.6074 0.6547 0.7607 0.9117 0.9863	0.4864 0.5116 0.5901 0.7459 0.9218 0.9891
		K	D		$B_3 = 10^{-5}$ Variable B_4	Calculated Concentrations & Corrected				
400 401 402 403 404		$k_{13}/k_{11} = 0.1$	$D_3/D_1 = 0.015$		10 1 0.1 10^{-3}	0.2160 0.1981 0.1800 0.1730	0.0132 0.0683 0.1473 0.209	0.0072 0.0500 0.1551 0.280	0.0771 0.734 0.673 0.618	0.0980 0.882 0.5901 0.7459 0.9117
405 406 407 408 409		$k_{13}/k_{11} = 0.5$			10 1 0.1 10^{-3}	0.2010 0.1893 0.1777 0.1730	0.0132 0.0680 0.1469 0.2068	0.0072 0.0500 0.1550 0.2778	0.786 0.743 0.675 0.620	0.980 0.882 0.698 0.515
	Deviation from Standard III									
271A 271B 271C					1 10 0.1	0.1798 0.2170 0.1474	0.1351 0.0269 0.2778	0.0317 0.0444 0.1080	0.685 0.756 0.575	0.833 0.969 0.614

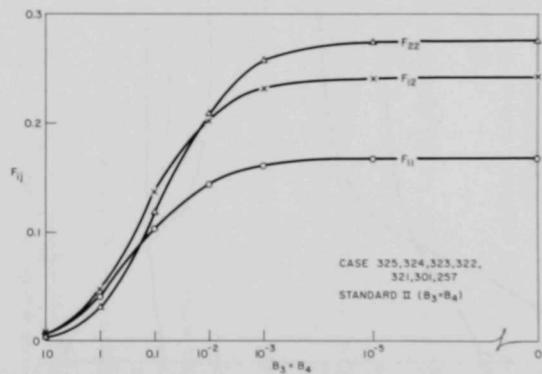
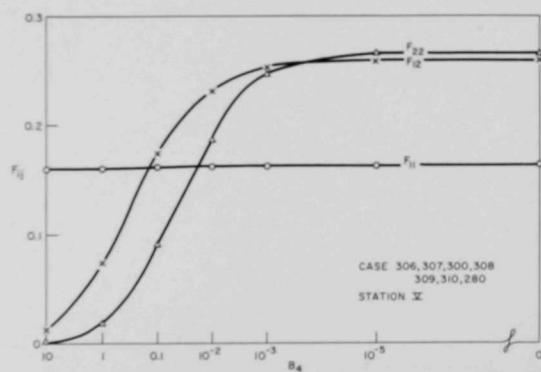
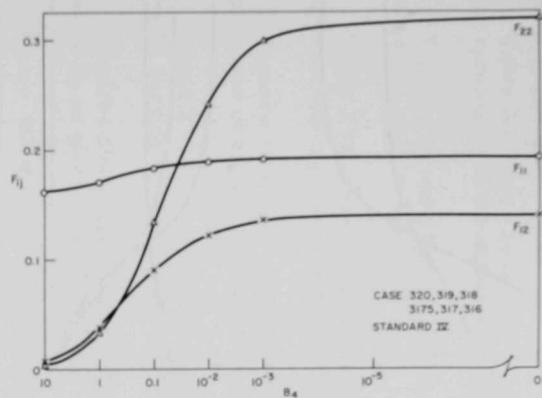
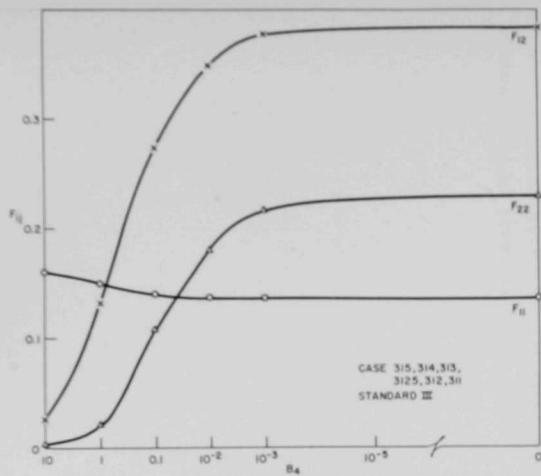
*55 points instead of the usual 33.



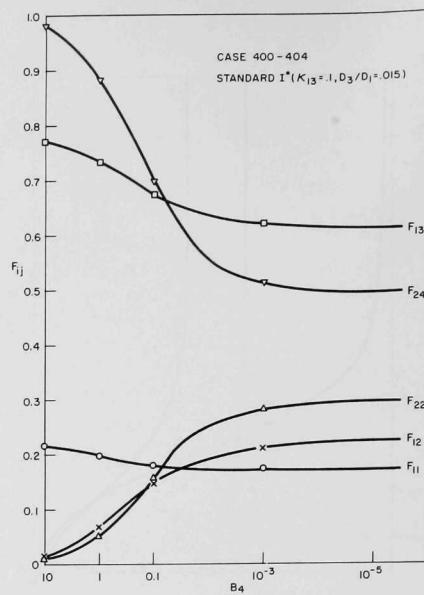
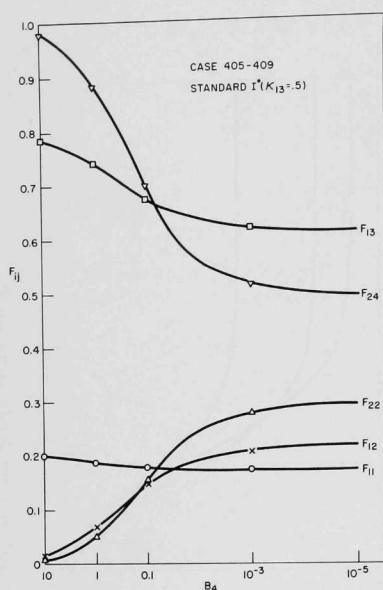
Figs. 23-25. Dependence of Final Recombination Fractions on B_1 .



Figs. 26-29. Dependence of Final Recombination Fractions on B_i .



Figs. 30-33. Dependence of Final Recombination Fractions on B_i .



Figs. 34-35. Dependence of Final Recombination Fractions on B_i .

SECTION THREE: INFLUENCE OF PARAMETERS ON RESULTS FOR α -RAY AND γ -RAY CASES

Table XVI gives results of cylindrical cases grouped to facilitate making comparisons for different values of E.

Figures 36 and 37 are plots of normalized F_{ii} vs. B_{i+2} for the different values of E in Table XVI.

Table XVII gives results of the Standard Spherical cases, grouped to facilitate making comparisons for different values of κ_{12} and D_2/D_1 .

Figures 38 and 39 are plots of normalized F_{22} vs. B_4 for the different values of κ_{12} and D_2/D_1 in Table XVII.

Table XVIII gives results of spherical cases grouped to show the effects of varying κ_{13} and D_3/D_1 .

Figures 40-43 are graphs of F_{ij} vs. B_4 , κ_{13} , or D_3/D_1 for certain values of B_4 as given in Table XVIII.

Table XIX gives results of spherical cases grouped to show the effects of varying κ_{24} and D_4/D_1 .

Figures 44-45 are graphs of F_{ij} vs. B_4 , κ_{24} , or D_4/D_1 for certain values of B_4 as given in Table XIX.

Table XVI

RESULTS OF CYLINDRICAL CASES FOR DIFFERENT VALUES OF E TO PLOT NORMALIZED F'S VS. B

Case No.	E	$B_3 = 10^{-5}$, $B_4 =$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}	0^*
520-	5.305 (10.61)	F_{22} $F_{22}/F(0)$ 1-Avidac	0.0530 0.115 0.190	0.2126 0.462 0.547	0.3625 0.788 0.824	0.4397 0.956 0.957	0.4505 0.979			0.46 1 1
530-	2.48 (4.96)	F_{22} $F_{22}/F(0)$ 1-Avidac	0.0289 0.063 0.101	0.1493 0.325 0.411	0.3191 0.694 0.715	0.4329 0.941 0.923	0.4494 0.977			0.46 1 1
540-	1.29 (2.58)	F_{22} $F_{22}/F(0)$ 1-Avidac	0.0160 0.035	0.1008 0.219	0.2697 0.586	0.4212 0.916	0.4474 0.973	0.4539 0.987	0.4555 0.990	0.46 1 1
550-	0.675 (1.35)	F_{22} $F_{22}/F(0)$ 1-Avidac	0.0087 0.019	0.0632 0.137	0.2122 0.462	0.3995 0.869	0.4401 0.957		0.4541 0.988	0.46 1 1
560-	0.3535 (0.707)	F_{22} $F_{22}/F(0)$ 1-Avidac	0.0046 0.010 0.020	0.0372 0.081 0.110	0.1528 0.332 0.320	0.3616 0.787 0.643	0.4219 0.918 0.760		0.4463 0.971	0.46 1 1
570-	0.1875 (0.375) (0.0707)	F_{22} $F_{22}/F(0)$ 1-Avidac	0.0025 0.005	0.0212 0.046	0.1013 0.220	0.3057 0.665	0.3863 0.840	10^{-10} 0.4156 0.903	10^{-15} 0.4303 0.935	0.46 1
Case No.	E	$B_4 = 10^{-5}$, $B_3 =$	10	1	0.1	10^{-3}	10^{-5}	10^{-7}	10^{-10}	0^*
525-	5.305	F_{11} $F_{11}/F(0)$	0.0859 0.202	0.2619 0.616	0.3712 0.873	0.4137 0.973	0.4213 0.991			0.425 1
535-	2.48	F_{11} $F_{11}/F(0)$	0.0487 0.115	0.1960 0.462	0.3279 0.772	0.3992 0.940	0.4128 0.972			0.425 1
545-	1.29	F_{11} $F_{11}/F(0)$								
555-	0.675	F_{11} $F_{11}/F(0)$	0.0151 0.036	0.0886 0.208	0.2146 0.505	0.3391 0.798	0.3758 0.884		0.4049 0.953	0.425 1
565-	0.3535	F_{11} $F_{11}/F(0)$	0.0081 0.019	0.0532 0.116	0.1528 0.360	0.2875 0.676	0.3379 0.795		0.3825 0.900	0.425 1
575-	0.1875	F_{11} $F_{11}/F(0)$	0.0044 0.010	0.0306 0.072	0.1004 0.236	0.2260 0.532	0.2859 0.673		10^{-15} 0.3699 0.870	0.425 1

* Rough extrapolated values.

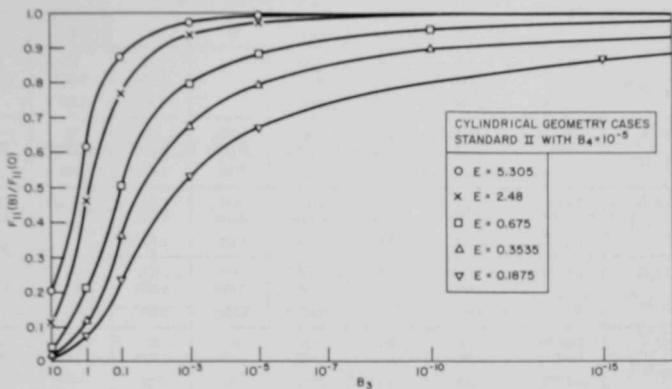


Fig. 36. Influence of Initial Free Radical Concentrations on $F_{11}(B)/F_{11}(0)$

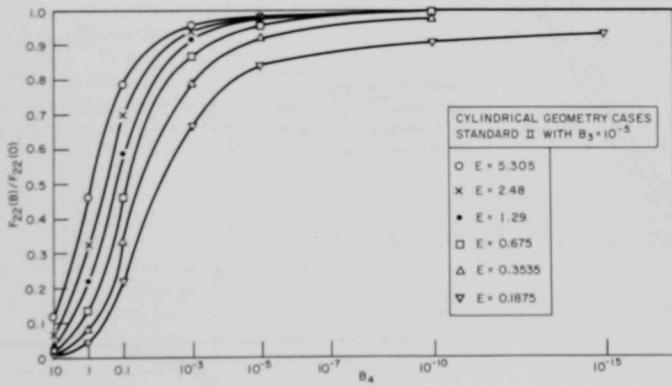


Fig. 37. Influence of Initial Free Radical Concentrations on $F_{22}(B)/F_{22}(0)$

Table XVII

RESULTS OF STANDARD CASES WITH SPHERICAL SYMMETRY

	B_4	10	1	0.1	10^{-2}	10^{-3}	10^{-5}	0
Std. I $B_3 = 10^{-5}$	Case No. $F_{22}(B)$	145 0.0070	144 0.0498	143 0.1547	-	142 0.2776	141 0.2951	253 0.2951
	$F(B)/F(0)$	0.024	0.169	0.524		0.941	1.000	1
Std. II $B_3 = 10^{-5}$	Case No. $F_{22}(B)$	305 0.0039	304 0.0312	303 0.1195	3025 0.2092	302 0.2575	301 0.2713	257 0.2735
	$F(B)/F(0)$	0.014	0.114	0.437	0.765	0.941	0.992	1
Std. III $B_3 = 10^{-5}$	Case No. $F_{22}(B)$	315 0.0044	314 0.0317	313 0.1080	3125 0.1799	312 0.2170	311 -	271 0.2293
	$F(B)/F(0)$	0.020	0.138	0.471	0.785	0.946	-	1
Std. IV $B_3 = 10^{-5}$	Case No. $F_{22}(B)$	320 0.0040	319 0.0331	318 0.1345	3175 0.2409	317 0.2993	316 -	265 0.3186
	$F(B)/F(0)$	0.029	0.104	0.422	0.756	0.939	-	1
Std. V $B_3 = 10^{-5}$	Case No. $F_{22}(B)$	310 0.0022	309 0.0187	308 0.0902	3075 0.1862	307 0.2470	306 0.2657	280 0.2633
	$F(B)/F(0)$	0.008	0.071	0.343	0.707	0.938	1	1
Std. II* $B_3 = B_4$	Case No. $F_{11}(B)$	325 0.0068	324 0.0412	323 0.1032	322 0.1435	321 0.1610	301 0.1667	257 0.1670
	$F_{11}(B)/F(0)$	0.041	0.247	0.618	0.859	0.964	0.998	1
	$F_{22}(B)$	0.0040	0.0310	0.1180	0.2081	0.2571	0.2731	0.2735
	$F_{22}(B)/F(0)$	0.014	0.113	0.431	0.761	0.940	0.999	1

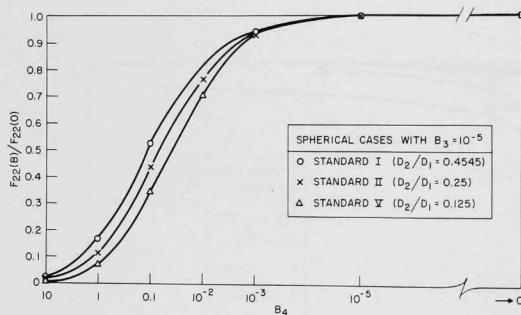


Fig. 38

Influence of Diffusion Coefficients on $F_{22}(B)/F_{22}(0)$

Fig. 39
Influence of Reaction Rates on $F_{22}(B)/F_{22}(0)$

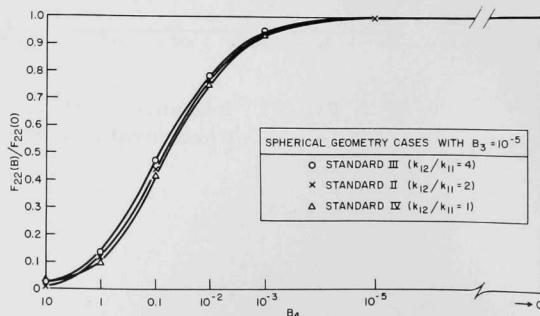


Table XVIII

RESULTS WHEN k_{13}/k_{11} AND D_3/D_1 VARY FOR γ -RAY CASES

Case No.	Deviation from Std. I k_{13}	D_3/D_1	Final Values of F_{11} @ B_4				
			10^{-5}	10^{-3}	10^{-1}	1	10
141-145	2.0		0.1720	0.1720	0.1695	0.1642	0.1603
405-409	0.5			0.1730	0.1777	0.1893	0.2010
246-250	0.1		0.1720	0.1722	0.1789	0.1969	0.2149
151-155	10^{-2}		0.1718	0.1720	0.1792	0.1987	0.2185
211-215	10^{-4}		0.1720	0.1720	0.1795	0.1993	0.2197
203-201	0.4545..		0.1720	-	0.1709	-	0.1663
141-145	0.15		0.1720	0.1720	0.1695	0.1642	0.1603
236-240	0.015		0.1720	0.1720	0.1690	0.1633	0.1591

Case No.	Deviation from Std. I k_{13}	D_3/D_1	Final Values for $B_4 = 10$				
			F_{11}	F_{12}	F_{22}	F_{13}	F_{24}
145	2.0		0.1603	0.0129	0.0070	0.8267	0.9800
405	0.5		0.2010	0.0132	0.0072	0.786	0.980
250	0.1		0.2149	0.0130	0.0070	0.7720	0.9799
155	10^{-2}		0.2185	0.0130	0.0070	0.7685	0.9800
215	10^{-4}		0.2197	0.0133	0.0072	0.7670	0.9796
201	0.4545..		0.1663	0.0129	0.0070	0.8207	0.9800
145	0.15		0.1603	0.0129	0.0070	0.8267	0.9800
240	0.015		0.1591	0.0129	0.0070	0.8280	0.9800

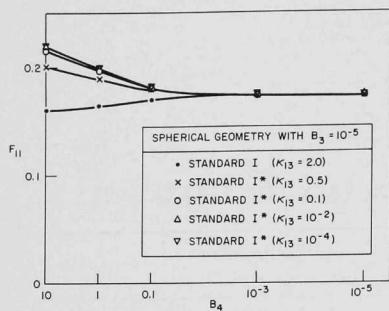


Fig. 40. Influence of Reaction Rates on F_{11}

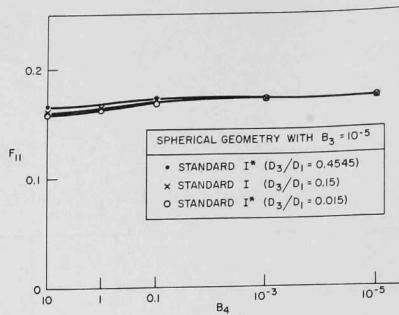


Fig. 41. Influence of Diffusion Rates on F_{11}

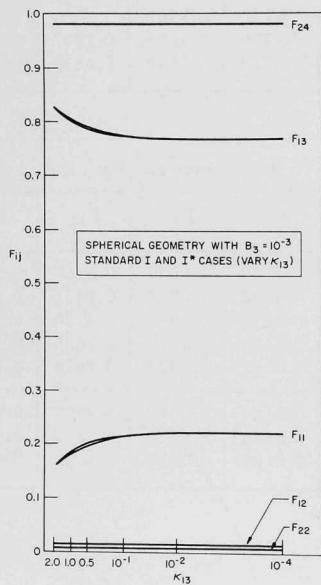


Fig. 42. Influence of Reaction Rate on F_{ij} for $B_4 = 10$

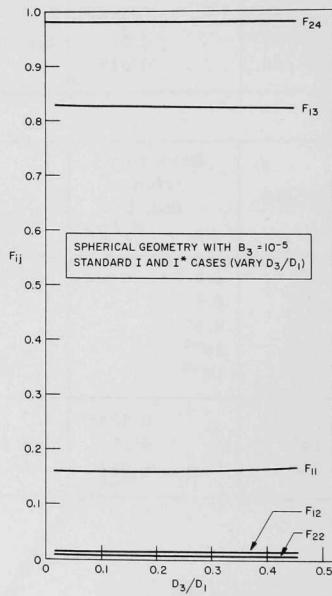


Fig. 43. Influence of Diffusion Rate on F_{ij} for $B_4 = 10$

Table XIX

RESULTS WHEN k_{2d}/k_{11} AND D_4/D_1 VARY FOR γ -RAY CASES

Case No.	Deviation from Std.		Final Values of $F_{22} @ B_4$					
	K_{24}	D_4/D_1		10^{-5}	10^{-3}	10^{-1}	1	10
141-145	2.0		Std.	0.2951	0.2776	0.1547	0.0498	0.0070
231-235	0.02			0.2951	0.2770	0.1507	0.0485	0.0072
208-206		0.4545		0.2951	-	0.1541	-	0.0070
141-145	0.15		Std.	0.2951	0.2776	0.1547	0.0498	0.0070
221-225	0.05			0.2951	0.2760	0.1550	0.0498	0.0070

Case No.	Deviation from Std.		Final Values for $B_4 = 10$					
	K_{24}	D_4/D_1		F_{11}	F_{12}	F_{22}	F_{13}	F_{24}
145	2.0		Std.	0.1603	0.0129	0.0070	0.8267	0.9800
235	0.02			0.1603	0.0128	0.0070	0.8268	0.9802
206		0.4545		0.1603	0.0129	0.0070	0.8267	0.9800
145	0.15		Std.	0.1603	0.0129	0.0070	0.8267	0.9800
225	0.05			0.1603	0.0129	0.0070	0.8267	0.9800

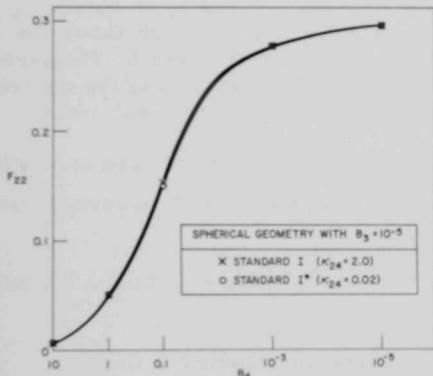


Fig. 44

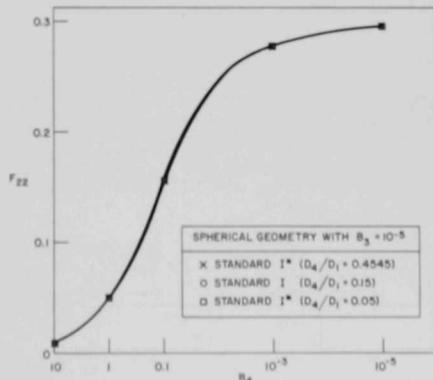
Influence of Reaction Rate
on F_{22} 

Fig. 45

Influence of Diffusion Rate
on F_{22}

SECTION FOUR: FIGURES TRACING THE REACTIONS OVER TIME
AND SPACE FOR γ -RAY CASES

As indicated previously, transformed time T goes from 1 to 0, while real time goes from 0 to ∞ ; and transformed space R goes from 1 to 0, so P goes from some integer at the origin down to 0, while the real space goes from 0 to ∞ . All but Figure 46 are based on actual cases described in Table XV.

Figure 46: General shapes of solutions.

Figures 47-57: Graphs of the amounts of X_i ($i=1,2,3,4$) at the origin (center of initial concentration of free radicals) as a function of the real time plotted on a log scale. Figures 47-51 are for Standard I at different values of B_4 , whereas Figures 52-57 are all for $B_4 = 1$ for different parameter combinations.

Figures 58-61: Similar plots for either X_1 and X_3 or X_2 and X_4 for $B_4 = 10$ only, with different cases grouped so each graph shows the influence of some parameter for cases similar to Standard I. The parameters being varied are D_3/D_1 , κ_{13} , D_4/D_1 , and κ_{24} ; in each case the concentration of X_i at the origin is plotted against the log of the real time.

Tables XX to XXIII: Values of U_i ($i = \frac{1}{2} | \frac{3}{4}$) to be used in plotting U_i vs. T at certain values of R (or P) and to plot U_i vs. R at certain values of T for Standard II cases.

Figures 62-89: Plots based on the information in Tables XX-XXIII for the cases described in Table XV.

Figures 90 and 91 are similar plots for Standard V Cases.

Figures 92-103: Plots of F_{ij} vs. $\log t$ for Standard I cases and others with selected values of B_4 .

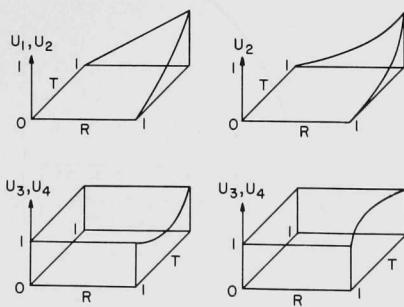
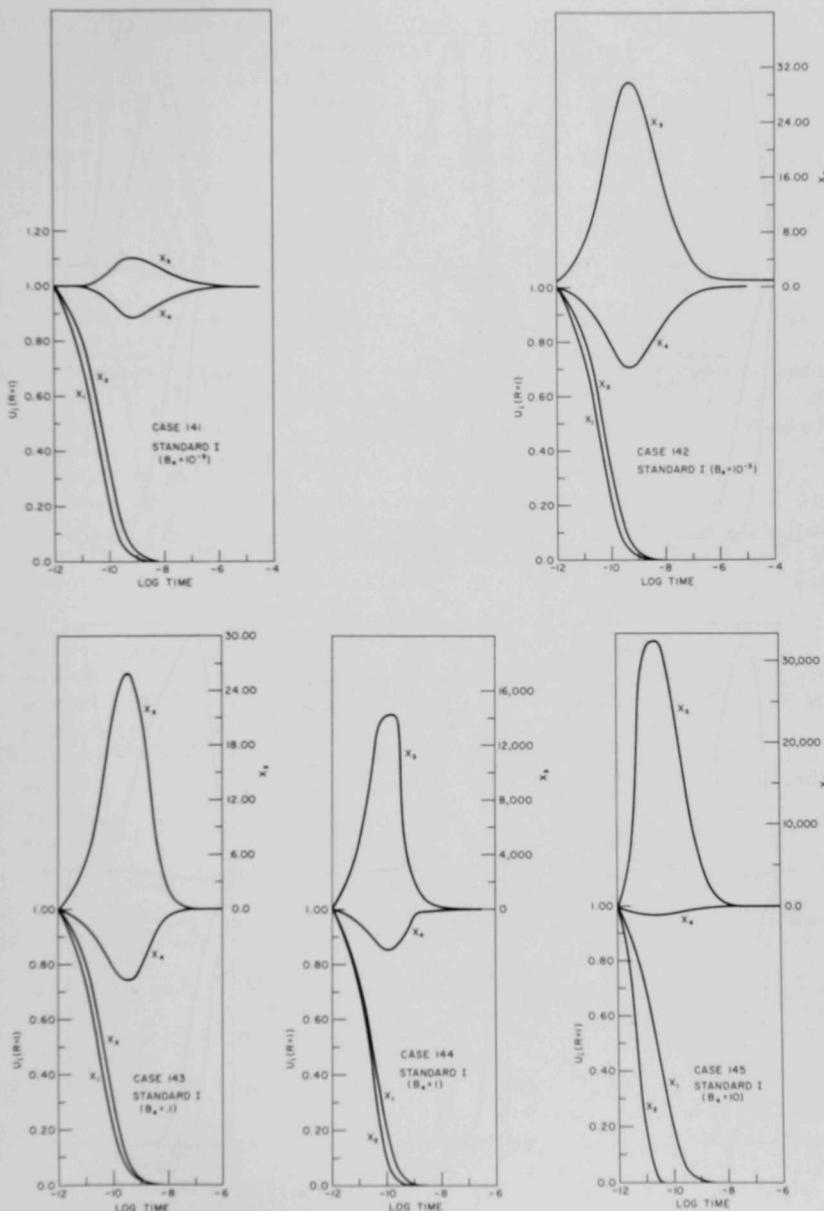
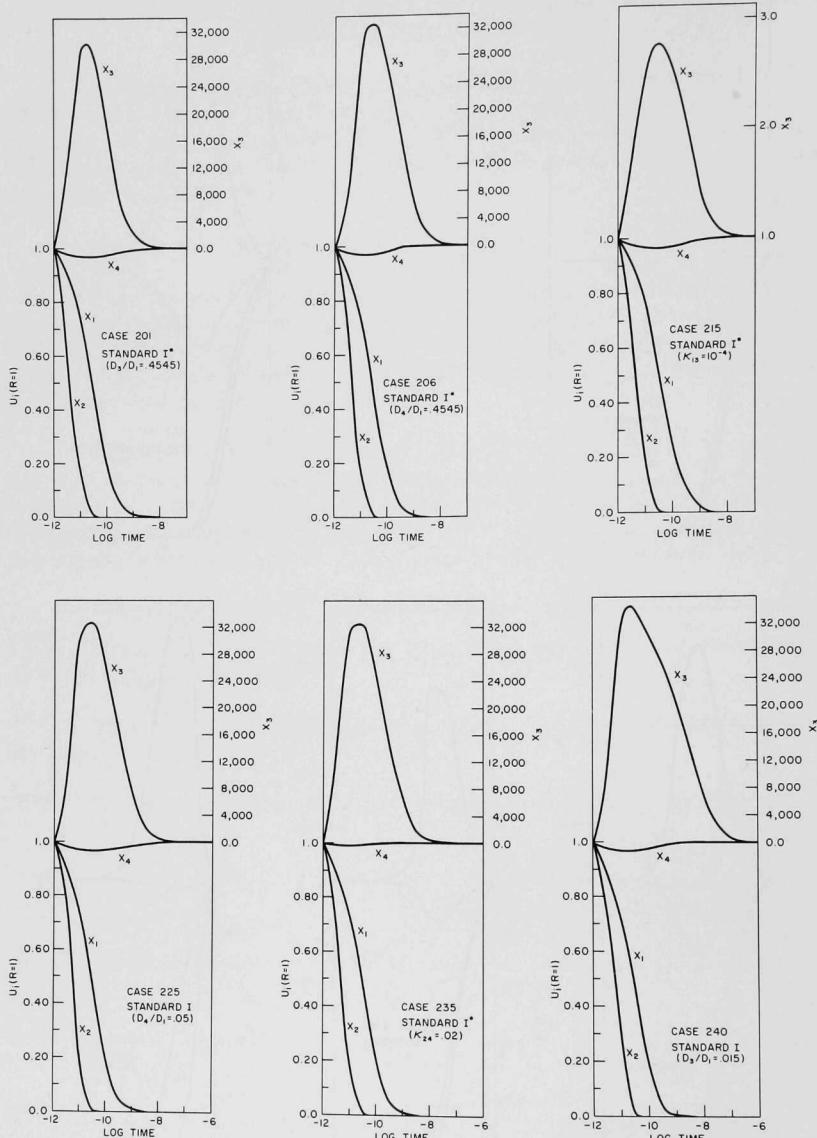


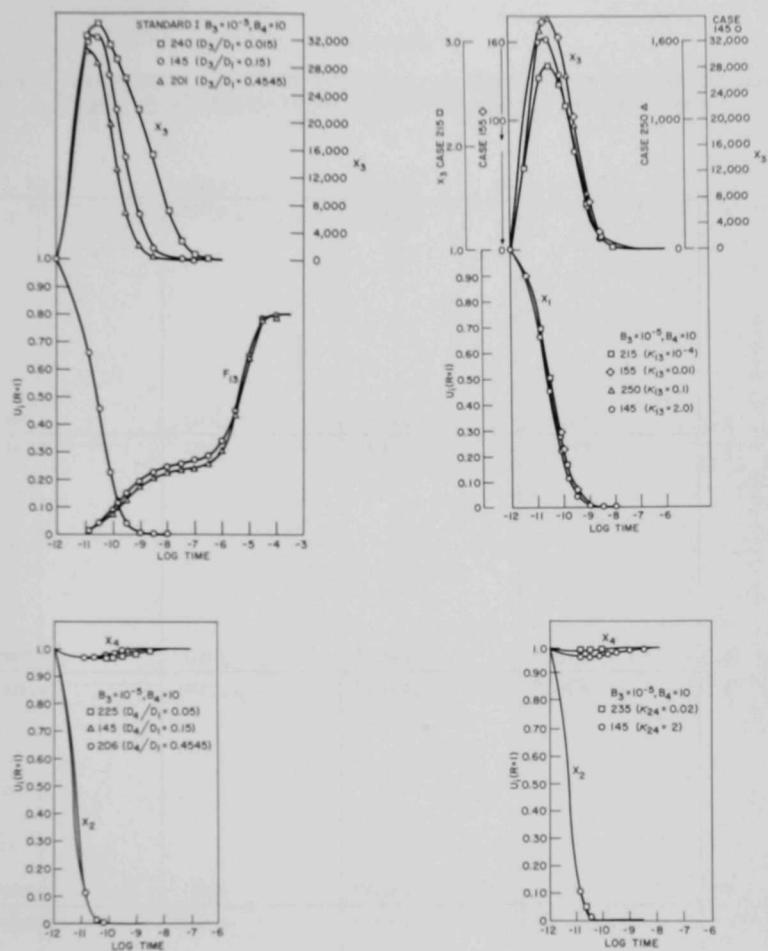
Fig. 46
General Shapes of Solutions
 $U_i(R, T)$



Figs. 47-51. Time Dependence of Recombination Fractions



Figs. 52-57. Time Dependence of Recombination Fractions



Figs. 58-61. Time Dependence of Recombination Fractions

Table XX

CONCENTRATIONS OF REACTANTS AT VARIOUS TIMES AND POSITIONS IN SPACE
FOR CASE 257: SPHERICAL GEOMETRY; STANDARD II; $B_3 = B_4 = 0$

		0.2727	0.5152	0.7576	1.0
		0.2727	0.5152	0.7576	1.0
T	0.75	0.1009	0.1780	0.2467	0.3084
	0	0.1033	0.2472	0.4083	0.5748
T	0.50	0.2611^{-1}	0.4527^{-1}	0.6167^{-1}	0.7569^{-1}
	0	0.2011^{-1}	0.7421^{-1}	0.1575	0.2614
T	0.25	0.2822^{-2}	0.5012^{-2}	0.6947^{-2}	0.8612^{-2}
	0	0.9436^{-3}	0.7008^{-2}	0.2258^{-1}	0.5067^{-1}
T	0	0.1233^{-9}	0.2328^{-9}	0.3422^{-9}	0.4516^{-9}
	0	0.1460^{-10}	0.1961^{-9}	0.9303^{-9}	0.2865^{-8}

Table XXI

CONCENTRATIONS OF REACTANTS AT VARIOUS TIMES AND POSITIONS IN SPACE
FOR CASE 305: SPHERICAL GEOMETRY; STANDARD II; $B_3 = 10^{-5}$, $B_4 = 10$

1.0	0	1.0	0.2727	1.0	0.5152	1.0	0.7576	1.0	1.0	1.0
	0	1.0	0.2727	1.0	0.5152	1.0	0.7576	1.0	1.0	1.0
0.75	0	1.0	0.1008	4491.04	0.1772	11675.78	0.2443	20495.45	0.3037	30363.72
	0	1.0	0.5694(-4)	0.9955	0.1466(-3)	0.9883	0.2626(-3)	0.9795	0.4032(-3)	0.9696
T										
0.50	0	1.0	0.2591(-1)	689.47	0.4435(-1)	3528.97	0.5920(-1)	9406.88	0.7054(-1)	18788.33
	0	1.0		0.9993		0.9965		0.9906		0.9812
0.25	0	1.0	0.2750(-2)	11.91	0.4806(-2)	236.53	0.6461(-2)	1469.55	0.7539(-2)	5495.83
	0	1.0		1.0		0.9998		0.9985		0.9945
0	0	1.0	0.9217(-14)	1.0	0.1741(-13)	1.0	0.2560(-13)	1.0	0.3378(-13)	1.0002
	0	1.0	0	1.0	0	1.0	0	1.0	0	1.0

P

0

9

17

25

33

Table XXII

CONCENTRATIONS OF REACTANTS AT VARIOUS TIMES AND POSITIONS IN SPACE
 FOR CASE 303: SPHERICAL GEOMETRY; STANDARD II; $B_3 = 10^{-5}$, $B_4 = 0.1$

		0	1.0	0.2727	1.0	0.5152	1.0	0.7576	1.0	1.0	1.0
1.0	0	1.0	0.2727	1.0	0.5152	1.0	0.7576	1.0	1.0	1.0	1.0
	0	1.0	0.2727								
0.75	0	1.0	0.1009	328.34	0.1780	803.50	0.2466	1329.24	0.3082	1873.71	
	0	1.0	0.9585(-1)	0.9673	0.2300	0.9197	0.3812	0.8666	0.5383	0.8127	
T											
0.50	0	1.0	0.2609(-1)	197.66	0.4517(-1)	827.43	0.6139(-1)	1867.38	0.7512(-1)	3171.24	
	0	1.0	0.1514(-1)	0.9803	0.5685(-1)	0.9174	0.1234	0.8134	0.2104	0.6830	
0.25	0	1.0	0.2808(-2)	18.12	0.4963(-2)	208.60	0.6811(-2)	920.34	0.8283(-2)	2598.76	
	0	1.0	0.2240(-3)	0.9983	0.1793(-2)	0.9792	0.6432(-2)	0.9081	0.1676(-1)	0.7402	
0	0	1.0	0.6029(-6)	0.9995	0.1132(-5)	1.0181	0.1654(-5)	1.2718	0.2162(-5)	2.8250	
	0	1.0	0	1.0	0	1.0	0	1.0	0	0.9998	

P

0	9	17	25	33
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Table XXIII

CONCENTRATIONS OF REACTANTS AT VARIOUS TIMES AND POSITIONS IN SPACE
FOR CASE 301: SPHERICAL GEOMETRY; STANDARD II, $B_3 = B_4 = 10^{-5}$

1.0	0	1.0	0.2727	1.0	0.5152	1.0	0.7576	1.0	1.0	1.0
	0	1.0	0.2727	1.0	0.5152	1.0	0.7576	1.0	1.0	1.0
0.75	0	1.0	0.1009	0.9992	0.1780	1.0122	0.2467	1.0320	0.3084	1.0551
	0	1.0	0.1033	1.0008	0.2472	0.9878	0.4083	0.9680	0.5747	0.9448
T										
0.50	0	1.0	0.0261	0.9902	0.0453	1.0160	0.0617	1.0809	0.0757	1.1749
	0	1.0	0.0201	1.0098	0.797	0.9840	0.1575	0.9191	0.2614	0.8251
0.25	0	1.0	0.2822 ⁽⁻²⁾	0.9885	0.5012 ⁽⁻²⁾	0.9953	0.6946 ⁽⁻²⁾	1.0656	0.8611 ⁽⁻²⁾	1.2413
	0	1.0	0.9000 ⁽⁻³⁾	1.0115	0.7008 ⁽⁻²⁾	1.0047	0.2258 ⁽⁻¹⁾	0.9343	0.5067 ⁽⁻¹⁾	0.7586
0	0	1.0	0.9857 ⁽⁻¹⁴⁾	0.9999	0.1862 ⁽⁻¹³⁾	0.9999	0.2738 ⁽⁻¹³⁾	0.9999	0.3614 ⁽⁻¹³⁾	1.0
	0	1.0	0.1173 ⁽⁻¹⁴⁾	1.0	0.1576 ⁽⁻¹³⁾	1.0	0.7483 ⁽⁻¹³⁾	0.9999	0.2307 ⁽⁻¹²⁾	0.9999

P

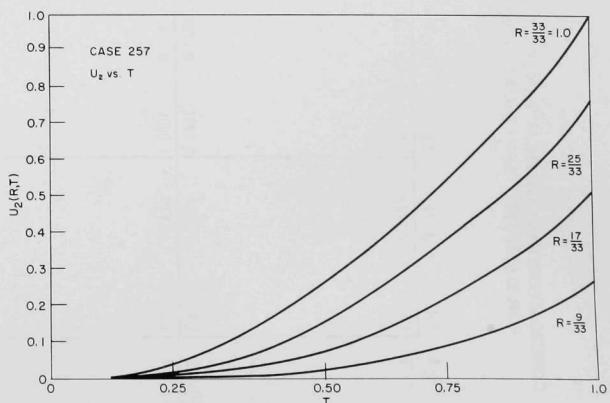
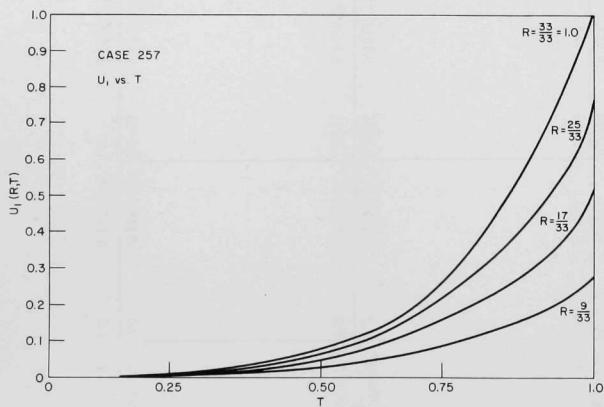
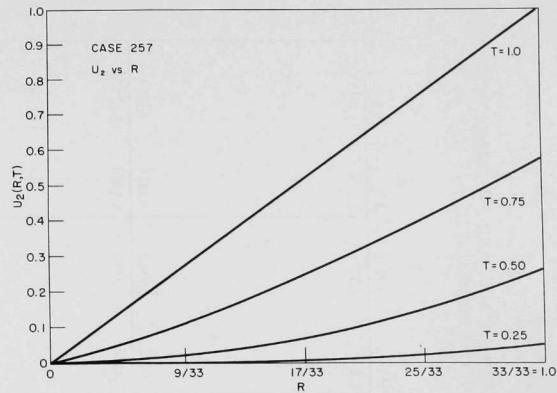
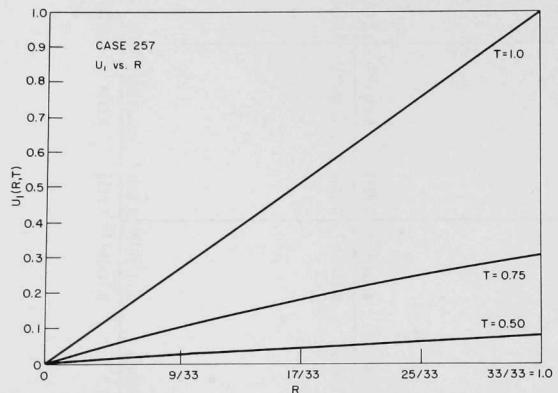
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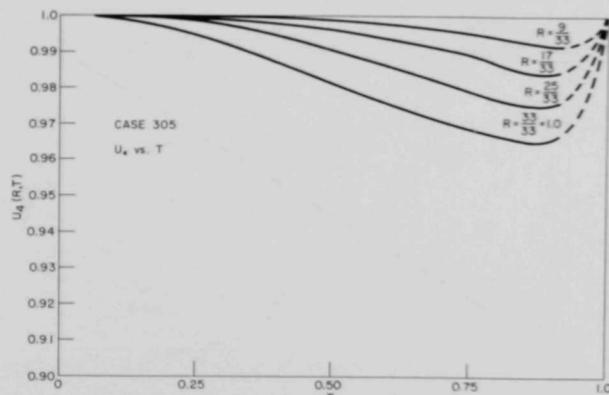
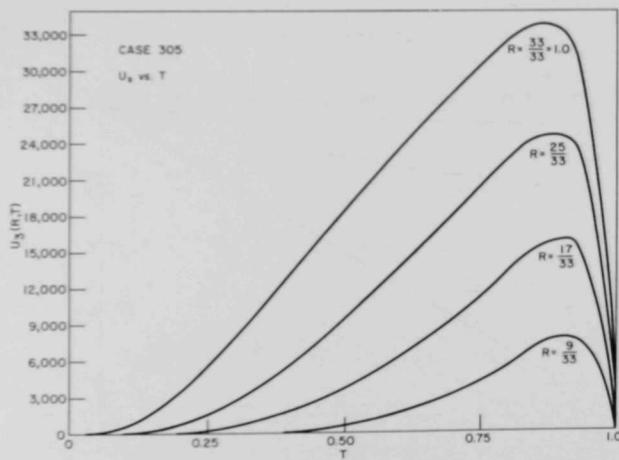
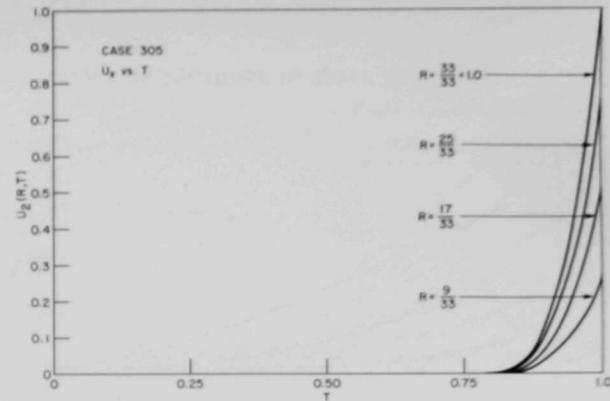
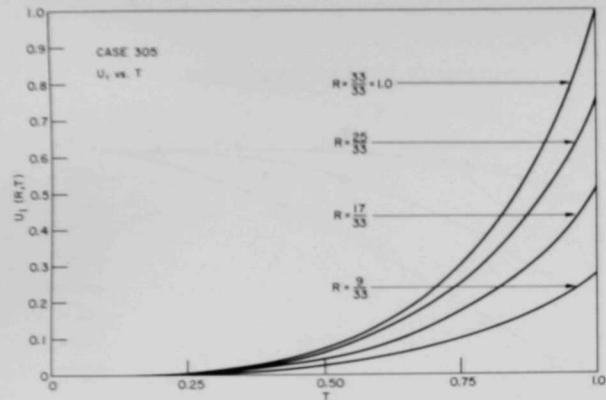
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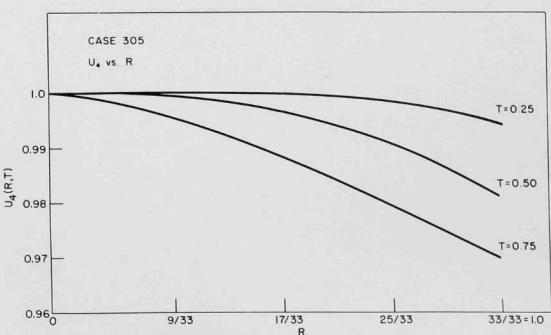
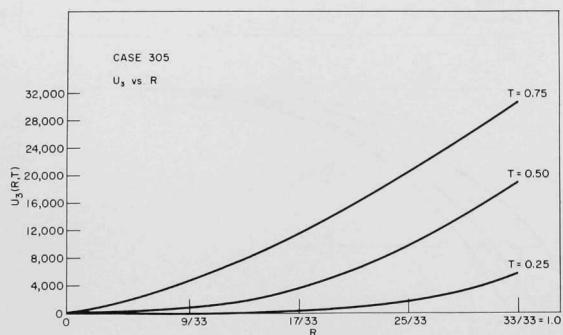
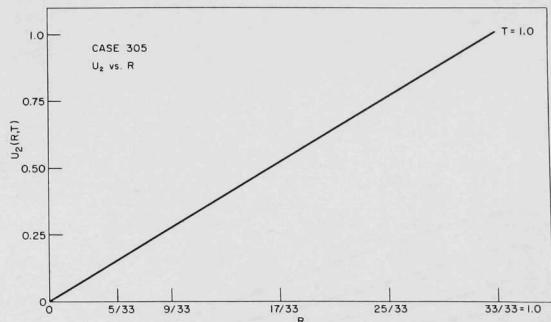
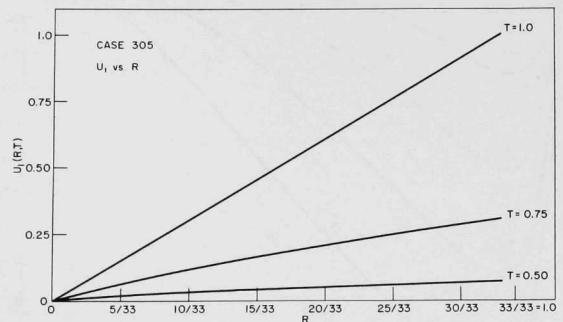
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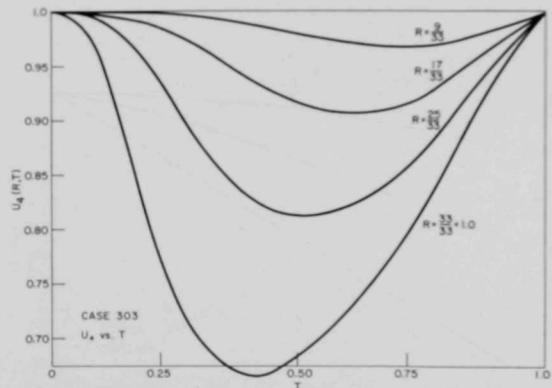
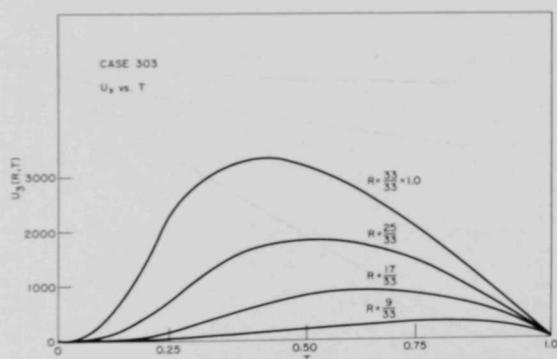
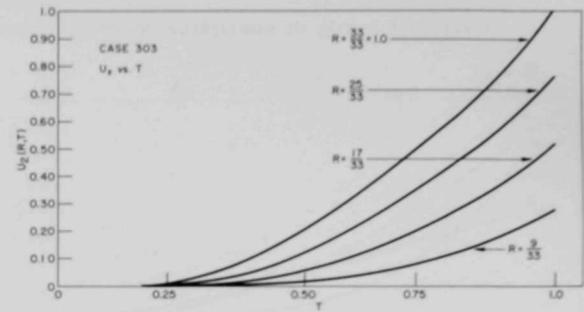
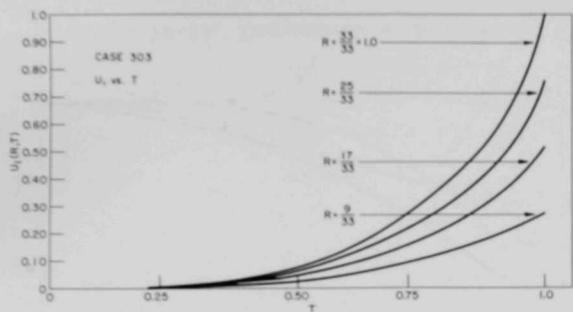
Figs. 62-65. Dependence of Normalized Concentrations on Positions in Space and Time.



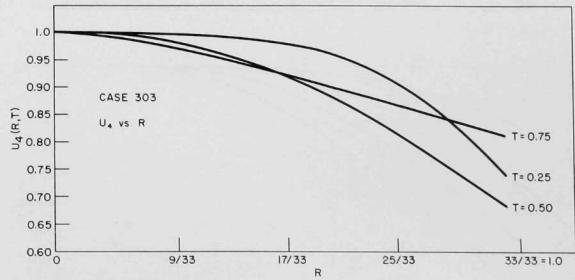
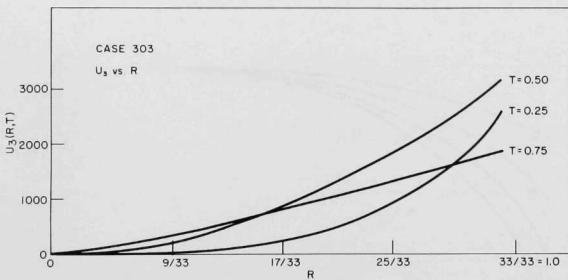
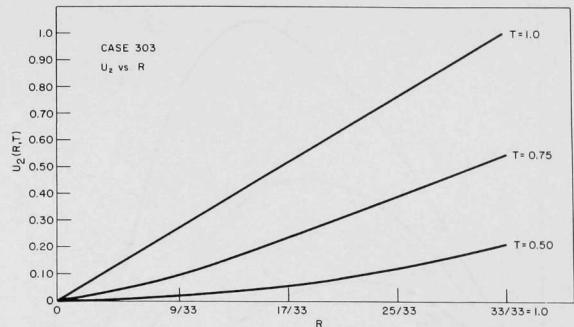
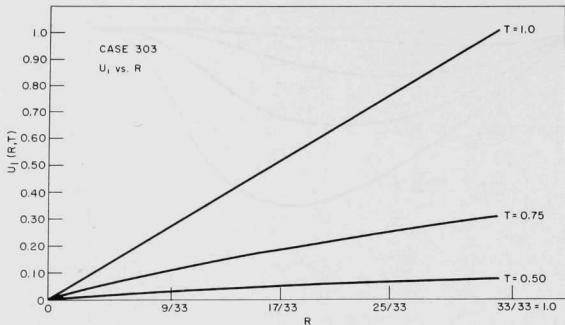
Figs. 66-69. Dependence of Normalized Concentrations on Positions in Space and Time.



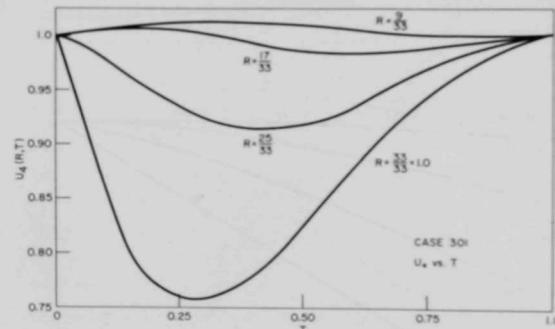
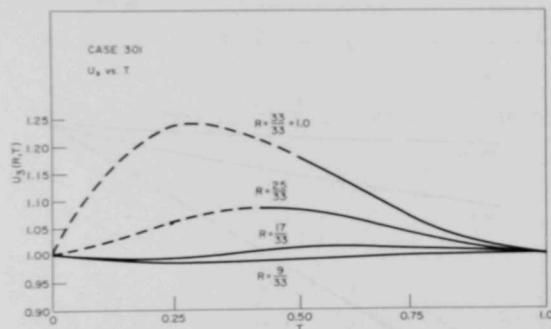
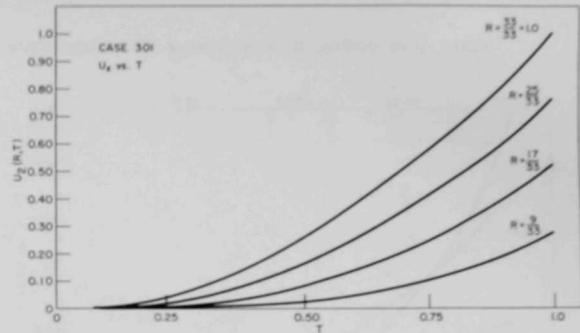
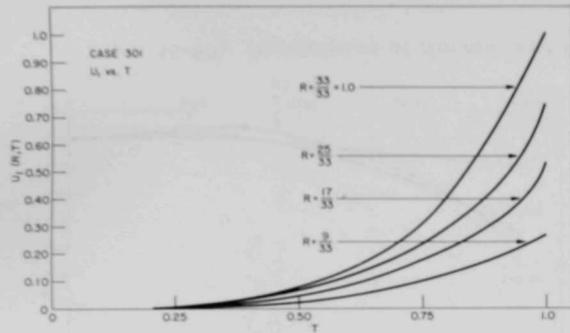
Figs. 70-73. Dependence of Normalized Concentrations on Positions in Space and Time.



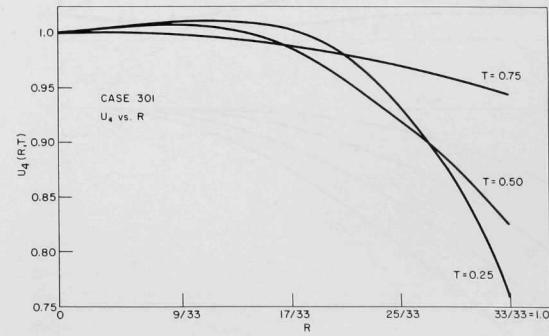
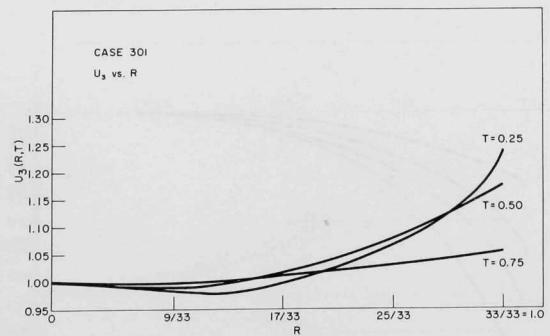
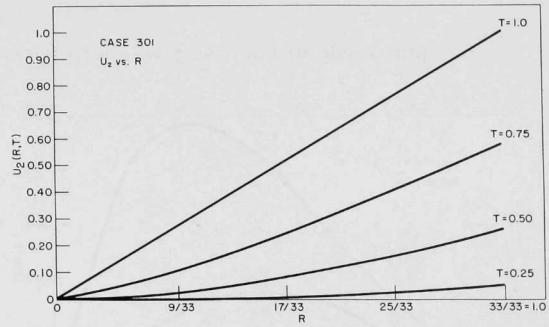
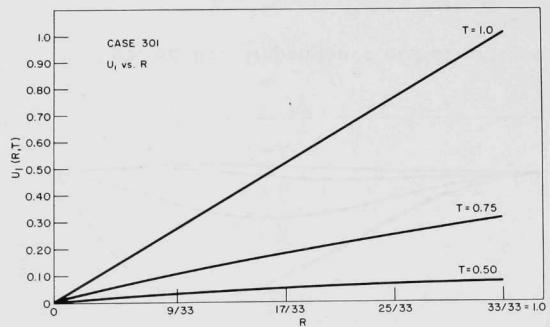
Figs. 74-77. Dependence of Normalized Concentrations on Positions in Space and Time



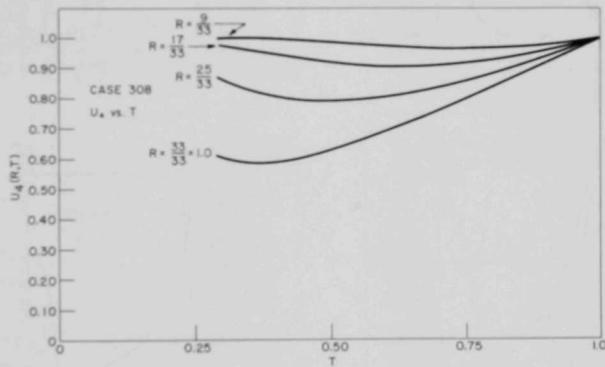
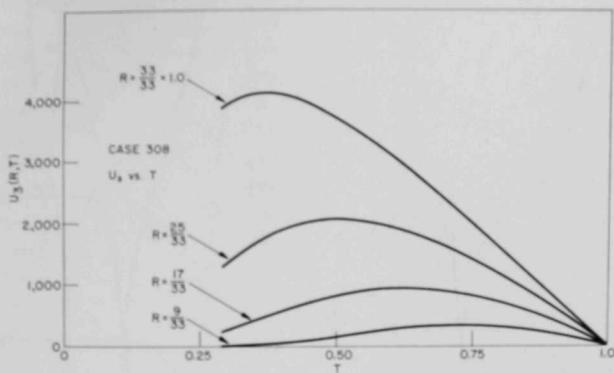
Figs. 78-81. Dependence of Normalized Concentrations on Positions in Space and Time



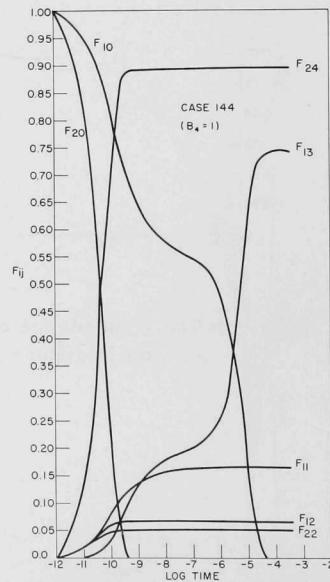
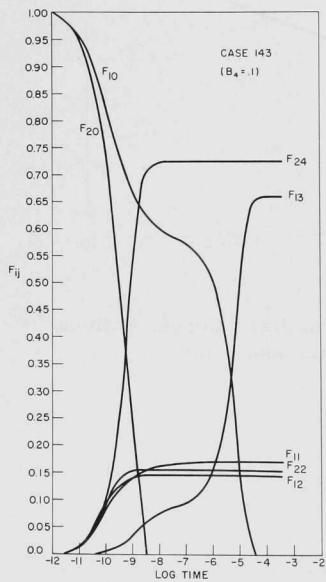
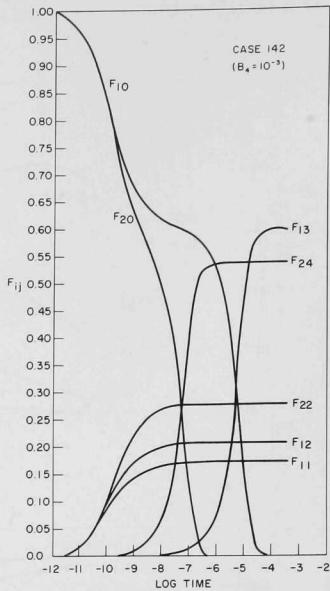
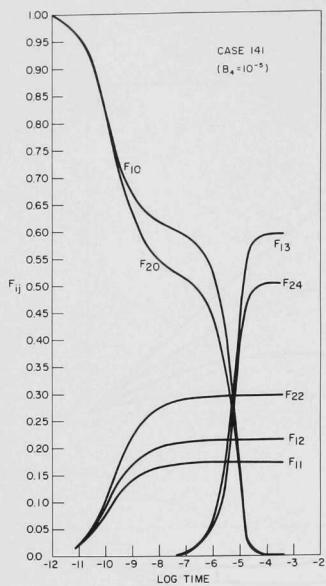
Figs. 82-85. Dependence of Normalized Concentrations on Positions in Space and Time



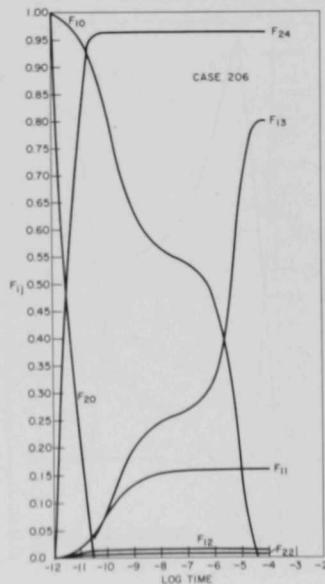
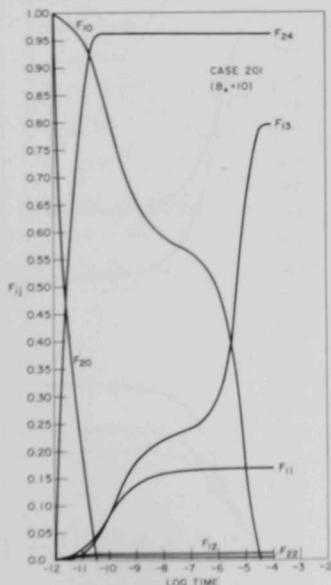
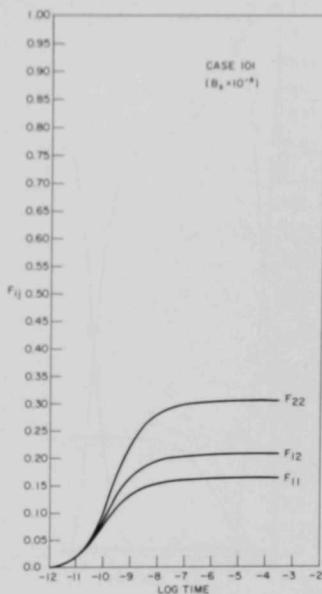
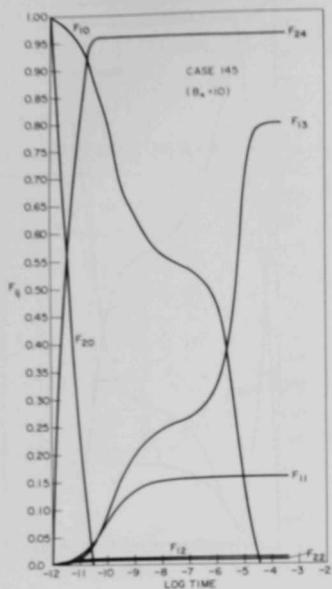
Figs. 86-89. Dependence of Normalized Concentrations on Positions in Space and Time



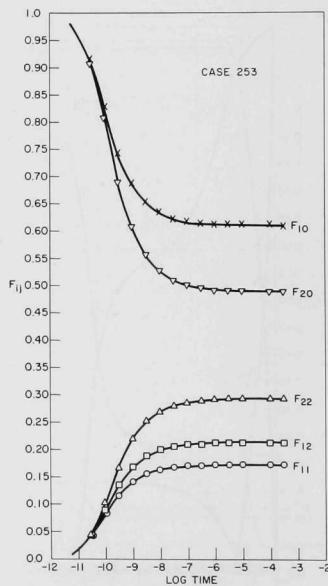
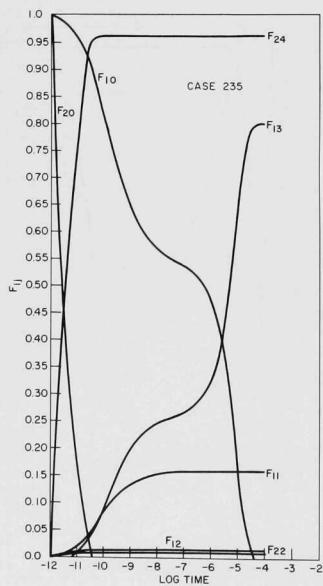
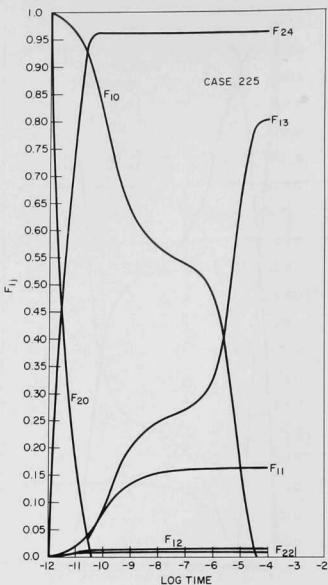
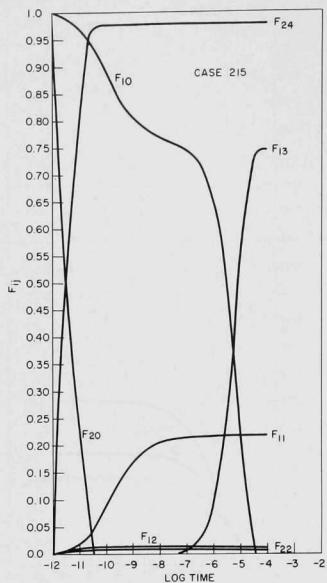
Figs. 90-91. Dependence of Normalized Concentrations on Positions in Space and Time



Figs. 92-95. Time Dependence of Recombination Fractions



Figs. 96-99. Time Dependence of Recombination Fractions



Figs. 100-103. Time Dependence of Recombination Fractions

SECTION FIVE: RESULTS OBTAINED FROM CODE C, FOR THREE PRIMARY AND ONE SECONDARY REACTION.
THUS, D_3/D_1 , κ_{13} , AND B_3 ARE ALL ZERO.

Table XXIV

PARAMETERS FOR STANDARD II CASES RUN WITH CODE C

Case No.	ϵ	β	E	D_2/D_1	D_4^*/D_1	κ_{12}	κ_{22}	κ_{24}^*	B_4^*
1000	2	1	0.87	0.25	0	2	0.55	0.1	0.02175
1001	2	1	0.87	0.25	1.0	2	0.55	0.1	0.02175
1002	2	1	0.87	0.25	0.5	2	0.55	0.1	0.02175
1003	2	1	0.87	0.25	0.125	2	0.55	0.1	0.02175
1004	1	1	1.60	0.25	0.125	2	0.55	0.1	0.08

Table XXV

RESULTS OF CASES DESCRIBED IN TABLE XXIV

Case No.	F_{11}	F_{12}	F_{22}	$F_{24}^* = HO_2$	$H_2 = \frac{1}{2}F_{11}$	$HO_2 = \frac{1}{2}F_{22} - F_{24}^*$
1000				No Result (unstable)		
1001	0.1670	0.2410	0.2731	0.0014	0.0835	0.1351
1002	0.1670	0.2410	0.2724	0.0023	0.0835	0.1339
1003	0.1670	0.2410	0.2720	0.0042	0.0835	0.1318
1004	0.475	0.525	0.437	0.038	0.238	0.181

ACKNOWLEDGEMENTS

Sandra Janoucek and Joanne Griffin of Argonne National Laboratory's Applied Mathematics Division assisted with the calculations and graph plotting.

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