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FIELD MEASUREMENTS AND INTERPRETATION OF TMI-2 INSTRUMENTATION: CF-2-LT4

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Section 1

INTROlJUCTION

During and following the TMI-2 accident, a number of instruments failed or were suspected of providing erroneous readings. Eecause of this problem, industry concerns were focused uporl the behavior of instrumentation under adverse conditions. To better understand failure mechanisms, the Technical Integration Office (TIO) contracted Technology for Energy Corporation (TEC) to perform field .neasurements on a set of selected TMI-2 instruments to determine in-situ operating characteristics. For some instruments, these measurements were to be performed prior to removal (and replacement with new instruments) in order to have a cross reference with post removal observations. For other instruments, an indication of the condition of the instrument (i. e., fully operational or failed) was desired.

This report describes the measurements and rerults of the Core Flood Tank IB level monitor CF-2-LT4. This instrument consists of a Bailey Type BY Process Computer Transmitter connected to a readout module by approximately \circ 30 feet of cable through a penetration junction and an instrument mounting junction. The status of this instrument is uncertain, but it was producing a reasonable output reading which implied it had not failed. As a result, measurements on this instrument were designed to determine if it was properly functioning.

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Section 2

INSTRUMENT LOCATION, CABLING, AND TERMINATIONS

A review of appropriate drawings from Bailey Meter Company and Burns & Roe (itemized in the Appendix in the measurement procedure, pages $A-5$ and $A-6$) resulted in the composite electrical diagram shown in Figure 2··1. From this information, Table 2-1 gives a list of the appropriate termination points for performing measurements in Control Cabinet 156. Also noted in Figure 2-1 are the cable lengths pulled during instrument installation and lengths after trimming between each termination and/or junction point.

The level sensing assembly is a Bailey Type BY which consists of a differential pressure LVDT, temperature compensation, and calibration adjustment for conversion of pressure difference to level. This instrument has a normal range of $0-14$ feet, producing an output of -10 to $+10$ volts. The functional diagram of the unit is shown in $Figure 2-2.$

Since measurements were being made in Control Cabinet 156, the effect of the readout meter (attached to the signal line) was present on the observed instrument response. However, since this readout was located outside containment, it did not experience severe operating environments, and thus was not considered to have failed.

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Composite Electrical Diagram for Core Flood Tank
Level Transmitters CF-2-LT2 and CF-2-LT4. Figure $2-1$.

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Table 2-1

TERMINATION POINTS FOR CF-2-LT4 MEASUREMENTS

* From cables IT1730I (signal lines) and IT2751C (118 VAC).

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Continued in A

Figure 2-2. Functional Diagram of Bailey Type BY Differential Pressure Transmitter.

Section 3

PREPARATION OF MEASUREMENT PROCEDURES

As a result of generating the composite electrical diagram and from a review of the Bailey Meter Product Instruction E21-17 Manual, the major types of measurements to be performed were identified as:

- 1. Determine as-found condition of level indication and record signal output.
- 2. Perform passive measurements (i.e., passively monitor signals) on each electrical connection consisting of time domain waveforms, very-high frequency spectrum analysis (i.e., MHz region), and frequency spectra below 100 kHz.
- 3. Perform resistance, capacitance, impedance, and Time Domain Reflectometry (TOR) active measurements (i.e., actively introducing a test signal).

These measurements were designed to verify the operation of the Readout Module and the power supplies, but the focus of the measurement was on the level measurement assembly, cabling, and terminations/connections to the assembly. The Appendix contains the detailed procedure which was followed during the measurement program, and a summary of measurements is presented in the next section.

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Section 4 MEASUREMENTS

Since the output of CF-2-LT4 was designed to cover the range of -10 to +10 volts, the signal could be directly measured without amplification. Before performing measurements, the readout of CF-2-LT4 indicated 11 feet for the core flood tank level. The level indication signal was then recorded for approximately 10 minutes on an FM recorder and the voltage outputs measured (with a DVM). The output of the level signal was 5.72 VDC, and the power supply was 116 VAC.

The next measurements consisted of photographing the output waveforms of the level signal and line voltage flom a storage oscillosco \sim o. Figures 4-1 and 4-2 show the results of these time trace measurements. Along with the time traces, both high and low frequency spectra (frequency domain) were taken of the level signal. Figure 4-3 shows the measured spectra over both a 6 MHz and 500 kHz bardwidth, while Figure 4-4 shows spectra over both a 100 kHz and 1 kHz range.

Following the frequency spectra measurements, electrical calibration was performed on the CF-2-LT4 readout module by a TMI technician. No significant adjustments were noted during this calibration. After electrical calibration, power was removed from CF-2-LT4. The test fixture was removed and all signal lines from cables IT17301 and IT2751IC to cabinet 156 were disconnected.

A series of active measurements (i.e., actively introducing a test signal into the circuit) was then performed. Table 4-1 shows the

4-1

Photo 109-2 Time - 0.5msec/div Gain - 20 mV/div

Figure 4-1. Oscilloscope Traces of Level Signal.

Photo 109-3 Time - O.5msec/div $Gain - 10 V/div$

Figure 4-2. Oscilloscope **Trace of 118 VAC Supply.**

Photo 109-4 $BW - 3$ KHz Scan width - 1 MHz/div Scan time - 1 sec/div

Photo 109-5 $BW - 3$ KHz Scan width - 100 KHz/div Scan time - 1 sec/div

Figure 4-3. High Frequency Spectra of Level Signal.

Enequency (kHz)

0.000478 RMS

 $-30d\overline{t}$

Photo - $109-6$ 100 KHz Range

1 KHz Range

Frequency (Hz)

$4 - 6$

Table $4-1$

CAPACITANCE, IMPEDANCE, AND RESISTANCE MEASUREMENTS

 γ \star nF = Nang-farads.

**Values in parentheses are reverse polarity values.

 $[†]$ OF indicates overflow condition.</sup>

results of capacitance, impedance, and DC resistance measurements on some of the field cable lines (see Appendix page A-12 for a complete set). A set of TDR measurements were taken on the signal lines to determine possible cable defects. These TOR traces are shown in Figures 4-5 to 4-8.

Figure 4-5. TOR Trace of Level Signal Lines

STRIP CHART 109-2

Figure 4-6. TOR Trace of (+) Signal to Shield

4-9

Setting - 500 up/div Kange - 52.6 ft/div Sensitivity - 0.25 Filter - 5 a Cable dielectric - other 2nd plot begins @500 ft

Figure 4-7. TDR Trace of 118 VAC Lines

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 $\frac{1}{2} \sum_{i=1}^n \frac{1}{2} \sum_{j=1}^n \frac{1}{2} \sum_{j=$

STRIP CHART $iC9-5, 6, 8$ 7

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Figure 4-8. TOR Trace of 118 VAC (H) to Shield

Section 5

INTERPRETATION OF MEASUREMENTS

This section presents a summary of the interpretation of the measurements taken on CF-2-PT4. This interpretation is intended to indicate the condition of the device based on observed data.

Since this device varies from -10 to +10 volts for a 0 to 14 foot level range, the observation of 11 foot level readout indicates that the voltage should be 5.71 volts. The measured value of 5.72 volts matches within 1% of this expected value, which indicates the readout meter is correctly calibrated. The 116 VAC value on the power supply line is also well within a normal operating range.

The time traces and frequency spectra do not indicate any serious contamination which would affect the DC readout. Table 5-1 lists the low level AC components present on the level signal. Note that even though up to 60 mV P-P fluctuations are present, readout devices normally respond at low frequencies. As a result, the worst-case effect of these AC variations is likely to be less than the 0.5 mV RMS value given for the 60 Hz components.

One feature of the frequency spectrum of the level signal gives an indication that the differential pressure LVDT *(see* Figure 2-2) is operating. Since the LVDT AC output is "demodulated" by a full-wave rectifier and Resistance-Capacitance (RC) smoothing. a low level ripple must be present at the frequency of the internal oscillator. The oscillator for this type device operates at 1000 hertz and the component

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5-2

Table 5-1

MAJOR AC COMPONENTS ON THE LEVEL SIGNAL

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values of the RC smoothing circuit ($R = 100k$ ohms, $C = 0.68 \text{ }\mu\text{F}$) would produce a ripple factor (fraction of AC RMS fluctuations) of 0.001. With the device producing a five volt output (15 volts above base output of $-10V$, the expected RMS ripple would be approximately 5 mV (15 mV). From Table 5-1, this AC ripple value was measured to be 6 mY. which is in close agreement. Also, the reduction in amplitude of the higher harmonics (see Figure 4-4) is consistent with the expected attenuation cf a rectified signal.

The capacitance) impedance, and resistance data given in Table 4-1 is difficult to quantitatively interp: 't, but qualitative results are nnssible. Most of the data indicates very low effective capacitance values, ~hich would be expected from the amplifier section of the transmitter. However, the 118 VAC (H) to 118 VAC (L) measurement passes through the primary of a transformer. This creates an inductance which appears as negative capacitance at the 100 hertz measurement.

The presence of a 10.000 ohm resistor in the transmitter amplifier and the absence of other direct electrical paths indicates that a resistance measurement near this value should be obtained. The measured values for the level signal were 7100 and 8800 ohms for two polarities. The variation would be caused by active electrical components, and the values are of the magnitudes expected. Since the expected responses are present, there is no obvious indication of instrumentation degradation from these measurements.

5-3

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The results of TOR measurements performed on the cable (shown in Figures 4-5 to 4-7) are summarized in Table 5-2. Note that the lengths identified in the table are only approximate, since no calibration of the cable resistance and material composition was performed on the TDR instrument. Some junction points were not identified by these measurements, but no indication of cabling problems is present in this data.

5-5

E.

Table 5-2

SUMMARY OF TDR MEASUREMENTS

Note: Distances are not calibrated due to lack of prior information on the cable type which prevented calibration tests.

* TDR to tenninal block test cable (15 ft) not included in distance. ** R is the abbreviation for resistance.

Section 6

CONCLUSIONS

Based on the measurements, data reduction, and circuit analysis of CF-2-LT4, there is no indication of degradation of the instrument. The only significant contamination present in the pressure signal that appeared to be abnormal was the 96 kHz component. However, the amplitude of this signal was relatively low and, from other measurements performed at TMI, this low-level 96 kHz component is probably due to a widespread l6 kHz (with harmcnics) signal found in various circuits. In addition to the observation of no abnormal characteristics of the instrument, the low level oscillator ripple on the level signal indicates that the LVDT is working. Therefore, it appears that CF-2-LT4 is operating correctly, but these measurements could not determine if it is calibrated.

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APPENDIX

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ORIGINAL FIELD PROCEDURES AND DATA SHEETS FOR CF-2-LT4

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REVIEW - CLASSIrium Page A-2 nuuriNG CONTROL FORM

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WORK I **EDURE** Page $A-3$ Maintenance Procedure Format and Approval $\mathbf{2}$ Unit No. This form outlines the format and acts as a cover sheet for a maintenance procedure. Due to the limited size of the form, additional pages may be attached as required. Work Request procedure AP 1016 Section 6 should be used as a guide in preparing the maintenance procedure. \mathbf{L} Procedure Title & No.: Sensor/Cable measurements on CF-Z-LT4 To determine signal characteristics on CF-2-LT4. $\overline{2}$ Purpose: $\overline{3}$. Description of system or component to be worked on. $CF - 2 - 174$ $\overline{4}$ References: See attached Special Tools, and Materials required. $5.$ See attached 6. Detailed Procedure (attach additional pages as required See affached Date $9/2$ Supervisor of Maintenance recommends approval Whenon Kevien 1 * PORC RECOMMENDS APPROVAL Unit No. 1 Chairman **Example 12** Date Unit No. 2 Chairman Date * UNIT SUPERINTENDENT APPROVAL Unit No. 1 **Date** Unit No. 2 Date * Standing Procedure Supervisor of QC Date *Note: These approvals required only on Nuclear Safety Related/Radiation work permit jobs. MI-04 2-78

 \mathbf{A}

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IT1730I and IT2751C (Terminations shall be removed) and replaced on TB 8-9-3 of Cabinet 156).

Table 4-1 Active Measurements

B. Prerequisites

- 1. The Shift Supervisor/Shift Foreman shall be notified for concurrence prior to the performance of those measurements.
- $2.$ Instrumentation personnel shall be assigned to assist in the performance of these measurements.
- 3. All measurements and test instrumentation shall be in current calibration (traceable to NBS).
- 4. The Shift Supervisor/Shift Foreman shall be notified prior to starting and upon completion of the measurements.
- C. Procedure for Performing Measurements

References:

- 1. Bailey Meter Company Transmitter #BY-8231X-A.
- 2. Bailey Product Instruction E 21-17.

 2 of 11 $AGE =$

 118 VAC (H)
 118 VAC (L) TB $8-9-3/16$
TB $8-9-3/16$ **IT2751C** IT2751C Shield IT1730I TB 8-9-3/17 (Signal)

STEPS

 $\mathcal{L}^{\text{max}}_{\text{max}}$

1. Notify Shift Supervisor/Shift Foreman of start of test on CF-2-LT4.

Verify power is applied to CF-2-LT4. $2.$

3. Record present readings from CF-2-LT4 Readout Module.

 3 of Π 2445

Page A-7

*CAUTION: 118 VAC

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5. Using a Tektronix Model SC502 (or equivalent) oscilloscope observe the de-coupled waveform at the following test points:

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*CAUTION 118 VAC; Use X10 Probe.

Sync the oscilloscope and photograph the waveform using up to three time base and vertical gain settings. Mark the back of the photographs with the instrument tag number and parameter measured.

Date

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6. Using a Hewlett-Packard Spectrum Analyzer (Models 141T, 8533B and 8552 or equivalent) perform an analysis of the following signal for spectral content:

Before photographing each scope display adjust analyzer for best spectral resolution. Record critical analyzer parameters e.g., RF bandwidth, RF bandwidth and sweep speed on rear of photograph as well as parameter analyzed.

> 5 of 11 $2442.$

Page A-S **NC.** TP-109 IN-SITU MEASUREMENTS OF CABLES AND SIGNALS TEL $\overline{}$ FROM CORE FLOOD TANK LEVEL TRANSMITTER $F E$, 0 $CF-2-LT4$ SPECTRUM IDENT **FREQUENCY** AMPLITUDE REMARKS Log REF SENS BANDWOTH SCON WIDTH INAVY AFTEN SCON TINIC 1046206 $109 - 4$ $\overline{\mathcal{O}}$ $3Kt_{3}$ / $m\neq 1/\sqrt{210}$ 1562 \varnothing $-20d$ $15/095$ $100K$ $+3$ L_1 I_I 1_k δ $\frac{1}{2}$ 9/24/86 7. Using the Nicolet Model 444 FFT Analyzer (or equivalent) perform FFT annalysis of signals for the following test point: SIGNAL CABINET 156 **PARAMETER** PHOTO # _Iook Ronge
IK Ronge $109 - 6$ $(+)$ SIG
(-) SIG TB 8-9-3/19 a. $109 - 7$ TB 8-9-3/18 <u> {| g/eu</u> | go 3. Inside Cabinet 156 perform usual electronic calibrations using applicable instrument shop procedures. Attach instrument shop calibration data sheet and record any significant adjustments or problems in the space below. 6 of 11 PAGE.

 $\label{eq:2} \frac{1}{2}\sum_{i=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{1}{2}\sum_{j=1}^n\frac{$

<u>y</u>
19/24/80

11. Using the Hewlett-Packard Model 4274 (or equivalent) Impedance Bridge, measure
the capacitance and impedance at the following test points:

 8 of 11

 $ACE =$ $\overline{}$

Record the data required below:

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۸

 $\frac{8}{2}$ 9/24/80 Signature/Date

 $\frac{1}{2}$

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12. Using the Tektronix Model 1502 (or equivalent) TDR unit peform TDR measure-
ments at the following test points.

 9 of 11 RGE

 $\frac{1}{20} \frac{1}{2} \frac{1}{2} \frac{1}{4} \frac{1}{8}$ ろignature/Data

109,5, 109-6, 109-7

13. Using the Kaithley Model 144 (or equivalent DMM) perform resistance measurements on the test points specified and record values in the space provided.

73 8-9-3/15-20 (118 VAC/SHLD)

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