

Predicting Safety Rod Reactivity Insertion in the Advanced Test Reactor

November 2023

John Charles Tortorello

Idaho National Laboratory

nanging the World's Energy Future

INL is a U.S. Department of Energy National Laboratory operated by Battelle Energy Alliance, LLC

DISCLAIMER

This information was prepared as an account of work sponsored by an agency of the U.S. Government. Neither the U.S. Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness, of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. References herein to any specific commercial product, process, or service by trade name, trade mark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the U.S. Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the U.S. Government or any agency thereof.

INL/CON-23-75079-Revision-0

Predicting Safety Rod Reactivity Insertion in the Advanced Test Reactor

John Charles Tortorello

November 2023

Idaho National Laboratory Idaho Falls, Idaho 83415

http://www.inl.gov

Prepared for the U.S. Department of Energy Under DOE Idaho Operations Office Contract DE-AC07-05ID14517





National Nuclear Security Administration (NNSA)

Defense Nuclear Nonproliferation (DNN)

ATR Core Safety Assurance Package Modernization Efforts

John Tortorello, MPR Associates Inc. ANS Winter Meeting November 14, 2023

This work was funded in whole, or in part, by the National Nuclear Security Administration's (NNSA) Office of Material Management and Minimization (M3) through programs at the Idaho National Laboratory (INL).



- This work was funded in whole, or in part, by the National Nuclear Security Administration's (NNSA) Office of Material Management and Minimization (M3) through programs at the Idaho National Laboratory (INL).
- This work made use of Idaho National Laboratory's High Performance Computing systems located at the Collaborative Computing Center and supported by the Office of Nuclear Energy of the U.S. Department of Energy and the Nuclear Science User Facilities under Contract No. DE-AC07-05ID14517.



Unique Geometry of the ATR







The mission to convert research reactors to LEU fuel is the inspiration to redesign these elements with a new fuel composition



Unique Geometry of the ATR

1 of 40 Fuel Elements

NE Lobe – 8 fuel elements



- The 5 lobes are referred to as NW, NE, C, SW, SE
- ATR fuel cycles have limiting requirements on the lobe powers















CSAP (Core Safety Assurance Package)

- Purpose of the CSAP is to verify that the selected fuel loading meets the following criteria:
 - operational
 - Example: Ensure use of 3 primary coolant pumps
 - experimental
 - Example: Experiment power exposure limits
 - safety
 - Example: Reactivity margin (safety rod worth)





Reactivity Worth Calculation

$$\rho = \frac{\left(\frac{k_2 - k_1}{k_1 * k_2}\right)}{\beta_{eff}}$$

Where:

ρ

 β_{eff}

= Reactivity worth (\$)

 k_{1}, k_{2}

Final k-effective before the control element insertion and after, respectively
 The delayed neutron fraction (approximately 0.007)





MC21 Model of ATR

- Detailed MC21 model created with the Physics Unified Modeling and Analysis (PUMA) system - Naval Nuclear Laboratory code
- Used for reactivity worth calculations
- One low uncertainty reactivity worth calculation can take ~1 hour of HPC time





ATR is Designed for Varied Conditions

- Test reactor contains varied experiments no two cycles or timesteps are identical
- High power "tilt" the plot of flux versus distance across the core has a large slope

Increasing power tilt



Each power distribution is called a **power split**

Varied Conditions Cause Varied Reactivity Worth

To a first order approximation, **reactivity insertion is proportional to the square of the neutron flux** at the position of the geometry change

• higher worth

- 3.5

- 3.0

- 2.5

- 2.0

- 1.5

- Safety rod worth is dependent on local flux trap power
- The minimum safety rod worth is dependent on specific cycle conditions

Historical Methodology to Predict Minimum Safety Rod Worth

- Five lobe powers for each cycle have required **nominal**, **minimum**, and **maximum**
- All permutations of the max and min: 2⁵ = 32 power splits
- Each power split has unique **restart** and **delayed restart** conditions (64 additional power splits)
- Powers in startup, nominal operation, restart, and delayed restart (4 additional power splits)
- 32×3 + 4 = **100 power splits**
- With brute force computation on MC21, this could be 600 hours of HPC time

Problem Statement

Our solution: Use MC21 as a data collection tool and run a regression on the outputs

Shim Movement to Change Power -Safety Rod NW NE Ν Neck Shim – Fuel Element E w с Regulating Rod Flux Trap sw S SE 1 OSCCs

Reactivity Worth Dataset

- Expected positive correlation between power and reactivity worth
- Monte Carlo uncertainty is kept very low, approximately the width of the shown dots

Reactivity Worth Dataset

Improved correlation when normalizing – reactivity worth a function of relative flux

Reactivity Worth Multivariate Regression

 $CP = \rho$

[-7.003	2.598	11.292	-6.727	1.712	ן1.873	$[P_{NW}]$		$[\rho_E]$	
4.420	3.406	3.372	-4.590	-4.575	2.033	P_{NE}		ρ_N	
3.425	-6.760	10.744	1.455	-6.976	1.889	P_{C}	_	$ ho_W$	
-3.633	-3.045	-0.976	15.217	-5.87	1.676	P_{SW}	-	ρ_{SW}	
-8.848	-8.044	13.222	2.832	2.966	2.129	P_{SE}		ρ_S	
L-3.631	-3.332	-1.257	-5.951	15.815	1.644			$\lfloor \rho_{SE} \rfloor$	

Where:

С

Р

ρ

= A matrix of coefficients

The normalized lobe powers, such that
 the sum of the lobe powers is unity. The vector of *P* also includes a constant value

= The worth of the safety rods in units of \$

Conclusions

- This methodology has the potential to be used to predict many different incore parameters
- It is important to look for trends that are backed by a first-principled explanation
- Computational methods can shine when perturbing one variable at a time for many iterations – this can reveal general trends that would otherwise be impossible to visualize

Questions/Discussion

 $CP = \rho$

Equation 2

[−7.003	2.598	11.292	-6.727	1.712	1.873	$[P_{NW}]$		ρ_E	
4.420	3.406	3.372	-4.590	-4.575	2.033	P_{NE}	=	ρ_N	
3.425	-6.760	10.744	1.455	-6.976	1.889	P_{C}		ρ_W	
-3.633	-3.045	-0.976	15.217	-5.87	1.676	P_{SW}		ρ_{SW}	
-8.848	-8.044	13.222	2.832	2.966	2.129	P_{SE}		ρ_S	
L-3.631	-3.332	-1.257	-5.951	15.815	1.644	$\lfloor 1 \rfloor$		$\lfloor \rho_{SE} \rfloor$	l

Where:

Р

C = A matrix of coefficients

The normalized lobe powers, such that
 the sum of the lobe powers is unity. The vector of *P* also includes a constant value

 ρ = The worth of the safety rods in units of \$

