VISION User Guide VISION (Verifiable Fuel Cycle Simulation) Model

Jacob J. Jacobson Robert F. Jeffers Gretchen E. Matthern Steven J. Piet Benjamin A. Baker

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VISION User Guide VISION (<u>Verifiable Fuel</u> Cycle <u>Simulation</u>) Model

Advanced Fuel Cycle Initiative

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SUMMARY

The purpose of this document is to provide a guide for using the current version of the \underline{V} er<u>i</u>fiable Fuel Cycle \underline{Si} mulation (VISION) model. This is a complex model with many parameters; the user is strongly encouraged to read this user guide before attempting to run the model.

This model is an R&D work in progress and may contain errors and omissions. It is based upon numerous assumptions. This model is intended to assist in evaluating "what if" scenarios and in comparing fuel, reactor, and fuel processing alternatives at a systems level for U.S. nuclear power. The model is not intended as a tool for process flow and design modeling of specific facilities nor for tracking individual units of fuel or other material through the system. The model is intended to examine the interactions among the components of a fuel system as a function of time varying system parameters; this model represents a dynamic rather than steady-state approximation of the nuclear fuel system.

VISION models the nuclear cycle at the system level, not individual facilities, e.g., "reactor types" not individual reactors and "separation types" not individual separation plants. Natural uranium can be enriched, which produces enriched uranium, which goes into fuel fabrication, and depleted uranium (DU), which goes into storage. Fuel is transformed (transmuted) in reactors and then goes into a storage buffer. Used fuel can be pulled from storage into either separation of disposal. If sent to separations, fuel is transformed (partitioned) into fuel products, recovered uranium, and various categories of waste. Recycled material is stored until used by its assigned reactor type. Note that recovered uranium is itself often partitioned: some RU flows with recycled transuranic elements, some flows with wastes, and the rest is designated RU. RU comes out of storage if needed to correct the U/TRU ratio in new recycled fuel. Neither RU nor DU are designated as wastes.

VISION is comprised of several Microsoft Excel input files, a Powersim Studio core, and several Microsoft Excel output files. All must be co-located in the same folder on a PC to function. We use Microsoft Excel 2003 and have not tested VISION with Microsoft Excel 2007. The VISION team uses Powersim Studio 2008, the latest release. (In final testing, we discovered that it will run in Powersim Studio 2005, but the connections to the output file are gone.)

VISION 3.0 has more flexibility than previous versions, which were structured for only three reactor types - LWRs that can use only uranium oxide (UOX) fuel, LWRs that can use multiple fuel types (LWR MF), and fast reactors. One could not have, for example, two types of fast reactors concurrently. The new version allows 10 reactor types and any user-defined uranium-plutonium fuel is allowed. (Thorium-based fuels can be input but several features of the model would not work.) The user identifies (by year) the primary fuel to be used for each reactor type. The user can identify for each primary fuel a contingent fuel to use if the primary fuel cannot be made, e.g., a reactor designated as using mixed oxide fuel (MOX) would have UOX as the contingent fuel. Another example is that a fast reactor using recycled transuranic (TRU) material can be designated as either having or not having appropriately enriched uranium oxide as a contingent fuel.

Because of the need to study evolution in recycling and separation strategies, the user can now select the recycling strategy and separation technology, by year. Recycling strategy means how fuel is routed from used fuel storage into one or more separation facility types. As an example, a separation plant could be designated to use one source of UOX fuel for three decades and then shift to having a combination of UOX and MOX. Separation technology means how fuel is separated into products, which are routed into one of the 10 subsequent fuel types, or waste. So, for example, the user can designate a separation plant type to change efficiency (fraction of TRU into waste) or change from not recovering minor actinides (Np, Am, Cm, Bk, Cf) to later recovering them.

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ACRONYMS

AFCI	Advanced Fuel Cycle Initiative		
Aq	Aqueous separation		
BC	Base Case		
BU	Burnup, sometimes incorrectly used as burned uranium		
CANDU	CANada Deuterium Uranium reactor		
CFR	Converter Fast Reactor		
COEX	Co-Extraction producing RU and UPu as products and everything else as a waste		
CR	Transuranic Conversion Ratio (TRU produced/TRU destroyed)		
CY	Calendar Year		
DU	Depleted uranium, the low U235 tailings from uranium enrichment		
E-chem	Electrochemical separation, also known as pyroprocessing		
EU	Enriched uranium, the high U235 produce from uranium enrichment		
FBR	Fast Breeder or Burner Reactor		
FPY	Full Power Year		
FR	Fast Reactor		
GNEP	Global Nuclear Energy Partnership		
GWe	Gigawatt-electric		
GWth	Gigawatt-thermal		
HEU	Highly Enriched Uranium		
HWR	Heavy water reactor		
IMF	Inert Matrix Fuel (thermal reactor fuel without uranium)		
INL	Idaho National Laboratory		
Iso	Isotope		
kt	Kilotonne		
LSF	Legacy Spent Fuel, pre-2000 inventory of discharged LWR fuel		
LTD	Long-Term Dose, a metric describing the hypothetical dose to the maximally exposed		
	individual at a specific time after repository emplacement, scaled from 2004-vintage Yucca		
	Mountain groundwater pathway calculations		
LTH	Long-Term Heat, a metric describing the heat committed to waste disposal from time of		
	repository closure to ~1500 years		
LTR	Long-Term Radiotoxicity, a metric describing the radiotoxicity of isotopes at a specific		
	time after repository emplacement		
LWR	Light Water Reactor		
LWR MF	Light Water Reactor Mixed Fuel, LWR that can use multiple fuels, e.g., MOX and/or IMF		
LWR MOX	MOX fuel in Light Water Reactors		
MF	Mixed Fuel in a thermal reactor, e.g., MOX or IMF		
MOX	Mixed Oxide fuel, a mixture of uranium oxide and one or more transuranic element oxides,		
	e.g. MOX-Pu or MOX-TRU		
MRS	Managed Retrievable Storage		
MT	Montana, sometimes used as metric ton (1000 kg), but the proper System Internationale		
	unit would be Mg for megagram		
PUREX	Plutonium-Uranium Extraction, producing RU and Pu as products and everything else as a		
	waste stream		
Rxtr	Reactor		
RU	Recovered uranium from a separation process		
SF	Spent Fuel, also called used fuel		
SWU	Separative Work Unit		

t	Tonne (metric ton)		
TR	Thermal Reactor		
TRU	Transuranics (Plutonium and higher on periodic table)		
UOX	Uranium Oxide		
UREX	Uranium Extraction		
UREX+1	UREX producing U, and all-TRU as product streams and several sets of fission products as		
	individual waste streams		
UREX+2	UREX producing U and NpPu as product streams, and several sets of fission products as		
	individual waste streams. AmCm goes into waste.		
UREX+3	UREX producing U, NpPu, and AmCm as product streams and several sets of fission		
	products as individual waste streams		
UREX+4	UREX producing U, NpPu, Am, and Cm as product streams and several sets of fission		
	products as individual waste streams		
VHTR	Very High Temperature Reactor		
VISION	Verifiable Fuel Cycle Simulation		

TERMINOLOGY

Base case	A set of parameters in the main input file that defines a self-consistent scenario.		
Decay products	Decay products of uranium, specifically Pb, Bi, Ra, Ac, Th, Pa		
Fast burner or converter reactor	A fast reactor with transuranic conversion ratio < 1		
Fast breeder reactor	A fast reactor with transuranic conversion ratio > 1		
File	If extension xls - Excel2003 spreadsheet files, file names are in bold in this document.		
	If extension sip - Powersim Studio files		
Fuel recipe	Either the input or output composition of a reactor fuel, normalized so that the total recipe equals 1.00. Recipes are contained in the file vision recipes ver5.xls		
Group 1A/2A	Alkali/Alkali earths, specifically Rb, Sr, Cs, Ba. For fuel cycle management, the most important radioactive Group 1A/2A are Sr90, Cs134, Cs135, Cs137.		
Halogens	Group VII of the Periodic Table, specifically Br and I. For fuel cycle management, the most important radioactive halogen is I129.		
Inert gases	Group O of the Periodic Table, specifically Kr and Xe. For fuel cycle management, the most important radioactive inert gases are Kr81 and Kr85.		
Lanthanides	Elements La through Lu. For fuel cycle management, the most important isotopes are Ce144, Pm147, Sm146, Sm147, Sm151, Eu154, Eu155, Ho166m.		
Legacy	Any reactor or used fuel that exists before the simulation begins, typically the year 2000.		
Minor actinides	Transuranic isotopes other than plutonium, specifically Np, Am, Cm, Bk, Cf.		
Prioritization - order A facility capacity is used by a set of incoming flows such that source of first, then source two, etc. until the full capacity of the facility type is used by a set of incoming flows such that source of first, then source two, etc. until the full capacity of the facility type is used by a set of incoming flows such that source of first, then source two, etc. until the full capacity of the facility type is used by a set of incoming flows such that source of first, then source two, etc. until the full capacity of the facility type is used by a set of incoming flows such that source of first, then source two, etc. until the full capacity of the facility type is used by a set of incoming flows such that source of first, then source two, etc. until the full capacity of the facility type is used by a set of incoming flows.			
Prioritization - percentage	A facility capacity is used by allocating a percentage of the capacity among a set of potential flows.		
Powersim Studio	Commercial system dynamic software in which the core part of the VISION suite is written.		
Routing - pull	A receiving facility attempts to pull material from a designated set of sending facilities. Thus, there must be a buffer inventory at each sending facility because the material may or may not be requested by one or more receiving facilities.		
Routing - push	Material is sent by a facility independent of whether the receiving facility has sufficient capability for it. Thus, there must be a buffer inventory at the receiving facility.		
Transition metals	In this report, literally elements not otherwise categorized, including Se, Mo, Ru, Pd, Pd, Cd, Sn, Sb, Te.		
Transuranic	Isotopes above uranium in the Periodic Table, specifically Np, Pu, Am, Cm, Bk, Cf.		
Ratio (CR) Ratio of transuranic material created during residence in a reactor divided transuranic material destroyed. This is related to but different from the breeding ratio, which is the ratio of fissile material created/destroyed.			
Separation efficiency matrix	Also can be described as separation technology matrix or separation partition matrix. User-defined matrices allocate percentages of each component of used fuel into fuel product streams, recovered uranium (RU), and/or waste streams.		

VISION The suite of Excel input files, Powersim core, and Excel output files the nuclear fuel cycle system.	
Worksheet (or page)	Worksheets within a spreadsheet file, worksheet names are in bold in this document

VISION USER GUIDE

1. INTRODUCTION

The purpose of this document is to provide a guide for using the current version of the <u>Verifiable Fuel Cycle Simulation</u> (VISION) model. This is a complex model with many parameters; the user is strongly encouraged to read the user guide before attempting to run the model.

VISION is comprised of several Microsoft Excel input files, a Powersim Studio core, and several Microsoft Excel output files. All must be co-located in the same folder on a PC to function. We use Microsoft Excel 2003 and have not tested VISION with Microsoft Excel 2007. The VISION team uses Powersim Studio 2008, the latest release. (In final testing, we discovered that it will run in Powersim Studio 2005, but the connections to the output file are gone.)

VISION 3.0 has more flexibility than previous versions, which were structured for only three reactor types - LWRs that can use only uranium oxide (UOX) fuel, LWRs that can use multiple fuel types (LWR MF), and fast reactors. One could not have, for example, two types of fast reactors concurrently. The new version allows 10 reactor types and any user-defined uranium-plutonium fuel is allowed. (Thorium-based fuels can be input but several features of the model would not work.) The user identifies (by year) the primary fuel to be used for each reactor type. The user can identify for each primary fuel a contingent fuel to use if the primary fuel cannot be made, e.g., a reactor designated as using mixed oxide fuel (MOX) would have UOX as the contingent fuel. Another example is that a fast reactor using recycled transuranic (TRU) material can be designated as either having or not having appropriately enriched uranium oxide as a contingent fuel.

Because of the need to study evolution in recycling and separation strategies, the user can now select the recycling strategy and separation technology, by year. Recycling strategy means how fuel is routed from used fuel storage into one or more separation facility types. As an example, a separation plant could be designated to use one source of UOX fuel for three decades and then shift to having a combination of UOX and MOX. Separation technology means how fuel is separated into products, which are routed into one of the 10 subsequent fuel types, or waste. So, for example, the user can designate a separation plant type to change efficiency (fraction of TRU into waste) or change from not recovering minor actinides (Np, Am, Cm, Bk, Cf) to later recovering them.

So, the user has three major year-by-year ways to control the fuel cycle: fuel recipes, recycling routing matrices that route used fuel to separation types, and separation efficiency matrices, which separate products from waste and also serve to route separation products back to fuel/reactor types.

This flexibility comes with two disadvantages. First, the magnitude of the required input has grown sixfold; the main input file (**base case settings ver6.xls**) has grown from 4.5 to 30 MB. So, we have started to create some Excel macro's to assist in data entry; please comment on their usefulness. Second, we cannot pre-define most of the output files a user might want, nor anticipate how a user would want them labeled. For example, fast reactors might be reactor type 3 or reactor 6 or not exist. So, we have added a page in the input file that asks users to supply their names for each run, each reactor type, each fuel type, and each separation type; these are used in the various output files. And, we have added Graph Viewer and Graph Builder macro's into relevant output files so the user can see pre-existing graphs as well as be guided into making new graphs. Pre-existing graphs will generally have to be modified before use, e.g., by deleting reactor, fuel, or separation types that are not used in a particular simulation.

1.1 Purpose

This model is an R&D work in progress and may contain errors and omissions. It is based upon numerous assumptions. This model is intended to assist in evaluating "what if" scenarios and in comparing fuel, reactor, and fuel processing alternatives at a systems level for U.S. nuclear power. The model is not intended as a tool for process flow and design modeling of specific facilities nor for tracking individual units of fuel or other material through the system. The model is intended to examine the interactions among the components of a fuel system as a function of time varying system parameters; this model represents a dynamic rather than steady-state approximation of the nuclear fuel system.

This is a model that is still being actively developed, and we invite feedback:

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As of this writing, there are a few features not yet working. These are noted in this guide as it is hoped they will be working soon.

1.2 Underlying Theory and Terminology of VISION

Even if you are very familiar with nuclear fuel cycles, we encourage you to read this subsection as it explains the underlying theory and terminology of VISION.

VISION models the nuclear cycle at the system level, not individual facilities, e.g., "reactor types" not individual reactors and "separation types" not individual separation plants. Nonetheless, to avoid repeating the word "types" countless times, this manual will often simply refer to "reactors" and "separations."

Figure 1-1 shows the basic VISION model of the nuclear fuel cycle. Natural uranium can be enriched, which produces enriched uranium, which goes into fuel fabrication, and depleted uranium (DU), which goes into storage. (DU) only comes out of storage if used in a reactor. Fuel is transformed (transmuted) in reactors and goes into a storage buffer. Used fuel can be pulled from storage into either separation of disposal. If sent to separations, fuel is transformed (partitioned) into fuel products, recovered uranium, and various categories of waste. Recycled material is stored until used by its assigned reactor type. Note that recovered uranium is itself often partitioned: some RU flows with recycled transuranic elements, some flows with wastes, and the rest is designated RU. RU comes out of storage if needed to correct the U/TRU ratio in new recycled fuel. Neither RU nor DU are designated as wastes.

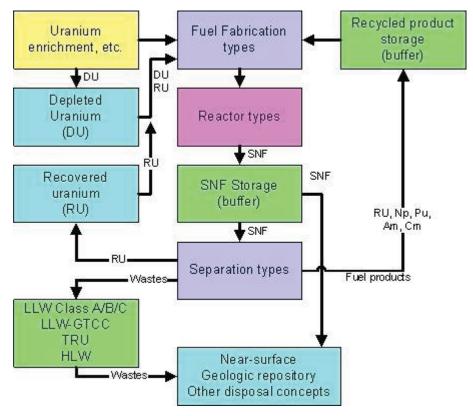


Figure 1-1. Basic VISION structure.

Thus, as fuel moves through the fuel cycle, there are two primary functions - transformation and routing. Transformation occurs at facilities and routing occurs between facilities. Routing does not change the material, it merely moves mass from one place to another. In the parlance of system dynamics, types of facilities are inventories or stocks; routing are flows. Facilities transform material in various ways, e.g.

- Transmutation at reactors,
- Separation (or partition) at separation plants,
- Fabrication at fabrication plants,
- Waste form creation and waste form packaging at waste processing plants, and
- Isotopic decay at waste storage and all of the above.^a

Generally, the performance of each transformation operation is under the user's control. Transformation occurs by user-selected "recipes" that translate an input composition to an output composition. Separation occurs by user-selected "separation efficiency matrices" that partition incoming used fuel into fuel products, recovered uranium, and waste streams. At present, fabrication is not user controlled, material sent to a given fabrication plant always undergoes the type of fabrication appropriate for associated reactor type's fuel, which is itself specified by the fuel recipe selected for that reactor. That is, there is a 1:1 correspondence between fuel fabrication plant types and reactor types.

a. Exception - Isotopes are not decayed once put into a repository as our primary waste management concern is estimating the amount and character of waste forms at the time of emplacement.

Routing is also generally under the user's control. The primary exception is again fuel fabrication to reactor. There is no provision to route fuel from one fabrication plant type to a different reactor type.

In principle, routing can be specified either by "pushing" or "pulling."

- Push Material is sent by a facility independent of whether the receiving facility has sufficient capability for it. Thus, there must be a buffer inventory at the receiving facility.
- Pull A receiving facility attempts to pull material from a designated set of sending facilities. Thus, there must be a buffer inventory at each sending facility because the material may or may not be requested by one or more receiving facilities.

A real fuel cycle system could have both push and pull routing and thus buffers at both sending and receiving facilities. In VISION 3.0, we have chosen to primarily model routing from reactors to separation as "pull", hence buffers are closely associated with reactors, i.e., where used fuel is located such as wet and dry storage. That is, used fuel stays in used fuel storage unless or until pulled by separations or pulled by waste disposal. The routing of separation to fabrication/reactors is primarily modeled as "push", i.e., buffers are envisioned at receiving fuel fabrication plants. Whether push or pull, routing can theoretically be controlled either by priority order or percentage. Priority order means that some capacity is used by a set of incoming flows such that source one is used first, then source two, etc. until the full capacity of the facility type is used. VISION models reactor-to-separation as push/priority-list. Percentage means that material is received or sent to a set of places allocated by percentages. VISION models separation-to-fabrication/reactor by pull/percent.

Figure 1-2 shows the routing approach in VISION as well as two of the many alternatives to help differentiate among options. As noted above, VISION uses pull/priority routing from reactors to separation plants and push/percent from separation plants to fuel fabrication (hence reactors). The first alternative shown is pull/priority (reactor to separation) then pull/percent (separation to fuel fabrication). The second alternative is push/percent for both reactor-separation and separation-reactor. All options require at least one buffer between reactor and separation and one between separation and fuel fab; the diagram shows the buffer shifting position. (Here, "position" means in a logical sense, the physical location of buffers is not addressed.)

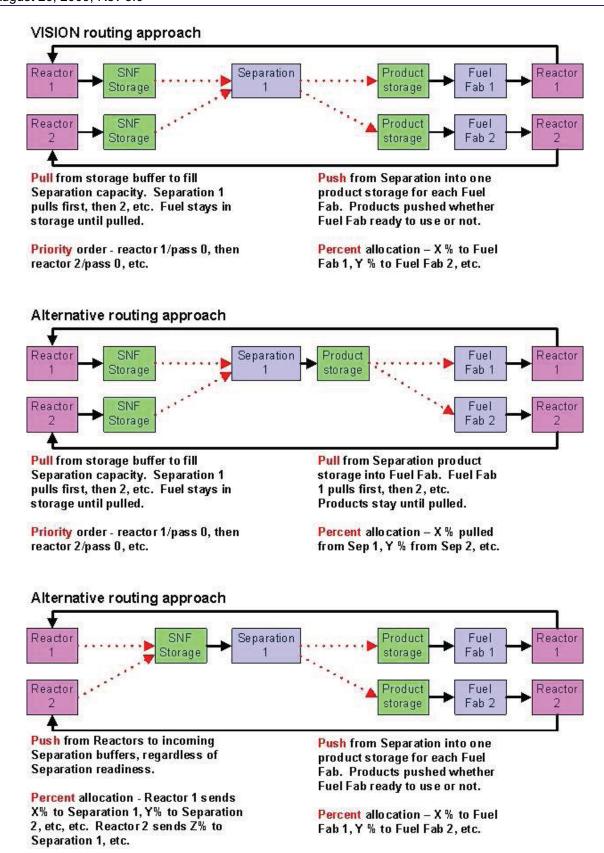


Figure 1-2. VISION Routing Approach.

1.3 Scope and Organization of VISION

VISION can be run two ways:

- Pre-defined base cases provide the simplest way to use VISION but the least flexibility. In this mode, the user selects a predefined base case, and the model automatically enters all of the parameters necessary by reading parameters from Microsoft Excel spreadsheets. Currently, when the user selects a predefined base case, they cannot change any of the parameters with the user interface. Use of predefined base cases allows the user to select among several dozen different strategies, but the user cannot select any of the parameters for each case.
- User-defined base cases provide the most flexibility but require the user to identify each input parameter. For both predefined and user-defined base cases, VISION reads input parameters from Microsoft Excel spreadsheets prior to running the simulation. The user defined base cases allow the user to access the full flexibility of the model (available without making changes to the code itself) and to easily save those defined cases for repeated runs or varying specific parameters. Once all the parameters for a user defined case are defined in the Excel input files, the user defined cases can be run as simply as the predefined base cases. The user can copy parameters from one of the predefined base cases into the five slots for user-defined base cases in the Excel files and then modify them.

Previously, VISION could also be run via a user interface. The increased flexibility (and complexity) of the model now precludes this mode of operation.

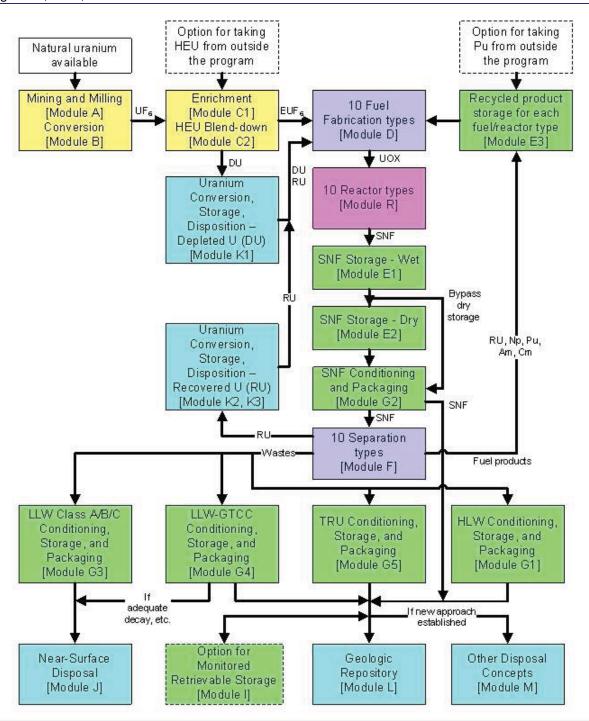
We discourage users making changes directly in the model; if your needs suggest model changes, please contact us.

The typical user does not need to know the inner structure of the VISION model as long as they are familiar with the basics of the nuclear cycle and follow this user guide. Nonetheless, it is instructive to consider the full scope of the model as shown in Figure 1-3. The color coding of the modules is the same as Figure 1-1 and designates the following:

- White fundamental source material (uranium ore, high enriched uranium, Pu)
- Yellow front end of the fuel cycle (uranium mining, enrichment, etc.)
- Blue fuel recycling (separation and fabrication)
- Pink reactors
- Green in-process storage, packaging, etc.
- Bright blue long-term storage and ultimate disposal

b. We have requested a change to the Powersim Studio software that would allow for users to make such changes.

c. There is also a methodology document, which is being updated.



Transportation for High-Level Radioactive Materials (SNF, HLW, TRU, LLW-GTCC, recycled fuel) [Module O1]

Transportation for Low-Level Radioactive Materials (LLW-near-surface, unirradiated fuel, RU, DU, EU) [Module O2]

Figure 1-3. VISION Modules.

This color scheme is used where practical in this document and in the input and output Excel files.

As can be seen, the model addresses the entire fuel cycle from fundamental source material to ultimate disposal and the various steps and options in-between. After separations, all outputs are tracked. Based on the options selected by the user the model controls how much of each chemical element goes where.

1.4 Changes from Previous Versions

Table 1-1 summarizes the increase in flexibility (and complexity) between VISION 2.2 and 3.0. These have been motivated by the following:

- Requested benchmarks against other codes with scenarios lasting more than 100 years. The new model can run for 200 years.
- Interest in studying more reactor types than before, i.e., more than LWR-UOX, LWR-MF, and fast reactors. The new model can handle any uranium-plutonium fuel. It cannot yet reliably calculate the range of thorium fuel cycles.
- Interest in studying more reactor types concurrently.
- Interest in allowing yearly evolution of reactor type and separation type.

Table 1-1. Major Changes from Version 2.2

Table 1-1. Major Changes from Version 2.2		
Number of	VISION 2.2	VISION 3.0
years of simulation	100	200
reactor types	3 (hardwired)	10 (user-defined)
isotopes tracked	60	81
times reactor capacity can be changed	Yearly by 2	Yearly by 3
	methods	methods
user-defined fuel recipes that can be entered	2 thermal/run	Hundreds
	2 fast/run	
times a reactor type's fuel recipe can be changed	2	Yearly
times the routing from reactor to separation plant can be changed	Yearly (only	Yearly (any
	by changing	reactor to any
	number of	separation)
	recycles)	
separation types	3 (hardwired)	10 (user-defined)
times a separation type's capacity can be changed	Yearly	Yearly
user-defined separation fuel partition matrix that can be entered	15	40
times a separation type's fuel partition matrix can be changed	Never	Yearly
times the routing from separation to fabrication can be changed	Yearly (only	Yearly (any
	by changing	separation to any
	number of	fuel fab)
	recycles)	
times the routing from fabrication to reactor can be changed	Never	Never
times the routing from separation to waste streams can be	Never	Yearly
changed		
waste management metrics	7	Most currently
		inactive
Size of base case setting file	4.5 MB	30 MB

2. KEY ASSUMPTIONS AND INITIAL PARAMETERS

2.1 Assumptions

2.1.1 Facility Behavior and Sizes

Each reactor, separation, and fuel fabrication type can represent one or more discrete facilities. All facilities of a given type have the same functional behavior and the same unit size, e.g., reactor capacity (GWe/reactor). They generally start and end at different times. If it is important to differentiate among behaviors of reactors or separation plants, the groups should be modeled as different types. For example, we typically model two "types" of LWRs - those that can only use UOX fuel and those with multiple fuel (MF) capability and thus can use either UOX or MOX (or IMF) fuel. Similarly, one might have a separation type for UREX+3, in which the products would be NpPu and AmCm, and another separation type for UREX+1, in which the product is all-TRU. All separation facilities of a given "type" do the same separation at each time step, so much to fuel products, so much to waste, etc. One can change the behavior over time, but that change applies to all facilities of the same type.

2.1.2 Combinations

Users of the model must ensure that the appropriate combinations of reactor, fuel, and operating conditions are selected when setting up a user defined base case or manual scenario. For example, fast reactors will not recycle fuel if no fuel is sent to fast reactors by routing LWR fuel to one or more separation types that then route fuel products to a separation-to-reactor buffer so that it can be used to make the appropriate type of fuel.

2.1.3 Priority among Reactors, Separations, and Fuel Fabrication Types

Generally, the priority among reactor types, among separation types, and among fuel fabrication types is controlled by the user through various input matrices. For example, by "pushing" fuel products from separation to fuel fabrication (by percent) and the 1:1 correspondence between fuel fabrication and reactor fuel type, there is no additional prioritization required at fuel fabrication. Recycled material has already been allocated by the separation efficiency matrices that push fuel products into each fuel fabrication.

There are two exceptions. First, recycling routing matrices define for each separation type the order in which that separation type pulls used fuel, e.g., pull from Fuel type 1, then Fuel type 3, then Fuel type 2. That separation type will pull fuel each time step until its separation capacity is used. If the user allows more than one separation type to pull the same fuel type, then the separation type with the lower number goes first - a hard-wired prioritization not under user control except by the order in which the user defined separation types.

Example: Separation 2 and 3 are allowed to pull from Fuel type 2, whether or not they pull from other fuel types. So, Separation 2 is allowed to pull from any available Fuel type 2 to use its current separation capacity. After Separation 2 is completed, Separation 3 could use any remaining available fuel type 2. Separation 2 goes before Separation 3.

Second, legacy reactors retire in the order reactor-1 first, then reactor-2, and so forth.

2.1.4 Units

Unless otherwise stated, the model uses the following units:

• Reactor capacity in GWe, i.e., unit of power

- Energy and electricity generation in GWe-FPY (full power years), i.e., unit of energy
- Mass in kilotonnes (kt or ktonnes) these are converted to t (tonnes) in output files
- Time in calendar years (CY) or full power years (FPY).
- Separation and fuel fabrication capacities are generally in units of kt/CY.

2.1.5 Reactor and Fuel Types

The assignments are made by the selection of fuel input and output recipes in the input Excel files. VISION does not perform reactor physics calculations. Instead, it uses input and output recipes that designate, by isotope, the composition of fuel entering and leaving a reactor.

A recipe represents core-averaged compositions.

VISION keeps track of the flow of material by recycle pass through 5 recycle passes. Recycle pass 0 is virgin material that has not been recycled. Since U235 is the only fissile isotope in nature, all pass 0 fuel is based on uranium. Pass 1 is the first recycle pass. Material that is recycled after the fifth recycle is reallocated to recycle pass 5. Keeping track of recycle passes is critical to making VISION work as intended.

Material's recycle pass is remembered (conserved) in going from reactor to separation plant, in separation plants, and in fuel fabrication.

Material recycle pass is updated between separation and fuel fabrication.

- Material going from separation X to fuel fabrication X, is increased by 1, except that pass 5 goes to pass 5.
- Material going from separation X to some other fuel fabrication is reset to 1. So, material recovered from first-pass used MOX (pass 1) that goes to fuel fabrication for a fast reactor is reset to pass 1 and enters fast reactors as such. Material recovered from first-pass used MOX that stays as MOX gets updated to MOX pass 2.

Any type of uranium-plutonium fuel recipe can be used. We have not tested the model with thorium recipes, partly because we are still assembling appropriate recipes. Off course there are as many thorium fuel cycle options as uranium-based options. The model already tracks relevant Th isotopes. The current model will not track use of thorium resources. Once-through thorium options (Th + U235 or Th + TRU) might work; the model would simply create Th to make the fresh fuel. Thorium options with recycled U233+TRU (or Pu) might work, provided uranium with appropriate U233 content was separated and sent to the appropriate fuel fabrication type. The "flow control" would be sent to the TRU (orPu). Thorium options in which the recycled U233 content should be the control on flow will not work.

The sum of mass fractions in a fuel recipe must equal 1.0. Otherwise, mass will be created or destroyed each time fuel enters or leaves a reactor type.

All recipes for used fuel assume 0 years of cooling (time after exiting the reactor) have occurred. In the model, the used fuel can be decayed while in an interim or longer term storage facility.

Unless otherwise stated, Cm is meant to include Cm, Bk, and Cf isotopes. TRU means all elements above U, specifically Np, Pu, Am, Cm, Bk, Cf.

Figure 2-1 shows the Periodic Table from our perspective. The color coding (unavoidably different than the VISION module color coding) denotes groups of elements with similar behavior in chemical

separations. Although the user is free to define chemical separation performance by isotope, the examples that come with VISION assume elements of the same color coding behave the same during chemical separation. For example, all of the lanthanides (plus yttrium) are assumed to be separated as a group. The only Group 1A/2A elements of significance as fission products are Rb, Sr, Cs, and Ba. The only halogens of significance are Br and I. The only inert gases of significance are Kr and Xe. H3 and C14 are considered separately because of their ubiquitous role in biological systems. More details can be found in Piet2009.

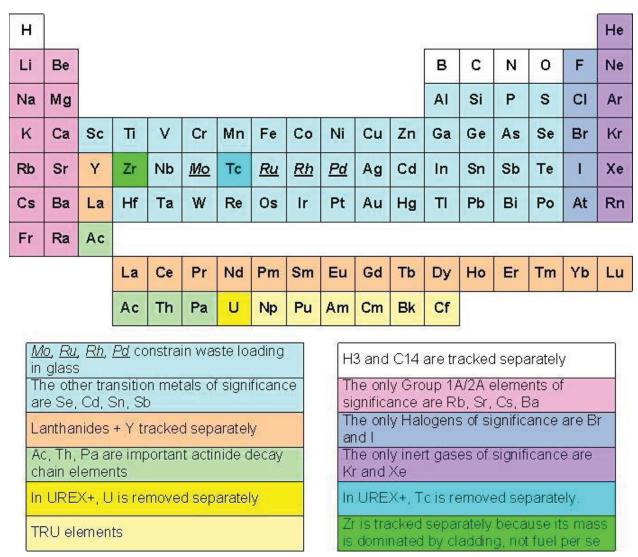


Figure 2-1. Periodic Table as seen from fuel cycle system analysis perspective. [Piet2009]

Table 2-1 lists the isotopes tracked in VISION. Only isotopes with halflives greater than 0.5 years are tracked. (Exception: Cm242 at 0.45 year.) The most important isotopes in each chemical group are included, as well as the residual mass (considered stable) in that group.

Table 2-1. Tracked Isotopes and Chemical Elements [Piet2009]

	and Decay Chain	Fission Pro	oducts
He4 (stable)		Н3	
Pb206		C14	Other gases
Pb207		C-other	
Pb208	Transition metals	Kr81	_
Pb210		Kr85	Inert gases
Bi209		Inert gas other (Kr, Xe)	(Group 0)
Ra226	~	Rb	
Ra228	Group 2A	Sr90 w/Y90 decay	Group 1A/2A
Ac227		Sr-other	
Th228		Zr93 w/Nb93m decay	
Th229	A 1. 1	Zr95 w/Nb95m decay	Zirconium
Th230	Actinides	Zr-other	
Th232		Tc99	m 1
Pa231		Tc-other	- Technetium
U232		Ru106 w/Rh106 decay	Transition metals that
U233		Pd107	constrain glass waste
U234	T.T. •	Mo-Ru-Rh-Pd-other	forms
U235	Uranium	Se79	
U236		Cd113m	
U238		Sn126 w/Sb126m/Sb126	Other transition metals
Np237	Neptunium	Sb125 w/Te125m decay	
Pu238	•	TM-other (Co-Se, Nb, Ag-Te)	
Pu239		I129	Halogens
Pu240	Dintarion	Halogen-other (Br, I)	(Group 7)
Pu241	Plutonium	Cs134	
Pu242		Cs135	
Pu244		Cs137 w/Ba137m decay	Group 1A/2A
Am241		Cs-other	
Am242m	Americium	Ba	
Am243		Ce144 w/Pr144m/Pr144 decay	
Cm242		Pm147	
Cm243		Sm146	
Cm244		Sm147	
Cm245	Curium	Sm151	Lanthanides (plus Y)
Cm246	Cultuili	Eu154	
Cm247		Eu155	
Cm248		Ho166m	
Cm250		LA-other plus Yttrium	
Bk249	Berkelium		
Cf249			
Cf250	Californium		
Cf251	Californiulli		
Cf252			

2.1.6 Fuel Flow Control

For each reactor type, the user can select among these approximations for how the model estimates how much fuel can be made from separated material available in the separated product storage.

- 0. Minimum of Pu239, Pu240, and Pu241, i.e., whichever isotope is most restrictive.
- 1. Pu239
- 2. Pu240
- 3. Pu241
- 4. TRU (sum of all TRU isotopes required in the fuel)
- 5. Pu (sum of all Pu isotopes required in the fuel)

For example, with "Pu" flow control (option 5), the model determines from the fresh fuel recipe the fraction of Pu in the fuel, say 10%. Then, based on the amount of Pu in separated product storage (downstream of the separation plant) the model determines the amount of fuel that can be made, regardless of the mix of individual Pu isotopes in separated material. The model then fabricates that fuel for use in the reactors. This has the effect of alchemy - the "wrong" mix of Pu isotopes is replaced with the "right" mix of Pu isotopes. The amount of isotope mismatch is tracked. *An improved approach whereby the recipe is adjusted to match the available mix of isotopes is in testing.* Meanwhile, the situation can be bracketed. Flow control "0" is the most restrictive and will see the least amount of recycled fuel produced. Flow control "4" (TRU is appropriate for fast reactors) or "5" (Pu is appropriate for thermal reactors) are the least restrictive and will see the most amount of recycle fuel produced.

The flow control options will have to be expanded in order for some thorium fuel options to work.

2.1.7 Isotope Decay

The model tracks and radioactively decays mass at an isotopic level. Isotope decay is currently applied to all locations in the model where mass remains in a facility for 1 or more years. This can be adjusted to no decay or decay only in wet storage when running user defined base cases or manual cases.

There is one exception. Once material has entered a repository, further isotopic decay is not performed as our primary waste management concern is estimating the amount and character of waste forms at the time of emplacement.

2.2 Initial Parameters

This section describes appropriate initial parameters when simulating the U.S. nuclear power plant fleet. All can be changed by the user to simulate the world or any other set of nuclear fuel cycle facilities.

2.2.1 Growth Rates

The amount of nuclear power capacity throughout the simulation depends on three types of user input, as follows:

- Total electrical growth rate (by year)
- Nuclear market share (by year)
- Nuclear generation in 2000, which was 86.002 GWe-FPY/CY but is nonetheless a user-controlled input.

The user is encouraged to set input parameters to replicate the following 2000 values:

- Total electrical generation of 433.7 GWe-FPY.
- Nuclear electrical generation of 86.002 GWe-FPY.
- Nuclear market share of 19.83%.

Table 2-2 provides a set of input parameters that closely replicates actual data from 2000 to 2006 even though VISION is constrained to a fixed reactor capacity factor and fixed average reactor capacity. Furthermore, VISION cannot decrease nuclear generation year by year except by retiring reactors. The actual ups and downs in nuclear generation from 2000 to 2006 arose from slight fluctuations in reactor capacity and increases in capacity (uprates), plus the addition of the 104th operational reactor. VISION was never designed to calculate precise yearly values; nonetheless, by starting the simulation with 2 reactors needing fuel and 3 more reactors starting construction, VISION will calculate nuclear generation similar to the actual data, as shown in Table 2-2.

Table 2-2. Nuclear Generation Data

	User I	nput	Actual Data [a,b,c]	Calculated by VISION	
Year	Total Electricity	Nuclear Market	Nuclear Generation	Nuclear Generation	
	Growth Rate	Share	(GWe-FPY)	(GWe-FPY)	
2000	1.2	19.83	86.00	86.00	
2001	1.2	20.58	87.71	86.00	
2002	1.2	20.22	88.99	86.83	
2003	1.2	19.67	87.12	88.50	
2004	1.2	19.86	89.95	89.34	
2005	1.2	19.28	89.21	90.17	
2006	1.2	19.42	89.80	90.17	
2007	1.2	19.19	91.42	90.17	

2000 nuclear power generation = 86.0019 GWe-FPY

Average LWR/LWRmf capacity = 0.928 GWe

Average LWR/LWRmf capacity factor = 0.90 FPY/CY

Reactors in 2000 = 103

Reactors under construction need fuel in 2000 = 2 (these become operational in 2002-2003, representing the effect of uprates)

Reactors under construction in 2000 = 3 (these become operational in 2003-2005, representing the effect of uprates and reactor104)

a. Conversion from thousand kW-hr generated each year (i.e., MWe-full power hr/CY) to GWe-FPY/CY by 0.001 GWe/MWe x 1 day/24 hour x 1 yr/365.25 days = 1.14e-7 GWe-FPY/CY.

2.2.2 Legacy Reactors

Nuclear reactors currently operating in the U.S. are designated as legacy reactors. The following four user-input parameters should be self-consistent:

- Nuclear capacity in 2000 (86.0 GWe-FPY/CY).
- Number of legacy reactors, i.e., in 2000 (103 reactors)
- Average capacity factor (0.90 FPY/CY)
- Average capacity per reactor (0.928 GWe/reactor)

The above four values are self-consistent. Indeed, the fourth parameter (0.928 GWe/reactor) was set to be consistent with the other three parameters.

103 reactors x 0.928 GWe/reactor x 0.90 FPY/CY = 86.0 GWe-FPY/CY

b. DOE EIA2006a

c. DOE EIA2006b

If the number of legacy reactors, average capacity factor, and average capacity is less than the user-input for 2000 nuclear generation, the model will start the simulation by ordering new reactors to catch-up with the desired nuclear generation.

If the number of legacy reactors, average capacity factor, and average capacity is greater than the user-input for 2000 nuclear generation, those reactors will continue to operate. No new reactors will be ordered until the nuclear demand (escalated from 2000 on the basis of nuclear market share and total electrical growth rate) exceeds the capacity from the legacy reactors.

As there are 103 reactors in 2000, if the case being studied involves MOX, then the allocation of legacy reactors should be 17 LWR-MF (16%) and 86 LWR (84%), see Table 2-3. If the case being studied is IMF, then the allocation should be 7 LWR-MFR (6%) and 96 LWR (94%), although this may be too conservative for the heterogeneous, blended IMF cases.

Table 2-3. Thermal Reactor Safety Constraints on MOX/IMF [adapted from M. Todosow]

	Single-Pass MOX			Single-Pass IMF		
	% of		% of All Fuel in	% of		% of All Fuel in
	Reactors	% of	Fleet (Reactors	Reactors	% of	Fleet (reactors x
	That Can Use	Core	x Core)	That Can Use	Core	core)
Current PWRs	50%	33%	16%	25%	25%	6%
and BWRs						
Future PWRs and	100%	100	100%	50%	100	50%
BWRs		%			%	

2.2.3 Legacy Fuel

All used fuel (also known as spent fuel) generated by these reactors, prior to 2000, is called legacy used fuel. Coupled with the LWR/LWR-MF split implied in Table 2-3, U.S. DOE EIA data [DOE EIA2002] have been used to generate Table 2-4. We model the legacy fuel such that all fuel at least 10 years old in 2000 is (or could have been) in dry storage; all fuel less then 10 years is assumed to be in wet storage. To use these data, the user inputs the values of mass into the **Wet and Dry Storage** worksheet with fuel recipe numbers that correspond to the composition reflecting the average burnup.

Table 2-4. U.S. Used Fuel, Prior to 2000

Suggested allocation in reactor/storage type in	Mass	Average	Average	Years
2000	(kilotones)	burnup (GWth-	age	discharged
		day/tonne)	(years)	
LWR-UOX (86 of 103 reactors) - wet storage	17.704	38.19	4.4	1991 to
LWR-MOX (17 of 103 reactors) - wet storage	3.459			2000
LWR-UOX (86 of 103 reactors) - dry storage	17.946	26.89	16.6	1968 to
LWR-MOX (17 of 103 reactors) - dry storage	3.507			1990
Total	42.616	32.50	10.6	

d. After initialization, used fuel generated during the simulation stays in wet or dry storage according to user inputs discussed later.

e. The current recipe file has recipes 106 for 38.19 burnup and 107 for 26.89 burnup; these recipes do not include the impact of aging, but they could be adjusted accordingly.

3. MECHANICS OF RUNNING VISION

The Powersim software functions on a presentation level or a modification level.

- In presentation level, the user sees only an unchangeable model interface.
- In modification level, the user can see the actual model (graph representation of the relationship among variables and all sorts of details) or the interface.

If you are using VISION via a free reader, you only have access to the presentation level. If you have a full version of Powersim, then you can access both levels. [Opening the model directly from the file name rather than opening the Powersim software and then opening the model file will access only the presentation level.] This section supports both levels of operation.

3.1 Files Required to Run VISION

There are a set of files required to run the model. If the user has Powersim Studio 2005, we recommend that it be updated to service release 6. If the user does not have Powersim Studio software, she needs the free Powersim player, which can be downloaded at http://www.powersim.com/download/player.asp. The required files as follows:

- VISION Release 3.0.sip this is the main model
- vision base case settings ver6.xls input most of the specifications for pre-defined or user-defined simulations.
- vision recipes ver5.xls contains the fuel recipes
- vision half life ver4.xls contains the decay information for different isotopes
- **vision heatdosetox ver4.xls** contains the isotope-specific dose conversion factors and other parameters used in calculations for dose, radiotoxicity, and heat
- **output data-1.xls** collects the data produced by Powersim.

The system will store data for up to 5 runs in the input and output files.

The user will rarely, if ever, need to access or change the **heatdosetox** and **half life** files, which contain isotope-specific data used by VISION.

The file **vision base case settings ver6.xls** reads the list of available recipes from **vision recipes ver5.xls**. Powersim will work fine if the link between these two files isn't updated, but the list of available recipes in **vision base case settings ver6.xls** will not be up to date.

Cautions:

1. The only one of these files that can be renamed is **VISION Release 3.0.sip**.

All others are called by the main model, which will fail if files with those names do not exist.



f. The Powersim VISION model file has an extension of sip. If opened by clicking on the filename, you can only access the presentation level. If you open the file by first launching Powersim and then having it open the file, you can access the modification level.

- 2. All Excel files must remain in Office2003 format (extension xls); they cannot be Office2007 format (extension xlsx).
- 3. The Excel files must be in the same folder as the sip file.
- 4. Do not change the format of any of the above files, e.g., add or delete columns or rows. Do not re-order the sequence of rows or columns. Do not rename the worksheets within a file. One can re-order the sequence of worksheets within a given file, except for **output data-2.xls** in which even the sequence of worksheets is fixed.
- 5. Several of these Excel files contain macros, when you open the file, Excel will ask you whether you want to enable the macros, click "Enable Macros."

The following files are not required to run the model, but they are very valuable and are described in section 6:

output data-2.xls - reformats the data in output data-1
output checks.xls - assists the user in checking the validity of the simulations just run
output fuel masses by class.xls - graphs fuel masses by class, e.g., mass of TRU
output fuel masses.xls - graphs fuel masses (summed over all classes)
output reactors.xls - graphs reactor information
output separations.xls - graphs separation information
output waste.xls - graphs waste management information (not currently available)

Cautions:

- 6. **output data-1.xIs** will have a varying number of columns of data because the number of reactors, separations, or fuels can vary from 1 to 10. Before using any of the graphing files, use **output data-2.xIs**, which copies data from **output data-1** and puts into a standard 10-reactor, 10-fuel, 10-separation format. All the graphing files read from **output data-2.xIs** via links.

 Therefore, the graphing files will not show the results of new Powersim runs until both **output data-2.xIs's** data loading macro is run and the link between **output data-2** and the graphing file is updated.
- 7. After completing a run, the following files should be saved base case settings ver6.xls, output data2.xls, and any relevant graphing files.

Users experienced in using Excel may find it convenient to develop their own output files that extract only data relevant from their studies from **output data-2.xls**. For example, it is possible to copy the existing graphical output files and then modify them.

3.2 Getting to the Main Page

Whether you open VISION by clicking on the model icon or by starting Powersim and then opening the main model file, VISION will first open Excel files - vision base case settings ver6.xls and output data-1.xls. It will ask you whether you wish to update vision base case settings ver6.xls, it is easiest to say "no". (The update is simply to check the link to the recipe file for the most recent list of available fuel recipes.) If you say "yes", VISION will want then ask whether you wish to save the changes. If you then try to save it as its original name, VISION and Excel get into an infinite loop mating dance.

Cautions:

8. Do not close these files until you are finished running VISION.



VISION then opens in the presentation level with a title page that indicates the version and date of the model you have opened.

If you will be using the presentation level, follow these steps:

- 1. Pressing "enter" brings you to the disclaimer page
- 2. Once you read this, press "I agree" to continue

If you would like to use the modification level, press the icon, shaped like a projection screen (), in the toolbar at the top (remember to +first open Powersim and then open the model if you want to access the modification level). It will open in one of the pages of the model, depending on what was open when the model was last saved. To get to the Main Page, go to the "interface" page, which is third from the left. The left-most page is "Program Directory," which has links to the interface page as well as the others. You may wish to resize the image so that the entire main page fits on your screen.

Either way, you should see the Main Page (figure 3-1).

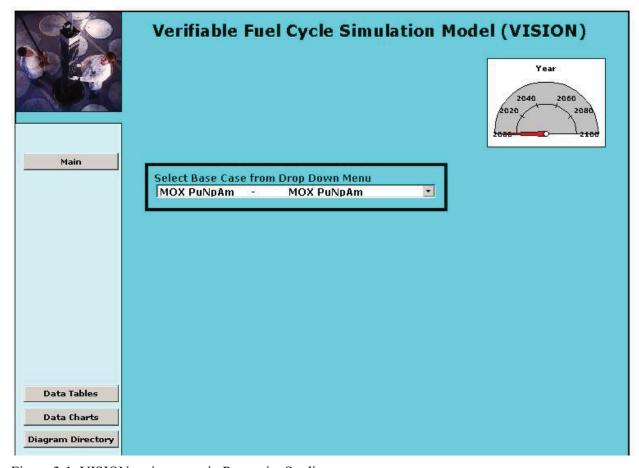


Figure 3-1. VISION main screen in Powersim Studio.

3.3 Running VISION

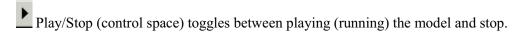
There is one pull-down menu and three key Powersim buttons needed to run the model:

The pull-down menu selects the case to run, each case corresponds to a set of parameters in a column in **base case settings ver6.xls**, either a pre-defined case or the last five options, which are allocated for user defined cases.



Within the box, is listed the entire selection of base cases from which the user may choose. At the end of the list are "User Defined" base cases that can be set by the user. To run one of the base cases, click the base case you want to run and then hit the play button on the tool bar. All of the pre-defined cases are constructed with two phases that often have a technology change between the two phases. The example above shows MOX transitioning to a burner fast reactor.

Reset (control-R) resets all the settings to their defaults and erases any data generated during the execution. The model will return to "run 1." Data already saved in **output data-1.xls** will not be immediately erased, but will be written over as soon as additional runs are executed.



Advance simulation one step (control shift space) advances a stopped simulation one time step (a quarter year). After completing a run, use this button to advance to the next run, to a maximum of "run 5."

Cautions:

- 9. Do not attempt to go to the next "run" without clicking on the "advance simulation" button.
- E
- 10. When you advance to a new run, the settings in the interface return to their defaults.
- 11. After the 5th run, clicking on the "advanced simulation" button will return the model to the 1st run. If you proceed to additional runs without copying and saving output files, VISION will write over your previously performed run 1 data in **output data-1**.



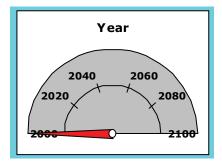
12. The model is currently set to use a 0.25 year time step and we recommend not changing this.⁹

g. The time step can be adjusted by going to "Simulation" on the tool bar and then going to "simulation settings" at the bottom of the pull down menu. However, we have not tested the model at alternative time steps. At higher time steps, it is likely that use of input parameter smaller than the time step, e.g., 0.25 years for enrichment time, would not work.

Depending on whether you opened presentation level or modification level, you will also see various Powersim software buttons above this VISION page and a Powersim list of models and variables to the left of this VISION page.

The left-hand buttons in the left-hand column allow you to navigate among the various pages of the control panel, while the rest of this page provides access to data output and different sections of the model. In later sections of this document we will discuss how to load input values using Excel files and we will also present how to set-up VISION to run several scenarios.

The "Year" gauge in the top right corner indicates the progress of the model while running a scenario.



3.3.1.1 Data Tables

The tables within Powersim provide limited output values from latest run of the VISION model. A more extensive set of output values is available via the Excel output tables. The data tables only show one run of the VISION model. Use the Excel outputs to save data from the run; these tables are intended only to help observe what is happening during a simulation.

3.3.1.2 Data Charts

The user can scroll down and see a number of charts that provide output values from the VISION model, although this is limited. A more extensive set of output values is available via the Excel output tables. The data charts will show only the latest run of the VISION model. Use the Excel outputs to save data from the run; these charts are intended only to help observe what is happening during a simulation.

3.3.1.3 Diagram Directory

Clicking on any of the buttons in the diagram directory will take the user to that portion of the model specified. The model will show all the dynamic logic within the VISION model. In order to get back to the main interface from this screen, use the arrows in the bottom left corner to scroll to the farthest right and then click on the "Interface" tab from the bottom set of tabs.

3.4 Suggestions for Inputting Data

If you have used VISION in the past, be aware that much of the information formally input on the **Reals 1** worksheet page are now in reactor, separation, or fuel fabrication worksheets. This actually makes input easier as data are grouped more logically.

It helps if you go methodologically through the worksheets in sequence (same sequence whether you use the navigation buttons or the tabs at the bottom). Previous versions of the model did not have worksheets in the same sequence as mass actually flows. While doing so, it is very helpful to color code the cells in the Excel input files appropriate to your cases and to how you conceptualize the problem. The **vision base case settings ver6.xls** file has many examples.

It helps to print out the three base case settings worksheets that merely list the available recipes, separation efficiency matrices, and recycle routing strategy matrices.

We suggest you keep consistency by "numbers" among reactors, separation, and fuel fabrication such that (1) = LWR/UOX/UOX separation, (2) = LWR MF/MOX/MOX separation, (3) = FR/FR/FR separation, etc even if one doesn't have MOX in a particular simulation so that S2 = 0.

4. VISION INPUT VIA BASE CASE SETTINGS FILE

This is the master input file. The Excel file **vision base case settings ver6.xls** contains multiple worksheets. If the file does not open at the **NAVIGATION** worksheet, click on that tab, it is the most left of the tabs and is colored red.



From the **NAVIGATION** worksheet, one goes to the other worksheets to input the required data. One can, of course, manually go to different worksheets by clicking on the tabs at the bottom of the page. Other than the basic information worksheets, which have red-colored tabs and just provide information, each worksheet follows the same general arrangement.

Explanations of the variables in that worksheet appear on the left most and right most columns. These denote the variable names (as they are called in Powersim), units, and ranges of appropriate variables. In between are the various base cases, pre-defined on the left and user-defined on the right, typically columns CU to CY. There are five columns set aside for user-defined cases. The buttons on the **NAVIGATION** worksheet page will take you to the user-defined columns.

The first three rows of most worksheets contain column labels, data must be entered starting in row 4.

Cautions:

13. If VISION is not open when you change an input file, save the file before opening VISION to ensure VISION reads your updated information. If VISION is open when you change an input file, VISION will not see the change until you save the file and advance to the next run in VISION.



The rest of this section explain what information appears in each worksheet, listed in order they appear in the base case settings ver6.xls file.

4.1 Basic Information (RED) Worksheets

These worksheets do not accept information from the user; they provide navigation and lists of options currently entered into appropriate locations. The four worksheet tabs are colored red, they are as follows:

- NAVIGATION
- List of reactor types & recipes
- List of separation types
- List of routing strategies

4.1.1 Basic (RED) - NAVIGATION

The NAVIGATION page (figure 4-1) has a link for each one of the pages within the vision base case settings ver2.xls file. There are links on each of the pages within the file that return to the NAVIGATION page for convenience. Some pages have cross-linked buttons, e.g., the worksheet List of separation types has a button to the separation matrices on Separation Stream Splits, which is where new separation matrices are entered. It has a button back to List of separation types for the user to verify that the new matrix name was registered.

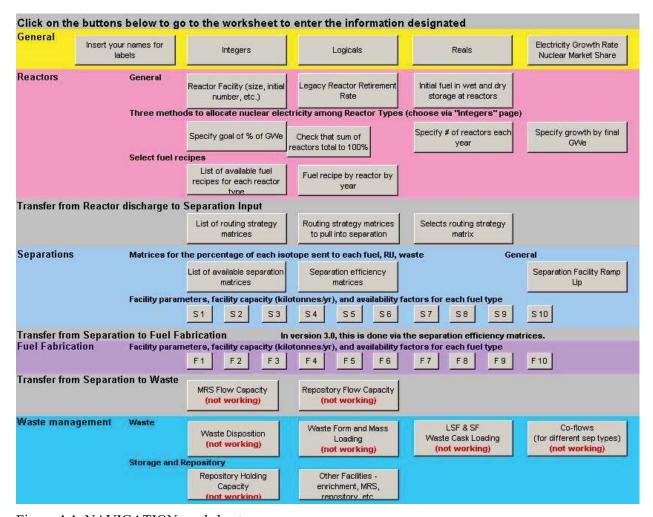


Figure 4-1. NAVIGATION worksheet page.

4.1.2 Basic (RED) - List of reactor types and recipes

This worksheet lists the available recipes by reading what information has been entered into **vision recipes ver5.xls**. If you wish to use a recipe that is not listed on this worksheet, go to vision **vision recipes ver5.xls** (section 5) and enter it. It should then appear on this worksheet.

There are also three special options that are available to the user.

- A correlation for LWR UOX fuel as function of burnup between 33 and 100 GWth-day/tonneiHM.
- A correlation for fast reactor metal fuel as a function of TRU CR between 0.00 and 1.00.
- A correlation for fast reactor oxide fuel as a function of TRU CR between 0.00 and 1.00.

Table 4-1 explains how to select fuel recipes. The user can add recipes to the blank columns in the 100, 200, 300, 400, 500, 600, or 700 pages, sequentially from the left. Changing any of the pre-defined recipes would invalidate base cases that use them.

Table 4-1. Fuel Recipe Numbering Scheme

Transformation Performance

Transmutation - change from input composition to output composition is determined by which reactor fuel recipe is used.

Fuel recipes are found in the fuel recipe file, numbered from -2 to at high as 799. At present, only a limited number of columns are used and linked back to the **List of reactor types & recipes**, but in principle the user could add columns up to x99 for each recipe type.

-2 to 0 - Correlation for fast reactor oxide fuels

0 to 2 - Correlation for fast reactor metal fuels

2 to 100 - Correlation for LWR burnup

101 to 199 - LWR uranium fuels

201 to 299 - Uranium fuels for other reactors

301 to 399 - LWR MOX

401 to 499 - LWR IMF

501 to 599 - Fuels to recycle in other reactors

601 to 699 - Fuels for metal-fueled fast reactors

701 to 799 - Fuels for other fast reactors

Fuel recipes are later user selected for each reactor type for each year.

4.1.3 Basic (RED) - List of separation types

This worksheet lists the separation types from 01 to 40 by reading what information has been entered into the **Separation Stream Splits** worksheet. If you wish to user a matrix that is not listed on this worksheet, go to **Separation Stream Splits** and enter it. Table 4-2 shows the numbering scheme. The user is encouraged to add separation matrix values to any of the blank matrices. Changing any of the pre-defined matrices would invalidate pre-defined base cases that use them.

Table 4-2. List of Separation Efficiency Matrices

Transformation Performance

Partition - how the contents of used fuel are allocated among fuel product streams, 3 grades of recovered uranium (RU), and several waste form options.

Separation efficiency matrices are numbered from 1 to 40.

1 to 20 - aqueous

21 to 30 - electrochemical

31 to 39 - other

40 - once through

About half are blank and available for user definition.

4.1.4 Basic (RED) - List of routing strategies

Recall that the recycle routing matrices send fuels from used fuel storage to separation types. This worksheet lists the recycling routing options from 01 to 15 by reading what information has been entered into the **Recycle Strategy Matrix** worksheet. If you wish to user a matrix that is not listed on this worksheet, go to **Recycle Strategy Matrix** and enter it. The current matrices are listed in Table 4-3. Changing any of the pre-defined matrices would invalidate pre-defined base cases that use them.

Table 4-3. List of Recycling Routing Matrices

1	Reserved for development testing
2	Reserved for development testing - 3 region base case (see Appendix A)

3	Reserved for development testing - 10 reactor case (see Appendix A)
4	Blank
5	Blank
6	1-tier recycling
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	FR fuel (assumed to be pass1 thru pass5 of fuel-3) is routed to separation-3
7	2-tier recycling
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	MOX (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-2
	FR fuel (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-3
8	One thermal recycle, then dispose
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	MOX ((or IMF) assumed to be pass1 of fuel-2) is routed to disposal
9	Multiple thermal recycle
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	MOX ((or IMF) assumed to be pass1 thru pass5 of fuel-2) is routed to separation-2
10	Blank
11	Blank
12	Stop fast recycling, send everything to thermal reactors. This is actually the same routing as 2-tier
	assuming that FR fuel is separated and then the products are sent to thermal reactors. So, the routing used
	fuel-to-separation is the same as 2-tier, but the routing from separation-to-fuel is different. The latter is set
	by separation efficiency matrices.
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	MOX (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-2
	FR fuel (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-3
13	Stop thermal recycling, send everything to fast reactors. This is actually the same routing as 2-tier
	assuming that MOX fuel is separated and then the products are sent to fast reactors. So, the routing used
	fuel-to-separation is the same as 2-tier, but the routing from separation-to-fuel is different. The latter is set
	by separation efficiency matrices.
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	MOX (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-2
	FR fuel (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-3
14	Stop recycling, send everything to disposal
	Passes 0 through 5 of fuels 1, 2, and 3 are routed to disposal.
15	Once through
	Pass 0 of fuels 1, 2, and 3 are routed to disposal. In once through, no fuel every gets past pass0, therefore
	no routing is required for passes 1 to 5.

4.2 General (YELLOW) Worksheets

The general worksheets require the user to provide general information about cases. Compared to previous versions of VISION, relatively little information remains in these worksheets. Virtually all data on reactors, separation, and fuel fabrication are now on worksheets dedicated to each of those functions. The six general worksheet tabs are colored yellow, they are as follows:

- Run Information
- Integer 1
- Logical 1
- Reals 1

- Growth Rate
- User help on growth rates

4.2.1 General (YELLOW) - Run Information

This worksheet requests the user to provide labels for

- Your name for each simulation run
- Names for fuel types
- Names for reactor types
- Names for separation types

The user does not need to enter anything into rows 5-7, but should ensure that the numbers calculated there are correct. The spreadsheet looks at the number of names entered for each case and thus determines (via the number of blanks) how many fuel, reactor, and separation types there are. Then, cells 15, 16, and 17 denote the maximum number of those types among the five runs.

Cautions:

- 14. These data are for five runs, which may or may not be user-defined cases 1-5.
- 15. The cells I5, I6, and I7 tell **output data-2.xls** how many fuel types, reactor types, and separation types have data in **output data-1.xls**. If these parameters are incorrect, then the translation from **output data-1** to **output data-2.xls** will be incorrect.

4.2.2 General (YELLOW) - Integer 1

This worksheet page allows the user to set basic parameters that control all reactors, all fuel types, all separations for the entire simulation. Table 4-4 lists the parameters and recommended values for this worksheet.

Table 4-4. Integer Worksheet Parameters

Parameter Units or Allowed Variables		Impact	Recommended Values	
Base case 1&2	Positive Integer between 1 and	This is a sequential number	Do not change,	
Selection	102	starting from the left.	for information only	
Base case uranium	1 = Known	The corresponding values are	Select "3"	
resource to use switch	2 = Known and Unknown	input on the Reals 1 Worksheet.		
	3 = Known + Unknown +	The model keeps track of how		
	Imagined	uranium resource is depleted.		
Base case used fuel	0 = Decay All	Which inventories calculate	Select "0"	
decay switch	1 = Decay Wet Storage Only	isotope decay?		
	2 = Decay None			
Base case repository	Date between 2000 and 2100	Overridden by Repository	2017 or	
open date		Capacity Worksheet. Zero flow	thereafter	
		means repository is closed.		
Base case TR Pu	Moved to Reactor Facility workship	eet, to be deleted here	_	
control switch				
Base Case FR Pu control switch	Moved to Reactor Facility workship	eet, to be deleted here		

Parameter	Units or Allowed Variables	Impact	Recommended Values
Base case start legacy reactor retirement date	Date between 2000 and 2100	This determines when legacy reactors start the retirement process and move into the condition of readying to retire, which means the model can order replacement reactors and then stops ordering fuel for them. Reactors actually go off line about six years (legacy reactors retirement delay + legacy reactors shut down delay) years later.	
Base case date to switch to ramp 2	To be deleted, no longer used		
Base case separation capacity basis	To be deleted, no longer used		
Separations combination switch	To be deleted, function replaced with reactor-to-separation recycle routing strategy matrices		
Manually set FBR switch	To be deleted, no longer used, no l	longer needed	
Base case reactor order case	 0 - let system optimize reactor mix using the percent goals set on Reactor %s worksheet times the nuclear power growth specified on Growth Rate. Not working reliably yet for FR. 1 - force VISION to use the number of reactors input by the user on the Reactor #'s worksheet. 2 - force VISION to build reactors to match the user specified growth for each reactor type via the end-simulation value on Reactor Facility worksheet times the year by year fraction of that value on Reactor Growth % of Final worksheet. 		Select "0" for cases without FR
Base case fuel fab order case	0 - let system optimize fuel fabrica 1 - force VISION to build fuel fabrica through 10 worksheets	Select "0"	
Base case separations order case	0 - let system optimize separation of 1 - force VISION to build separation through 10 worksheets	Select "0"	

4.2.3 General (YELLOW) - Logical 1

It is particularly important that the user correctly set all these switches appropriate for their scenario. Do not depend on one switch overriding another. Table 4-5 lists the parameters for this worksheet.

Table 4-5. Logical 1 Worksheet Parameters

- Logical 1 W			Recommended
Parameter	Units or Allowed Variables	Impact	Values
Base case send SF to	TRUE means used fuel is allowed to		Generally TRUE
repository	settings determine which parts		
	(permanent or retrievable or bo		
	and the receipt rate at the repos		
	FALSE means used fuel can never		
	other switch settings imply the		
D GD	HLW and other wastes are sent to t		D 1
Base case retrieve SF	TRUE creates a retrievable reposito	Depends on your	
from repository switch	FALSE means that used fuel in the		scenario
	retrieved. If material is sent to		
	allowed to be retrieved from the		
	act as though a permanent repo		
	equal to the repository holding HLW and other wastes are not retri		
	either way.	leved from the repository	
Base case unlimited	If TRUE, set repository flow receip	at limit on Dools workshoot as	Liqually got to
repository flow capacity	a generic high upper limit.	of fillit off Reals worksheet as	Usually set to FALSE
switch	If FALSE, set repository flow recei	nt on Donository Flow	FALSE
SWITCH	Capacity worksheet	pt on Repository Flow	
	Either value applies to used fuel re-	ceint at a nermanent and/or	
	retrievable repository. Receipt of I		
	never limited.	TEW and other wastes are	
Base case unlimited	If TRUE, then the retrievable repos	itory canacity is unlimited	Usually set to
repository holding	i.e., the year-by-year settings in		FALSE
capacity switch	Capacity worksheet are overri		TALSE
capacity switch	repository limit set on Reals 1		
	If FALSE, set repository holding ca		
	Holding Capacity Worksheet.		
	repository capacity limit is set		
	repository capacity limit is the		
	repository holding capacity (R		
	Worksheet) and the permanen		
	(Reals 1).		
	Capacity for HLW and other waste	s is not limited.	
Base case SF	TRUE creates a permanent repositor		Depends on your
permanent repository	the permanent repository(ies) i		scenario
switch	size of the permanent repositor	y should always be less than	
	or equal to the size of the repos	sitory holding capacity set on	
	the Repository Holding Capa		
	FALSE means that there is no perm		
	overridden if "retrieve from re		
	repository acts as if it is perma		
	HLW and other wastes can go to a		
	retrieved from the repository either way.		
Base case BU is waste	To be deleted, function now handle		
Base case use burned U phase 1	To be deleted, function now handle		
Base case unlimited TRUE means the MRS capaci			Not yet working,
MRS capacity switch	FALSE means the MRS capacity is	s limited.	MRS holding
			capacity always
			unlimited.

			Recommended
Parameter	Units or Allowed Variables	Impact	Values
Base case unlimited	TRUE means Storage Facilities have unlimited product storage.		Not yet working,
product storage	FALSE means Storage Facilities ha	ave limited capacity.	always unlimited.
capacity switch	_		
Base case use youngest	To be deleted, function handled by	separation-to-reactor recycle	
least cycled fuel first	routing strategy matrices		
Base case use MRS	TRUE / FALSE TRUE creates an MRS		Depends on scenario
switch		(managed retrievable	
		storage) or centralized	
	storage facility.		
	FALSE turns off the option		
		of an MRS/ centralized flow	
		facility	

4.2.4 General (YELLOW) - Reals 1

These are often the most important parameters of the entire simulation, see Table 4-6.

Table 4-6. Reals Worksheet Parameters

	Units or Allowed		Recommended
Parameter	Variables	Impact	Values
Base case known uranium resources	Kilotonnes of U	Gives the model the values for these three benchmarks	3,100 kt-U
Base case estimated conventional uranium resources (includes known uranium resources) Base case estimated unconventional uranium			16,000 kt-U
Base case natural enrichment	Units or allowed	Impact	4,200,000 kt-U 0.711
Base case tail enrichment	variables		0.25
Base case USA year-2000 demand level	>0 GWe-FPY/year (not zero)	Initial nuclear power generation rate ^h	86.00193 GWe- FPY to match 2000 U.S. data
Base case Initial Nuclear Power Percent	>0 to 100 (do not use % symbol)	VISION calculates the initial total electricity demand in 2000 from the nuclear electricity / nuclear market share, = 433.7 GWe-FPY for U.S.	19.83 to match 2000 U.S. data
Base case unlimited repository flow capacity	≥0 kilotonne/yr	This specifies the flow rate of material to the repository when the unlimited repository flow capacity switch in Logical 1 worksheet is set to TRUE. The repository flow capability only applies to unprocessed used fuel; the receipt rate for HLW and TRU waste is unlimited.	50 kt/year

_

^h Average LWR/LWRmf capacity x average LWR/LWRmf capacity factor x number of legacy reactors should equal to the nuclear power generation in 2000.

	Units or Allowed		Recommended
Parameter	Variables	Impact	Values
Base case unlimited	≥0 kilotonne	This specifies the overall repository	7000 kilotonne
repository holding capacity		holding capacity (permanent	
		repository capacity + retrievable	
		repository capacity), when the	
		unlimited repository holding	
		capacity is set to TRUE on Logical	
		1 worksheet.	
		The capacity limit only applies to	
		unprocessed used fuel, the	
		repository has unlimited capacity	
		for HLW and TRU waste.	
Base case permanent	≥0 kilotonne	This specifies the permanent	63 kilotonne
repository limit		repository capacity; it should be	
		less than the repository holding	
		capacity, which is set with the	
		Repository Holding Capacity	
		worksheet or the above value.	
		The capacity only applies to	
		unprocessed used fuel, the	
		repository has unlimited capacity	
		for HLW and TRU waste.	
Delete last row			

4.2.5 General (YELLOW) - Growth Rate Worksheet and User Help on Growth Rates Worksheet

The growth rate of nuclear power demand is set by a combination of the total electricity growth rate and the market share of nuclear power. In the upper table on **Growth Rate**, the annual percent growth rate of electricity is specified, year by year. In the lower table on **Growth Rate**, the annual market share of nuclear reactors as a percent of electricity is specified.

This worksheet is used if "Base case reactor order case" on the Integer 1 worksheet is set to 0, in which case nuclear power demand is set on Growth Rate for the entire reactor fleet. If "Base case reactor order case" is set to 1, then growth is not determined by Growth Rate, but instead is determined by the precise number of reactors specified on Reactor #'s. If "Base case reactor order case" is set to 2, then growth is not determined by Growth Rate, but instead is determined by each reactor type separately using a combination of the end-simulation capacity set on Reactor Facility and the year by year values set on Reactor Growth % of Final.

A second worksheet, **User Help on Growth Rates**, is provided to help the user calculate the appropriate nuclear market share when a electricity grow rate and nuclear growth rate are known, or when specific nuclear market penetrations at specific times are known.

4.3 Reactor (PINK) Worksheets

The set of reactor worksheets provide input for the reactor fleet. The worksheets **Reactor Facility**, **Legacy Reactor Retirement Rate**, **Wet and Dry Storage**, and **Reactor Fuel Types** are used in all simulations. In a given simulation, only one of the worksheets **Reactor %s**, **Reactor #'s**, or **Reactor Growth % of Final** are used, depending on which reactor order case on Integer 1 was selected. When **Reactor %s** is used, then **Reactor %s Total** provides the user with the total of the percentages he

specified on **Reactor %s**; that total should be 100. Table 4-7 summarizes how these worksheets work together.

Table 4-7. Reactor Capacities and Transformation Performance in VISION

Capacity	Transformation Performance
Reactor Order Case switch in "Integer 1"	Transmutation - change from input composition to output
among	composition determined by which reactor fuel recipe is selected
0. Let system optimize reactor mix by	by year on Reactor Fuel Types.
giving VISION a goal of the percent	
allocation among the reactor types (by	Fuel recipes are found in the vision recipe ver5.xls file,
year). VISION uses Reactor %s time	numbered from -2 to 799.
Growth Rate.	-2 to 0 - Correlation for fast reactor oxide fuels
1. Force VISION to use specific number of	0 to 2 - Correlation for fast reactor metal fuels
reactors each year. VISION uses	2 to 100 - Correlation for LWR burnup
Reactor #'s.	101-199 - LWR uranium fuels
2. Force VISION to build reactors	201-299 - Uranium fuels for other reactors
according to the product of (a) end-	301-399 - LWR MOX
simulation GWe-year goal times (b) the	401-499 - LWR IMF
percent of that goal to be achieved each	501-599 - Fuels to recycle in other reactors
year. VISION uses Reactor Facility and	601-699 - Fuels for metal-fueled fast reactors
Reactor Growth % of Final.	701-799 - Fuels for other fast reactors
	Fuel recipes are set for each reactor type for each year.
Reactors that are operational when the	
simulation starts are retired according to the	The user can add recipes to the blank columns in the 100, 200,
Legacy Reactor Retirement Rate data. All	300, 400, 500, 600, or 700 pages, sequentially from the left.
other reactors retire when their lifetime (set	Changing any of the pre-defined recipes would invalidate base
on Reactor Facility) is met.	cases that use them.

4.3.1 Reactor (PINK) - Reactor Facility

Table 4-8 lists the parameters entered on this worksheet. Note that fuel residence time, fuel burnup, and capacity factor are not entered here, but instead are entered with fuel composition data in **vision recipe ver5.xls**.

Table 4-8. Reactor Capacities and Transformation Performance in VISION

Parameter	Units or Allowable	Impact	Recommended Value for	Recommended Value for Fast
	Values		LWRs	Reactors
Licensing Time	≥0.25 years (≥ time step)	Sets duration of licensing, between when reactors are ordered and when they start construction.	2	2
Construction Time	≥0.25 years (≥ time step)	Sets duration of construction between when they are licensed and when they are ready for fuel. Reactors don't actually start operation unless fuel is available.	4	4
Lifetime	≥0.25 years (≥ time step)	How long reactors operate.	60	60
Reactor power	GWe/reactor	Converts #s of reactors into power. If reactor order case = 0 or 2, it only determines the number of reactors	0.928 GWe per reactori	Depends on your scenario

i. 103 reactors x 0.928 GWe/reactor reactor size x 0.90 FPY/CY capacity factor = 86.0 GWe-FPY/CY in 2000.

		T	1	
		but the mass flows are really controlled by energy demand and		
		fuel burnup. If reactor order case =		
		1, this parameter times Reactor #'s		
		divided by fuel burnup determines		
		mass flows.		
Fuel Flow Control	0, 1, 2, 3, 4, 5	Controls the limiting isotope(s)	5 (total Pu)	4 (total TRU)
switch		which will determine the amount of		
		new fuel that can be produced given		
		the minimum amount of that		
		specific isotope in a given fuel		
		recipe.		
		$0 = \min(Pu239, Pu240, Pu241)$		
		1 = Pu239		
		2 = Pu240		
		3 = Pu241		
		4 = TRU		
		5 = Pu		
Thermal Efficiency	0.01 to 1.00		0.34	0.38
Legacy Reactors	Integer	Number of reactors operational	86 LWR-UOX	0
		when simulation starts	17 LWR-MOX	
Fresh Reactors	Integer	Number of reactors just beginning	0	0
		service when simulation starts		
	Integer	Number of reactors starting the	0	0
retirement		retirement process when simulation		
		starts		
	Integer	Number of reactors starting	3	0
construction		construction when simulation starts	(See Table 2-2)	
	Integer		0	0
construction need				
fuel				
	Integer	Number of reactors starting	2	0
licensed		licensing when simulation starts	(See Table 2-2)	
Final GWe for %	GWe-year	Used when reactor order case on	0	0
Growth		Integer $1 = 2$.	1	

4.3.2 Reactor (PINK) - Legacy Reactor Retirement Rate

As of 2000, there were 103 operating reactors in the U.S. In this model, these reactors are called legacy reactors, reactors present before the simulation starts. Many, if not most, of these reactors have or will obtain license extensions to operate beyond their original lifespan. To specify the retirement of these legacy reactors, the user must specify the number of reactors remaining during a 30-year period in the **Legacy Reactor Retirement Rate** worksheet and specify the Base Case Start Legacy Reactor Retirement Date on the **Integer 1** worksheet. A retirement rate that considers both the start date and the expected lifetime of these reactors has been calculated and is used for all of the base case options.

4.3.3 Reactor (PINK) - Wet and Dry Storage

When fuel is discharged from a reactor, it goes into "wet" storage, where "wet" is meant to imply that cooling of the fuel is required. For UOX or MOX or IMF, this is the traditional water pool. Regardless of its destination, fuel must stay in wet storage for a minimum time set by the user for each reactor type. That is, the model never allows fuel to move from wet storage until the minimum time set by the user is achieved.

When fuel is moved from "wet" storage, it goes to "dry" storage. It can move into repository or separation capacity to the extent that either has sufficient capacity to process that fuel; in such cases the model ignores the time period for "dry" storage. Otherwise, used fuel accumulates in dry storage until moved to a centralized monitored retrievable storage at the end of the time period specified by the user, provided that the MRS is turned on. If the MRS is not turned on, the used fuel stays in dry storage until there is capacity to move it to separations or repository.

All used fuel (also known as spent fuel) generated by these reactors, prior to 2000, is called legacy used fuel. Coupled with the LWR/LWR-MF split implied in Table 2-3, U.S. DOE EIA data [DOE EIA2002] have been used to generate Table 2-4, repeated below. To use these data, the user inputs the values of mass into the **Wet and Dry Storage** worksheet with fuel recipe numbers that correspond to the composition reflecting the average burnup. We make the simplifying assumption that legacy fuel prior to 2000 is modeled as being in wet storage if younger than 10 years and being in dry storage if older than 10 years. The 10-year threshold is set to be consistent with the 10-year minimum time in wet storage we use in LWR simulations.

Table 2-4. U.S. Used Fuel, Prior to 2000 (replic	ated here)			
Suggested allocation in reactor/storage type in	Mass	Average	Average	Years
2000	(kilotones)	burnup (GWth-	age	discharged
		day/tonne)	(years)	
LWR-UOX (86 of 103 reactors) - wet storage	17.704	38.19	4.4	1991 to
LWR-MOX (17 of 103 reactors) - wet storage	3.459			2000
LWR-UOX (86 of 103 reactors) - dry storage	17.946	26.89	16.6	1968 to
LWR-MOX (17 of 103 reactors) - dry storage	3.507			1990
Total	12 616	32.50	10.6	

Table 2-4. U.S. Used Fuel, Prior to 2000 (replicated here)

4.3.4 Reactor (PINK) - Reactor %s and Reactor %s Total

This worksheet is used when reactor order case on **Integer 1** is set to 0. It allows the user to set the percent of each type of reactor to be requested for new reactors being ordered. The user sets the percent for each type of reactor as a function of time. The sum must equal 100 and can be quickly checked by looking on the **Reactor% Total** worksheet.

4.3.5 Reactor (PINK) - Reactor #'s

This worksheet is used when reactor order case on **Integer 1** is set to 1. This option should be used with caution by the user, since specifying the number of reactors will override the specifications for reactor power generation and possibly order fast reactors for which there is no fuel. When using this option, the number of reactors must be specified for the full 100 years or 200 years of the simulation and for each type of reactor.

4.3.6 Reactor (PINK) - Reactor Growth % of Final

This worksheet is used when reactor order case on **Integer 1** is set to 2. This option should be used with caution by the user, since specifying the end-simulation growth value input on Reactor Facility times these values will override the specifications for reactor power generation and possibly order fast reactors for which there is no fuel.

j. The current recipe file has recipes 106 for 38.19 burnup and 107 for 26.89 burnup; these recipes do not include the impact of aging, which would transform some Pu241 into Am241, but they could be adjusted accordingly.

4.3.7 Reactor (PINK) - Reactor Fuel Types

The worksheet specifies the reactor fuel recipe for each reactor type for each year, see Table 4-9. It is recommended that the user not attempt to use a "reactor type" beyond the range of fuel types that an actual reactor technology could reasonably be expected to accommodate, e.g., burn fast reactor fuels in a LWR or use fast breeder reactor fuel compositions in a reactor initially using fast burner reactor fuel compositions.^k

Recall that selecting a fuel recipe number invokes several parameters from **vision recipes ver5.xls**, as described further in section 5. These factors are interconnected and therefore they reside together in the recipe file. They are follows:

- Fuel burnup (GWth-day/tonne-iHM)
- Capacity factor
- Fuel residence time (calendar years)
- The input and output compositions for this primary fuel.
- The number of a contingent fuel (if any) that VISION will use in this reactor if the primary fuel cannot be made. The contingent fuel should be a uranium-based fuel.
- Uranium priority 1 to 6 what type of uranium supply (EU, NU, DU, RU) should be used to make up the correct amount of uranium in the fuel once the uranium in the incoming separation-to-fuel buffer is accounted for.

k. Breeders typically require blankets surrounding the core; burners do not. So, a reactor initially built only for burner fuels would not be capable of later using breeder fuel compositions without substantial modification.

Table 4-9. Fuel Types

Reactor technology	Appropriate reactor fuel numbers in vision recipe ver5.xls
LWR	33 to 100 - LWR burnup correlation
	101 to 110 - recipes in 100 UOX Once Thru worksheet
LWR MF (multiple fuel)	33 to 100 - LWR burnup correlation
	(Values from 2 to 100 are allowed by VISION but values from 2 to 32
	produce unreliable results in the current burnup correlation.)
	101 to 110 - recipes in 100_UOX_Once_Thru worksheet
	301 to 315 - recipes in 300 LWR MOX worksheet
	401 to 415 - recipes in 400_LWR_IMF worksheet
HWR or VHTR	Appropriate recipes among
	201 to 210 - recipes in 200_Other_Once_Thru worksheet
HWR or VHTR possibly	Appropriate recipes among
using recycled material	201 to 210 - recipes in 200_Other_Once_Thru worksheet
	501 to 510 - recipes in 500_Other_Thermal_Recycle worksheet
	Currently all the 500 recipe slots are blank.
Fast burner reactor, sodium	-1.00 to 0.00 - fast reactor oxide TRU CR correlation
cooled	0.00 to 1.00 - fast reactor metal TRU CR correlation
	(Values from -2.00 to 0.00 and 0.00 to 2.00 are allowed by VISION but
	values below -1 and above +1 produce unreliable results in the current
	TRU CR correlations.)
	Appropriate recipes among
	601 to 630 - recipes in 600_Metal_Cooled_FR worksheet
Fast breeder reactor,	Appropriate recipes among
sodium cooled	601 to 630 - recipes in 600_Metal_Cooled_FR worksheet
Fast reactors with other	701 to 710 - recipes in 700_Other_Cooled_FR worksheet
coolants	Currently all the 700 recipe slots are blank.

If for example you want to vary the capacity factor of a reactor type, create duplicate recipes that vary only by the capacity factor and select among them.¹

The appropriate primary fuel in a LWR capable of using multiple fuels (LWR-MF) is one of the MOX (fuel numbers 2xx) or IMF (fuel numbers 3xx) recipes. If the contingent fuel is a UOX recipe (typically fuel number 103, for 51 GWth-day/tonne burnup UOX), then that UOX is used when the supply of MOX or IMF is inadequate. That UOX is considered by VISION to be MOX recycle pass0 and is distinct from UOX that may be used as the primary fuel in UOX-only LWRs.

Recipes 101, 601, and 602 are special cases as they evoke the LWR burnup correlation (recipe 101) or fast reactor TRU CR correlations (recipes 601, 602). In these cases, the user must specify the burnup in the appropriate places in **vision recipes ver5.xls**, which is used whenever such recipes are selected. If you want to use the LWR burnup or TRU CR correlations by year, use 33 to 100 (LWR burnup correlation), 0 to +2 (fast reactor metal TRU CR), or -2 to 0 (fast reactor oxide TR CR).

4.4 Reactor to Separation Routing (GREY) Worksheets

These two worksheet control the routing of used fuel from reactor wet/dry storage into separation types.

1. Strictly speaking, one should also modify the recipe slightly to account for differences as the capacity factor during irradiation is varied.

4.4.1 Reactor to Separation Routing (GREY) - Recycle Strategy Option

The user specifies on this page which of the recycle routing strategy matrices defined on the **Recycle Strategy Matrix** worksheet is used for each year. Since each recycle routing strategy matrix addresses all recycle passes, all reactor/fuel types, and all separation types, only one matrix is selected for each year.

Changing recycle routing strategy matrix from one year to the next means that the fleet's recycling strategy has fundamentally changed.

4.4.2 Reactor to Separation Routing (GREY) - Recycle Strategy Matrix

These matrices provide the priority for separations and disposal. Within a fuel type, the prioritization by pass and reactor source must also be specified for each separation facility type. This is accomplished through the matrices in this page. Each separation facility type is assumed to accept one type of fuel. In cases where more than one type of fuel is sent to a single type of separations facility, all of the fuel entering that separations facility will be considered the nominal fuel type for that facility when it exits. At any given point in time, material coming from a given Reactor, Pass can only be specified as a single Fuel Type, Pass. At any given point in time, material coming from a given Reactor, Pass can only be specified as going all to separations or all to disposal. The matrices must be filled out using a 3 numeral code. The first e numerals indicate the reactor type and the fourth numeral indicates the pass.

Fuel types correspond to codes 10 to 19.

Recycle passes correspond to code 0 to 5.

Each matrix defines the priority order for fuel to enter a given separation type.

Recall that the same fuel recipe can be used in multiple places. For example, in a MOX capable reactor, the primary fuel is one of the MOX recipes (fuel number 2xx) and the contingent fuel is a UOX recipe (typically fuel number 103). Thus, a strategy of one recycle pass in a MOX-capable reactor means that there are both pass0 and pass1 fuel in that fuel slot. Consider an example where MOX is fuel-2, hence code "11x". So, the recycling routing matrix must account for both 110 (MOX, pass 0 = UOX) and 111 (MOX, pass 1). The user can then decide which of two approaches to use, as follows:

- Pull 110 (MOX, pass 0 = UOX) to the same separation plant as 100 (UOX, pass 0) and 111 (MOX, pass 1 = MOX) to a separate separation plant designed for MOX. This implicitly assumes there is a mechanism to physically separate MOX from UOX in the LWR-MOX reactors, as is appropriate if the fuels are different assemblies.
- Pull 110 and 111 to the same separation plant, designed for a UOX-MOX fuel mix. This would be appropriate if the fuels are co-mingled within fuel assemblies.

Said another way, the underlying cause for the complexity and the different ways of modeling a scenario correspond to actual variations in how a scenario would work in reality. The complexity isn't the model, the model is reflecting the complexity of the real world.

The user determines the priority order in which each separation plant capacity is used, e.g., specifying if fast reactor fuel is fuel type-3 (hence code 12x), then two strategies can be created:

- Pull 125, 124, 123, 122, 121 into the separation type means that the most recycled fuel goes first.
- Pull 121, 122, 123, 124, 125 into the separation type means the least recycled fuel goes first.

In this example, if the user has defined a contingent (uranium) fuel for the fast reactor, that fuel (code 120) would need to be added to the list.

Cautions:

16. The recycle routing strategy matrix must account for all fuels and recycle passes that may exist during a simulation.



Tab	le 4-3. List of Recycling Routing Matrices (repeated from earlier subsection)
1	Reserved for development testing
2	Reserved for development testing
3	Reserved for development testing
4	Blank
5	Blank
6	1-tier recycling
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	FR fuel (assumed to be pass1 thru pass5 of fuel-3) is routed to separation-3
7	2-tier recycling
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	MOX (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-2
	FR fuel (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-3
8	One thermal recycle, then dispose
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	MOX ((or IMF) assumed to be pass1 of fuel-2) is routed to disposal
9	Multiple thermal recycle
	UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1
	MOX ((or IMF) assumed to be pass1 thru pass5 of fuel-2) is routed to separation-2
10	Blank
	D1 1
11	Blank
11	Stop fast recycling, send everything to thermal reactors. This is actually the same routing as 2-tier
	Stop fast recycling, send everything to thermal reactors. This is actually the same routing as 2-tier assuming that FR fuel is separated and then the products are sent to thermal reactors. So, the routing used
	Stop fast recycling, send everything to thermal reactors. This is actually the same routing as 2-tier assuming that FR fuel is separated and then the products are sent to thermal reactors. So, the routing used fuel-to-separation is the same as 2-tier, but the routing from separation-to-fuel is different. The latter is set
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12	Stop fast recycling, send everything to thermal reactors. This is actually the same routing as 2-tier assuming that FR fuel is separated and then the products are sent to thermal reactors. So, the routing used fuel-to-separation is the same as 2-tier, but the routing from separation-to-fuel is different. The latter is set by separation efficiency matrices. UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1 MOX (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-2 FR fuel (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-3
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13	Stop fast recycling, send everything to thermal reactors. This is actually the same routing as 2-tier assuming that FR fuel is separated and then the products are sent to thermal reactors. So, the routing used fuel-to-separation is the same as 2-tier, but the routing from separation-to-fuel is different. The latter is set by separation efficiency matrices. UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1 MOX (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-2 FR fuel (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-3 Stop thermal recycling, send everything to fast reactors. This is actually the same routing as 2-tier assuming that MOX fuel is separated and then the products are sent to fast reactors. So, the routing used fuel-to-separation is the same as 2-tier, but the routing from separation-to-fuel is different. The latter is set by separation efficiency matrices. UOX (assumed to be pass0 of fuel-1 and fuel-2) is routed to separation-1 MOX (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-2 FR fuel (assumed to be pass1 up to pass5 of fuel-2) is routed to separation-3 Stop recycling, send everything to disposal Passes 0 through 5 of fuels 1, 2, and 3 are routed to disposal.

4.5 **Separation (BLUE) Worksheets**

There are three types of separation worksheets, as follows:

- **Facility Ramp Up** defines for each separation type what fraction of the facility's rated capacity is operational during the first several years of operation.
- **Separation 1 through 10** defines several parameters for that separation type, including capacity and which separation efficiency matrix is to be used, by year.
- **Separation Stream Splits** defines the performance of a separation type.

Table 4-10 summarizes how these worksheets work together.

Table 4-10. Separation Facility Capacities and Transformation Performance in VISION

Capacity	Transformation Performance
Separations Order switch in Integer 1	Partition - how the contents of used fuel are allocated
among	among fuel product streams, 3 grades of recovered
0. Let VISION optimize separation	uranium (RU), and several waste form options. This is
capacity. VISION builds separation	determined by the separation efficiency matrices defined
capacity subject to the Separations	on the Separation Stream Splits worksheet.
Data, which is set on the	
Separations worksheets.	Separation efficiency matrices are numbered from 1 to 40.
1. Force VISION to build specific	1 to 20 - aqueous
separation capacity each year, the	21 to 30 - electrochemical
capacity is also set on the	31 to 39 - other
Separation s worksheets. Note: The	40 - once through
Separations Date switch in	About half are blank and available for the user to define.
Separation X worksheets overrides	
capacity specifications; capacity is	The user is encouraged to add separation matrix values to
built but not used.	any of the blank matrices. Changing any of the pre-
	defined matrices would invalidate base cases that use
Capacity specified above is then reduced	them.
by the defined facility rampup specified	
on the Facility Ramp Up worksheet.	The list of recipes (including any the user has added) is
	given on page "List_of_separation_types"

4.5.1 Separation (BLUE) - Facility Ramp Up

This page allows the user to specify the speed with which a Separation Facility comes on line. The first column specifies the year number (1-20). The second column represents the percentage of the facility completed with one representing 100% or the facility is complete. This column is cumulative. Years (1-20) must total 100%. Each reactor has a rate 1 and rate 2. The second rate is more efficient than the first.

4.5.2 Separation (BLUE) - Separation 1 through Separation 10

Table 4-11 lists the parameters set on these worksheets, one for each separation type. Most of the parameters are straightforward, with exception of specification of separation efficiency matrix by recycle pass. Except in rare circumstances, the array of selection of separation efficiency matrices for the six recycle passes (0 through 5) will be identical. The only known exception is recycling 2 or more times in one type of reactor, e.g., LWR-MOX, and then sending fuel to another type of reactor, e.g., fast reactor. Otherwise, all recycle passes in a given separation facility should have the same separation efficiency matrix.

Table 4-11. Parameters set on the Separation Worksheets

	Units or Allowed		Recommended
Parameter	Variables	Impact	Values
Construction Time	≥0.25 years	Sets delay for construction of	5
	(≥ time step)	separation facilities.	
Lifetime	≥0.25 years	How long separation plants operate.	60
	(≥ time step)		
Separation duration	≥0.25 years	How long material resides in the	1
	(≥ time step)	separation plant	
Unlimited separation		ot limit separation by capacity	FALSE
capacity	FALSE = VISION does 1	imit separation by capacity	
	TRUE is unrealistic but a	helpful option for debugging a case if	
	one suspects that mass flo	ow is choked at separations.	
Separation facility size	> 0 kilotonnes/	Determines the unit size of these	Depends on
	calendar year	facilities. Only integer number of	your scenario
	(not zero)	these facilities can be built. If allowed	
		by user input settings, VISION will	
		calculate the number of required	
		facilities and round up.	
Initial Pu239 stockpile	≥0 kilotonnes-Pu239	This allows the user to specify the	Depends on
		amount of Pu239, available from	your scenario
		sources external to the fuel cycle.	
Separations date	Date between 2000 and	This date overrides the separation	2020
	2100, inclusive	capacity specified elsewhere. This	
		means that separation capacity can	
		exist before the specified start date but	
		that separations will not start before	
		that date.	
Number of recycle passes	To be deleted, function he	andled by recycle routing and separation	efficiency
(200 rows)	matrices		55
Capacity for that separation	0 to 1000 Kilotonnes/	Determines the capacity each year if	
facility type by year (200	calendar year	Separations Order switch in Integer 1	
rows)		= 1, otherwise no impact.	
Separation efficiency matrix	1 to 40	This decides which of the separation	
numbers by year (200 rows)		efficiency matrices is used for each	
for recycle pass 0, then pass		recycle pass for each year.	
1, 2, 3, 4, and 5.			
Separations capacity	0.00 to 1.00	Determines the fraction of time during	1.0
availability factor	FPY/calendar year	a year that separation facilities	
-		generate 100% of their rated capacity	

Some examples:

Matrix 1 - simulates UREX+1 or electrochemical separation, sends TRU to fuel-2, with waste segregated into several types, appropriate to use for separation-1 (all recycle passes) if these are operating on UOX or MOX and all TRU is to be recovered and sent to fuel-2.

Matrix 2 - same as matrix 1 except sends TRU to fuel-3, appropriate to use for separation-2 (all recycle passes) if these are operating on UOX or MOX and all TRU is to be recovered and sent to fuel-3. So, material separated from used MOX (if a 1-pass MOX strategy) is sent elsewhere. TRU

gets into MOX not from separation-2 but from separation-1. TRU sent from UOX pass 0 goes to fresh MOX pass 1.

Matrix 6 - simulates UREX+2 so that NpPu is recovered and sent to fuel-2, AmCm goes into waste.

Matrix 13 - simulates UREX+4 so that NpPuAm is recovered and set to fuel-2, Cm goes into waste.

Matrix 16 - simulates COEX so that U and Pu is recovered and sent to fuel-2, NpAmCm goes into waste.

4.5.3 Separation (BLUE) - Separation Stream Splits (Separation Efficiency Matrices)

This worksheet specifies the isotopic composition (on a mass percent basis for each isotope) for each stream exiting a given separations option. There are 40 separations options available, including various versions of UREX+, COEX, Electrochemical (Table 4-12). One separation strategy can be defined for each fuel type for each year.

The separation efficiency matrices perform several functions, as follows:

- Identify which TRU elements are recovered and how they are grouped, see examples in Table 4-12.
- Identify what fraction of fission product become impurities in fuel material.
- Identify where fuel products go, i.e., new fuel fabrication 1 through 10. This separation-to-fuelfab routing could instead by done by a different set of routing matrices of fuel products into fuel fabrication. That alternative modeling approach would be appropriate if we wanted to specify fuel fabrication by *pulling* feedstock from multiple separation facilities, instead of the current approach of *pushing* fuel products from separation into fuel fabrication buffers.
- NOTE: The RU buffers are not yet working. Instead, send RU to the appropriate fuel product buffers. Unused RU will accumulate there and not be counted as waste.

FUTURE: Identify which of three recovered uranium storage buffers to send uranium that is recovered separately from one or more TRU products. It is anticipated that some scenarios will involve multiple reactor types in which case the stockpile of RU would need to be kept separate, e.g., relatively high enriched used uranium from VHTR would be put into RU-H and moderately enriched uranium from LWR would be RU-M, and low enriched uranium from used HWR fuel would be RU-L.

- Define how many and which waste streams are produced.
- Identify which chemical elements go into which waste stream.
- Identify how much uranium and TRU does into each waste stream.

Table 4-12. Definition of Separation Efficiency Matrices

	Technology	Fuel goes to fuel fabrication number	Waste strategy
1	UREX+1 (all TRU recovered)	2	Segregated waste streams
2	UREX+1 (all TRU recovered)	3	Segregated waste streams
3	UREX+1 (all TRU recovered)	2	All to HLW

4 UREX+1 (all TRU recovered		3	All to HLW
5 Blank	/		
6 UREX+2 (NpPu recovered,	AmCm to waste)	2	Segregated waste streams
7 UREX+2 (NpPu recovered,		3	Segregated waste streams
8 UREX+2 (NpPu recovered,		2	All to HLW
9 UREX+2 (NpPu recovered,		3	All to HLW
10 Blank	,		
11 UREX+3 (NpPu and AmCm	,	NpPu to 2 AmCm to 3	Segregated waste streams
12 UREX+3 (NpPu and AmCm	,	NpPu to 2 AmCm to 3	All to HLW
13 UREX+4 (NpPu, Am, and C	m recovered)	NpPuAm to 2 Cm to waste	Segregated waste streams
14 Blank			
15 Blank			
16 COEX		2	All to HLW
17 COEX		3	All to HLW
18 Blank			
19 Blank			
20 Blank			
21 Electrochemical (all TRU re		3	Segregated waste streams
22 Electrochemical (all TRU re		3	All to HLW
23 Electrochemical (all TRU re		4	Segregated waste streams
24 Electrochemical (all TRU re	covered)	5	Segregated waste streams
25 Blank			
26 Blank			
27 Blank			
28 Blank			
29 Blank			
30 Blank			
31 Dry (only volatile fission pro		2	All to HLW
everything else becomes qui			
32 Dry (only volatile fission pro		3	All to HLW
everything else becomes qui			
33 Dry (only volatile fission pro everything else becomes qui		7	All to HLW
34 Blank	/		
35 Blank			
36 Blank			
37 Blank			
38 Blank			
39 Blank			
40 Once through (everything to	HLW)	NA	All to HLW

The samples in **base case settings ver6.xls** denote two bounding waste management strategies. Of course, the user can define whatever strategy she wants.

- Segregated waste streams waste is segregated into several streams with the intention that many would not be classified as HLW. See Table 4-13, 4-14, and 4-15.
- All to HLW other than volatile species, all waste goes into a single waste form that would be HLW.

Table 4-13. Illustrative UREX+1 Separation Efficiency Matrix

	Pu Np Am Cm									
	Recycle	RU	I	Gas	Tc	Cs Sr	LnFP	Discard	UDS	Zr SS
	Stream	Stream	Stream	Stream	Stream	Stream	Stream	Stream	Stream	Stream
Ra to							100		m, te	
Pa									rea ma	S
U		99.9					0.1		s st ılti	ΜC
Np	99.9						0.1		this or u	via co-flows
Pu	99.9						0.1		th e f	00 1
Am	99.9						0.1		goes with this stream, Tc waste for ultimate nyway	
Cm-	99.9						0.1	p	c goes w Tc was anyway	Not used, accounted for
Cf								ıse		ise ed i
Н3				99.9			0.1	Not used	of the To with the disposal	Not used, counted fo
C14							100	Ž	the ith spo	Ž O
Kr				99.9			0.1		of d w dis	
Sr, Cs						99.9	0.1		5% dec	ass
Tc					99.9		0.1		l, 2. clu	m r
I			99.9				0.1		sed s in	such mass
FP							100		Not used, 25% of the Tc but is included with the disposal a	S
otherr									Nc bu	

 $RU = recovered \ uranium, \ FP = fission \ product, \ Ln = lanthanides, \ UDS = undissolved \ solids.$

Sum of numbers in each row must equal to 100.

The separation efficiency matrix does not address cladding isotopes, e.g., steel

Table 4-14. Illustrative Separation Efficiency for U+UPu+NpPuAm+CsSr+I+Tc Separation of UOX

		110011000			<i>J</i> 101 0				Сорыни		
	RU										
	Pu Np	Pu Np									
	Am Cm	Am Cm									
	Recycle	Recycle	RU	I	ora c	Tc	Cs Sr	Lnfn	Discard	UDS	Zr SS
		•			gas			Lnfp			
	Stream	Stream	Stream	Stream	Stream	Stream	Stream	Stream	Stream	Stream	Stream
Ra to								100		<u>.</u>	
Pa										this stream for ultimate	
U	1.3		98.6					0.1		er er	Š
	1.5	00.0	70.0							s st	MC
Np		99.9						0.1		his r	-fl
Pu	99.9							0.1		h fl fo	93
Am		99.9						0.1		goes with this stream, Tc waste for ultimate myway	ia o
Cm-		99.9						0.1	_	goes w Tc was	r v
Cf									ed,		ed,
Н3					99.9			0.1	Not used,		Not used, ounted fo
C14								100	Zo1	he' h tl	Nov Sur
Kr					99.9			0.1	_	of the T with the disposal	J
Sr,							99.9	0.1		25% of the luded with t	ss s
Cs										25°	ma
Tc						99.9		0.1		sd, incl	Not used, such mass accounted for via co-flows
I				99.9				0.1		Not used, 25% of the Tc but is included with the disposal	suc
FP								100		lot out	
otherr										Z -	

RU = recovered uranium, FP = fission product, Ln = lanthanides, UDS = undissolved solids.

Sum of numbers in each row must equal to 100.

The 1.3% U mixed with Pu produces a 50:50 UPu product

The separation efficiency matrix does not address cladding isotopes, e.g., steel

	RU Pu Np			· · · · · ·						Zr SS Stream
	Am Cm					Cs Sr				(Metal
	Recycle	RU		gas		Strea	LnFP	discard	UDS	Waste
	Stream	Stream	I Stream	Stream	Tc Stream	m	Stream	Stream	Stream	Stream)
Ra to								п		100
Pa								, io		
U	3.4	93.3			Е			te Te	я	3.3
Np	99.9		п		rea			vas n	stream	0.1
Pu	99.9		ear		st			the wastream	str	0.1
Am	99.9		m, str		ı, aste			as the waste form P stream	FP	0.1
Cm-	99.9		No iodine stream, included with CsSr stream		No Tc stream, included with metal waste stream			id ras FP	Not used, included in	0.1
Cf			e st		stre			use I fo he	ıse led	
Н3			din /ith	99.9	i Si			Not used inted for for the F	Not used, ncluded i	0.1
C14			ioo d w		No Tc with m			Not used salt accounted for a material for the FP		100
Kr			No 1de	99.9	Z \$			occo erria	ass	0.1
Sr, Cs			ոշև		iqe,	99.9		olt a nato	such mass	0.1
Tc			-::		ch			× _	ıch	100
I					.≘	99.9		Ses	S	0.1
FP							50	Process		50
other								F		

Table 4-15. Illustrative Electrochemical Separation Efficiency of FR Metal Fuel

RU = recovered uranium, FP = fission product, Ln = lanthanides, UDS = undissolved solids. Sum of numbers in each row must equal to 100.

4.6 Fuel Fabrication (PURPLE) Worksheets

The set of fuel fabrication worksheets is simpler than reactors or separations, primarily because of the 1:1: correspondence between fuel fabrication and fuel type, i.e., there is one fuel fabrication type dedicated to each fuel type. There are other simplifying factors. There is no fuel fab facility rampup specification. The routing coming into fuel fabrication is a "push" time from separations, whereas the routing from reactors into separations is a "pull" type. And, the transformation in fuel fabrication facilities is effectively to blend recycled TRU (if any) with a uranium stream. Because of the 1:1 correspondence, those composition requirements are set via fuel recipes, not on fuel fab worksheets.

Thus, there is a single type of fuel fabrication worksheet, **Fuel Fab 1 through 10**, which defines several parameters for that separation type, including capacity and which separation efficiency matrix is to be used, by year. Table 4-16 shows how fuel fabrication capacities and transformation performance are set.

Table 4-16. Fabrication Facility Capacities and Transformation Performance in VISION

Capacity	Transformation Performance
Fuel Fab Order switch in Integer 1	Blending - Fuel is made according to the compositions
among	according to the selection of fuel recipes available in
0. Let VISION optimize fuel fab	vision recipes ver5.xls by fuel number in the Reactor
capacity.	Fuel Types worksheet.
1. Force VISION to build specific fuel	
fab capacity each year, the capacity is	Each fuel fab type has two types of source material,
set on the Fuel Fab worksheets.	recycled and uranium. The only available recycled
	material is what is in the separation-to-fuel-fab buffer,
	which is controlled by Separation Stream Splits .
	Uranium is used according to uranium priority set with the
	fuel recipes, e.g., whether to use enriched uranium (EU) or
	recovered uranium (RU).

The separation efficiency matrix does not address cladding isotopes, e.g., steel and Zr.

4.6.1 Fuel Fabrication (PURPLE) - Fuel Fab 1 through Fuel Fab 10

Table 4-17 lists the parameters set on the **Fuel Fab** worksheets, one for each separation type. Most of the parameters are straightforward and generally similar to analogous settings in the **Separations** worksheets.

Table 4-17. Parameters Set on Fuel Fab Worksheets

Parameter	Units or Allowed Variables	Impact	Recommended Values
Fuel Fab construction time	≥0.25 years (≥ time step)	Sets delay for construction of fabrication facilities , does not impact fuel flows.	2 years
Fuel Fab lifetime	≥0.25 years (≥ time step)	Determines lifetime of fuel fab facilities, does not impact fuel flows.	60 years
Fuel Fab license time	≥0.25 years (≥ time step)	Sets delay for facility licensing	1 year
Enrichment time	≥0.25 years (≥ time step)	Determines the delay for the enrichment process. Individual enrichment plant types are not tracked.	1 year
Used fuel wet storage time	1 to 10 years (integer values only) (≥ time step)	Determines the minimum time used fuel must stay at the reactor before going anywhere else.	Before on-site separation - 1 year Before off-site separation - 10 year
Used fuel dry storage time	1 to 5 years (integer values only) (≥ time step)	Has no effect on when fuel can move to repository or separation facilities, which are controlled by their processing rates. Determines how long fuel must wait in dry storage before going to an MRS (if there is one).	1 year
Unlimited fuel fabrication capacity for LWR	>0 kilotonne/yr (not zero)	This allows the user to set a number such that the Fuel Fab Facilities will be able to produce as much fuel as is necessary. The associated "logical" switch must be set to use unlimited fuel fabrication.	1000 kt/year
Base case fuel fabrication facility size	> 0 kilotonnes/year (not zero)	Determines the unit size of these facilities. Only integer number of these facilities can be built. If allowed by user input settings, VISION will calculate the number of required facilities and round up.	Depends on your scenario
Capacity for that fuel fabrication facility type by year (200 rows)	0 to 1000 Kilotonnes/ calendar year	Determines the capacity each year if Fuel Fab Order switch in Integer 1 = 1, otherwise no impact.	
Base case fuel fabrication capacity factor (200 rows)	0.00 to 1.00 FPY/calendar year	Determines the fraction of time during a year that fuel fabrication facilities generate 100% of their rated capacity	1.0 FPY/CY

4.7 Waste Management (BRIGHT BLUE) Worksheets

The final set of worksheets primarily address waste management. This includes Other Facilities. The mass of waste is defined by the flow through separations and the separation efficiency matrices selected on the **Separation** worksheets and defined on the **Separation Stream Splits** worksheets. Waste (kilotonnes) times the waste loading provides the mass of waste forms (kilotones). The waste form mass times the waste form density provides the waste form volume. The waste loadings (kilotonne-waste/kilotone-wasteform) and waste form density (kilotone-wasteform/m3-wasteform) are input on the **Waste Form and Mass Loading** worksheet. Unprocessed used fuel mass is converted to wasteform volume by the parameters on the **LSF & SF Waste** worksheet. The **Waste Disposition** worksheet provides the parameters that determine the type of disposition facility that each waste stream goes to - (1) decay storage, (2) LLW ABC Class waste, (3) LLW GTCC waste, (4) HLW, (5) HLW, and (6) not waste. The **Repository Holding Capacity** and **Repository Flow Capacity** worksheets provide the allowable inventory and receipt rate of repositories.

4.7.1 Waste Management (BRIGHT BLUE) - Other Facilities

This worksheet accepts input for facilities not defined elsewhere, see Table 4-18.

Parameter	Units or Allowed Variables	Impact	Recommended Values				
Enrichment duration	To be deleted, parameter	To be deleted, parameter on Fuel Fabrication worksheets					
Wet storage duration	To be deleted, parameter	on Fuel Fabrication worksheets					
Dry storage duration	To be deleted, parameter	on Fuel Fabrication worksheets					
MRS duration	Integer values only		Depends on your scenario				
MRS construction time	≥0.25 years (≥ time step)	Has no effect on mass flows	Depends on your scenario				
MRS lifetime	≥0.25 years (≥ time step)		Depends on your scenario				
Repository Construction Time	≥0.25 years (≥ time step)		Depends on your scenario				
Repository Lifetime	Integer values only		Depends on your				

Table 4-18. Parameters Set on Other Facilities Worksheet

4.7.2 Waste Management (BRIGHT BLUE) - Coflows (Inactive for VISION 3.0)

This page allows the definition of 6 co-flow streams for each of the 15 separation strategies. The first five materials, ZR, SS, process discard, salts and metals 3, require the user to specify the number of kilograms of material per kilogram of fuel. The sixth material, Rags and Bags, requires the user to specify the volume (in cubic meters) per kilogram of fuel. These materials are part of the fuel cycle, but are not active parts of the fuel. They are important however for waste, storage, and economic purposes. The numbers are currently approximations and need further refining.

4.7.3 Waste Management (BRIGHT BLUE) - Waste Disposition (*Inactive for VISION 3.0*)

The "Waste Disposition" page is split up into three parts, one for each fuel type. This page specifies the waste classification for each stream from separations. The type of separations process (aqueous or

electrochemical) is set elsewhere in the base case settings file, but the user needs to have decided what separation strategy will be used for each fuel type in order to properly specify the waste classification for each stream from separations. The rows beneath each fuel type list the possible separation streams; different separation strategies and fuels will use different subsets of the streams. There are six categories listed at the bottom of the page which are as follows: 1-Decay Storage, 2-LLW ABC, 3-GTCC, 4-HLW, 5-TRUW, 6-Not Waste. Next to each option listed beneath the "Separation Stream" the user can enter numbers (1-6) corresponding to the numbers listed above. Numbers (1-5) deal with different levels of storage and disposal. Number (6) allows the user to specify what elements go through recycling.

4.7.4 Waste Management (BRIGHT BLUE) - Waste Form and Mass Loading (*Inactive for VISION 3.0*)

This page allows the user to specify mass and volume of the wasteform for each separation stream in a given fuel type. The values for wasteform loading are in the form of a mass fraction defined as mass of contaminant stream/mass of wasteform. The user is encouraged to specify a low, mid, and high waste loading (and accompanying waste density). The values for wasteform density are in the form of tonne of wasteform per cubic meter of wasteform. The color coding allows the user to see where the information was obtained from. To the far right of the users screen is a list showing the same colors and the sources associated with those colors. From the different documents, there may be ranges given with respect to the different amounts of mass contributed and so forth. The low end of the range corresponds to the "low" in the Excel file. The same goes for the "Med" and "High".

4.7.5 Waste Management (BRIGHT BLUE) - Worksheet for LSF & SF Waste (*Inactive for VISION 3.0*)

This page allows the user to set the cask mass loading (kilotonnes of casked fuel per kilotonne of fuel) and cask (with fuel) density (kilotonnes of casked fuel per cubic meter) for legacy spent fuel and spent fuel. The numbers currently in the worksheet are preliminary and should be used with caution.

4.7.6 Waste Management (BRIGHT BLUE) - MRS Flow Capacity (*Inactive for VISION 3.0*)

The user can include a monitored retrievable storage (MRS) facility in the analysis. The parameters that can be specified are

- Whether MRS is present or not.
- Dry storage time before material can be moved to the monitored retrievable storage.
- MRS capacity.

4.7.7 Waste Management (BRIGHT BLUE) - Repository Holding Capacity

The user can include a retrievable repository facility in the analysis. The retrievable repository capacity is not limited in total mass, but the rate that material can be sent to the repository is limited. The oldest (longest time out of the reactor) and then most cycled fuel has priority for entering the repository.

The user can include a permanent repository facility. The user can specify a limit on the permanent repository in terms of either legacy used fuel (pre-2000), used fuel, or both. The user specified repository receipt rate for the retrievable repository also applies to the permanent repository.

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This page allows the user to specify the total repository holding capacity (permanent and retrievable) as a function of time. This page is used when Base Case Unlimited Repository Holding Capacity Switch (on the **Logical 1** worksheet) is set to FALSE.

4.7.8 Waste Management (BRIGHT BLUE) - Repository Flow Capacity

This page allows the user to specify the total repository flow capacity as a function of time. This page is used when Base Case Unlimited Repository Flow Capacity Switch (on the **Logical 1** worksheet) is set to FALSE.

5. VISION INPUT VIA RECIPES VER1.XLS file

This file contains the following types of input information:

- Fuel recipes described below
- Fuel interpolation correlations described below
- Worksheets for a future 1-group perturbation approach (not currently used)

Each recipe data column contains the following information:

- Fuel burnup (GWth-day/tonne-iHM)
- Capacity factor (FPY/calendar years)
- Fuel residence time (calendar years)
- The input and output compositions for this primary fuel.
- Uranium priority 1 to 6 what type of uranium supply (EU, NU, DU, RU) should be used to make up the the correct amount of uranium in the fuel once the uranium in the incoming separation-to-fuel buffer is accounted for.
- The number of a contingent fuel (if any) that VISION will use in this reactor if the primary fuel cannot be made. The contingent fuel should be a uranium-based fuel.
- The mass fractions for the input fuel composition. These must sum to 1.0
- The mass fractions for the output fuel composition. These must sum to 1.0.
- 1-Group cross sections for (n,fission) not yet used
- 1-Group cross sections for (n,gamma) not yet used
- 1-Group cross sections for (n,2n) not yet used

Table 4-10 (replicated here) lists the available fuel recipes, which are found on seven worksheets in this file.

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Table 4-10. Fuel Types (replicated here)

Reactor technology	Appropriate reactor fuel numbers in vision recipe ver5.xls
LWR	33 to 100 - LWR burnup correlation
	101 to 110 - recipes in 100_UOX_Once_Thru worksheet
LWR MF (multiple fuel)	33 to 100 - LWR burnup correlation
	(Values from 2 to 100 are allowed by VISION but values from 2 to 32
	produce unreliable results in the current burnup correlation.)
	101 to 110 - recipes in 100_UOX_Once_Thru worksheet
	301 to 315 - recipes in 300_LWR_MOX worksheet
	401 to 415 - recipes in 400_LWR_IMF worksheet
HWR or VHTR	Appropriate recipes among
	201 to 210 - recipes in 200_Other_Once_Thru worksheet
HWR or VHTR possibly	Appropriate recipes among
using recycled material	201 to 210 - recipes in 200_Other_Once_Thru worksheet
	501 to 510 - recipes in 500_Other_Thermal_Recycle worksheet
	Currently all the 500 recipe slots are blank.
Fast burner reactor, sodium	-1.00 to 0.00 - fast reactor oxide TRU CR correlation
cooled	0.00 to 1.00 - fast reactor metal TRU CR correlation
	(Values from -2.00 to 0.00 and 0.00 to 2.00 are allowed by VISION but
	values below -1 and above +1 produce unreliable results in the current
	TRU CR correlations.)
	Appropriate recipes among
	601 to 630 - recipes in 600_Metal_Cooled_FR worksheet
Fast breeder reactor,	Appropriate recipes among
sodium cooled	601 to 630 - recipes in 600_Metal_Cooled_FR worksheet
Fast reactors with other	701 to 710 - recipes in 700_Other_Cooled_FR worksheet
coolants	Currently all the 700 recipe slots are blank.

Cautions:

17. Do not reorder or change the list of isotopes on each worksheet; all must be the same.



18. Changing any of the pre-defined recipes will invalidate case cases that use them.

5.1 List of Recipes Worksheet

This worksheet page simply lists the recipes that have been entered on the seven pages of recipes. **Base case settings ver6.xls** reads this page.

5.2 User Help Worksheet

This worksheet page is not used by any other file or worksheet. It is simply an aid to the user. Recall that the recipe pages require the following data:

- Fuel burnup (GWth-day/tonne-iHM)
- Capacity factor (FPY/calendar years)
- Fuel residence time (calendar years)

And, the base case settings ver6.xls file will have a thermal efficiency (GWe/GWth). The user may not have these parameters and may instead have fueling rate or electricity generation rate or # of refueling batches. This page guides the user to calculate the required values from other combinations of parameters.

5.3 100 - LWR Once Through Recipes

This page contains the UOX fuel recipes. Recall that as an alternative to selecting one of there recipes, the user can input a value from 33 to 100, which VISION will interpret as a value for LWR UOX burnup and use the LWR burnup correlation (Interpolation LWR BU worksheet) instead of one of these recipes.

Recipe 101 is a special case as it uses the LWR burnup correlation (recipe 101) in a different way. In these cases, the user must specify the burnup in cell N5. If you want to use the LWR burnup or TRU CR correlations by year, use 33 to 100 (LWR burnup correlation). Recipe 101 can be used, for example, to create a series of user defined recipes for particular purposes. For example, recipes 106 and 107 were created from recipe 101 by inputting the appropriate pre-2000 burnup value for legacy fuel, then copying and pasting into those columns. Thus, recipes 106 and 107 approximate the average composition of fuel 0-10 and 11-40 years old in 2000. Having these recipes allows the user to then define in the **Wet and Dry Storage** worksheet the appropriate composition.

Similarly, one would want to create a new 100-series recipe if you wanted a contingent fuel to be 45 GWth-day/tonne burnup instead of 51, which is recipe 103.

Recipes for 33 and 51 GWth-day/tonne-iHM UOX come from [Stillman2004]. The LWR burnup correlation comes from [Yacout2008], so that the recipes for wet and dry storage are derived from that correlation.

The "Depleted U Composition" column is used to calculate the depleted U and should not be changed.

5.4 200 - Other Once Thru Recipes

This worksheet contains recipes for other thermal reactors using once-through or all-uranium fuel.

5.5 300 - MOX Recipes

This worksheet page contains the MOX recipes. VISION is structured to allow up to 5 recycle passes. Therefore, all recycle fuels (300s, 400s, 500s, 600s, 700s) are structured to have 5 columns of data. If one has data for only a single recycle pass, those data must be in the column for pass 1, the other four columns left blank.

It is important to remember that VISION tracks core-averaged compositions. So, a strategy in which a mixture of MOX pins and UOX pins are used requires a single recipe that averages over the sets of pins.

Similarly, a complex blending of multiple fuel sources is invisible to VISION, the core-averaged recipe must be input. This is the strategy used in the multi-recycle recipes on this worksheet.[Youinou2009]

5.6 400 - IMF Recipes

This worksheet page contains the IMF recipes. VISION is structured to allow up to 5 recycle passes. Therefore, all recycle fuels (300s, 400s, 500s, 600s, 700s) are structured to have 5 columns of data. If one has data for only a single recycle pass, those data must be in the column for pass 1, the other four columns left blank.

It is important to remember that VISION tracks core-averaged compositions. So, a strategy in which a mixture of IMF pins and UOX pins are used requires a single recipe that averages over the sets of pins. This is what is used in the multi-recycle recipes on this worksheet.[Pope2009]

5.7 500 - Other Thermal Recycle Recipes

This worksheet page is reserved for recycle fuels other than MOX or IMF. There is one draft recipe for the DUPIC fuel composition (direct use of uranium and plutonium in CANDUs).

5.8 600 - Metal-Cooled Fast Reactor Recipes

This page contains the fast reactor fuel recipes. Recall that as an alternative to selecting one of there recipes, the user can input a value from 0.00 to 1.00, which VISION will interpret as a value of fast reactor TRU conversion ratio. If positive, metal-fueled metal-cooled. If negative, oxide-fueled, metal-cooled. The FR TRU CR correlations are on **Interpolation FR-metal CR** and **Interpolation FR-oxide** CR worksheets. The burner fast reactor data come from [Hoffman2006, Hoffman2007]. The correlation approach is described in [Yacout2008].

VISION is structured to allow up to 5 recycle passes. Therefore, all recycle fuels (300s, 400s, 500s, 600s, 700s) are structured to have 5 columns of data. If one has data for only a single recycle pass, those data must be in the column for pass 1, the other four columns left blank. Currently in the AFCI program, we have only recipes for the first (startup) and equilibrium recycle pass, in which case the startup composition is entered into recycle pass 1 and the equilibrium composition is entered into recycle pass 5.

Recipes 601 and 602 are special cases as they use the FR TRU CR correlations. In these cases, the user must specify the burnup in cell E2 (metal) or K2 (oxide).

5.9 700 - Other-Cooled Fast Reactor Recipes

This worksheet page is reserved for fast reactor recipes other than metal-cooled. It is currently blank but you can input recipes if you wish.

5.10 Other Worksheets

The other worksheets in this file should not be changed by the user.

5.10.1 Interpolation Burnup Worksheet

This worksheet shows how a burnup of 51 can then be changed to anything else specified by the user and have the correct recipes produced for the different burnups.[Yacout2008]

Caution: Nothing on this page should be changed by the user.

5.10.2 Interpolation FR-metal CR Worksheet

This worksheet contains correlations for modifying recipes as a function of TRU conversion ratio. The methodology is described in [Yacout2008] but those correlations have been updated by extracting more details from [Hoffman2007] for isotopes that are tracked by VISION 3.0 that were not tracked by VISION 2.2.

Caution: Nothing on this page should be changed by the user.

5.10.3 Interpolation FR-oxide CR Worksheet

This worksheet contains correlations for modifying recipes as a function of TRU conversion ratio. The methodology is described in [Yacout2008] but those correlations have been updated by extracting more details from [Hoffman2007] for isotopes that are tracked by VISION 3.0 that were not tracked by VISION 2.2.

Caution: Nothing on this page should be changed by the user.

5.10.4 Worksheets Named Yellow, Blue, Green, Nu, VISION k-infinity

These worksheets are for a new submodel in VISION, which is not yet operational.

6. VISION OUTPUTS

There are two types of output files, those that contain data dumps directly from the VISION Powersim model and those intended to organize and graph those data for user analysis.

The Powersim portion of VISION will store data for up to five runs in the Excel file **output data-1.xls**, which is typically at least 5 MB. The user can directly access and analyze those data. However, **output data-1.xls** will have a varying number of columns of data as the number of reactor types, fuel types, and separation types varies. And, if you leave your data in **output data-1.xls**, the next time you run VISION, Powersim will overwrite whatever is in **output data-1.xls**.

Instead, we recommend a two-step process that will provide the user with various graphs and a macro to help you produce other graphs of the data. The first step uses **output data-2.xls**, which copies data from **output data-1.xls** and puts it into a standard format of 10 reactors types, 10 separation types, and 10 fuel types - many of which will be blank. This allows other graphing files to reliably link to **output data-2**; several such files are described in following subsections.

output checks.xls - helps the user perform some checks of the output data output reactors.xls - graphs reactor and electricity generated information output fuel masses by class.xls - graphs fuel masses by class, e.g., mass of TRU or U output fuel masses.xls - graphs fuel masses (summed over all classes) output separations.xls - graphs separation information output waste.xls - not included with VISION 3.0

Cautions:

- 19. The **output data-2.xls** expects **output data-1.xls** to be in the same folder. If it is not, the macro in **output data-2.xls** that copies data from **output data-1.xls** will not function.
- 20. Data are not transferred automatically from **output data-1.xls** to **output data- 2.xls**, you must either run the macro in output data-2.xls or copy data manually.
- 21. The other output files expect **output data-2.xIs** and **base case settings ver6.xIs** to be in the same folder. If not, you will have to update the "link" from those file to the output file in question. And, the Graph Builder macro in the other output files will not function.
- 22. The macros in the output files will work faster if the files are not "minimized" in Windows.
- 23. Data are generally automatically transferred from output data-2 to other output files. Due to quirks in Excel, sometimes you have to manually update links. Go to "Edit" then "Links" and manually update the links.
- 24. After running up to five cases, the user should make a copy of **base case settings ver6.xls**, **output data-2**, and other output file of interest.
- 25. Until you have saved the files and broken links, all Excel files must remain in Office2003 format (extension xls); they cannot be Office2007 format (extension xlsx).



6.1 Output Data-1.xls

The vision model dumps directly to this file for up to five runs which corresponds to the tabs. The tabs will be numbered according to which runs they correspond with. This information will be used in the savable output files.

This file is not intended for direct user use, nonetheless, the user may find need to go to the raw data and hence this guide will provide an overview of the file and how it is organized.

The worksheets all have names of the form XXXX-n, where n is the number of the run from 1 to 5. All "1" worksheets appear before all "2" worksheets, etc. The order of the set of "n" worksheets is kept the same. The top two or three rows of each worksheet may have labels indicating the variable name in VISION and the unit. All other rows proceed from 1/1/2000 to 1/1/2100, showing yearly data.

Note that some cells do not contain data, only #Num!, which means that the Powersim model is not currently dumping appropriate data to those cells. This generally denotes an obsolete part of validationdata, which are no longer used but not removed because it would change the order of columns.

Each worksheet in **output data-1.xls** corresponds to a particular page in the Powersim model to make it easier to trace backward. The worksheets in **output data-1.xls** are as follows:

- US Reactor Park- contains the number (not capacity and not electricity generated) of reactors that are legacy reactors, legacy reactors near retirement, legacy reactor near shutdown, retired legacy reactors, reactors during licensing license, reactors during construction, reactors during contruction needing fuel, ready reactors, fresh reactors, reactors near retirement, reactors near shutdown, retired reactors, and operating reactors. Each of those parameters is divided by reactor type. It also contains the total number of operating reactors, summed over all reactor types, the capacity (by reactor type), and the total capacity.
- **Fuel Cycle** contains several mass flow parameters, notably the mined ore, accumulated depleted uranium, and how much fuel is in enrichment, fuel fabrication, ready fuel, reactors, wet storage, dry storage, MRS.
- **Separations Facilities** contains the number of separation facilities at the stages of design and license, construction, ready to operate, working (operating), new retirement, or retirement. Each stage has as many columns as there are separation facility types.
- Fuel fabrication Facilities contains the number of fuel fabrication facilities at the stages of design and license, construction, ready to operate, working (operating), new retirement, or retirement. Each stage has as many columns as there are fuel fabrication facility types.
- Mass Calcs contains the mass of fuel by chemical element by stage of the fuel cycle (fuel fabrication, ready fuel, fuel in reactors, wet storage, dry storage, MRS, retrievable repository, permanent repository). Each has as many columns as there are fuel types.
- U ore inventory contains (by fuel type) the consumed U ore and consumed U.
- Enrichment Capacity contains the cumulative SWUs (by fuel type) and total SWUs.
- **Repository** contains the mass of fuel (by fuel type) in permanent and retrievable repository.
- Fuel Makeup from Separations contains information on the mass of material in the buffers between separations and fuel fabrication.

• Future Demand - contains information on total and nuclear electricity predictions.

6.2 Output Data-2.xls

Start on the **START HERE** worksheet, which will guide you through use of this spreadsheet file. This spreadsheet translates the raw VISION output file (**output data-1.xls**) into a common format with 10 reactor types, 10 separation types, and 10 fuel types. It reads and copies from **output data-1.xls** and pastes information into itself. Therefore **output data-2.xls** does not have an automatic link back to **output data-1.xls**.

First, open the input (base case settings ver6.xls) and output (output data-1.xls) files, or whatever you may have renamed them. The macros in output data-2.xls will not work unless those two files are open.

Second, if appropriate, clear the data in **output data-2.xls**. There are buttons to clear a specific run or clear all runs. Remember, data cleared are data gone! You do not have to clear previous data to bring in replacement data from **output data-1.xls**; however, we recommend doing so because your new data may have fewer numbers of reactors, fuels, and separation types. Note that the "clear run" feature allows you to run various simulations and decide to keep only some of the runs, clearing the other ones.

Third, set the input and output file names for the macros to use. The files must be in the same folder as **output data-2.xls** and must include the extension .xls. The defaults names are **base case settings ver6.xls** and **output data-1.xls**.

Fourth, load data from the input and output files. There are buttons to load a specific run or all the runs. Note that the "load run" feature allows you to replace just one of the runs you've previously calculated with a new data set. It is not possible to load new run X, however, into anything other than run X.

Fifth, open the graphic output files of interest.

Cautions:

26. Do not alter the worksheets in any way - names, order, format, etc.



6.3 Output Files with Graphs

Other than **output data-1.xls** and **output data-2.xls**, all output files have the same format and same macros.

All require **output data-2.xls** and **base case settings ver6.xls** to be properly populated. You can have the output files read some a file with a name different that **output data-2.xls** but its format must be the same. If you chose to read from a differently named file you have to correct the connections from output data-2.xls to that output file, which means editing the links from **output data-2.xls** and **base case settings ver6.xls** by going to "Edit" on the Excel menu, then "Links".

All output files have multiple worksheets.

- START HERE guides you through that output file.
- **By run** a worksheet that sums all of the parameters in question over reactor types, fuel types, separation types, whatever is appropriate
- Parameter Run1 through Run5 worksheets with more detail, one for each simulation run.
- Other worksheets going into yet more detail if appropriate.

Each output file has several pre-defined graphs. For each type of graph, there is one pre-set for a 100-year simulation and one pre-set for a 200-year simulation.

There are two macros in each output file, accessible via buttons or by "control" shortcuts.

- Graph Viewer (control-shift-E) allows you to view thumbnails of all graphs in that currently active worksheet, in sets of 9. Click of a thumbnail to go directly to it. Once there you can view it or alter it as with any Excel graph.
- Graph Builder (control U) guides you through the process of making a new graph from data in output data-2.xls. You can, of course, make graphs manually if you are adequately familiar with Excel graphs and linking data between Excel files.

6.3.1 Output_Checks

If the file does not open in the **START HERE** worksheet, please go to it. "**START HERE**" is the left most worksheet. This file helps the answer the following questions:

- Are the names you gave to each run what you intended?
- Are the runs that actually ran what you intended?
- Is the Reactor Order Case what you intended?
- Is the Separation Order Case what you intended?
- Does the sum of disposition paths for each isotope in each of the Separation Efficiency Matrices = 100%?
- Did you tell VISION to create enough legacy reactors to generate the nuclear electricity you wanted at the start of the simulation?
- Did you tell VISION to retire all the legacy reactors you created?
- Is the nuclear electricity that VISION calculated sufficiently close to what you intended?
- Is the number of "ready reactors" acceptable throughout the simulation?

6.3.2 Output_Reactors

If the file does not open in the **START HERE** worksheet, please go to it. "**START HERE**" is the left most worksheet. Verify the labels for reactor types. The spreadsheet is designed so that reactor types with a non-blank name will show data.

The worksheets in this file graph electricity generated per year (GWe-FPY/CY), operating capacity (GWe), capacity added each year (GWe/calendar year), capacity retired each year (GWe/calendar year). The first data worksheet has these data for all reactors for each run. The next five worksheets have these data by reactor type for each run.

There is also a ungraphed set of calculations that perform a "balance" check on the reactor capacity of each reactor type for each run. After the first year, the delta in capacity (new year - last year) should equal the capacity addition minus the capacity retired.

6.3.3 Output_Separations

If the file does not open in the **START HERE** worksheet, please go to it. "**START HERE**" is the left most worksheet.

This file pulls the data for the following parameters:

Separation capacity (tonnes/CY) requested by the user

Separation capacity (tonnes/CY) actually built

Separation flow (tonnes/CY) into separations from used fuel

Separation flow (tonnes/CY) from separations into buffer boxes

6.3.4 Output_Fuel_Masses

If the file does not open in the **START HERE** worksheet, please go to it. "**START HERE**" is the left most worksheet.

This worksheet examines the mass and flow of fuel throughout the system. This worksheet does not differentiate by chemical element or isotope.

There are three sets of worksheets.

- o By run (all fuels) total mass of fuel (all locations) for each run.
- o By fuel (all loc) runs 1 through 5 mass of fuel (all locations) by fuel type for each run.
- O By loc by fuel runs 1 through 5 mass of fuel, by location, by fuel type, for each run.

Even the last five worksheets group certain locations together to enable the graphs to be readable. The grouping is as follows:

- Uranium location = uranium conversion + uranium enrichment
- Fab location = fuel fabrication + ready fuel
- Reactor location = fuel in reactors
- Storage location = wet storage + dry storage + MRS
- Separations = separations processes + buffer between separations and fuel fabrication
- Repository = retrievable repository + permanent repository

The more detailed location breakdown can be found directly in **output data-1.xls** or **output data-2.xls**.

The last five worksheets also provide (ungraphed) the rate of reactor fuel input and reactor fuel output, by fuel type (not by reactor type).

6.3.5 Output Fuel Masses By Class

If the file does not open in the **START HERE** worksheet, please go to it. "**START HERE**" is the left most worksheet. The worksheet is similar to "Fuel Masses" with two key differences. It provides more detailed information in that the total mass is divided into uranium, individual TRU elements, and sum of fission products.

Similar to Fuel Masses, there are three sets of worksheets.

- o By run (all fuels) total mass of fuel (all locations) for each run.
- o By fuel (all loc) runs 1 through 5 mass of fuel (all locations) by fuel type for each run.
- o By loc by fuel runs 1 through 5 mass of fuel, by location, by fuel type, for each run.

Even the last five worksheets group certain locations together to enable the graphs to be readable. The grouping is as follows:

- Depleted uranium
- Uranium location = uranium conversion + uranium enrichment
- o Fab location = fuel fabrication + ready fuel
- Reactor location = fuel in reactors
- Storage location = wet storage + dry storage + MRS
- O Separations = separations processes + buffer between separations and fuel fabrication
- Repository = retrievable repository + permanent repository

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Appendix A Pre-Defined Base Cases

This appendix describes the pre-defined base cases, which have three purposes. First, we originally developed most of these cases for the Scenario Definition, Evaluation, and Trade-offs (SETS) study.[Piet2006] They therefore provide some of the benchmarking used upon subsequent model upgrades. Section A-3.7 describes newer benchmark cases. Second, user study of the base cases can help understand how to use VISION to model various types of situations. Third, running the pre-defined base cases can help the user understand fuel cycle system dynamics in general and VISION in particular.

A-1. Phases

In previous versions of VISION and its predecessor model, DYMOND, there were three phrases associated with reactor technology development and deployment. All of the SETS base cases have that structure. Separation and waste management technology is held constant but reactor technology can change twice: phase 0 is the initial condition and lasts until the beginning of phase 1, and phases 1 and 2 are the second and third time periods.

Phase 0 is the initial time period; this phase starts in 2000 and always uses light water reactors without recycle, reflecting the current U.S. reactor fleet. The end of this phase is set by the start time for Phase 1. Under default conditions, the initial U.S. fleet in 2000 is assumed to have 103 light water reactors, of these, 86 reactors are assumed to be capable of only utilizing UOX fuel and are designated as LWRs in the model, while the remaining 17 reactors are assumed to be capable of utilizing UOX or MF fuel and are designated as LWR-MF.

Phase 1 is the second time period; this phase starts between 2000 and 2100 as defined in the different base cases. The value in the SETS base cases was either 2020 or 2025. Phase 1 continues until the start of Phase 2 (the start of Phase 2 is defined by the user in manual mode by the slider bar). Phase 1 is and should be earlier than Phase 2.

Phase 2 is the last time period; this phase starts between 2000 and 2100, it was 2040 in the SETS base cases. The end of Phase 1 is specified by the start time for Phase 2. Phase 1 always precedes Phase 2.

A-2. Fuel and Reactor Types

This subsection describes the different reactor and fuel types in the SETS base cases.

Many of the fuels which are listed below have specific transuranics listed such as Pu, Np, Am, or Cm. When these are included with the fuel type, only the transuranics specified are used within that fuel recipe. Each fuel recipe is very specific. This allows the user to track the use of the different transuranic elements.

A-2.1 Once Thru - No Recycle

This is uranium oxide (UOX) fuel that can be utilized in an LWR or LWR-MF reactors; there is no recycle material included. Selecting this option continues the fuel type from Phase 0. This fuel requires thermal reactors for utilization; later in the set-up the relative proportion of LWR to LWR-MF reactors used can be varied. UOX is the only fuel that can be used by the LWRs.

A-2.2 MOX-NpPu

Note: originally we referred to this option as MOX-PuNp but later changed terminology so that the list of transuranic elements is always in Periodic Table order. This fuel is mixed oxide (MOX) fuel made with Np, Pu, and recovered U (uranium that has been through a reactor as fuel) that can be utilized by LWR-MF reactors; recycling of fuel must be present for MOX to be produced. The MOX-NpPu recipe is a full

core MOX or homogenous fuel assembly; it is intended to fill the entire core. The program is set-up to make as much MOX fuel as is requested and available; fuel requested but not available is made up by UOX fuel. This fuel requires LWR MF thermal reactors for utilization; later in the set-up the relative proportion of LWR to LWR MF reactors used can be varied. This base case uses the older MOX-NpPu recipe, which was for a single recycle. The **vision recipe ver5.xls file** now also contains a multi-recycle MOX-NpPu option.[Youinou2009]

A-2.3 MOX-NpPuAm

Note: originally we referred to this option as MOX-PuNpAm but later changed terminology so that the list of transuranic elements is always in Periodic Table order. This is mixed oxide (MOX) fuel made with Pu, Np, Am, and burned U (uranium that has been through a reactor as fuel) that can be utilized by LWR MF reactors; recycling of fuel (set later) must be present for MOX to be produced. The MOX PuNpAm recipe is a full core MOX; it is intended to fill the entire core. The program is set-up to make as much MOX fuel as is requested and available (this program carries an isotopic mass balance and uses the sum of elemental Pu as the determiner for the availability of MOX); fuel requested but not available is made up by UOX fuel. This fuel requires LWR-MF thermal reactors for utilization; later in the set-up the relative proportion of LWR to LWR-MF reactors used can be varied. MOX-NpPuAm fuel is user specified to have 1-5 passes (recycles). The original base case used older multi-recycle data for MOX-NpPuAm, which has been upgraded to higher quality data.[Youinou2009]

A-2.4 IMF NpPu

This is inert matrix fuel (IMF) made with Np and Pu and can be utilized by LWR MF reactors; recycling of fuel must be present for IMF to be produced. The IMF-NpPu recipe is a full core IMF; it is intended to fill the entire core. The program is set-up to make as much IMF fuel as is requested and available (this program carries an isotopic mass balance and uses the sum of elemental Pu as the determiner for the availability of IMF); fuel requested but not available is made up by UOX fuel. This fuel requires LWR MF thermal reactors for utilization; later in the set-up the relative proportion of LWR to LWR MF reactors used can be varied. This base case uses the older IMF-NpPu recipe, which was for a single recycle. The **vision recipe ver5.xls file** now also contains a multi-recycle IMF-NpPu option.[Pope2009]

A-2.5 IMF-NpPuAm

This is inert matrix fuel (IMF) made with Np, Pu,, Am, and depleted uranium (DU) and can be utilized by LWR MF reactors. Recycling of fuel must be present for IMF to be produced. The IMF-NpPuAm recipe is a blended core IMF, this means that in a single fuel assembly some of the pins will contain IMF and some will contain UOX made with DU. The program is set-up to make as much IMF fuel as is requested and available (this program carries an isotopic mass balance and uses the sum of elemental Pu as the determiner for the availability of IMF); fuel requested but not available is made up by UOX fuel. This fuel requires LWR MF thermal reactors for utilization; later in the set-up the relative proportion of LWR to LWR MF reactors used can be varied. IMF PuNpAm is user specified to have 1-5 passes (recycles). The original base case used older multi-recycle data for IMF-NpPuAm, which has been upgraded to higher quality data.[Pope2009]

A-2.6 IMF-PuNpAmCm

This is inert matrix fuel (IMF) made with Np, Pu, Am, and Cm can be utilized by LWR MF reactors. Recycling of fuel must be present for IMF to be produced. The IMF-NpPuAmCm recipe is a full core IMF; it is intended to fill the entire core. The program is set-up to make as much IMF fuel as is requested and available (this program carries an isotopic mass balance and uses the sum of elemental Pu as the

determiner for the availability of IMF); fuel requested but not available is made up by UOX fuel. This fuel requires LWR MF thermal reactors for utilization; later in the set-up the relative proportion of LWR to LWR MF reactors used can be varied. This base case uses the older IMF-NpPuAmCm recipe, which was for a single recycle and stopped at Cm246. The **vision recipe ver5.xls file** now also contains a multi-recycle IMF-TRU option, which covers the entire range of TRU elements Np, Pu, Am, Cm, Bk Cf.[Pope2009]

A-2.7 FR-Burner

This selects **burner fast reactors**, designated as FBR (the "B" stands for either breeder or burner) in the model. Recycling of fuel must be present for fast reactors to operate. Burner fast reactors are net consumers of transuranics. Later in the set-up the relative proportion of LWR, LWR MF, and FBR reactors used can be varied. New fast reactors are not brought online unless there is sufficient fast reactor fuel available (based on Pu). Thermal reactors, LWR MF, are brought online to replace the capacity of fast reactors that cannot be brought online due to insufficient fuel. The LWRmf reactors use MOX or IMF fuel if that is part of the scenario; otherwise they use UOX if no thermal recycling is included in the scenario. The fast reactor is user specified to have 1-5 passes (recycles). The original base case used older multi-recycle data for CR=0.25 metal fuel fast reactors, whereas these data have been retained for this base case, higher quality data for a range of CR is now available.[Hoffman2006, Hoffman2007]

A-2.8 FR-Breeder

This selects **breeder fast reactors**, designated as FBR (the "B" stands for either breeder or burner) in the model. Recycling of fuel must be present for fast reactors to operate. Breeder fast reactors are net producers of transuranics. Later in the set-up the relative proportion of LWR, LWR MF, and FBR reactors used can be varied. New fast reactors are not brought online unless there is sufficient fast reactor fuel available (based on Pu). Thermal reactors, LWR MF, are brought online to replace the capacity of fast reactors that cannot be brought online due to insufficient fuel. The LWR MF reactors use MOX or IMF fuel if that is part of the scenario; otherwise they use UOX if no thermal recycling is included in the scenario. The fast reactor is user specified to have 1-5 passes (recycles). The original base case used older multi-recycle data for CR=1.07 metal fuel fast reactors, whereas these data have been retained for this base case, higher quality data for a range of CR is now available.[Hoffman, in publication]

A-3. Phase 1 - Phase 2 Box

Within the "phase 1 phase 2" box, is listed the entire selection of base cases from which the user may choose. At the end of the list are "User Defined" base cases which can be set by the user. In order to run one of the base cases, click the base case you want to run and hit the play button on the tool bar. All of the base cases listed before the "1-tier" cases start phase 1 in 2025 and phase 2 in 2040.

These descriptions are grouped according to what fuel/reactor is chosen for phase 1 among the base cases. This extensive set of base cases were developed to survey the fuel cycle options in 2005-2007 studies as well as test the behavior of the model under diverse conditions. There are six groupings from the SETS report [Piet2006] discussed in sections 3.1 through 3.6, as follows:

Phase 1 = once-through, i.e., recycling is delayed to phase 2.

Phase 1 = IMF-NpPuAm, i.e., multiple passes of blended, heterogeneous core IMF is used in Phase 1

Phase 1 = MOX-NpPu, i.e., a single pass of MOX-NpPu is used in Phase 1

Phase 1 = MOX-NpPuAm, i.e., multiple passes of blended MOX is used in Phase 1

Phase 1 = FR burner with TRU conversion ratio of 0.25

Phase 1 = FR breeder with TRU conversion ratio of 1.07

The six groups include an explanation of why such a base case exists as well as the reasons for the differing phase 2 options given the same phase 1 option. Not all of the fuel types with all the different transuranic combinations are listed below.

A-3.1 Once-Through

The purpose of using UOX fuel in phase 1 is to see the affects of delaying recycling until 2040. In 2040 phase 2 begins and there are six options listed. The six options listed for phase 2 allow for further exploration within the nuclear fuel cycle.

	1.1 Phase out nuclear
1) Once-through	1.2 Continue
	1.3 Start IMF-NpPuAm (tree2 15 years later)
	1.4 Start MOX-NpPuAm (tree4 15 years later)
	1.5 Start UOX/CFR symbiosis (tree5 15 years later)
	1.6 Start BFR (tree6 15 years later)

A-3.2 IMF-NpPuAm

The purpose of using IMF-NpPuAm (which uses blended IMF/UOX cores) in phase 1 is to attempt the fastest possible reduction in LTH, LTD, and LTR using thermal reactors and UREX+ separation technology. Assumes n-pass IMF fuels and their separation are practical. This IMF approach uses blended fuel assemblies, with ¾ UOX and ¼ IMF, with the TRU in used fuel UOX and IMF in one generation making the IMF in the next generation. Other n-pass IMF approaches require analysis, including increasing the IMF/UOX ratio to further accelerate benefits or require fewer reactors to use the blend. 3 kt/yr separation plant starts in 2025. All fuel that can be made from that separation plant is assumed to be used in the growing TR fleet. The six options listed for phase 2 allow for further exploration within the nuclear fuel cycle.

	2.1 Phase out nuclear
	2.2 Phase out recycling
2) IMF-NpPuAm	2.3 Continue
Hot cell fuel fab Recycle youngest fuel first	2.4 Shift to MOX-NpPuAm
	2.5 Shift to IMF-NpPu/CFR symbiosis
	2.6 Shift to BFR, phase out TR

A-3.3 MOX-NpPu

The purpose of using MOX-NpPu in phase 1 is the fact that this option most accurately resembles the current international practice and current technology, while avoiding separation of Pu. It is restricted to 1-

recycling pass in current analyses. The six options listed for phase 2 allow for further exploration within the nuclear fuel cycle.

	3.1 Phase out nuclear
	3.2 Phase out recycling
3) MOX-NpPu (1-pass)	3.3 Continue
Least "gap" per technology maturity levels Closest to international practice Glovebox fuel fabrication	3.4 Shift to MOX-NpPuAm (n-pass)
Recycle oldest fuel first FY05 calculations: restrict to 1-pass (not	3.5 Shift to MOX-NpPu/CFR symbiosis
n-pass)	3.6 Shift to BFR, phase out TR

A-3.4 MOX-NpPuAm

The purpose of using MOX-NpPuAm in phase 1 is to attempt modest repository benefits using thermal reactors, UREX+ technology, and fuels relatively similar to current UOX and MOX-Pu.

Assumes RU is the uranium component in MOX; the Pu/U ratio increases each cycle to keep the cores critical. Other n-pass MOX approaches require analysis, including keeping the core critical by increasing the uranium enrichment instead of the Pu/U ratio. The six options listed for phase 2 allow for further exploration within the nuclear fuel cycle.

	4.1 Phase out nuclear
	4.2 Phase out recycling
4) MOX-NpPuAm	4.3 Continue
Hot cell fuel fab Recycle youngest fuel first	4.4 Shift to IMF-NpPuAm
	4.5 Shift to MOX-NpPu/CFR symbiosis
	4.6 Shift to BFR, stop building TR

A-3.5 FR Burner

The purpose of using FR burner fuel in phase 1 allows for the exploration of the different pros and cons of FR burner reactors. The early FR experience would set the stage for BFR when uranium resources warrant. Balancing all the components of this type of system is not straightforward. FR deployment is limited by the amount of Pu available for FR fuel, existing FR's have 1st priority on fuel over new FR's, if insufficient fuel is available for FR's to start, the missing capacity is met by starting thermal reactors. The six options listed for phase 2 allow for further exploration within the nuclear fuel cycle.

In DYMOND and versions of VISION prior to 2.2, it was possible to start fast reactors and then phase out fast reactors with fuel in the fast reactor loop (separation, fuel fab, reactor) moving back to LWRs. Version 2.2 did not have this capability so that options 5.2, 5.3, and 5.4 could not be simulated. Version 3.0 now allows these options and we are rebuilding those base cases.

	5.1 Phase out nuclear
	5.2 Phase out FR, keep once-thru TR
	5.3 Phase out FR, start MOX-NpPuAm
	5.3 Phase out FR, start IMF-NpPuAm
5) UOX/CFR symbiosis	5.5 Continue
i.e., deploy first FR in 2025	5.6 Shift to BFR, stop building TR

A-3.6 FR Breeder

Start breeder FR in 2025 and moves into FR, skipping recycling in TR. It aims to accommodate a hypothetical combination of limited uranium resources and high nuclear growth. It is unique among the options in that BFR uses depleted uranium.

In DYMOND and versions of VISION prior to 2.2, it was possible to start fast reactors and then phase out fast reactors with fuel in the fast reactor loop (separation, fuel fab, reactor) moving back to LWRs. Version 2.2 did not have this capability so that options 6.2, 6.3, 6.4 could not be simulated. Version 3.0 now allows these options and we are rebuilding those base cases.

	6.1 Phase out nuclear
	6.2 Phase out BFR, keep once-thru TR
	6.3 Phase out BFR, start MOX-NpPuAm
	6.4 Phase out BFR, start IMF-NpPuAm
6) Build a few BFR	6.5 Continue
	6.6 Accelerate BFR, phase out TR

A-3.7 Recent Pre-Defined Base Cases

The VISION benchmark and verification plan [Smith2007] identified 5 cases to use when testing new major releases of the model, see Table A-1. Three of those cases are among the SETS pre-defined base cases noted above. The last two use CR=0.50 fast reactors with and without a single recycle of MOX between UOX and fast reactors. We have defined five additional cases to exercise new capabilities in VISION 3.0, also in Table A-1.

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Table A-1. Benchmark Cases

Case (Reactor Specifications)	Source of Data	Why Include	Comments
1=UOX at 50 burnup	SETS report	VISION B&V	Tests front-end capabilities
1=UOX-51	[Piet2006	plan	Tests thermal recycle
2=Single-mass MOX-NpPu	VISION benchmark	[Smith2007]	
1=UOX-51	[Smith2008]	,	Tests use of EU for the blended
2=Multipass IMF-NpPuAm			heterogeneous IMF
			Tests multipass recycling in
			thermal reactors
1= UOX-50	VISION benchmark		Exercise 1-tier capabilities
3= CR=0.50 fast reactor	[Smith2008]		Exercise external Pu supply
1= UOX-50	,		Tests multi-tier dynamic
2= MOX			transition case to demonstrate
3= CR=0.50 fast reactor			most complex situation
1 LWR per reactor slot	Self-generated	Tests 10 reactor s	
1		Tests LWR BU co	orrelation
		Tests legacy react	tor retirement with 10 reactor slots
1=LWR	Modification of	Tests HWR capal	
2=HWR	INPRO GAINS		d of growth specification
	benchmark (LWR		
	and HWR business as		
	usual)		
1=LWR-UOX	Modification of	Test partial multi-	-region capability
2=LWR-MF	INPRO GAINS	Test having 4 read	ctor technologies
3=FR	benchmark (3 non-		
4=LWR-UOX	geographical regions)		
5=HWR			
6=LWR-UOX			
7=HWR			
Use all 10 slots	Self-generated	Tests 10 slots for	reactor, separation, fuels.
1 = LWR-UOX			of reactor and fuel types
2 = LWR MF		concurrently.	
3 = FR-burner-metal			atic ordering of reactors, fuels,
4 = FR-burner oxide			pacity Tests draft ORNL HWR-
5 = FR-breeder metal		DUPIC recipe	
6 = HWR-UOX (no sep)			
7 = HWR-DUPIC (new recipe)			
8 = VHTR			
9 = LWR-UOX region2 (no sep)			
10 = blank (multiregion sep)			
1=LWR UOX	Self-generated		eparation strategy
2=LWR MOX		Tests 4 phases	
3=FR			separation/fuel changes
Separation/fuel/reactor changes		Tests phase out or	f thermal recycling

A-3.7.1 One LWR per Reactor Type

This is a new case, designed to test 10 reactor slots, each has a single LWR in 2000. One LWR retires every 2 years starting in 2020, so that reactor-1 should retire first, then reactor-2, etc.

The fuels, however, differ among the 10 reactor slots, allowing test of the LWR burnup correlation feature, see Table A-2.

#	Reactor	Fuel	Fuel #	Separations	Separation #
1	LWR	UOX 51 burnup	103	None	None
2	LWR	UOX 51 burnup	51	None	None
3	LWR	UOX 50 burnup	50	None	None
4	LWR	UOX 33 burnup	102	None	None
5	LWR	UOX 33 burnup	33	None	None
6	LWR	UOX 51 burnup	103	None	None
7	LWR	UOX 51 burnup	51	None	None
8	LWR	UOX 50 burnup	50	None	None
9	LWR	UOX 33 burnup	102	None	None
10	LWR	UOX 33 burnup	33	None	None

Table A-2. Reactor, Fuel, and Separation Specifications for One LWR per Reactor Type

A-3.7.2 UOX-51 to CR=0.50 Fast Reactor

The 2007/2008 benchmark had the following basic parameters.

Table A-3. Reactor, Fuel, and Separation Specifications for Early 1-Tier Benchmark

#	Reactor	Fuel	Fuel #	Separations	Separation #
1	LWR	UOX	103	UREX+1	2
2					
3	FR	Metal CR=0.50	605	Electrochemical	21

A-3.7.3 UOX-51 to 1-pass MOX-Pu to CR=0.50 Fast Reactor

The 2007/2008 benchmark had the following basic parameters.

Table A-4. Reactor, Fuel, and Separation Specifications for early 2-Tier Benchmark

#	Reactor	Fuel	Fuel #	Separations	Separation #
1	LWR	UOX	103	UREX+3	11
2	LWR MF	MOX-NpPu	308	UREX+1	2
3	FR	Metal CR=0.50	605	Electrochemical	21

A-3.7.4 LWR and HWR Once Through

A new test case was developed from an INPRO GAINS benchmark described elsewhere. [Dixon2009] Key points of the scenario are as follows:

- Two types of reactors (LWRs and HWRs) in a once-through fuel cycle. Each 1 GWe capacity/reactor, 80% capacity factor, 33% thermal efficiency, and 40-year lifetime.
- 5000 GWe-year in 2100, 4700 for LWRs, 300 for HWRs
- Uses historic reactor capacities through 2008, then 6% HWRs thereafter
- Growth is based on fixed output at 2030, 2050, 2100 with linear growth between points. No additional growth after 2100.
- No growth after 2100.

The scenario is modeled using the third method of growth specification, namely set the target electricity production in 2100 and the percent of that target yearly from 2000 to 2100. Key specifications are in Table A-5.

	Table A-5. Reactor, F	el, and So	eparation S	pecifications 1	for LWR	and HWR	Once-Through
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#	Reactor	Fuel	Fuel #	Separations	Separation #
1	LWR	UOX (45 burnup)	108	None	None
2	HWR	Oxide (7 burnup)	203	None	None

A-3.7.5 Approximation of Three Regions

A new test case was developed from an INPRO GAINS benchmark described elsewhere.[Dixon2009] Key points of the scenario as they specified it are as follows:

- Region 1 = mature infrastructure, including recycling with fast burner reactors after 2040; 45% of historic growth, high future growth.
- Region 2 = mature infrastructure with both LWRs and HWRs, once-through fuel cycle with indefinite dry storage; 30% of historic growth moderate future growth.
- Region 3 = limited infrastructure with both LWRs and HWRs; 25% of historic growth, very high future growth.
 - o Independent case once-fuel fuel cycle, dry storage
 - Synergistic case gets fresh LWR fuel from other regions (2/3rd from Region 1, 1/3rd from Region 2), returns SNF -No conversion or enrichment capabilities

VISION 3.0 was not designed for full multi-region capability. However, it can model many dynamics of multiple regions, including the mix of reactor and fuel types and most routing among reactor fleets. There are four ways in which it cannot directly model the above specification.

First, it cannot model enrichment or uranium mining segregated by region or reactor type or fuel type. In the real world, uranium enrichment and uranium mining are international commodities and VISION merely calculates the required flows for each of the 10 reactor fleets. A user trying to directly model the above specification would have to manually add the specified mining, conversion, enrichment, and UOX fuel fabrication flows from region 3 to region 1 and region 2.

Second, it cannot directly model the above growth specification. Recall that users can specify reactor growth in three ways:

- Specify growth for the combined nuclear reactor fleets on **Growth Rate** worksheet, specify the percent of that total allocated (by year) for each of the reactor types on the **Reactor %s** worksheet.
- Specify the precise number of reactors for each reactor types, by year, on the Reactor #'s worksheet.
- Specify the year-2100 electricity generated for each reactor type on the **Reactor Facility** worksheet, then specify (by reactor type), the percent of the year-2100 value for each reactor type by year on the **Reactor Growth %** of Final worksheet.

The first method treats the entire simulation as a single "region" in the sense that there is a single nuclear energy growth specification; the third method treats each reactor type as its own "region" in the sense that it has its own energy growth specification independent of other reactor types (other regions). The INPRO GAINS specification lies between these, with reactors 1-3, 4-5, 6-7 having 3 growth specifications. This would be modeled by VISION by any of the three methods if external calculations were done to translate the specifications. This of course loses some hypothetical dynamics of multi-region scenarios in that VISION would not have reactors 1-2-3, 4-5, 6-7 interacting with regard to growth among themselves. For example, if region 1 was as specified and region 2 had LWR and FR (instead of LWR and HWR once through), then a true multi-region scenario would require algorithms for deciding FR/LWR interaction in regions 1 and 2 either independent or dependent on each other. Alternatively, if region 2 had LWR and HWR but the HWR used the DUPIC fuel option (using used LWR fuel), then there would be an intra-region interaction between HWR and LWR. In the current specification; however, there is no intra-region interaction between 4-5 and between 6-7.

Third, VISION cannot directly model the fuel routing from region 3 back to regions 1 and 2. The INPRO GAINS specification is that 2/3 goes to region 1 and 1/3 goes to region 2. This is a "push/percent" routing approach, whereas VISION uses a "pull/priority" routing from reactor to separations. For VISION 3.0 testing, we merely want to test having mass flows among reactor and separation types. Region 2 (reactors 4-5) do not make or receive fuel from region 3. Region 3 (reactors 6-7) do.

Fourth and final, VISION does not have the ability to specify legacy reactor retirement by reactor type; instead it retires reactor-1 first, then reactor-2, etc. A more exact simulation of the INPRO GAINS case would be simulated by starting before 2000 so that there were no legacy reactors.

The total fleet is assumed to start at 100 GWe-FPY/calendar year, which is assumed to be 15% of total electricity. With all initial reactors assumed to be 1 GWe capacity operating at 90% capacity factor, there must be 111 reactors in 2000, allocated as in Table A-6.

Table A-6. Reactor, Fuer, and Separation Specifications for LWK and HWK Once-Through							
#	Reactor	Assumed % in 2000	Fuel	Fuel #	Separations	Separation #	
1	LWR	$0.5 \times 45\% \times 111 \rightarrow 25$	UOX (45 burnup)	108	UREX+3	11	
2	LWR MF	$0.5 \times 45\% \times 111 \rightarrow 25$	MOX-NpPu	308	UREX+1	2	
3	FR	Zero	Metal CR=0.50	605	Electrochemical	21	
4	LWR	$0.5 \times 30\% \times 111 \rightarrow 17$	UOX (45 burnup)	108	None	None	
5	HWR	$0.5 \times 30\% \times 111 \rightarrow 17$	Oxide (7 burnup)	203	None	None	
6	LWR	$0.5 \times 25\% \times 111 \rightarrow 14$	UOX (45 burnup)	108	Back to sep-1		
7	HWR	$0.5 \times 25\% \times 111 \rightarrow 14$	Oxide (7 burnup)	203	Back to sep-1		

Table A-6 Reactor Fuel and Separation Specifications for LWR and HWR Once-Through

A-3.7.6 10 Reactor and Fuel Types

We created this test case to exercise all 10 reactor-separation-fuel-fab trains with a wide range of reactor types concurrently. It also gave us a chance to test a new (draft) fuel recipe supplied by ORNL for the DUPIC fuel cycle.

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#	Reactor	Fuel	Fuel #	Separations	Separation #
1	LWR	UOX	103	UREX+3	11
2	LWR MF	MOX-Pu	301	UREX+1	2
3	FR	Metal CR=0.50	605	Electrochemical	21
4	FR	Oxide CR=0.50	610	Electrochemical	23 (mod of 21 but send to fuel- 4 instead of 3)
5	FR	Metal CR=1.07	614	Electrochemical	24 (mod of 21 but send to fuel- 5 instead of 3)
6	HWR	Oxide	203	None	None
7	HWR	DUPIC	204	None	None
8	VHTR	Oxide	201	None	None
9	LWR	UOX	103	None	None
10	None	None	None	Into DUPIC fuel	33 (modification of 32 but send fuel to 7 instead of 3)

Table A-7. Reactor, Fuel, and Separation Specifications for LWR and HWR Once-Through

A-3.7.7 Separation Technology Change

We created this scenario to test multiple concurrent reactor/fuel/separation technology changes. There are effectively four phases:

- a once through
- b recycle used UOX via COEX, make MOX-Pu, start fast reactors
- c recycle used UOX via UREX+4, make MOX-NpPuAm, continue fast reactors
- d recycle used UOX via UREX+1, phase out thermal reactor recycling

The transition from 1 to 2 tests the change in separation technology from not recovering the so-called minor actinides (Np, Am, Cm, Bk, Cf) to recovering them. We modeled this by changing from COEX (separation matrix 16) to UREX+4 (separation matrix 11) for the separation-1 type. Note that the specifications for reactor-2/fuel-2 do change (deliberately) in this example from early/middle from MOX-Pu (fed by COEX) to MOX-NpPuAm (fed by UREX+4).

The third phase tests phase out of thermal reactor use of recycled material. This means that separation-1 changes (from UREX+4 to UREX+1) and fuel-2 changes (from MOX-NpPuAm back to UOX).

This scenario tests the model (and user's) ability to coordinate changes as follows:

- Reactor Fuel Type worksheet
- **Recycle Strategy Option** worksheet from once-through (matrix 15) to 2-tier recycling (matrix 7) for both "b" and "c" phases to phase out thermal recycling (matrix 13).
- Separation worksheets

Table A-8. Reactor, Fuel, and Separation Specifications for LWR and HWR Once-Through

					\mathcal{C}
#	Reactor	Fuel	Fuel #	Separations	Separation #
1-a	LWR	UOX	103	None	None
1-b	LWR	UOX	103	COEX	16
1-c	LWR	UOX	103	UREX+4	11
1-d	LWR	UOX	103	UREX+1	2
2-a	LWR MF	UOX	103	None	None
2-b	LWR MF	MOX-Pu	301	UREX+1	2
2-c	LWR MF	MOX-NpPuAm	306	UREX+1	2
2-d	LWR MF	UOX	103	UREX+1	2
3	FR	Metal CR=0.50	605	Electrochemical	21