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FIELD MEASUREMENTS AND INTERPRETATION OF TMI-2 INSTRUMENTATION: HP-R-212 ε

J. E. Jones J. T. Smith M. V. Mathis

Prepared for the U.S. Department of Energy **Three Mile Island Operations Office** Under DOE Contract No. DE-ACO7-76IDO1570

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GEND-INF-017 Volume VIII

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FIELD MEASUREMENTS AND INTERPRETATION OF TMI-2 INSTRUMENTATION: HP-R-212

GEND-INF--017 Vol. 8

J. E. Jones \mathcal{A}^{c} and \mathcal{A}^{c} J. T. Smith M. V. Mathis

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APPENDIX

 $\Delta \phi = 0.5$

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dia.

 $\frac{1}{2}\rho^{\frac{1}{2}}+4\pi$

 \mathcal{F}_{max}

 $\mathcal{L}^{\text{max}}_{\text{max}}$

 $\Delta \sim 10^5$

 $\sim 10^{11}$ km $^{-1}$.

A.

 $\mu=1/\sqrt{2}$

1. INTRODUCTION

During and following the TMI-2 accident, a number of instruments failed or were suspected of providing erromeous readings. Because of this problem, industry concerns were focused upon the behavior of instrumentation under adverse conditions. To better understand failure mechanisms, the Technical Integration Office (TIO) contracted Technology for Energy Corporation (TEC) to perform field measurements on a set of selected TMI-2 instruments to determine in-situ operating characteristics. For some instruments, these measurements were to be performed prior to removal (and replacement with new instruments) in order to have a cross reference with post-removal observations. For other instruments, an indication of the condition of the instrument (i.e., fully operational or failed) was desired.

This report provides the information gathered by TEC on the area radiation monitor HP-R-212. This detector was located at 305 feet elevation inside containment. This instrument consisted of a Victoreen Model 857-2 detector assembly connected to a Victoreen Model 856-2 panel alarm and approximately 1200 feet of interconnecting cable. This instrument was believed to have failed due to a constant 45 mR/hr radiation level indication and due to a lack of response to the manually activated checksource in the detector. As a result of this failure, the detector was a candidate for early replacement to provide long-term radiation monitoring capability inside containment.

 $1 - 1$

2. INSTRUMENT LOCATION. CABLING, AND TERMINATIONS

A review of appropriate drawings from V1ctoreen and Bums & Roe (itemized in the Appendix in the measurement procedure, page A-5) resulted in the composite electrical diagram shown in Figure 2-1. From this information, Table 2-1 gives a list of the appropriate termination points for performing measurements in the Control Room in Cabinet 12. Also noted in Figure 2-1 are the cable lengths pulled during instrument installation (before final trimming) between each termination and/or junction pOint.

The detector assembly is a V1ctoreen Model 857-2 which is shown in Figure 2-2 along with required interfacing connections to the readout module. Figure 2-3 shows the functional layout of the detector and associated readout module. This assembly is a "medium range" device with a range of 0.1 to 10^4 mR/hr. An electrical diagram of the detector circuit is shown in Figure 2-4. As shown in Figure 2-1, the circuit is somewhat complicated by the presence of a remote alarm/meter and a second remote alarm which are used as local indicators of the radiation levels.

Since measurements were being made in the control room, there was no way to remove the effect of the remote alarm/meter (attached to the signal line) from the observed instrument response. However, since the remote alarm/meter was located outside containment, it did not experience the severe operating environments and thus was not considered to present any measurement problems. (The remote alarm was located inside containment,

 \sim 2-1

 $2 - 2$

Table 2-1

TERMINATION POINTS FOR HP-R-212 MEASUREMENTS

*From cable IT18701

**CS = Checksource coil positive and return contacts (exact identification
not necessary).

Figure 2-2. Sketch of Instrumentation for HP-R-212.

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2·4

BALLA

Figure 2-3 Functional Layout of Detector and Readout Module.

 $\frac{1}{2}$

 $5 - 2$

but was isolated from the signal line by the remote alarm/meter circuitry.) Similarly, the Hodel 356-2 Readout Module, located in the control room, was not specifically considered to be a source of instrumentation problems excspt in its function of supplying power co the detector assembly.

 $\frac{1}{\ell}$

3. PREPARATION OF MEASUREMENT PROCEDURES

As a result of generating the composite electrical diagram and from a review of the Victoreen Area Monitor Operation Manual, the major types of measurements to be performed were identified as:

- 1. Determine as-found condition of Readout Module and Remote Meter and record signal output
- 2. Perform passive measurements (i.e., passively monitor signals) on each electrical connection consisting of time doma1n waveforms, very-high frequency spectrum analysis (i.e., MHz region), and frequency spectra below 100 kHz
- 3. Perform resistance, capacitance, impedance, and T1me Doma1n Reflectometry (TOR) active measurements (i.e., actively introducing a test signal).

These measurements were designed to verify the operation of the Readout Module (especially the power supplies), but the focus of the measurement was on the detector assembly, cabling, and terminations/connections to the assembly. The Appendix contains the detailed procedure which was followed during the measurement program, and a summary of measurements is presented in the next section.

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 $3 - 1$

4. MEASUREMENTS

Since the output of HP-R-212 was designed to cover the range of 0 to +10 volts, the signal could be directly measured without am91iffcation. Before performing measurements, the readout of HP-R-212 indicated 45 mR/hr for the ganma dose fnside containment. Activation of the check source had no effect on the output reading. The Signal In was then recorded for approximately 10 minutes on an FM recorder and various outputs measured with a DVM. These measurements yielded the following results:

10 V power Supply @ 10.1 V Signal Out @ 4.3 VDe 600 V Power Supply @ 469 VDe @ 599 VDe (no load)

Checksource $@13.8$ ma.

The next measurements consisted of photographing the output waveforms of the checksource, Signal In, and power, supplies from:a storage oscilloscope. Figures 4-1 to 4-6 show the results of these time trace measurements. Along with the time traces, both high and low frequency spectra (frequency domain) were taken of the Signal In and power supplies. Figures 4-7 to 4-9 show the measured spectra over high frequency bandwidths (>1 MHz), while Figures 4-10 to 4-12 show spectra over bandwidths below 100 kHz.

Following the frequency spectra measurements, electrical calibration was performed on the HP-R-212 readout module by a TMI technician. No significant adjustments were noted during this calibration. (See calibration

4.1

Photo # $102-1$ Time - 5msec $\sin - 0.1 \text{V/div}$ $\bar{\mathcal{L}}$

 $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$

 \mathbf{v}

Figure 4-1. Typical Fluctuations Present on
Checksource Line 1.

 $\frac{1}{2} \sum_{i=1}^{n} \frac{1}{i} \sum_{j=1}^{n} \frac{1}{j}$

ti
1990

Photo #102-2 Time - 2msec

 $Gain - 0.1V/Div$

Figure 4~2. Typical Fluctuations Present on Checksource Line 2.

4-3

:'hoto #102-3 Time -50 µsec .;ain - 10mv/d1v

Photo #102-4 rime - 5msec $3ain - 10mV/div$

Photo #102-5 Time - O.lmsec $3ain - 20mV/div$

Figure 4-3. AC Variations on the 600V Power Supply.

 $4 - 5$

Photo $#102-6$ Time -5μ sec $3ain - 2V/div$

Photo $#102-7$ Time -10μ sec $\sin - 2V/div$

Figure 4-4. AC Variations on the Signal Output.

4-6

D. 中国中国的一个国家

?hoto #102-8 Time -10μ sec $Jain - 50mV/div$

 $\frac{1}{2} \frac{1}{2} \frac{d^2}{dx^2}$

 $\sim 10^{11}$ km s $^{-1}$

 $\mathcal{O}(\mathcal{E}_\mathbf{a}^{\mathrm{max}})$

l'hoto *#102-9* Time - 2rnaee $\sin - 50$ mV/div

Figure 4-5. AC Variations on the lOV Power Supply.

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 $\frac{1}{2} \left(\frac{1}{2} \right)$, where $\frac{1}{2} \left(\frac{1}{2} \right)$

 ~ 10

Figure 4-8. High Frequency Spectrum **of** Signal Output.

Frequency (kHz)

100 kHz F-MAX

+10db Reference

20 kHz harmonics illuminated

(16 kHz also present)

走过度:

Figure 4-10. Low Frequency Spectra of 600V Power Supply.

 $4 - 11$

Photo #102-17 100 kHz F-MAX +10db Reference 40 kHz harmonics illuminated

 $\lesssim 51$

Photo #102-18

1 kHz F-MAX

... 10db Reference

- .. ; lW

60 Hz harmonics illuminated

Figure 4-11. Low Frequency Sprectra of Signal Output.

 $\Delta \sim 10^{-10}$ km

 ~ 10

 $\frac{1}{2}$, Δ , γ Photo #102-19 100 kHz F-MAX +10db Reference 20 kHz harmonics illuminated

 $\sqrt{N_{\rm L}}=N_{\rm C}$, where \sim

 $\frac{1}{2} \left(\frac{1}{2} \right) \left(\frac{1}{2} \right) \left(\frac{1}{2} \right)$

 $\label{eq:3} \mathbb{E}\left[\left\{f_{\alpha\beta}^{\dagger},\beta\right\} \left(\frac{f_{\alpha\beta}^{\dagger}}{2}\right)^{\beta}\right]_{\alpha\beta}$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\$

data sheet in the Appendix on page A-20.) After electrical calibration, power was removed from HP-R-212. The test fixture was removed and all signal lines from cable IT18101 to cabinet 12 were disconnected.

A series of active measurements (i.e., actively introducing a test signal into the circuit) was then performed. Table 4-1 shows the results of capacitance, impedance, and OC resistance measurements on some of the field cable lines (see Appendix pages A-14 and A-16 for a complete set). A set of TOR measurements was taken on the signal lines to determine possible cable defects. These TOR traces are shown in Figures 4-13 to 4-16.

4-14

7 **ZW7=**

Table 4-1

 $4 - 15$

CAPACITANCE, IMPEDANCE, AND RESISTANCE MEASUREMENTS

*Values in parentheses are reverse polarity values.

**Indicates variable response.

 $4 - 16$

STRIP CHART 102-1

TB110: 1 to 2

Signal - Check Source

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 $\label{eq:2.1} \begin{array}{ll} \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\mathcal{A}) \\ \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\mathcal{A}) & \mathcal{L}_{\mathcal{A}}(\math$

 $\mathbf{M}^{\text{M}}_{\text{H}}(\mathbf{g}^{\text{M}}_{\text{H}}(\mathbf{g}^{\text{M}}_{\text{H}}(\mathbf{g}^{\text{M}}_{\text{H}})))$

 S etting - 500mp/div \boxplus Range - 52.6 ft/div $\overline{\mathbb{B}}$ Sensitivity - 0.5 15 hz filter 2nd plot begins @ 800 ft. Cable dielectric - other

4-17

STRIP CHART 102-3 TBllO: 6 to 7 Signal - Signal In

~etting - 500mp/div Range - 52.6 ft/div Sensitivity - 0.5 15 hz filter 2nd plot begins @ 800 ft. Cable dielectric - poly

Figure 4-15. TOR Traces from the Signal-In Cable.

STRIP CHART 102-4 TB110: 8 to 10 $Signal - +10V$

Atter Chr 7

sto the Cips Filips

 $4-19$

Setting -500 mp/div Range - 52.6 ft/div Sensitivity - 0.5 15 hz filter 2nd plot begins @ 800 ft. Cable dielectric - poly

5. SUMMARY AND INTERPRETATION OF MEASUREMENTS

This section presents a surrmary of the interpretation of the measurements taken on HP-R-212. This interpretation is intended to indicate the condition of the device based on observed data.

5.1 SUMMARY OF MEASUREMENT S

The 10 V power supply measurements indicated a 10.1 VDC output value, which is within the expected range. The 600 V power supply was measured at 469 VDC when connected to the detector assembly, but 599 VDC when the connecting cable to the assembly was removed. This indicates an excessive load on the high voltage due to some problem in the detector or cable, or a defective power supply. The Signal In measurement produced a 4.3 VDC reading, which is lower than the expected value of 5.0 VDC for a 0-10 V pulsing output. Measurements on the checksource produced a 13.8 ma current load, which indicates the electrical path through the checksource coil is 1ntact.

The time traces and frequency spectra were used to summarize the major characteristics of the measured waveforms. Results of this summary are presented in Table 5-1. Both the power supplies exhibit normal characteristics when compared to other TMI-2 measurements. The only indication of a possible problem is from the relatively large 100 mV P-P 120 hertz ripple in the 10 V supply; however, this is not believed to be large enough to cause failure of the instrument.

5-1

 $\sum_{i=1}^{n} \frac{1}{i}$

Table 5-1

CHARACTERISTICS OF MAJOR SIGNAL LINES

 $\label{eq:2.1} \mathcal{L}(\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}})) = \mathcal{L}(\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}})) = \mathcal{L}(\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}}))$ $\label{eq:2.1} \frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^{2} \left(\frac{1}{\sqrt{2}}\right)^{2} \left(\$ $\mathcal{E}_{\rm eff}$, and $\mathcal{E}_{\rm eff}$ $\{x_{1},x_{2},\ldots,x_{n}\}$, where $\{x_{i},x_{i}\}$ is the contribution of the contribution of \mathcal{A} $\sim 10^{11}$ m $^{-1}$

 $\label{eq:2.1} \begin{split} \mathcal{L}_{\text{max}}(\mathbf{r}) & = \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \\ & = \frac{1}{2} \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \\ & = \frac{1}{2} \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \mathcal{L}_{\text{max}}(\mathbf{r}) \\ & = \frac{1}{2} \mathcal{$ \mathcal{L}_{max} and \mathcal{L}_{max} . $\label{eq:2.1} \mathcal{L}(\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}})) \leq \mathcal{L}(\mathcal{L}^{\text{max}}_{\mathcal{L}}(\mathcal{L}^{\text{max}}_{\mathcal{L}}))$ $\mathcal{L}(\mathcal{A})$ and $\mathcal{L}(\mathcal{A})$ and $\mathcal{L}(\mathcal{A})$ and $\mathcal{L}(\mathcal{A})$ $\label{eq:2} \frac{d\mathcal{L}}{d\mathcal{L}} = \frac{1}{2\pi}\frac{d\mathcal{L}}{d\mathcal{L}} \left(\frac{d\mathcal{L}}{d\mathcal{L}} \right)^{2d\mathcal{L}} \left(\frac{d\mathcal{L}}{d\mathcal{L}} \right)^{2d\mathcal{L}} \left(\frac{d\mathcal{L}}{d\mathcal{L}} \right)^{2d\mathcal{L}}.$

 $\label{eq:2.1} \frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{i=1}^n\$

The Signal In waveform would normally be 0-10 V pulses with a frequency proportional to the radiation present. The oscilloscope photograph of the Signal Out line (Figure 4-4) shows that the output is a periodic waveform of approximately 6 volt peak-peak variation (and a 4.3 volt offset). Frequency spectra show the frequency of the signal to be 40 kHz and nearly sinusoidal. Resistance data (Table 4-1) similarly indicate a problem among the Signal In, +10V, and Shield 11nes. Table 5-2 gives a comparison of resistance data from a new detector assembly to that from HP-R-212. All resistances are higher than for the new assembly. but only the Signal In-Shield (+) and the Shield-l0 V (.) show a significant increase.

The capacitance and impedance data given in Table 4-1 is difficult to quantitatively interpret due to active components in the circuitry, but qualitative results are possible. Very low effective capacitance values would be expected from most signal lines except for the $+10$ V to ground. which has a 100 pF capacitor present. The checksource lines indicate the presence of the coil inductance (negative capacitance) which is also expected. Impedance data is reasonable and exhib1ts major trends expected from the circuitry such as reducing values at higher frequency for the Signal In.

The results of TDR measurements performed on the cable (shown in Figures 4-13 to 4-16 are summarized in Table 5-3. Note that the lengths identified in the table are only approximate, since no calibration of the cable resistance and material composition was performed on the TOR instrument. Some junction points were not identified by these

5-3

5-4 Table 5-2

rpw

COMPARISON OF MEASURED DETECTOR RESISTANCE

·Serial numbers III and 1405 composite data.

7

- Notes: (a) All values are in ohms x 10³ unless otherwise indicated.
	- (b) First signal to positive terminal. second s1gnal to negative terminal is considered Polarity + •.

 $\sim 10^{-1}$

 $\mathbf{x} = \mathbf{y}$

(c) All measurements made with a Keithley 177 DVM or 20×10^3 ohm scale. **College**

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Table 5-3

SUMMARY OF TDR MEASUREMENTS

Note: Distances are not calibrated due to lack of prior information on the cable type which prevented calibration tests.

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*TDR to terminal block test cable (15 ft) not included in distance. **R is the abbreviation for resistance.

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 $\mathcal{A}^{\text{max}}_{\text{max}}$

meastlrements, but this is not unusual due to the cable lengths involved and the small resistance changes that would occur at terminal block junctions. The only unusual inflection occurred on the 10 V power supply line which indicated an interface resistance at approximately 289 feet from the control room. However, measurements did not indicate a resistance change on the 10 V line, and this was not considered to be a problem.

5.2 INTERPRETATION OF MEASUREMENTS

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Based upon the observation of a periodic 40 kHz output on the Signal In line from the detector and the excessive loading on the 600 V power supply, it appears that the Geiger tube has f_{α}^{3} iled. If the tube failed in an ionized condition (i.e., depletion of the quench gas), there would be an excessive current load on the 600 V power supply which could result in the observed drop in the supply voltage. Similarly, the detector assembly contains an "anti-jam" circuit which is designed to produce a periodic output upon saturation of the Geiger tube. This was designed to prevent loss of signal in the event of over-range radiation levels, but would also be triggered by a "shorted" tube.

In addition, the output of the detector should consist of 0-10 V pulses even if the "anti-jam" circuit is active. The observed output was nearly sinusoidal, ranging from approximately 1.3 V to 7.3 V, and resistance measurements indicated an increase in the expected values. A review of the detector circuit shows that this behavior could be explained by a failure of transistor Q7. The measurements indicate that

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6. CONCLUSIONS

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Based on the measurements, data reduction, and circuit analysis of HP-R-212, there is an indication of failure of the instrument. The observed output signals and resistance measurements suggest that the Geiger tube is in a continuously ionized state and that the output is being generated by the "anti-jam" circuit. Also, there is an indication that one of the output driver transistors, Q7, has failed. The result of these failures is a nearly sinusoidal 40 kHz output that spans approximately 6 volts peak-peak and is erroneously interpreted as a 45 mR/hr detector response by the readout module.

 $\mathcal{L}^{\text{max}}_{\text{max}}$ and $\mathcal{L}^{\text{max}}_{\text{max}}$ $\label{eq:2.1} \mathcal{L}_{\mathcal{A}}(\mathbf{q}) = \math$ $\mathcal{L}^{\mathcal{L}}(X)$ and $\mathcal{L}^{\mathcal{L}}(X)$ are the set of the contribution of the 医牙状细胞 医慢性呼吸 计数据存储器 医牙状细胞 计结构

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Control Room Panel 12, 331elov. L ocafion:

Limits and Precautions: a) Personnel

b) Equipment

 \bullet

c) Environment

d) Nuclear

Post Maintenance Testing required and Acceptance Criteria.

ORIGINATOR—SUPERVISOR—SUPERVISOR OF MAINTENANCE—MAINTENANCE FOREMAN—
JOB PERFORMER—MAINTENANCE FOREMAN—SUPERVISOR OF MAINTENANCE

Page A-2 WORK REQUEST PROCEDURE **TMI Nuclear Station** .. Maintenance Procedure Format and Approval Unit No. $\angle Z$ This form outlines the format and acts as a cover sheet for a maintenance procedure. Due to the limited size of the form, additional pages may be attached as required. Work Request procedure AP 1016 Section 6 should be used as a guide in preparing the maintenance procedure. ocedure Title & No.:
Cable & Detector Performance Check for HP R. 212 ure Title & No.:
bll & Detector Performance Check for HPR.
e: To olitermine if improper reading ols to 1. Procedure Title & No.: encours response use for more en 3. Description of system or component to be worked on: $HP-L. 212$ 4. References: Victoren Manual 5. Special Tools, and Materials required. See attached 6. Detailed Procedure (attach additional pages as required) See attached Supervisor of Maintenance recommends approval *L'Aught* Unit No. 1 Chairman __________________ Date __________________ Unit No. 2 Chairman, _____________ Date ______ • UNIT SUPERINTENDENT APPROVAL Unit No.1 ______ - Dllte_~.,...-~_ Unit No.2 _____ Dati _____ _ • Standing Procedure ______ ~_-_~ ___ ---- Supervisor of OC Oate * Note: These approvals required only on Nuclear Safety Related/Radiation work permit jobs. TMI-94 2-78

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt$

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Page A-4

IN-SITU MEASUREMENTS OF CABLES AND SIGNALS TITLE FROM AREA RADIATION MONITOR HP-R-212

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integretary measurements on the appropriate instrumentation cables by inserting test signals on appropriate conductors of Cable IT1870I (terminations shall be removed and replaced on TB110 of Cabinet 12). Should these tests reveal cable integretary problems further verification measurements will be made at TB1 of the appropriate Remote Alarm/Meter (Victoreen Model 858-3) located in the anteroom.

Table 4-1 Active Measurements

d. In the calibration verification measurements section, baseline data on the as-found condition will be recorded prior to the performance of any adjustments or electronic calibrations.

- B. Prerequisites
	- 1. The Shift Supervisor/Shift Foreman shall be notified for concurrance prior to the performance of those measurements. At $5 - 1$
	- 2. Instrumentation personnel shall be assigned to assist in the perfort mance of these measurements.
	- 3. All measurements and test instrumentation shall be in current calibration (traceable to NBS).

PAGE 2 of 15

 $\label{eq:2.1} \lim_{\lambda\to 0} \frac{1}{\lambda} \left(\frac{1}{\lambda} \int_{\mathbb{R}^3} \frac{1}{\lambda} \right) \frac{1}{\lambda} \right) \right) \lambda \, d\lambda \right) = \frac{1}{\lambda} \int$

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{0}^{\pi} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\pi} \frac{1}{\sqrt{2\pi}}\int_{0}^{\pi} \frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2\pi} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\int_{0}^{\pi} \frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{2\pi}}\frac{1}{\sqrt{$

 $\label{eq:2} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{d\mu}{\mu}\left(\frac{d\mu}{\mu}\right)^2\frac{d\mu}{\mu}\left(\frac{d\mu}{\mu}\right)^2\frac{d\mu}{\mu}\left(\frac{d\mu}{\mu}\right)^2.$

 $\label{eq:3.1} \begin{split} \mathcal{L}_{\text{in}}(\mathbf{r},\mathbf{r}) = \mathcal{L}_{\text{in}}(\mathbf{r},\mathbf{r}) \times \mathcal{L}_{\text{in}}(\mathbf{r},\mathbf{r}) \times \mathcal{L}_{\text{in}}(\mathbf{r},\mathbf{r}) \times \mathcal{L}_{\text{in}}(\mathbf{r},\mathbf{r}) \times \mathcal{L}_{\text{in}}(\mathbf{r},\mathbf{r},\mathbf{r}) \times \mathcal{L}_{\text{in}}(\mathbf{r},\mathbf{r},\mathbf{r}) \times \mathcal{L}_{\text{in}}(\mathbf{r},\mathbf$

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{0}^{\infty}\frac{1}{\sqrt{2\pi}}\left(\frac{1}{\sqrt{2\pi}}\right)^{2}d\mu\,d\mu\,.$

STEPS

1. NOtify Shift Supervisor/Shift Foreman of start of test on HP-R-212.

2. Verify power is applied to H?-R-212.

 $\frac{1}{2}$ Signature/Date ~/

3. Record present signals and readings and indications on 856-2 Readout Module (Local & Remote). Record Signal-in at TBllO-6/7 and record output for 30 minutes on FM Tape Recorder. Remove recorder when finished.

Page A-7 **NO.**
TP-102 IN-SITU MEASUREMENTS OF CABLES AND SIGNALS TE TITLE FROM AREA RADIATION MONITOR HP-R-212 REV. n Meter/Indicator/Switch Local Rmte N/A ДK mR/hr Meter Reading Off-Operate-Alarm Function Switch OPERATE N/A Fail Safe Indicator On 0ff N/A 0 ff High Alarm-Reset Indicator 0n N/A $(\tau \epsilon c)$ quature/ Date 9/11/90 4. Using a Keithley Model 177 DMM (or equivalent) and an electrostatic voltmeter ($Z_i \ge 10^{12}$ OHMS, Range 0-2000 V, Precision = \pm 1%) measure the DC voltage or current at the following test points. NOTE: For signal d. it will be necessary to depress Fall-Safe Check Source push button during the measurement. Note: GPU Fluke Differential Voltmeter SE Jus **PAGE 5 of 15**

*Decouple DC Voltage.

Sync the oscilloscope and photograph the waveform using up to three time base
and vertical gain settings. (The necessity of 3 photographs will be deter-
mined by visual analysis by the field engineer.) Mark the back of the

 (TEC) $9/17/30$ Signature/Date

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Sandhi dheerika

Page A-11 NO.
TP-102 IN-SITU MEASUREMENTS OF CABLES AND SIGNALS TITLE FROM AREA RADIATION MONITOR HP-R-212 REV. Ω 7. Using the Nicolet Model 444 FFT Analyzer (or equivalent) perform FFT analysis of signals from the following test points: SIGNAL CABINET 12 **PARAMETER** PHOTO # $0 - 100$ kHz $102 - 15$ $+600V$ \star a. TB110-5 $0 - 1 kH$ $102 - 16$ TB110-10 **GND** $0 - 100R$ H_2 $102 - 17$ SIG IN TB110-6 b. $0 - 1$ h H _{t} TB110-7 **GND** $102 - 18$ TB110-8 $+10V$ $102 - 19$ $0 - 100hHz$ ċ. TB110-10 **GND** *Decouple DC voltage input to Spectrum Analyzer (50VDC Max input) If PSD plots from any one of the three signals show high or unusual amplitudes, utilize the zoom feature to provide finer resolution and obtain PSD data in the frequency band of interest. Λ (TEC) 9/17/80 gnature/Date $8.$ Inside Cabinet 12 perform usual electronic calibrations using applicable instrument shop procedures. Attach a copy of the instrument shop calibration data sheet and identify any significant adjustments in the space below: PAGE⁹ of 15

S Shan 17 (TEc) $9/18/5c$

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11. Using the Hewlett-Packard Model 4274 (or equivalent) Impedance Bridge measure the capacitance and impedance of the following test points:

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*Numbers in parentheses refer to TB110 terminal numbers (field side).

Record the data required below:

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 $\hat{\mathcal{A}}$

 $\mathcal{L}_{\rm{max}}$

 $\label{eq:2.1} \mathcal{A}_{\mathcal{A}} = \mathcal{A}_{\mathcal{A}} \left(\mathcal{A}_{\mathcal{A}} \right) \otimes \mathcal{A}_{\mathcal{A}} \left(\mathcal{A}_{\mathcal{A}} \right)$

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 $\label{eq:1} \frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1}{\sqrt{2}}\sum_{i=1}^n\frac{1$

 $\frac{1}{2}$

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Page A-18

JOB TICKET (WORK REQUEST)
REVIEW - CLASSIFICATION - ROUTING CONTROL FORM

GENERATION CORRECTIVE MAINTENANCE SYSTEM CM STATUS ACTIVITY FORM Page A-19

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Page A-20

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Model
Serial

 $\bar{\epsilon}$

MTX-501

Area Monitor

 $40 - R - 212$

DETECTER

RATEMETER \pm

 $\mu_{\rm{max}}$, $\mu_{\rm{max}}$, $\sigma_{\rm{max}}$

Model
Serial

 \mathcal{L}

Check Source Rdg. _________ Mr/Hr

Fail Safe Volts

Ratemeter

Section

STRIP CHART 102-5 TB110: 10 to 10

 $Signal - GND$

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