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Changing the World's Energy Future

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U₃Si₂ is being considered as a potential accident-tolerant fuel

- Compared with UO₂:
 - Lower melting temperature
 - But higher thermal conductivity may give higher margin to melting temperature
- U₃Si₂ swelling/fission gas release behavior less well characterized
 - Evidence from higher-temperature irradiation suggests pellet-form fuel would remain crystalline, have similar microstructure to UO₂ fuel
- BISON model recently developed based on these assumptions

Barani et al., J. Nuclear Mater., 522, 97-110 (2019)



 U_3Si_2 implanted with Xe at 873K (Miao et al., J. Nuclear Mater., 503, 314-322 (2018)



 U_3Si_2 irradiated at ~950 K and ~6 GWd/tU (Shimizu, NAA-SR-1062,



Lower length scale calculations to reduce uncertainty in BISON



- Sensitivity analysis of Bison U₃Si₂ swelling and gas release predictions showed strong dependence on <u>inter-granular bubble</u> <u>dihedral angle</u> and <u>surface energy</u>
 - Measured values also not available
- Surface energy and grain boundary energies were determined for U₃Si₂ using molecular dynamics (MD) calculations
 - Dihedral angle (θ) calculated from surface energy and grain boundary energy; input to Bison
- Data also used to parameterize the Marmot phase-field Beeler, Baskes, Andersson, Cooper, Y. Zhang, J. Nucl. Mater., 514, 290-298 (2019)

Lower length scale calculations to reduce uncertainty in BISON





- Sensitivity analysis also showed strong dependence on <u>saturation</u> <u>coverage of grain faces</u> (*F_{c,sat}*)
 - No measured value available for U_3Si_2
- Phase-field simulations¹ showed progress of grain boundary venting was strongly dependent on <u>intergranular bubble areal density</u> and <u>dihedral angle</u>
 - New phase-field simulations are being used to determine $F_{c,sat}$ using U_3Si_2 parameters

¹Millett, Tonks, Biner, L. Zhang, Chockalingham, Y. Zhang, *J. Nucl. Mater.*, 425, 130-135 (2012)



Phase-Field Model: Essential Physics

- Represent bubble phase and multiple grains of U₃Si₂
- Track vacancies and fission product species (Xe only)
 - Source terms for production
- Set surface energy and grain boundary energy
 - Controls dihedral angle θ
 - Remove bulk energy contribution to interfacial energy





Phase-Field Model: Grand-Potential Functional

$$\Omega = \int_{V} \left(m \left[\sum_{\alpha} \sum_{i=1}^{p_{\alpha}} \left(\frac{\eta_{\alpha i}^{4}}{4} - \frac{\eta_{\alpha i}^{2}}{2} \right) + \sum_{\alpha} \sum_{i=1}^{p_{\alpha}} \left(\sum_{\beta} \sum_{j=1,\alpha i \neq \beta j}^{p_{\beta}} \frac{\gamma_{\alpha i\beta j}}{2} \eta_{\alpha i}^{2} \eta_{\beta j}^{2} \right) + \frac{1}{4} \right]$$
$$+ \frac{\kappa}{2} \sum_{\alpha} \sum_{i=1}^{p_{\alpha}} |\nabla \eta_{\alpha i}|^{2} + \sum_{\alpha} h_{\alpha} \omega_{\alpha} \right) dV$$

- Multi-phase, multi-order parameter extension to grand-potential model
- Advantages:
 - Bulk free energy contribution is removed from interfacial energy
 - Allows interfacial thickness and energy to be set independently, enabling coarser mesh, improved computational performance
 - Similar to KKS in this respect, but do not need separate phase concentration variables, so performance is improved
 - Prevents spurious formation of additional phases at two-phase interfaces

L.K. Aagesen, Y. Gao, D. Schwen, K. Ahmed, *Phys. Rev. E*, 98, 023309 (2018). L.K. Aagesen, D. Schwen, M.R. Tonks, Y. Zhang, *Comp. Mat. Sci.*, 161, 35-45 (2019).



Phase-Field Model Evolution Equations

- Order parameters: Allen-Cahn
- Densities: change to chemical potential for each species

Gas:

Vacancies:

$$\frac{\partial \mu_g}{\partial t} = \frac{1}{\chi_g} \left[\nabla \cdot \left(D_g \chi_g \nabla \mu_g \right) + s_g \right] - \sum_{\alpha} \sum_{i=1}^{p_{\alpha}} \frac{\partial \rho_g}{\partial \eta_{\alpha i}} \frac{\partial \eta_{\alpha i}}{\partial t} \right]$$

ies:
$$\frac{\partial \mu_v}{\partial t} = \frac{1}{\chi_v} \left[\nabla \cdot \left(D_v \chi_v \nabla \mu_v \right) + s_v \right] - \sum_{\alpha} \sum_{i=1}^{p_{\alpha}} \frac{\partial \rho_v}{\partial \eta_{\alpha i}} \frac{\partial \eta_{\alpha i}}{\partial t} \right]$$



Phase-Field Model Initial Conditions

• Intergranular bubble areal density (n_a) : determine from rate theory simulations

– At 1035 K, *n*_a = 15 / μm²



Y. Miao, K.A. Gamble, D. Andersson, B. Ye, Z.-G. Mei, G. Hoffman, A.M. Yacout, *Nucl. Eng. Design*, 322, 336-344 (2017).



Phase-Field Model Initial Conditions

- Determine *F_{c,sat}*
- 1035 K
- θ/2 = 73
- No-flux Boundary Conditions
- 3 µm × 3 µm grain boundary
- Populate with randomly placed lenticular bubbles, $n_a = 15 / \mu m^2$, minimum spacing 160 nm



 $3\,\mu m \times 3\,\mu m$



Phase-Field Simulation Results



 $3 \,\mu\text{m} imes 3 \,\mu\text{m}$



Phase-Field Simulation Results



- Plot fractional coverage of GB (X_{GB}^C) and fraction of bubbles that are vented to edge of domain (X_{GB}^V) vs. time
 - Less rapid increase with respect to time compare to previous simulations of Millett et al. due to to slow buildup from source terms
- Areal density of bubbles versus time
 - Rate of coalescence relatively constant until the bubble density reaches approximately half its initial value, then slows

Informing BISON with Phase-Field Results

- Plot fraction of bubbles that are vented to edge of domain (X_{GB}^{V}) versus fractional coverage of GB (X_{GB}^{C})
- Implications for Bison:
 - Short term: set $F_{c,sat}$ where slope of curve is greatest (shown: $X_{GB}^{C} = 0.62$)



Effect of Simulation Assumptions on Predicted Value for BISON Model

Simulation initial conditions

- Maintain all simulation parameters the same including minimum spacing I_{min} = 160 nm
- Change seed in random number generator used to determine initial **bubble** positions
- 5 total configurations simulated using these parameters
- Mean $F_{c.sat} = 0.60$
- Standard deviation indicates calculated value of $F_{c.sat}$ is relatively insensitive to initial bubble configuration

Configuration	$F_{\alpha,gat}$
	0.54
2	0.62
3	0.61
:1	0.63
2	0.62
Mean	0.60
Standard Deviation	0.036



Effect of Minimum Bubble Spacing in Initial Conditions

- Also simulated *I_{min}* = 130 nm, 200 nm, 5 configurations each
- 200 nm: Initial portion of release curve delayed
- Slight decrease in $F_{c,sat}$ with I_{min} , but may be just



Min. spacing (<i>I_{min}</i>), nm	F _{c,sat}
130	0.61 ± 0.039
160	0.60 ± 0.036
200	0.58 ± 0.046



Effect of simulation domain geometry

- Compare venting curves for circular GB versus square GB
 - Circular GB: $F_{c,sat}$ = 0.61 ± 0.046, Square GB: 0.60 ± 0.036



Effect of simulation temperature

- Current BISON model assumes $F_{c,sat}$ is independent of temperature
- Primary effect of varying temperature: gas diffusivity D_g
- Ran 5 simulations with T = 1015 K (D_g decreased by 2x)
 - Much finer microstructure at same simulation time
 - No change in calcu'----'

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Microstructur
e at t = 1.98 \times 10^8 s:
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Conclusions

- BISON predictions of fission gas release and swelling are strongly dependent on dihedral angle, surface energy, *F_{c,sat}*
 - No measured values available
- Phase-field simulations were used to calculate $F_{c,sat}$
 - Determined without needing to wait for costly post-irradiation examination
- $F_{c,sat} = 0.60$ recommended for BISON U₃Si₂ model
- No strong effect on $F_{c,sat}$ from initial conditions, minimum bubble spacing, simulation domain geometry, temperature (in range considered)
- BISON simulations of U₃Si₂ ATR irradiation underway, using parameters determined from lower length scale calculation and their uncertainties





Questions?





