# AGR-1 Data Qualification Report

Mike Abbott Larry Hull Binh Pham Mitch Plummer

March 2010

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# **Next Generation Nuclear Plant Project**

# **AGR-1 Data Qualification Report**

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#### **ABSTRACT**

Projects for the very high temperature reactor (VHTR) Technology Development Office program provide data in support of Nuclear Regulatory Commission licensing of the VHTR. Fuel and materials to be used in the reactor are tested and characterized to quantify performance in high temperature and high fluence environments. The VHTR program has established the NGNP Data Management and Analysis System (NDMAS) to ensure that VHTR data are qualified for use, stored in a readily accessible electronic form, and analyzed to extract useful results.

This document focuses on the first NDMAS objective. It describes the data streams associated with the first Advanced Gas Reactor experiment (AGR-1), the processing of these data within NDMAS, and reports the qualification status of the data. Data qualification activities within NDMAS for specific types of data are determined by the data qualification category assigned by the data generator. They include: (1) capture testing, to confirm that the data stored within NDMAS are identical to the raw data supplied, (2) accuracy testing to confirm that the data are an accurate representation of the system or object being measured, and (3) documentation that the data were collected under an NQA-1 or equivalent Quality Assurance program. A summary of the NDMAS database processing and qualification status for the five AGR-1 data streams reported in this document is as follows:

- 1. *Fuel fabrication data*. All data have been processed into the NDMAS database and qualified (1,819 records).
- 2. Fuel irradiation data. Data from all 13 AGR-1 reactor cycles have been processed into the NDMAS database and tested (11,496,872 records). Of these, 85% have been qualified and 15% have failed NDMAS accuracy testing.
- 3. Fission Product Monitoring System data. Reprocessed (January 2010) data from all 13 AGR-1 reactor cycles have been processed into the database and capture tested (652,752 records). Final qualification of these data will be recorded after Quality Assurance approval of an Engineering Calculations and Analysis Report currently in review.
- 4. Advanced Test Reactor Operating Conditions Data. Data for all AGR-1 cycles have been stored and capture tested. These data, which come from outside the VHTR program, are assumed to be qualified by Advanced Test Reactor quality control procedures.
- 5. *Neutronics and Thermal Simulation Data*. NDMAS processing is in progress. Qualification of these data will be recorded after receipt of approved modeling reports produced by the data generators.

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#### **ACRONYMS**

AGR Advanced Gas Reactor

ASME American Society of Mechanical Engineers

ATR Advanced Test Reactor

BWXT BWX Technologies

DST daylight-saving time

ECAR Engineering Calculations and Analysis Report

FPMS Fission Product Monitoring System

HPGe High Purity Germanium (detector)

INL Idaho National Laboratory

IPyC inner pyrolytic carbon layer (fuel kernel coating layer)

MDT Mountain Daylight Time
MST Mountain Standard Time

NDMAS NGNP Data Management and Analysis System

NGNP Next Generation Nuclear Plant

NQA Nuclear Quality Assurance

ORNL Oak Ridge National Laboratory

OPyC Outer pyrocarbon (fuel kernel coating layer)

PDF Portable Document Format

QA Quality Assurance

QAPP Quality Assurance Program Plan

R/B release-to-birthrate [ratio]

SiC Silicon carbide (fuel kernel coating layer)

SQL Structured Query Language

TDO Technology Development Office

TFR Technical and Functional Requirements

VHTR Very High Temperature Reactor (program) and very high temperature gas-cooled reactor



# **AGR-1 Data Qualification Report**

#### 1. INTRODUCTION

This report provides the final FY 2009 status of Advanced Gas Reactor AGR-1 irradiation experiment data qualification as performed by the NGNP Data Management and Analysis System (NDMAS). AGR-1 is the first in a series of eight planned irradiation experiments for the AGR Fuel Development and Qualification Program, which supports development of the very high temperature gas-cooled reactor (VHTR) under the Next Generation Nuclear Plant (NGNP) Project. Irradiation of the AGR-1 test train was conducted over 13 Advanced Test Reactor (ATR) cycles beginning with Cycle 138B on December 23, 2006, and ending with Cycle 145A on November 6, 2009.

This report gives the data qualification status of the three primary AGR-1 data streams, or general types of data, currently being collected and processed by NDMAS from the AGR Fuel Development and Qualification Project: Fuel Fabrication, Fuel Irradiation, and Fission Product Monitoring System (FPMS) data. It also reports on processing of two additional data streams in NDMAS, ATR Operating Conditions and Neutronics and Thermal Simulation data, which are not qualified by NDMAS. Data qualification of graphite characterization data collected under the Graphite Technology Development Project is reported in a separate status report (Hull 2009). Post-irradiation examination of AGR-1 fuel will commence in FY 2010 and continue for several months. Qualification of post-irradiation examination data will begin as soon as data become available.

#### 2. OVERVIEW OF NDMAS DATA QUALIFICATION

NDMAS was developed to provide a single controlled repository for all NGNP data, documentation of and assistance in data qualification, advanced data analysis, and Web access of the data. A detailed discussion of the NDMAS structure and the data qualification requirements performed within NDMAS is given in the Very High Temperature Reactor Program Data Management and Analysis Plan (INL 2009a).

Data qualification is the act of reviewing, inspecting, testing, checking, or otherwise verifying and documenting whether data conform to specified requirements, as defined by the data users and the performing organization. Depending upon the data stream, data qualification may be performed by one or more entities, including independent technical reviewers, Quality Assurance (QA), data review committees, and testing performed within NDMAS. This process also considers whether the data were collected within a Nuclear Quality Assurance NQA-1 (American Society of Mechanical Engineers [ASME] 2000) or equivalent approved QA program. Data qualification within NDMAS is documented as one of three qualification states:

- Qualified. Data that are independently verified to meet requirements, including documentation of
  formal certification reviews for the Fuel Fabrication and FPMS data streams and NDMAS accuracy
  testing for the Fuel Irradiation data stream. All qualified data must have been collected within an
  NQA-1 or equivalent approved QA program.
- 2. *Trend.* Data collected within an NQA-1 or equivalent approved QA program where the qualification process identifies minor flaws or gaps in meeting data requirements, although the data are still considered useful by the program. Trend data captured into NDMAS are tested to verify capture, and may be subjected to some accuracy testing.
- 3. *Failed*. The data do not meet specified requirements. This may be for a number of reasons, including inadequate data collection methods, instrument failure or drift, or poor accuracy.

There may also be data types collected within the program that are for information only. These data are not qualified because specific data qualification requirements cannot be defined or independent verification is not needed or desired. One example of this data type is the gross gamma FPMS data, which

are binary detector output files used only as an early indicator of potential fuel particle failures (see Section 5). These data are processed by NDMAS for display on the web and are then archived or stored in their native file format for possible future use.

As part of the qualification process, capture testing is performed for all data uploaded into the NDMAS database. Capture testing includes automated checks to verify there are no obvious data processing errors in the source files (e.g., date/time chronology checks) and that the data stored within NDMAS are identical to the source data provided to NDMAS.

The primary component of data qualification is verifying data accuracy. For the Fuel Fabrication and FPMS data streams, program-specific data approval certifications or approved Engineering Calculations and Analysis Reports (ECARs) are used to verify and document data accuracy within NDMAS. For the Fuel Irradiation data stream, where no formal data certification exists, NDMAS accuracy testing is performed to identify anomalies in the data that may represent instrument drift or failure. For AGR-1, this accuracy testing included visual examination of the data, simple automated range tests (e.g., thermocouple temperature range of 0 to 1,300°C), and more detailed analyses that use statistical analysis of past behavior to determine whether current instrument readings are reliable. Anomalies identified by these tests are then examined with input from the technical leads and resolved to determine whether the anomalies represent (1) instrument failures or other errors that disqualify ("fail") the data or (2) values that are unusual but reliable thereby resulting in *qualified* data.

The final component of the qualification process is documentation of the NQA-1 requirements for specific data collection activities and documentation of the conformance of the actual data collection to those requirements. Within the VHTR program, these requirements are implemented through the *Very-High-Temperature Gas-Cooled Reactor Technology Development Office Quality Assurance Program Plan* (VHTR Technology Development Office [TDO] QAPP) (INL 2009b). The relevant documents that specify NQA-1 requirements and conformance for each data stream are given in the data stream sections of this report.

#### 3. FUEL FABRICATION DATA

AGR-1 fuel is fabricated from low-enriched uranium oxycarbide kernels that are coated with multiple layers to form particles. The first coating is a low-density carbon layer (buffer layer), followed by a high-density inner pyrolytic carbon (IPyC) layer, a silicon carbide (SiC) layer, and finally, a high-density outer pyrolytic carbon (OPyC) layer. Coating conditions for AGR-1 fuel were varied during particle fabrication to create a baseline and three variant particle composites. Process conditions for the baseline and three variants are described in Barnes (2006). Once the coatings are applied, thousands of particles are formed into cylindrical compacts using a graphite-resin matrix. Design specifications were established for this data stream, and the delivered hard copy data packages are the quality record that the design specifications were met or have been accepted as is.

# 3.1 Description of the Data Stream

The AGR-1 fuel fabrication data stream consists of properties obtained from measurements made on representative samples of fuel kernels, coated fuel particles, and fuel compacts. These properties are listed in the following sections along with specified acceptance criteria (Einerson 2006). The appropriate acceptance criterion depends on whether the property is a variable property or an attribute property. Variable properties are defined by a continuous distribution while attribute properties are discrete properties in the sense that the particle is either defective or not, in terms of that property. For variable properties, the criteria are stated in terms of a population mean and/or population dispersion with the mean having to lie within a specified interval. The acceptance criterion for attribute properties is stated in terms of the allowable fraction of defective particles.

#### 3.1.1 Kernel Data

A kernel composite consists of multiple kernel batches combined and mixed to ensure uniformity prior to sampling for acceptance. The composite lot of kernels (G73D-20-69302) used to make AGR-1 baseline and variant particles was fabricated by BWX Technologies (BWXT), now called Babcock and Wilcox, under a quality program that conformed to the requirements of NQA-1 1997 (ASME 1997) as per the requirements in effect at the time of kernel fabrication. Complete characterization data for this kernel lot are compiled in the Data Certification Package (BWXT 2005). Kernel composite properties included in NDMAS and corresponding specifications are listed in Table 1. Some kernel properties were also measured by ORNL prior to fabricating particles and compacts, but only the BWXT data were used for fuel certification. However, the Oak Ridge National Laboratory (ORNL) kernel data were included in NDMAS for comparison purposes.

Table 1. Properties and	l specifications for AGR-1 fuel kernels (	(Lot G73D-20-69302).

Kernel Property	Specified Range for Mean Value	
U-235 enrichment (wt%)	$19.80 \pm 0.10$	
Total Uranium (wt%)	≥87.0	
Oxygen/uranium (atomic ratio)	$1.50\pm0.20$	
Carbon/uranium (atomic ratio)	$0.50\pm0.20$	
[Carbon+oxygen]/uranium (atomic ratio)	≤2.0	
Sulfur impurity (ppm – wt)	≤1,500	
All other impurities <sup>(a)</sup>	Various	
Density (g/cm <sup>3</sup> )	≥10.4	
Diameter (µm)	$350\pm10$	
Aspect ratio (sphericity or ellipticity)	Not specified	
Not included in NDMAS because all impurities were below detection limits and within specifications.		

#### 3.1.2 Particle Data

AGR-1 fuel kernels were shipped to ORNL where the coatings were added and the compacts fabricated under a quality program that conformed to the requirements of NQA-1 2000 (ASME 2000). Particles were coated in batches and particle composites were made from three or four coated batches. There are four particle composites for AGR-1 fuel—one for the baseline and each of the three variants. Complete characterization data for the four particles composites are compiled in data packages by Hunn and Lowden (2009, 2006a, 2006b, and 2006c). Particle properties included in NDMAS and corresponding specifications are listed in Table 2.

#### 3.1.3 Compact Data

AGR-1 fuel compacts were fabricated by ORNL under a quality program that conformed to the requirements of NQA-1 2000 (ASME 2000). The same compacting process was used for the baseline fuel and all three variants, however the molding pressure did vary by compact. Complete characterization data for the four compact lots are compiled in data packages Hunn and Lowden (2009, 2006a, 2006b, and 2006c). Compact properties included in NDMAS and corresponding specifications are listed in Table 3.

Table 2. Properties and specifications for AGR-1 coated particle composites.

Property	Specified Range for Mean Value	
Buffer density (g/cm <sup>3</sup> )	$0.95 \pm 0.15$	
Buffer thickness (µm)	$100 \pm 15$	
IPyC density (g/cm <sup>3</sup> )	$1.90 \pm 0.05$	
IPyC thickness (μm)	$40 \pm 4$	
IPyC anisotropy (BAFo)	≤1.035	
SiC density (g/cm <sup>3</sup> )	≥3.19	
SiC thickness (µm)	$35 \pm 3$	
OPyC density (g/cm <sup>3</sup> )	$1.90 \pm 0.05$	
OPyC thickness (μm)	$40 \pm 4$	
OPyC anisotropy (BAFo)	≤1.035	
Gold spot defect fraction	$5.0 \times 10^{-3}$ (Variants 2 & 3);	
	1.0x10 <sup>-3</sup> (Baseline and Variant 1)	
Defective SiC coating fraction	$\leq 1.0 \times 10^{-4}$	
Defective OPyC coating fraction	$\leq 3.0 \times 10^{-2}$	
IPyC anisotropy post compact deconsolidation (BAFo)	Not specified	
OPyC anisotropy post compact deconsolidation (BAFo)	Not specified	
Aspect ratio (sphericity)	Mean not specified <sup>(a)</sup>	
a. Critical region is specified such that $\leq 1\%$ of the particles shall have an aspect ratio $\geq 1.14$ .		

Table 3. Selected properties for AGR-1 compacts.

Property	Specified Range for Mean Value
Mean uranium loading (g U/compact)	$0.905\pm0.04$
U contamination fraction <sup>(a)</sup> (g U <sub>exposed</sub> /g U)	$\leq 1.0 \times 10^{-4}$
Iron content (μg Fe outside SiC/compact)	≤25
Chromium content (µg Cr outside of SiC/compact)	≤75
Manganese content (μg Mn outside of SiC/compact)	≤75
Cobalt content (µg Co outside of SiC/compact)	≤75
Nickel content (μg Ni outside of SiC/compact)	≤75
Calcium content (µg Ca outside of SiC/compact)	≤90
Aluminum content (µg Al outside of SiC/compact)	≤45
Titanium content (μg Ti outside of SiC/compact)	Note <sup>(b)</sup>
Vanadium content (µg V outside of SiC/compact)	Note <sup>(b)</sup>
Diameter <sup>(c)</sup> (mm)	12.22–12.46
Length <sup>(c)</sup> (mm)	25.02-25.40
Compact mass (g)	Not specified
Molding pressure (MPa)	Not specified <sup>(d)</sup>

a. Value is an estimate of an attribute property, not the mean of a variable property.

b. Mean value specification of ≤400 µg Ti plus V outside of SiC/compact.

c. Allowable range corresponding to upper and lower critical limits specified with no compacts exceeding the limits which requires 100% inspection of all compacts.

d. Not a variable, but a process condition that varied by compact.

#### 3.1.4 Data Structure

Prior to capturing the data in NDMAS, a hierarchal data structure based on components was created to make the data easier to process and analyze. A component is the generic name for the object or system being measured. In NDMAS, the fuel properties shown in Tables 1, 2, and 3 are known as response variables, and each response variable is a measurement or property associated with a component. For AGR-1 fuel, the component types are kernels, particles, particle layers, and compacts. Table 4 shows the component naming structure for each of the component types. There are 336 unique components for all four variants.

Table 4. Component types and names for AGR-1 fuel data.

Component_type	Component_name	
Kernel Batch	LEU01	
Buffer Layer <sup>a</sup>	LEU01-XXB	
IPyC Layer <sup>a</sup>	LEU01-XXI and LEU01-XXT-ZI <sup>b</sup>	
SiC Layer <sup>a</sup>	LEU01-XXS and LEU01-XXT-ZOb	
OPyC Layer <sup>a</sup>	LEU01-XXO	
Particle Composite	LEU01-XXT	
Compacts	LEU01-XXT-ZYY	
Compact Lot	LEU01-XXT-Z	
	<u></u>	
a. Layers added to the kernels to make particles.		
b. Some layer properties were measured on particles from deconsolidated compacts.		
XX = number associated with variant (46=Baseline, 47=Variant 1, 48=Variant 2, 49=Variant 3).		
YY = compact number (79 each for Baseline, V1 and V3 variants, 67 for V2).		

Components in NDMAS are related to each other by an assembly tree. The component assembly tree

for AGR-1 fuel data is shown in Figure 1. The compact lot at the base of the tree is composed of particles from the particle composite, which is composed of kernels from the kernel batch. Individual compacts are associated with (a branch of) the compact lot, and particle layers are associated with the particle composite. All the chemical properties in Table 3 are representative of the compact lot. The physical properties (diameter, length, and mass) are measured on individual compacts.

A careful review of the data packages identified the 33 unique response variables listed in Table 5. Where a mean value is indicated, there is also a response variable for the standard deviation and the number of samples in the population. There is no standard deviation for defect fractions because these are attribute properties (defective or not defective).

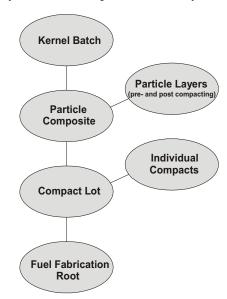


Figure 1. Fuel fabrication data component assembly tree structure.

Table 5. Response variables for AGR-1 fuel data.

Response_var_name	Response_var_description	Units
u235_enrich_mean	Mean weight percent of U-235 enrichment in kernel composite	wt%
u_wt_percent_mean	Mean total weight percent uranium in kernel composite	wt%
o_to_u_ratio_mean	Atomic ratio of oxygen to uranium in kernel composite	ratio
c_to_u_ratio_mean	Atomic ratio of carbon to uranium in kernel composite	ratio
c_plus_o_to_u_ratio_mean	Atomic ratio of carbon plus oxygen to uranium in kernel composite	ratio
sulfur_content_mean	Mean Sulfur content of kernel composite	ppm-wt
env_dens_mean	Mean envelope density measured by mercury porosimetry	g/cm <sup>3</sup>
diameter_kernel_mean	Mean kernel diameter	μm
aspect_ratio_mean <sup>a</sup>	Ratio of maximum to minimum diameter (a.k.a. sphericity)	$D_{\text{max}}\!/D_{\text{min}}$
aspect_ratio_defect_frac	Fraction of samples that exceed aspect ratio specification	fraction
thickness_mean	Mean thickness of TRISO composite layer	μm
sink_float_dens_mean	Mean density measured using density-gradient column	g/cm <sup>3</sup>
anisotropy_mean	Mean anisotropy of layer (BAFo equivalent)	BAFo
defective_SiC_frac	Fraction of particles with defective SiC layer	fraction
gold_spot_defects_frac	Fraction of particles with soot inclusion (gold spot) in SiC layer	fraction
diameter_compact	Diameter of compact (mean of 6 measurements 2-top, 2-mid, 2-bot)	mm
length_compact	Length of the compact	mm
mass_compact	Mass of the compact	g
molding_pressure	Molding pressure used to create the compact	MPa
u_loading_mean	Mean uranium loading per compact	g/compact
u_contamination_frac	Fraction of uranium in compact not encapsulated by retentive layer	g U <sub>exposed</sub> /g U
defective_IPyC_frac	Fraction of particles with defective IPyC layer	fraction
defective_OPyC_frac	Fraction of particles with defective OPyC layer	fraction
fe_content_mean	Mean Iron content per compact (outside SiC layer)	$\mu g/compact$
cr_content_mean	Mean chromium content per compact (outside SiC layer)	μg/compact
mn_content_mean	Mean manganese content per compact (outside SiC layer)	μg/compact
co_content_mean	Mean cobalt content per compact (outside SiC layer)	μg/compact
ni_content_mean	Mean nickel content per compact (outside SiC layer)	μg/compact
ca_content_mean	Mean calcium content per compact (outside SiC layer)	μg/compact
al_content_mean	Mean aluminum content per compact (outside SiC layer)	μg/compact
ti_content_mean	Mean titanium content per compact (outside SiC layer)	μg/compact
v_content_mean	Mean vanadium content per compact (outside SiC layer)	μg/compact
sink_float_dens_SiC_mean <sup>b</sup>	Mean SiC density measured using density-gradient column	g/cm <sup>3</sup>

a. Although a mean value for aspect ratio is included, there is not an accompanying standard deviation because it is an attribute property.

b. A separate response variable was used for the sink-float density of the SiC layer because it was measured using a different method than the other layers.

## 3.2 Fuel Fabrication Data Processing within NDMAS

The complete kernel data package (BWXT 2005) was transmitted to Idaho National Laboratory (INL) in hardcopy format. A summary of the kernel data package was transmitted in electronic Portable Document Format (PDF). The baseline and variant data packages for the particles and compacts (Hunn and Lowden 2009, 2006a, 2006b, 2006c) were transmitted in electronic PDF file format. None of the data in the data packages were in machine readable format. Before they could be captured into NDMAS, the data were entered into an Excel spreadsheet file named agr1 fuel fab data.xls.

The agr1\_fuel\_fab\_data.xls spreadsheet file contains a separate worksheet for components, response variables, response variable values, and methods. Most of the response variable values were entered directly from the data packages into the worksheet. However, the mean and standard deviation density values for the buffer layers, IPyC layers and OPyC layers were not available for the entire population used to make the composite particles. Recall the composite particles were made from three or four coated batches. Means and standard deviation values for individual batches were reported in the data packages, but not for the entire population. In these cases, the batch mean and standard deviation values were used to calculate an overall mean and standard deviation (IPyC layers), or the density values of all samples in all the batches were used to calculate the mean and standard deviations for the entire population (OPyc layers). This was done in a separate Excel spreadsheet file called agr1\_fuel\_fab\_density\_calculations.xls and documented in Engineering Calculation and Analysis Report ECAR-824 (Sondrup 2009). The calculated density values were then entered into the agr1\_fuel\_fab\_data.xls file. Both Excel files are archived on the NGNP SAS Server in the directory \\Sasngnp\ngnp\ngnp\NGNP\_Data\Fuel\_Fab\AGR1\\.

Each worksheet of agr1\_fuel\_fab\_data.xls was captured as a SAS dataset using the program \\Sasngnp\ngnp\ NDMAS Version 1.1\Fuel\_Fab\ Capture\_native\_fuel\_fab\_data.egp. The four new SAS datasets (COMPONENTS, VARS, VALUES and METHODS) are stored in the SAS Library FUEL\_FAB on the SAS Server. A different program, Capture\_native\_fuel\_fab\_data.egp, reads these SAS datasets and through a series of joins, filters, queries, and transposes, creates three additional datasets (EXP\_COMP\_for\_upload, EXP\_COMP\_ATTRIB\_for upload, EXP\_ASSY\_TREE\_for\_upload) to be appended to the appropriate files in the NDMAS Structured Query Language (SQL) database ("vault").

# 3.3 Description of Fuel Fabrication Data Qualification

Two general types of qualification tests are performed on data loaded into NDMAS:

- Capture tests, which verify that data captured and stored within NDMAS are identical to the source data provided to NDMAS.
- Accuracy tests, which verify the data are an accurate representation of the parameters they are intended to measure.

#### 3.3.1 Capture Tests

The transmitted data are manually entered into the Excel spreadsheet file agr1\_fuel\_fab\_data.xls. Once the data are transferred, every response variable value in the spreadsheet is manually checked against the values in the data packages to make sure they're identical. An independent person performs the comparison and the review is documented. The values used in the calculations for the calculated density values (see Section 3.2) are checked against the data in the data packages.

The second capture test is a referential integrity test to make sure that all components, component attributes and response variables, and response variable values are properly linked (see Section 3.1.4)

The third capture test verifies that the data in the SQL database are the same as the data loaded (pushed) into the SQL database. This test uses a SAS procedure (PROC-COMPARE) to compare the SAS dataset pushed to the SQL database with the database output.

The final capture test is to compare the SQL database output with the original data in the data packages. This is another manual inspection similar to the first capture test. An independent person checks response variable values in the database against the data in the data packages and documents the results. Values determined from calculations (see Section 3.2) are compared against ECAR-824 (Sondrup 2009).

# 3.3.2 Accuracy Tests

The scope of accuracy testing is limited to the certification that AGR-1 fuel data for kernels, particles (including layers), and compacts meet specifications as outlined in Einerson (2006). Certification is performed by the data generators and documented in the subcontract deliverable data packages (BWXT 2005, Hunn and Lowden 2009, 2006a, 2006b, 2006c). Nonconformance reports are included in the data packages for any data that does not meet specifications. Certified data are verified and accepted by the contractor. Nonconformance data are reviewed and either rejected or accepted by the contractor.

The process of verifying that all data in the data packages meet specifications is a thorough process with multiple checks to ensure data accuracy. Because this process is so rigorous, no additional accuracy tests are planned for the fuel fabrication data.

# 3.4 Verify Fuel Fabrication Data QA Documentation

Kernels for AGR-1 fuel were produced under a quality program that conformed to the requirements of the 1997 version of NQA-1, which was in effect at the time of kernel fabrication. Quality requirements were passed to BWXT in Statement of Work SOW-427. Supplier audits were conducted to provide independent verification that quality requirements for the data were met.

Coated particles and compacts were produced under a quality program that conformed to the requirements of the NQA-1 2000 as implemented and documented by the fuel fabricator's QAPP (ORNL, 2006). Engineering Design File EDF-4380, "AGR-1 Fuel Product Specification and Characterization Guidance" (Barnes 2006) provides the requirements necessary for acceptance of the fuel manufactured for the AGR-1 irradiation test. Section 6.2 of EDF-4380 provides the property requirements for the heat treated compacts. EDF-4542, "Statistical Sampling Plan for AGR Fuel Materials" (Einerson 2006), provides additional guidance regarding statistical methods for product acceptance and recommended sample sizes. The procedures for characterizing and qualifying the compacts are outlined in ORNL product inspection plan AGR-CHAR-PIP-05. The inspection report forms generated by this product inspection plan document the product acceptance for the property requirements listed in Section 6.2 of EDF-4380 (Barnes 2006). Independent verification that quality requirements for the data were met is provided by supplier audits conducted by INL (Roberts and Barnes 2005a, 2005b).

#### 3.5 Fuel Fabrication Data Qualification Status

A preliminary manual inspection was performed on a portion of the data in the Excel spreadsheet file agr1\_fuel\_fab\_data.xls. The check found one error out of 230 values checked. The printed file was signed by the independent reviewer and placed in the project file. After capturing the data to the NDMAS SQL database, a manual inspection of data pulled from the vault was performed by an independent person who compared the data pulled from the vault to the data in the original data packages (BWXT 2005; Hunn and Lowden 2006a, 2006b, 2006c, 2009) and EDF-824 (Sondrup 2009). This inspection included verifying that data were associated with the correct component (Table 4), thus verifying referential integrity. Errors found in data in the vault were corrected. All fuel fabrication data were flagged as capture passed after the manual verification was complete and corrections were made.

As stated previously, no additional accuracy testing beyond what was done for data certification will be performed. Nevertheless, all data in the data packages met specifications with three exceptions. The first nonconformance is the 95% lower confidence limit for kernel uranium enrichment was 19.6962 wt%,

slightly less than the specification of 19.7 wt%. The nonconformance report (included in the data package) shows the kernels were submitted for customer disposition and approved as is. The second nonconformance was also related to the kernels in that the carbon/uranium dispersion did not meet the specification as documented in Ebner (2005). Barnes (2005) provided the basis for the kernels to be used as is, and INL issued a Procurement Change Notice to BWXT releasing them from meeting the specification. The third nonconformance was that the length of some of the Baseline and Variant 2 compacts were slightly less than the specified minimum length. The nonconformance reports (provided as part of the data packages) document the recommendation and acceptance that the specimens be used as is for both irradiation and destructive characterization.

All of the fuel fabrication data entered into the NDMAS database has been verified against original documents provided by BWXT and ORNL. Independent verification that the data conform to requirements was obtained by site visits to BWXT and ORNL during data collection. All fuel fabrication data in the NDMAS data base is therefore qualified. A summary of the number of data records for each data package is shown in Table 6.

Table 6. Qualification status of fuel fabrication data.

Data Package	Qualified Records	Total Records
BWXT Kernel Data for G73D-20-69300	27	27
Baseline Fabrication Data for LEU01-46T-Z	466	466
Variant 1 Fabrication Data for LEU01-47T-Z	457	457
Variant 2 Fabrication Data for LEU01-48T-Z	409	409
Variant 3 Fabrication Data for LEU01-49T-Z	460	460
Total	1,819	1,819

#### 3.6 Fuel Fabrication Data Problems and Resolution

A problem with the AGR-1 fuel fabrication data is that it was not supplied in machine readable format. Some tables of data in the data packages appear to be scans of Excel spreadsheet files, but the Excel files were not readily available. The Excel files were scanned to preserve the signatures of operators, reviewers, and supervisors. These scanned images were high-quality reproductions and there were no problems discerning the data/numbers from the PDF files. Nevertheless, not having machine readable data requires each value to be entered by hand into a spreadsheet and checked manually. It is recommended that future fuel fabrication data packages be transmitted in machine readable format. Efforts should also be made, where possible, to standardize the formatting, especially for similar data types, with the goal of reducing any preprocessing required to handle distinct and unique files or tables. Having the data in standardized machine readable format may be more of a convenience issue than a problem, but it will be more efficient to process the data and reduce the possibility for errors.

#### 4. FUEL IRRADIATION DATA

# 4.1 Description of the Data Stream

The fuel irradiation experiment includes monitoring of the controlled gas flows to the capsule train that provide some temperature control and that collect emissions from the six fuel capsules and route them to the fission product monitoring system. Ten variables are measured as shown in Table 7. These data are subsequently processed and stored in NDMAS. The data include flow rates of helium and neon gases to and from each capsule, gas pressure upstream of each capsule, moisture content of the gas flow mixture downstream of each capsule, and thermocouple temperatures at several locations within each capsule. Gas pressure, flow rates, and moisture content are also collected for the leadout system—the pressurized space around each capsule that prevents leakage of capsule gas flows into adjacent capsules. These data are generally collected at 5-minute intervals, except where data management issues during the first two reactor cycles (138B, 139A) provided only 2-hour interval data (INL Issue Communication and Resolution Environment [ICARE] NCR 42791 2008).

Table 7. Measurement variables in the fuel irradiation data stream.

Measurement Variable	Description	Units
Moisture Content	Moisture content in gas flow line	Parts per million volume (ppmv)
Pressure	Pressure in gas flow line	Pounds per square inch atmosphere (psia)
Q_He	Helium flow rate	Standard cubic centimeters per min (sccm)
Q_Ne	Neon flow rate	sccm
Q_Total	Total outlet line gas flow rate	sccm
TC_1	Thermocouple No. 1 temperature	°C
TC_2	Thermocouple No. 2 temperature	°C
TC_3	Thermocouple No. 3 temperature	°C
TC_4	Thermocouple No. 4 temperature	°C
TC_5	Thermocouple No. 5 temperature	°C

The capsule thermocouples are of two different types and two different diameters, and thermocouple identification numbers may be associated with different positions and insertion depths in different capsules. A summary diagram of the thermocouples positions in the capsules is shown in Figure 2.

# 4.2 Fuel Irradiation Data Processing within NDMAS

Data processing and storage within NDMAS occurs via the following process. Raw data files covering about one week of measurements are placed in folders on the FSISC1 server as shown in Figure 3. Each folder contains one data file for each capsule with leadout system data included in the file for Capsule 1. A SAS Enterprise Guide project titled, "Update or build Irradiation dataset.egp," reads these data, assembles the data into a single SAS dataset, and stores the data in the NDMAS SQL database (vault). Processing and storage in NDMAS occurs approximately once per week so that several folders of data may be processed and entered as a single package. Data processing includes the following error checks to ensure that the data are accurately captured:

- Dates are checked for proper syntax and chronology.
- Data are checked for duplicated measurement times with conflicting variable values.
- Completed SAS datasets are visually inspected and compared against the raw data files.

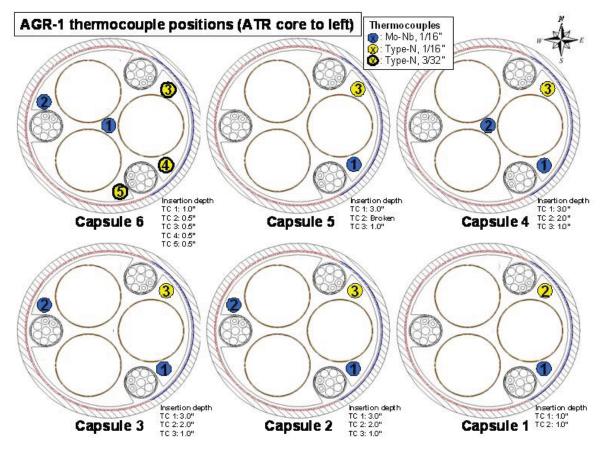


Figure 2. AGR-1 thermocouple descriptions and location information.

#### Raw AGR-1 Irradiation data:

FSISC server location:

\\FSISC1\Projects\AGRData

#### Foldernames:

- '2400' followed by ending date of dataset in 'mm-dd-yy' format) File names:
- 'AGR1x.RPT' (6 files per cycle, x = capsule 1-6)
- 'HE\_FLOW.RPT' (Gas flow data for FPMS)

#### AGR-1 Irradiation data processing steps:

- Copy new file folders from FSISC1 to \\Sasngnp\\WGNP\WGNP\_Data\AGR-1\
- FROM NDMAS directory, 'Vault\_PushPull'
  - 1) Run batch file 'update.bat' that creates/updates the list of relevant folder names to be processed
  - Run Enterprise Guide Project file 'Update or build Irrad dataset.egp' to construct SAS dataset for new data
    - Builds/appends all new data as SAS dataset
    - Pushes new data to SQL\_NDMAS (NDMAS vault)
    - Checks that vault data is correctly entered
  - 3) Update log file 'Irradiation capture-push instructions and log.doc'
  - 4) Run Enterprise Guide Project file 'Vault tests.egp' and examine any failed data
  - 5) Resolve failed data as necessary
  - 6) Run Enterprise Guide Project file 'Combine\_Irrad\_ATR\_FPMS.egp' to populate N\_MART directory with new SAS data sets and cubes containing updated irradiation data

Figure 3. Raw AGR-1 irradiation data and data processing steps.

• A mountain standard date/time is assigned to each measurement that corrects for the switching between daylight-saving time (DST) and standard time that occurs in the raw data measurements. The switch to DST leads to repeated measurement times with different variable values, while the switch to standard time leads to a gap in measurement times.

The process of entering each data packages is recorded in an electronic log, with appropriate notes about any problems or corrections encountered. After being entered into the NDMAS SQL database, capture testing is performed for each data package to compare the database output with the SAS dataset from which it was built to ensure that the data were correctly stored. Results are stored in the electronic log, "Irradiation capture-push instructions and log.doc."

# 4.3 Description of Fuel Irradiation Data Qualification Tests

Several tests, or analyses, are performed to attempt to identify data anomalies that may represent instrument drift or failure. Some of these methods are simple tests that, for example, check that the data are in a value range appropriate to the measurement. Others are more detailed analyses that rely on statistical analysis of past behavior as a guide to the range expected for new data values. These checks are programmed as a series of tests applied to each data package entered in the NDMAS SQL database. Anomalies identified by these tests are then examined with input from the technical leads and resolved to determine whether the anomalies represent (1) instrument failures or other errors that disqualify the data from use for their intended purpose, (2) values that are unusual but accurate, and therefore *qualified data*, or (3) instrument data that is reasonably precise, for use as *trend data*, but insufficiently accurate to be considered *qualified data*.

Range tests that detect data values outside expected ranges of measurement include the parameters and values listed in Table 8.

Table 8. Range test values.

Parameter	Requirement
Temperature	$0^{\circ}\text{C} < X < 1,300^{\circ}\text{C}$
Gas pressure	10  psia < X < 20  psia
Gas moisture content	0  ppm < X < 5  ppm
Gas flow	-2  sccm < X < 52  sccm

These range tests are based on a combination of physical limitations and/or requirements described in Technical and Functional Requirements (TFR) documents and other AGR-1 reference documents as follows:

- Requirements for gas moisture content are specified in TFR-248 (West et al. 2005), Section 3.1.2.4:
   "Moisture content of the inlet sweep gas shall be measured on the inlet side of the capsule at least once after each gas cylinder change and shall be <5 parts-per-million (ppm) H<sub>2</sub>O."
- Based on the desired volume-averaged temperatures for the fuel in the experiment, the AGR-1 test train design requires temperature measurements in the 970–1,290°C range (Palmer 2006). As initial data from the experiment suggested that operating temperatures did not generally approach the higher end of that range, 1,300°C was selected as an upper limit for the NDMAS range test. The lower limit for temperatures should be limited by that of the water surrounding the capsule train, which enters the reactor vessel at an average temperature of 52°C and, at full power, exits the vessel at a temperature of 71°C (INL 2008). However, because the thermocouples commonly read low in the low-temperature range, the prescribed lower limit for the range test is set at 0°C.
- The range test for gas flow rates to the capsules is based on the nominal flow rates specified in TFR-248 (West et al. 2005), Section 3.1.2.2: "The tubing, valves, and MFCs shall be sized for a flow

rate in each system up to 100 standard cubic centimeters per minute (sccm) with a nominal flow rate of 50 sccm thru the FPMS."

• Expert judgment. Monitoring data may be qualified according to physical principles or other information not revealed by statistical analyses. Temperature measurements, for example, are periodically compared to numerical simulations of heat flow that calculate temperatures at the thermocouple locations. Where the temperatures differ by greater than ~50°C, the thermocouples may be judged to have failed, sometimes by formation of a new junction. Such judgments, as recorded in controlled documents, are used to qualify the data where appropriate. For the AGR-1 experiment, examples include notes like the following from Maki (2007b):

These "TCs have provided measurements in excess of 200°C difference from calculated values (Ambrosek 2007). Such large differences indicate either the thermocouples have formed virtual junctions outside of the intended capsule or have developed another form of malfunction."

## 4.4 Verify Fuel Irradiation Data QA Documentation

The NGNP data collection process includes plans describing how data will be collected and the QA activities associated with those data. Review of those plans assures that the work will generate data of appropriate quality for use in the NQA-1 program. Metadata generated by the initial documentation, audits, and acceptance inspection provide the evidence that data meet the requirements of an NQA-1 data collection program. This is documented at the data stream level for fuel irradiation data. Documentation of the QA Program in NDMAS is primarily accomplished by references to documents. These include plans, audit reports, nonconformance reports, EDFs, and ECARs approved by the VHTR-TDO QA Lead.

The following documents provide evidence that the data for the fuel irradiation data stream meet the requirements of NQA-1, Part 1:

- 1. R. G. Ambrosek, "AGR-1 As-Run Thermal Evaluations Cycle 138B, 139A and B," ECAR-102, Draft, December 4, 2007.
- 2. J. T. Maki, "AGR-1 Irradiation Test Specification," EDF-4731, Rev. 1, July 2004.
- 3. J. T. Maki, AGR-1 Irradiation Experiment Test Plan, INL/EXT-05-00593, Rev. 2, March 2007.
- 4. J. T. Maki, 2007b, AGR-1 As-Run Analysis Status for FY-07, INL/EXT-07-13630, Rev 0, December 2007.
- 5. Email from John Maki to M. A. Plummer, with attachment, "AGR TC condition 10-28-08.doc"
- 6. A. J. Palmer, "Thermocouple recommendations for the AGR-1 test," EDF-6809, Rev. 0, May 2006.
- 7. P. B. West, G. A. Marts, E. W. Killian, J. K. Hartwell, and S. B. Grover, "Temperature Control and Off Gas Monitoring Systems for Advanced Gas Reactor Experiment AGR-1," TFR-248, Rev. 1, March 2005.
- 8. P. B. West, G. A. Marts, E. W. Killian, J. K. Hartwell, and S. B. Grover, "Requirements for Design of the Advanced Gas Reactor Experiment AGR-1 for Irradiation in the Advanced Test Reactor," TFR-249, Rev. 1, December 2004.
- INL ICARE NCR-42791, 2008, "ATR Experiment Data Collection System and Resulting Data," May 28, 2008.

# 4.5 Fuel Irradiation Data Analysis and Accuracy Testing

In addition to the basic qualification tests described in Section 4.3, data from AGR-1 are being used to develop additional accuracy testing methods for the fuel irradiation data that can be used in AGR-2 and subsequent irradiation experiments. Focusing on detecting thermocouple failure, NDMAS has explored several different methods that can predict thermocouple temperatures from ATR/AGR operating parameters and thus provide an independent measure of thermocouple deviation from expected values. NDMAS is also examining data from thermocouples that were judged to have failed during AGR-1 but still appeared to provide realistic temperatures. Using those examples of failures and the data used to differentiate failed data, NDMAS anticipates that additional failure detection methods may be developed. Examples of tests being developed using analyses of AGR-1 data include:

- Independent temperature estimation based on historical temperatures and observed relationships between temperature and ATR operating conditions. For sufficiently short time periods, fission power heating should be well correlated with ATR configuration. Thermocouple temperatures should thus be well predicted from ATR configuration and the thermal conductivity of the gas flow mixture delivered to each capsule. Preliminary regression modeling demonstrates, for example, that temperatures in Capsule 6 are well predicted by a first-degree polynomial expression involving only the angle of control cylinder S1D2 and the neon fraction of gas flow to the capsule. Subsequent analysis will examine how the uncertainty of the predicted temperature varies with ATR configuration and length of time.
- Gas flow tests were used to identify several thermocouple failures in the first three AGR-1 cycles. NDMAS posits that periodic, automatic, preprogrammed gas-flow tests that sequentially alter gas flow mixtures in the capsules and automatically analyze temperature response to those changes should offer a robust means of identifying thermocouple deviations.
- While temperatures between capsules are well correlated, increased correlation between
  thermocouples in different capsules may reflect formation of a new junction in the thermocouple
  leads from the distal capsule. NDMAS is currently examining failed data from cases where this is
  believed to have occurred in order to develop tests that can identify those and other failures.

#### 4.6 Fuel Irradiation Data Qualification Status

The overall qualification status for the separate AGR-1 fuel irradiation data packages is provided on the 'Qualification' page, INL NDMAS Web portal (<a href="https://sasweb.inl.gov">https://sasweb.inl.gov</a>). As of December 1, 2009, approximately 11 million irradiation data records have been stored in NDMAS, entered, and tested as 19 separate packages. The qualification status for these packages is summarized in Table 9.

#### 4.7 Fuel Irradiation Data Problems and Resolution

#### 4.7.1 Data Collection Issues

During most of the AGR-1 experiment, data from the capsule gas flow and temperature monitoring system were collected on one computer system and then transferred via floppy disk to another computer connected to the INL intranet. This system significantly limited NDMAS access to the data and thereby the frequency at which updates to NDMAS displays could be affected. In September 2009, a new data collection system was installed to record AGR and AGC data, and a temporary mode of file transfer was developed to provide data from that system to NDMAS. This altered the format of input files and NDMAS data capture systems were updated accordingly, yielding slight variants of the filenames and method described in Figure 3. During AGR-2 and subsequent experiments, it is expected that NDMAS will have a direct connection to the automated data collection system for the capsule gas flow and temperature monitoring data.

Table 9. Qualification status of fuel irradiation monitoring data received as of August 1, 2009.

·			
	Accuracy Failed	Qualified	Total
D . D . I			
Data Package	Records	Records	Records
Irradiation data ending 20070703	113,439	546,478	659,917
Irradiation data ending 20090216	1,136,008	6,742,058	7,878,066
Irradiation data ending 20090222	18,144	98,784	116,928
Irradiation data ending 20090301	18,144	98,784	116,928
Irradiation data ending 20090308	18,144	98,784	116,928
Irradiation data ending 20090315	18,144	98,784	116,928
Irradiation data ending 20090323	18,144	122,976	141,120
Irradiation data ending 20090412	54,324	368,196	422,520
Irradiation data ending 20090419	18,144	122,976	141,120
Irradiation data ending 20090621	39,332	242,908	282,240
Irradiation data from Folder 2400 04-26-09	18,144	122,976	141,120
Irradiation data from Folder 2400 05-24-09	18,144	122,976	141,120
Irradiation data from Folders 2400 05–09–09 and 2400 05–17–09	35,883	243,207	279,090
Irradiation data from Folders 2400 05-31-09 and 2400 06-07-09	36,288	245,952	282,240
Irradiation data from Folders 2400 06–14–09 and 2400 06–21–09	16,128	266,112	282,240
Irradiation data from folders 06-28-09 and 07-05-09	39,332	114,684	154,016
Irradiation data from 2009 Sep 04 to 2009 Oct 12	69,623	47,658	117,281
Irradiation data from 2009-10-05 through 2009-11-02	27,162	79,568	106,730
Revised irradiation gas flow data from Sep 4 to Nov 9 2009	16	324	340
Totals	1,712,687	9,784,185	11,496,872

Dates and times in the AGR-1 irradiation data collection system are recorded in USA Mountain Time, which shifts an hour ahead to DST in the spring, and back to standard time in the fall. This creates an apparent gap in the time domain data in the spring, and an hour of duplicate date-time records in the fall. These interruptions in the time domain sequences are generally identified automatically by the NDMAS data reading programs, and examination of those periods indicates that the data collection system transitioned to and from DST on dates inconsistent with the national implementation. Based on the records, the DST shifts appear to be made in a program that did not recognize the change in policy made in 2007. In addition, the Fall 2007 DST shift that should have been evident in the data was not found, and NDMAS assumed a change consistent with national policy. Dates and times where the AGR-1 DST shifts were made are shown in Table 10, with the corresponding correct dates for the shift and shift dates not accounting for the DST change made in 2007. To provide a consistent time and record for all data sets, it is recommended that subsequent AGR experiments also maintain a Mountain Standard Time (MST), or other standard time, date/time stamp for all records.

Table 10. Daylight saving time changes recorded in AGR-1 records, with corresponding dates and times

for the correct time of change and time using pre-2007 policy.

		DST Shift Date/Tim	e
	AGR-1	U.S.	Pre-2007 U.S.
Fall 2006	Insufficient data	10/29/06 2:00 AM	10/29/06 2:00 AM
Spring 2007	04/01/07 2:00 AM	03/11/07 2:00 AM	04/01/07 2:00 AM
Fall 2007	Not found	11/04/07 2:00 AM	10/28/07 2:00 AM
Spring 2008	Insufficient data	03/09/08 2:00 AM	04/06/08 2:00 AM
Fall 2008	10/26/08 3:00 AM	11/02/08 2:00 AM	10/26/08 2:00 AM
Spring 2009	04/05/09 2:00 AM	03/08/09 2:00 AM	04/05/09 2:00 AM
Fall 2009	11/01/09 2:00 AM	11/01/09 2:00 AM	2:00 AM

#### 4.7.2 Failed Irradiation Data

Data problems with the irradiation experiment include failures in the data collection system and failures in accuracy. The former failure occurred during all of the first AGR-1 cycle (ATR Cycle 138B) and the first week of the second AGR-1 cycle (ATR Cycle 139A) when all of the electronic data files were irretrievably lost. Available data from that period are therefore restricted to that contained in hardcopy log sheets which contain control thermocouple data and sweep gas data recorded at 2-hour intervals. Because data collection for that period did not conform to TFR-248 (West et al. 2005) requirements for the experiment, INL ICARE NCR 42791 (2008) was issued to address the issues associated with that data loss and ensure that future data management would comply with TFR-248 (West et al. 2005).

Data from the fuel irradiation data monitoring stream that have failed accuracy tests are plotted in Figures 4, 5, 6, and 7. The failed data generally reflect shakedown issues that occurred during the first three cycles, except for minor anomalies that likely reflect short-term interruptions to recording systems. A summary of the explanations for the failed data precedes each figure.

#### 4.7.2.1 Gas moisture Content Data

Most of the failed gas moisture data (see Figure 4) reflects "repair of minor gas leaks, repair of faulty gas line valves; the need to position moisture monitors in regions of low radiation fields for proper functioning; the enforcement of proper online data and the need to monitor thermocouple performance." (Maki 2007b). By the end of the third cycle, it was concluded that the moisture monitors had degraded and then failed because of radiation damage to the sensor electronics. This implied that all moisture readings through the first three cycles were erroneous. During the reactor outage, between the third and fourth cycles, the moisture monitors were replaced with new sensors and relocated to an area with significantly reduced radiation fields. Other anomalous data were identified in Capsules 5 and 6 on one occasion in March 2008 and a second occasion in January 2009.

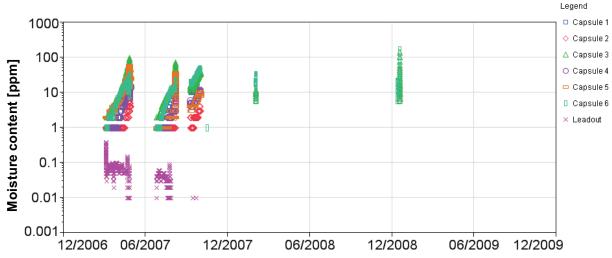


Figure 4. Gas moisture content data (log scale) from AGR-1 that failed accuracy tests implemented by NDMAS.

#### 4.7.2.2 Gas Pressure Data

Relatively few anomalous gas pressure events (see Figure 5) were identified. The first of these was likely associated with the replacement of gas moisture monitoring instruments, as described above. Similarly, anomalies in gas moisture data in March 2007 and January 2009 correspond to anomalies in gas moisture content data and may thus reflect maintenance activities.

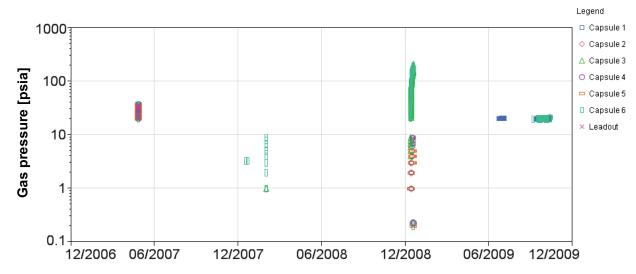


Figure 5. Gas pressure data (log scale) from AGR-1 that failed accuracy tests implemented by NDMAS.

#### 4.7.2.3 Gas Flow Data

Relatively few anomalous gas flow events were identified (see Figure 6), and with the exception of erroneous values from September 14, 2009, these anomalies reflected only slightly excessive flows in the range of 52 to 63 sccm. Out of range values in September 2009 were associated with a data gap in flow values for many of the capsules and are believed to reflect an adjustment to the data collection system.

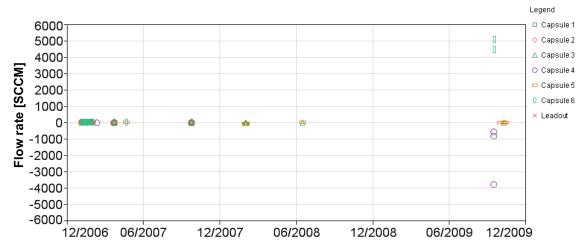


Figure 6. Gas flow data from AGR-1 that failed accuracy tests implemented by NDMAS.

#### 4.7.2.4 Thermocouple Data

Thermocouple failures that occurred during fabrication and the experiment were generally identified by the NGNP technical leads via gas flow tests or the comparison of neutron transport and heat flow within the capsules to numerical simulations. The failure chronology, as provided to NDMAS (personal communication, J. Maki to M. Plummer, Oct 28, 2008; Maki 2007b), is summarized in Table 11 and the failed data, as recorded in NDMAS, are plotted in Figure 7.

Table 11. Chronology of thermocouple failures during AGR-1, based on NDMAS-assigned failure dates. Information provided to NDMAS is shown in the "AGR TC Table" column. Because thermocouple failure does not always coincide with complete failure of the instrument to respond to reactor conditions, the date of that failure, if it occurred, is shown as the 'Failure to respond' date.

NDMAS-Assigned Failure Date	Thermocouple	AGR thermocouple Table Notes	'Failure to respond' Date
11/30/06	Capsule 5 TC-2	Failed 11/30/06 during fabrication	11/30/06
11/30/06	Capsule 1 TC-1#	Failed 11/30/06 during fabrication	12/02/07
11/30/06	Capsule 2 TC-1*	Failed 11/30/06 during fabrication	04/28/08
04/01/07	Capsule 3 TC-2*	Failed mid 2 <sup>nd</sup> cycle	04/29/08
04/22/07	Capsule 2 TC-2†*	Failed 04/22/07 after end of 2 <sup>nd</sup> cycle	04/28/08
9/22/07	Capsule 1 TC-2‡	Failed mid 3 <sup>rd</sup> cycle	9/22/07
09/30/07	Capsule 2 TC-3	Failed 09/30/07 after end of 3 <sup>rd</sup> cycle	04/28/08
12/02/07	Capsule 3 TC-3	Failed 12/02/07 after end of 4 <sup>th</sup> cycle	11/30/07
03/09/08	Capsule 3 TC-1	Failed 03/09/08 after end of 6 <sup>th</sup> cycle	NA
10/16/08	Capsule 4 TC-3	Failed 10/16/08 after end of 9th cycle	11/20/08

<sup>#</sup> As a result of the neon injection tests, it was concluded that Capsule 1 TC-1 had failed via formation of a virtual junction near the location of Capsule 6.

<sup>†</sup> Capsule 2 TC-2 shows declining temp while other thermocouples (1 and 3) are increasing, beginning early in the 2nd cycle.

<sup>‡</sup> No apparent failure before total failure in second full-power period of 3rd cycle (139B).

<sup>\*</sup> These thermocouples provided measurements in excess of 200°C difference from calculated values (Ambrosek 2007), indicating that the thermocouples had either formed virtual junctions outside of the intended capsule or had developed another form of malfunction.

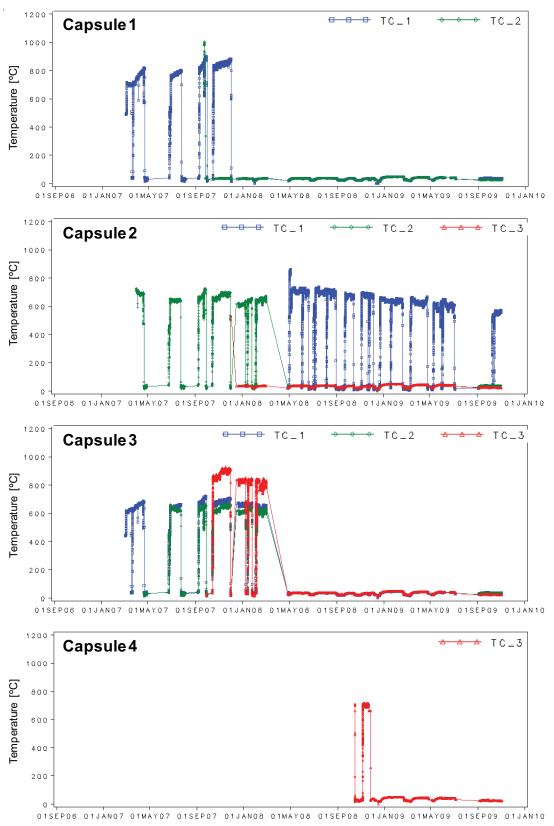


Figure 7. Failed thermocouple temperature data from AGR-1, based on information provided to NDMAS by the NGNP technical leads.

#### 5. FPMS DATA

## 5.1 Description of the Data Stream

The gas effluent in each of the six capsules of the AGR-1 experiment is monitored by a radiation detector system consisting of a sodium iodide detector for measuring gross gamma activity and a high purity germanium spectrometer for quantifying isotopic activities. The collection of radiation measurement systems is known as the AGR-1 FPMS. The two types of FPMS data provided to NDMAS by the FPMS technical staff are:

- Processed (by FPMS staff) spectral files consisting of radionuclide release rates (in atoms/sec) and release-to-birthrate (R/B) ratios for 12 noble gas fission product gases (Kr-85m, Kr-87, Kr-88, Kr-89, Kr-90, Xe-131m, Xe-133, Xe-135, Xe-135m, Xe-137, Xe-138, and Xe-139). These data are classified as *Qualified* data.
- Gross gamma data consisting of sequential 8-hour binary files of 3.5-sec gross gamma counts.

Gross gamma count data are processed by NDMAS to provide graphical displays on the INL NDMAS Web portal (https://sasweb.inl.gov). These data are used to provide an early indicator of potential fuel particle failures. As such, they do not undergo any capture or accuracy testing within NDMAS, are not qualified, and are not stored in the NDMAS SQL database. The native binary files are currently archived on FSISC1\Projects\SASDATA\SAS Projects\NGNP\NGNP\_Data\spectra.

Separate spectral release rate and R/B ASCII text files for each capsule were supplied to NDMAS at the end of each reactor cycle (six release files and six R/B files) throughout the AGR-1 experiment. In February 2010, FPMS data from all of 13 cycles of the AGR-1 test were reprocessed to correct the Kr-87 activity for interference from Xe-138 and the Kr-88 activity for spectral shifts as documented in PLN-3392, "Fission Product Monitoring System PCGAP Software Modifications and Operability Test Plan" (in press).

Each data record in the processed FPMS files consists of fission product release rates (in atoms/sec) or R/B data (unitless) with associated uncertainty (%) over nominal 8-hour counting intervals as shown in Table 12. A detailed description of the FPMS data processing done by the FPMS technical staff can be found in the User's Guide for the Fission Product Monitoring System (Drigert, Scates, and Walter 2009) and PLN-3392. Qualification of the processed data in these files is performed outside of NDMAS by the FPMS technical staff and documented in ECAR-907 (Scates 2010) for all reactor cycles. This ECAR is approved by the VHTR-TDO QA Lead and the VHTR-TDO Irradiations Technical Lead. Data capture testing was performed within NDMAS to ensure the data stored in the database are identical to the original data (see next section). In addition, NDMAS performed data analysis (e.g., statistical distributions and plotting) and is displaying the results on the NDMAS Web portal to assist researchers in data interpretation.

# 5.2 FPMS Data Processing within NDMAS

#### 5.2.1 Gross Gamma Counts

The gross gamma count data are captured in their original binary file format, converted to text data, processed within SAS, and displayed as graphs on the "FPMS Gross Gamma Data" page of the NDMAS Web Portal (https://sasweb.inl.gov). The raw binary (.dgt) files are automatically transferred on a daily basis by FPMS staff to \FSISC1\Projects\SASDATA\SAS Projects\NGNP\NGNP\_Data\spectra\[ATR cycle#] where they are archived and accessed for SAS plotting.

Table 12. FPMS release and R/B data provided to NDMAS.

Variable Name	Description
---------------	-------------

Variable Name	Description
SpecID	Sample record name in the form $GxYmmddhhzz$ , where $Gx =$ detector number $(G1 - G7)$ , $Y =$ last digit of year, mm = month $(01 - 12)$ , dd = day of month $(01 - 31)$ , hh = hour of day $(00 - 23)$ , zz = index number for detector restart
Date/Time	Local (MST or MDT) start time of sample
<flow></flow>	Detector gas flow rate in standard cm <sup>3</sup> per second
n	Number of gas flow readings used in the FPMS post-processing
Kr_85M_Rel/_Err	Release rate (atoms/s) and associated error (%) for Kr-85m (2 variables)
Kr_87_Rel/_Err	Release rate (atoms/s) and associated error (%) for Kr-87 (2 variables)
Kr_88_Rel/_Err	Release rate (atoms/s) and associated error (%) for Kr-88 (2 variables)
Kr_89_Rel/_Err	Release rate (atoms/s) and associated error (%) for Kr-89 (2 variables)
Kr_90_Rel/_Err	Release rate (atoms/s) and associated error (%) for Kr-90 (2 variables)
Xe_131M_Rel/_Err	Release rate (atoms/s) and associated error (%) for Xe-131m (2 variables)
Xe_133_Rel/_Err	Release rate (atoms/s) and associated error (%) for Xe-133 (2 variables)
Xe_135_Rel/_Err	Release rate (atoms/s) and associated error (%) for Xe-135 (2 variables)
Xe_135M_Rel/_Err	Release rate (atoms/s) and associated error (%) for Xe-135m (2 variables)
Xe_137_Rel/_Err	Release rate (atoms/s) and associated error (%) for Xe-137 (2 variables)
Xe_138_Rel/_Err	Release rate (atoms/s) and associated error (%) for Xe-138 (2 variables)
Xe_139_Rel/_Err	Release rate (atoms/s) and associated error (%) for Xe-139 (2 variables)
Kr_85M_Rat/_REr	R/B ratio and associated error (%) for Kr-85m
Kr_87_Rat/_REr	R/B ratio and associated error (%) for Kr-87)
Kr_88_Rat/_REr	R/B ratio and associated error (%) for Kr-88
Kr_89_Rat/_REr	R/B ratio and associated error (%) for Kr-89
Kr_90_Rat/_REr	R/B ratio and associated error (%) for Kr-90
Xe_131M_Rat/_REr	R/B ratio and associated error (%) for Xe-131m
Xe_133_Rat/_REr	R/B ratio and associated error (%) for Xe-133
Xe_135_Rat/_REr	R/B ratio and associated error (%) for Xe-135
Xe_135M_Rat/_REr	R/B ratio and associated error (%) for Xe-135m
Xe_137_Rat/_REr	R/B ratio and associated error (%) for Xe-137
Xe_138_Rat/_REr	R/B ratio and associated error (%) for Xe-138
Xe_139_Rat/_REr	R/B ratio and associated error (%) for Xe-139

Specific data processing steps for the SAS plotting of the gross gamma data are:

- 1. Daily run of 'Read\_Binary\_GrossGamma.bat,' located on \\Sasngnp\\NGNP\\NDMAS Version 1.1\\FPMS\\GrossGamma\\Capture.
- 3. Plots of the data are developed in the SAS E-Guide file, 'GrossGammaPlots.egp,' located on \\Sasngnp\NGNP\NDMAS Version 1.1\FPMS\GrossGamma\Graphics. This file contains three stored

processes that control processing of the (1) "Plot Recent Gross Gamma Counts" – a 7-day plot of the most recent processed data, (2) "Plot Short Term Gross Gamma Counts" – a plot of the data for any user-selected time period <24 hours, and (3) "Plot Long Term Gross Gamma Counts" – a plot of the data for any user-selected time period ≥24 hours.

#### 5.2.2 Release and R/B Data

The six capsule-specific release rate and R/B data files for each ATR reactor cycle are pushed by FPMS technical staff to server location \\\FSISC1\\Projects\\AGRData\\BirthRates\[ATR cycle\] name]. Each cycle-specific set of files comprised an FPMS data package for processing within NDMAS. NDMAS processing for these files is summarized in Figure 8.

#### **FPMS Raw Data:**

- Copy files from FSISC1 to Sasngnp
- Rename each file (remove "#")

\\Sasngnp\ NGNP\ NGNP\_Data\ AGR-1\ FPMS data\ Clean\ BirthRates\ [cycle #] Release \_D\*.txt (6 files per cycle, capsules 1-6) Ratios D\*.txt (6 files per cycle, capsules 1-6)

#### **FPMS SAS Data Sets:**

\\Sasngnp\ Ngnp\ AGR 1\ NDMAS Version 1.1

· Update or build FPMS dataset.egp

that there are no obvious data processing errors in the source files:

- Builds/appends all cycle data: AGR01.FPMS\_Wide
- Push to SQL\_NDMAS (SQL database)
- Combine\_Irrad\_Power\_FPMS.egp (merged AGR-1 data)
  - Pull from SQL database to Depot: N\_Depot.FPMS\_1
  - Merge with irradiation/power data: N\_Depot.AGR01\_DATA
  - Export to Data Mart: N\_Mart.AGR01\_DATA
  - Create cube for Tabular Drilldown plots: AGR01 Data.cube

Figure 8. SAS processing of FPMS data (radionuclide release rates and R/B ratios).

# 5.3 Description of FPMS Data Qualification Tests

The FPMS release and R/B data are in the *Qualified* data category. Two general types of qualification tests are performed on these data in NDMAS:

- Capture tests verify that there are no simple raw data processing errors in the source files and that the
  data captured and stored within the NDMAS database are identical to the source data provided to
  NDMAS.
- Accuracy tests verify that the data are an accurate representation of the system parameters they are intended to measure.

The qualification tests for the FPMS release and R/B data are listed in the 'NDMAS Test Library.srx'on 'Qualification' page of the NDMAS Web portal (<a href="https://sasweb.inl.gov">https://sasweb.inl.gov</a>). Two time-related capture tests are currently performed on these data using the SAS E-Guide file, '\\SASNGNP\\\GNP\\\DMAS \\Version 1.1\\\Vault\_\PushPull\\\Update \\operator \text{build FPMS dataset.egp}' to check

- Test to ensure data records are in chronological order; if a data record is not in chronological order, an error is recorded for that record in the SAS dataset.
- Test to ensure the date/time entries for each data record are consistent with those in the SpecID variable in the data file (sample record ID). SpecID is in the form "GxYmmddhhzz," where Gx = detector number (G1–G7), y = last digit of year (e.g., 9 for 2009), mm = month (00–12), dd = day of month (01–31), hh = hour of day (00–23), and zz = index number for detector restart (e.g., 00 = initial start). If the SpecID does not match the sample date/time, an error is recorded for that record in the SAS dataset.

A final capture test is performed in the same SAS E-Guide file to verify that the data captured and stored within the NDMAS SQL database are identical to the source data provided to NDMAS. This test uses a SAS procedure (PROC-COMPARE) to compare the SAS dataset used as input to the SQL database with the SQL database output. Records of these test results are maintained for each FPMS reactor cycle data package processed within NDMAS.

The accuracy of the release and R/B data files for all 13 AGR-1 reactor cycles is being verified by the FPMS technical staff in ECAR-907. After ECAR approval notification, the NDMAS staff will log an ECAR "accuracy test" as complete in the SQL database for each AGR-1 cycle data package. FPMS release and R/B data for a given reactor cycle are considered *Qualified* after successful completion and documentation (i.e., database logging) of both the NDMAS capture tests and approval of the ECAR.

# 5.4 Verify FPMS Data QA Documentation

The data collection process includes writing a plan describing how data will be collected and the QA activities associated with that data. Review of the plan assures that the planned work will generate data of appropriate quality for use in the NQA-1 program. Metadata generated by the initial documentation, audits, and acceptance inspection provide the evidence that data meet the requirements of an NQA-1 data collection program. This is documented at the data stream level and, for FPMS data, at the data package level (for each end-of-cycle file package).

Documentation of the QA Program in NDMAS is primarily accomplished by reference to documents. These include plans, audit reports, nonconformance reports, and ECARs approved by the VHTR-TDO QA Lead. The following documents provide evidence that the data for the FPMS data stream meet the requirements of NQA-1, Part 1:

- 1. J. T. Maki, AGR-1 Irradiation Experiment Test Plan, INL/EXT-05-00593, Rev 2, March 2007.
- 2. D. M. Scates and J. K. Hartwell, *Fission Product Monitoring System Operability Test Plan for the AGR-1 Experiment: Phase II*, PLN-2350, December 2006.
- 3. D. M. Scates, "Fission Product Monitoring System PCGAP Software Modification and Operability Test Plan," PLN-3392, in press February 2010.
- 4. M. W. Drigert, D. M. Scates, and J. B. Walter, "Users' Guide for the Fission Product Monitoring System," GDE-503, Rev 0, 04/16/09.
- J. K. Hartwell, J. B. Walter, D. M. Scates, and M. W. Drigert, *Determination of the AGR-1 Capsule to FPMS Spectrometer Transport Volumes from Leadout Flow Test Data*, INL/EXT-07-12494, May 2007.
- 6. D. M. Scates, "Release to Birth Ratios for AGR-1 Operating Cycles 138B through 145A," ECAR-907 (in press February 2010).

## 5.5 FPMS Data Analysis and Web Display

Data analyses and presentations not currently associated with FPMS data qualification are performed on the FPMS data stored in the NDMAS SQL database to assist in data interpretation by researchers. The results are displayed on the NDMAS Web portal (<a href="https://sasweb.inl.gov">https://sasweb.inl.gov</a>, 'FPMS Release and R/B Data' page). ATR cycle-specific release and R/B datasets are accessible using a SAS "Data Exploration" tool which allows user selection of display variables; filtering by date, capsule, or response value; plotting of small datasets; and download of the data to an Excel spreadsheet. Comprehensive data plots and distribution analyses for all cycles and capsules are also posted on the web page (Figures 9 through 12). Additional FPMS data analyses (e.g., correlation of fission product release rates with capsule thermocouple temperatures) can be added to the Web page at the request of users.

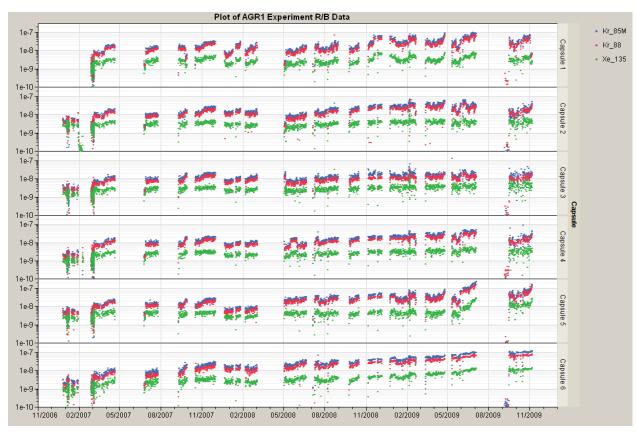


Figure 9. Example of an R/B data plot available on the NDMAS Web portal.

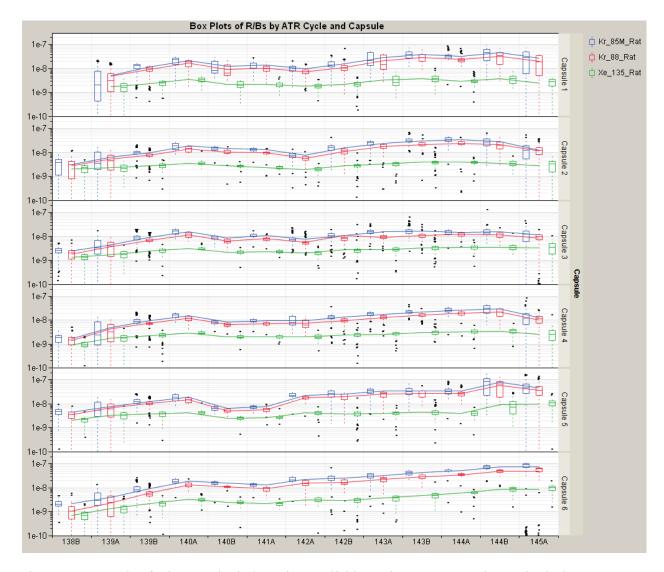


Figure 10. Example of release and R/B box plots available on the NDMAS Web portal. The boxes represent the 75% and 25% quartiles, with the center line representing the median R/B for each ATR cycle by capsule.

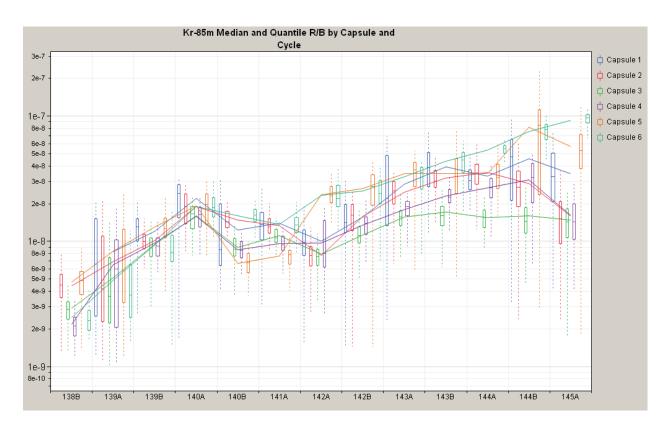


Figure 11. Example of FPMS box plots on the NDMAS Web portal showing Kr-85m R/B variations across capsules.

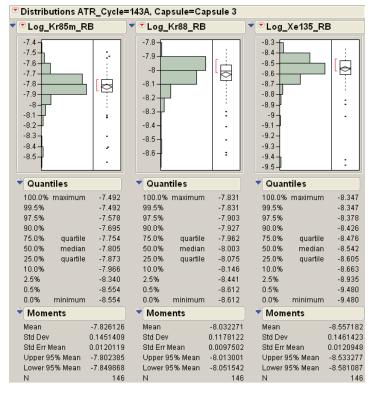


Figure 12. Example of [Log] R/B data distribution analysis available on the NDMAS Web portal.

#### 5.6 FPMS Data Qualification Status

The overall qualification status of all data stored in NDMAS is provided on the *Qualification* page of the NDMAS Web portal (<a href="https://sasweb.inl.gov">https://sasweb.inl.gov</a>). All of the FPMS data packages received have passed NDMAS capture testing with no identified errors, and the most current version of the data (January 2010 processing date) have been made available on the NDMAS web portal (FPMS Release and R/B Data page). Final qualification of these data will be formally documented within NDMAS after VHTR TDO QA approval of ECAR-907, which has been submitted by the FPMS technical staff and is currently under review. The FPMS R/B data may be revised in the future based on revisions or refinements in the modeled birth rate data used to calculate the R/B values. Revisions to the FPMS data such as these will be recorded with a source file date stamp in both the NDMAS database and Web portal to ensure users have the most recent data.

The ATR cycle data package start and end dates, number of records, and the most current FPMS source file dates stored in the NDMAS database are listed in Table 13.

Table 13. Current NDMAS database status of AGR-1 FPMS release and R/B data.

ATR Cycle Data Package/ID <sup>a</sup>	Start Date/Time <sup>b</sup>	End Date/Time <sup>b</sup>	Number of Records <sup>c</sup>	Source File Dates <sup>d</sup>
138B/75	25DEC2006:00:13	10FEB2007:21:02	33,120	2/2/2010
139A/76	27FEB2007:01:45	23APR2007:08:40	77,712	2/2/2010
139B/77	23JUN2007:20:32	30SEP2007:05:50	57,312	1/31/2010
140A/78	14OCT2007:19:48	02DEC2007:19:00	44,160	1/31/2010, 2/1/2010
140B/79	21DEC2007:07:52	28JAN2008:23:56	34,272	2/2/2010
141A/80	03FEB2008:05:45	02MAR2008:23:56	25,680	1/31/2010
142A/81	01MAY2008:06:47	23JUN2008:08:19	47,376	1/31/2010
142B/82	03JUL2008:07:40	01SEP2008:04:00	55,440	1/30/2010
143A/83	22SEP2008:07:24	10DEC2008:07:39	60,384	1/30/2010
143B/84	21DEC2008:10:01	23FEB2009:14:57	64,128	1/30/2010
144A/85	11MAR2009:16:34	26APR2009:20:34	41,712	1/30/2010
144B/86	09MAY2009:11:44	05JUL2009:23:17	52,416	1/30/2010
145A/88	04SEP2009:08:03	09NOV2009:10:54	59,040	2/9/2010
		Total number of records =	652,752	

a. Database identification number for ATR cycle.

### 5.7 FPMS Data Problems and Resolution

Several revisions to the processed FPMS data have been generated by the FPMS technical staff after the initially-supplied preliminary data files were loaded into NDMAS, requiring that the NDMAS data be deleted, reloaded, and retested. These revisions were made because of a number of technical issues discovered after the initial data package submittal, including a discrepancy between the FPMS time scale (calendar days) and that used for modeled birthrates (effective power days), an error in the assumed reactor startup time for ATR Cycle 143A, and a problem on the spectral analysis of Kr-88. These issues led to the recent reprocessing of all FPMS release and R/B data files for all 13 AGR-1 cycles. The primary NDMAS issue with revisions to the FPMS data packages is how to best track and report these revisions within the NDMAS SQL database and on the Web portal, to ensure researchers are using the

o. Source (raw data) date/time of first and last FPMS data record in that data package.

c. Single response variable records in the NDMAS (tall) database.

d. Latest source file date supplied by FPMS technical staff.

most current data. Old versions of FPMS data files are not currently maintained in the NDMAS SQL database, although they are maintained by the FPMS technical staff on the FSISC1 server. Data files available on the NDMAS Web portal ('FPMS Release and R/B Data' page) have the most recent source file date in the file name (e.g., Release\_143A\_01312010) and a text warning that all data files available for downloading are subject to revisions.

# 6. ATR OPERATING CONDITIONS DATA

# 6.1 Description of the Data Stream

ATR operators collect data describing the configuration and state of the reactor at high frequency (sub-minute intervals), and some of those parameters are collected and stored in the NDMAS to facilitate various analyses of the AGR experimental data (e.g., thermocouple temperatures). At the beginning of the AGR-1 experiment, ATR operating conditions data were provided in miscellaneous files that contained data recorded at 1-hour intervals. Since April 25, 2008, ATR data have been provided to NDMAS in daily files with measurements at 1-minute intervals. The data provided and stored in NDMAS include the parameters summarized in Table 14.

Table 14. ATR operating conditions variables stored in NDMAS.

Variable NDMAS         Description         Raw Data from 6-18- 08:00:00:28         Units           TNRD         Number of readings total         1.00         [-]           FPRD         Number of readings at full power         1.00         [-]           FPTM         Time at full power         1.00         [-]           FPTM         Time at full power         1.00         [-]           FPTM         Time at full power         1.00         [-]           LCNW         * Current power for NW lobe         22.94         MW           LCNE         * Current power for NE lobe         18.05         MW           LCS         * Current power for SW lobe         24.70         MW           LCSE         * Current power for SE lobe         23.11         MW           LINW         Integrated power for NW lobe         1024.75         MW           LINE         Integrated power for SE lobe         1097.50         MW           LISE         Integrated power for SW lobe         1105.75         MW           LISE         Integrated power for quadrant 1         22.50         MW           TPQ1         Thermal power for quadrant 1         22.50         MW           TPQ2         Thermal power for quadrant 2         29.52 <th>Table 14.</th> <th>ATR operati</th> <th>ing conditions variables stored in NDMAS.</th> <th></th> <th></th>	Table 14.	ATR operati	ing conditions variables stored in NDMAS.		
Variable NDMAS         Description         from 6-18-08(00:00:28)         Units           TNRD         Number of readings total         1.00         [-]           FPRD         Number of readings at full power         1.00         [-]           FPTM         Time at full power         1.00         [-]           LCNW         * Current power for NW lobe         22.94         MW           LCNE         * Current power for NE lobe         18.05         MW           LC C         * Current power for SW lobe         25.20         MW           LCSW         * Current power for SW lobe         24.70         MW           LCSE         * Current power for SE lobe         23.11         MW           LINE         Integrated power for NW lobe         1024.75         MW           LINE         Integrated power for NE lobe         801.69         MW           LISE         Integrated power for SW lobe         1105.75         MW           LISW         Integrated power for SU lobe         1105.75         MW           LISE         Integrated power for quadrant 1         22.50         MW           TPQ1         Thermal power for quadrant 1         22.50         MW           TPQ2         Thermal power for quadrant 2         <				Example of	
Variable NDMAS         Description         08:00:00:28         Units           TNRD         Number of readings total         1.00         [-]           FPRD         Number of readings at full power         1.00         [-]           FPTM         Time at full power         1.00         [-]           LCNW         * Current power for NW lobe         22.94         MW           LCNE         * Current power for NE lobe         18.05         MW           LC C         * Current power for NW lobe         25.20         MW           LCSW         * Current power for SW lobe         24.70         MW           LCSE         * Current power for SW lobe         23.11         MW           LINW         Integrated power for NW lobe         1024.75         MW           LINE         Integrated power for NE lobe         801.69         MW           LISW         Integrated power for SW lobe         1105.75         MW           LISW         Integrated power for SW lobe         1105.75         MW           LISW         Integrated power for Quadrant 1         22.50         MW           TPQ1         Thermal power for quadrant 1         22.50         MW           TPQ2         Thermal power for quadrant 2         29.52 <td></td> <td>•</td> <td></td> <td></td> <td></td>		•			
TNRD					
FPRD         Number of readings at full power         1.00         [-]           FPTM         Time at full power         1.00         [-]           LCNW         * Current power for NW lobe         22.94         MW           LCNE         * Current power for NE lobe         18.05         MW           LC C         * Current power for SW lobe         25.20         MW           LCSW         * Current power for SW lobe         24.70         MW           LCSE         * Current power for SE lobe         23.11         MW           LINE         Integrated power for SE lobe         1024.75         MW           LINE         Integrated power for NW lobe         1097.50         MW           LISW         Integrated power for C lobe         1097.50         MW           LISW         Integrated power for SW lobe         1105.75         MW           LISW         Integrated power for SE lobe         1023.88         MW           N16R         0.70         0         0.70         0           TPQ1         Thermal power for quadrant 1         22.50         MW           TPQ2         Thermal power for quadrant 2         29.52         MW           TPQ4         Thermal power for quadrant 4         29.21		NDMAS	1		Units
FPTM         Time at full power         1.00         [-]           LCNW         *         Current power for NW lobe         22.94         MW           LCNE         *         Current power for NE lobe         18.05         MW           LC C         *         Current power for C lobe         25.20         MW           LCSW         *         Current power for SW lobe         24.70         MW           LCSE         *         Current power for SE lobe         23.11         MW           LINW         Integrated power for SE lobe         801.69         MW           LINW         Integrated power for NE lobe         801.69         MW           LISW         Integrated power for SW lobe         1105.75         MW           LISW         Integrated power for SE lobe         1023.88         MW           N16R         0.70         0         0.70           TPQ1         Thermal power for quadrant 1         22.50         MW           TPQ2         Thermal power for quadrant 2         29.52         MW           TPQ3         Thermal power for quadrant 4         29.21         MW           TPSM         *         Thermal power for quadrant 4         29.21         MW           TPSM<				1.00	[-]
CURN					[-]
CUNE   * Current power for NE lobe   18.05   MW	FPTM		Time at full power	1.00	[-]
LC_C         * Current power for C lobe         25.20         MW           LCSW         * Current power for SW lobe         24.70         MW           LCSE         * Current power for SE lobe         23.11         MW           LINW         Integrated power for NW lobe         1024.75         MW           LINE         Integrated power for NE lobe         801.69         MW           LISW         Integrated power for SW lobe         1097.50         MW           LISW         Integrated power for SW lobe         1105.75         MW           LISW         Integrated power for SE lobe         1023.88         MW           N16R         0.70         0.70         0.70           TPQ1         Thermal power for quadrant 1         22.50         MW           TPQ2         Thermal power for quadrant 2         29.52         MW           TPQ3         Thermal power for quadrant 3         32.54         MW           TPQ4         Thermal power - sum         113.77         MW           TPTO         * Thermal power - total         112.88         MW           REG1         * Position of regulating rod 1         28.65         [in]           REG2         * Position of shim cylinders         88.50         [degrees		*	Current power for NW lobe	22.94	MW
CCSW   * Current power for SW lobe   24.70 MW		*	Current power for NE lobe	18.05	
Current power for SE lobe   23.11 MW	LC_C	*	Current power for C lobe	25.20	MW
LINW Integrated power for NW lobe	LCSW	*	Current power for SW lobe	24.70	MW
LINE Integrated power for NE lobe 801.69 MW  LI C Integrated power for C lobe 1097.50 MW  LISW Integrated power for SW lobe 1105.75 MW  LISE Integrated power for SE lobe 1023.88 MW  N16R 0.70  TPQ1 Thermal power for quadrant 1 22.50 MW  TPQ2 Thermal power for quadrant 2 29.52 MW  TPQ3 Thermal power for quadrant 3 32.54 MW  TPQ4 Thermal power for quadrant 4 29.21 MW  TPSM * Thermal power - sum 113.77 MW  TPTO * Thermal power - total 112.88 MW  REG1 * Position of regulating rod 1 28.65 [in]  REG2 * Position of regulating rod 2 47.73 [in]  N3D4 * Position of shim cylinders 88.50 [degrees]  E1D2 * Position of shim cylinders 92.98 [degrees]  E3D4 * Position of shim cylinders 92.98 [degrees]  S1D2 * Position of shim cylinders 92.98 [degrees]  S3D4 * Position of shim cylinders 115.48 [degrees]  W1D2 * Position of shim cylinders 93.52 [degrees]  N1D2 * Position of shim cylinders 93.52 [degrees]  N1D2 * Position of shim cylinders 93.52 [degrees]  PCIT * Reactor process water inlet temperature 113.16 [°F]	LCSE	*	Current power for SE lobe	23.11	MW
LI C         Integrated power for C lobe         1097.50         MW           LISW         Integrated power for SW lobe         1105.75         MW           LISE         Integrated power for SE lobe         1023.88         MW           N16R         0.70         TOPQ1         Thermal power for quadrant 1         22.50         MW           TPQ1         Thermal power for quadrant 2         29.52         MW           TPQ2         Thermal power for quadrant 3         32.54         MW           TPQ3         Thermal power for quadrant 4         29.21         MW           TPQ4         Thermal power - sum         113.77         MW           TPTO         * Thermal power - total         112.88         MW           REG1         * Position of regulating rod 1         28.65         [in]           REG2         * Position of regulating rod 2         47.73         [in]           N3D4         * Position of shim cylinders         88.50         [degrees]           E1D2         * Position of shim cylinders         88.50         [degrees]           S1D2         * Position of shim cylinders         92.98         [degrees]           S1D2         * Position of shim cylinders         92.98         [degrees] <td< td=""><td>LINW</td><td></td><td>Integrated power for NW lobe</td><td>1024.75</td><td>MW</td></td<>	LINW		Integrated power for NW lobe	1024.75	MW
LISW Integrated power for SW lobe 1105.75 MW  LISE Integrated power for SE lobe 1023.88 MW  N16R 0.70  TPQ1 Thermal power for quadrant 1 22.50 MW  TPQ2 Thermal power for quadrant 2 29.52 MW  TPQ3 Thermal power for quadrant 3 32.54 MW  TPQ4 Thermal power for quadrant 4 29.21 MW  TPSM * Thermal power - sum 113.77 MW  TPTO * Thermal power - total 112.88 MW  REG1 * Position of regulating rod 1 28.65 [in]  REG2 * Position of regulating rod 2 47.73 [in]  N3D4 * Position of shim cylinders 88.50 [degrees]  E1D2 * Position of shim cylinders 92.98 [degrees]  E3D4 * Position of shim cylinders 92.98 [degrees]  S1D2 * Position of shim cylinders 92.98 [degrees]  S3D4 * Position of shim cylinders 115.48 [degrees]  W1D2 * Position of shim cylinders 93.52 [degrees]  W1D2 * Position of shim cylinders 93.52 [degrees]  N1D2 * Reactor process water inlet temperature 113.16 [°F]	LINE		Integrated power for NE lobe	801.69	MW
LISE         Integrated power for SE lobe         1023.88         MW           N16R         0.70         0.70           TPQ1         Thermal power for quadrant 1         22.50         MW           TPQ2         Thermal power for quadrant 2         29.52         MW           TPQ3         Thermal power for quadrant 3         32.54         MW           TPQ4         Thermal power - sum         113.77         MW           TPTO         * Thermal power - total         112.88         MW           REG1         * Position of regulating rod 1         28.65         [in]           REG2         * Position of shim cylinders         88.50         [degrees]           E1D2         * Position of shim cylinders         88.50         [degrees]           E3D4         * Position of shim cylinders         92.98         [degrees]           S1D2         * Position of shim cylinders         92.98         [degrees]           S3D4         * Position of shim cylinders         115.48         [degrees]           W1D2         * Position of shim cylinders         93.52         [degrees]           W3D4         * Position of shim cylinders         93.52         [degrees]           W1D2         * Position of shim cylinders         93.52<	LI_C		Integrated power for _C lobe	1097.50	MW
N16R         0.70           TPQ1         Thermal power for quadrant 1         22.50         MW           TPQ2         Thermal power for quadrant 2         29.52         MW           TPQ3         Thermal power for quadrant 3         32.54         MW           TPQ4         Thermal power for quadrant 4         29.21         MW           TPSM         * Thermal power - sum         113.77         MW           TPTO         * Thermal power - total         112.88         MW           REG1         * Position of regulating rod 1         28.65         [in]           REG2         * Position of regulating rod 2         47.73         [in]           N3D4         * Position of shim cylinders         88.50         [degrees]           E1D2         * Position of shim cylinders         88.50         [degrees]           E3D4         * Position of shim cylinders         92.98         [degrees]           S1D2         * Position of shim cylinders         92.98         [degrees]           W1D2         * Position of shim cylinders         115.48         [degrees]           W1D2         * Position of shim cylinders         93.52         [degrees]           N1D2         * Position of shim cylinders         93.52         [degrees	LISW		Integrated power for SW lobe	1105.75	MW
TPQ1Thermal power for quadrant 122.50MWTPQ2Thermal power for quadrant 229.52MWTPQ3Thermal power for quadrant 332.54MWTPQ4Thermal power for quadrant 429.21MWTPSM* Thermal power - sum113.77MWTPTO* Thermal power - total112.88MWREG1* Position of regulating rod 128.65[in]REG2* Position of regulating rod 247.73[in]N3D4* Position of shim cylinders88.50[degrees]E1D2* Position of shim cylinders88.50[degrees]E3D4* Position of shim cylinders92.98[degrees]S1D2* Position of shim cylinders92.98[degrees]S3D4* Position of shim cylinders115.48[degrees]W1D2* Position of shim cylinders115.48[degrees]W3D4* Position of shim cylinders93.52[degrees]N1D2* Position of shim cylinders93.52[degrees]N1D2* Position of shim cylinders93.52[degrees]PCIT* Reactor process water inlet temperature113.16[°F]	LISE		Integrated power for SE lobe	1023.88	MW
TPQ2 Thermal power for quadrant 2 29.52 MW  TPQ3 Thermal power for quadrant 3 32.54 MW  TPQ4 Thermal power for quadrant 4 29.21 MW  TPSM * Thermal power - sum 113.77 MW  TPTO * Thermal power - total 12.88 MW  REG1 * Position of regulating rod 1 28.65 [in]  REG2 * Position of regulating rod 2 47.73 [in]  N3D4 * Position of shim cylinders 88.50 [degrees]  E1D2 * Position of shim cylinders 88.50 [degrees]  E3D4 * Position of shim cylinders 92.98 [degrees]  S1D2 * Position of shim cylinders 92.98 [degrees]  S3D4 * Position of shim cylinders 115.48 [degrees]  W1D2 * Position of shim cylinders 115.48 [degrees]  W3D4 * Position of shim cylinders 93.52 [degrees]  N1D2 * Position of shim cylinders 93.52 [degrees]  N1D2 * Position of shim cylinders 93.52 [degrees]  N1D2 * Position of shim cylinders 93.52 [degrees]  PCIT * Reactor process water inlet temperature 113.16 [°F]	N16R		-	0.70	
TPQ3 Thermal power for quadrant 3 32.54 MW TPQ4 Thermal power for quadrant 4 29.21 MW TPSM * Thermal power - sum 113.77 MW TPTO * Thermal power - total 112.88 MW REG1 * Position of regulating rod 1 28.65 [in] REG2 * Position of regulating rod 2 47.73 [in] N3D4 * Position of shim cylinders 88.50 [degrees] E1D2 * Position of shim cylinders 88.50 [degrees] E3D4 * Position of shim cylinders 92.98 [degrees] S1D2 * Position of shim cylinders 92.98 [degrees] S1D2 * Position of shim cylinders 115.48 [degrees] W1D2 * Position of shim cylinders 115.48 [degrees] W3D4 * Position of shim cylinders 93.52 [degrees] N1D2 * Position of shim cylinders 93.52 [degrees] N1D2 * Position of shim cylinders 93.52 [degrees] N1D2 * Reactor process water inlet temperature 113.16 [°F]	TPQ1		Thermal power for quadrant 1	22.50	MW
TPQ4 Thermal power for quadrant 4 29.21 MW  TPSM * Thermal power - sum 113.77 MW  TPTO * Thermal power - total 112.88 MW  REG1 * Position of regulating rod 1 28.65 [in]  REG2 * Position of regulating rod 2 47.73 [in]  N3D4 * Position of shim cylinders 88.50 [degrees]  E1D2 * Position of shim cylinders 92.98 [degrees]  E3D4 * Position of shim cylinders 92.98 [degrees]  S1D2 * Position of shim cylinders 92.98 [degrees]  S3D4 * Position of shim cylinders 115.48 [degrees]  W1D2 * Position of shim cylinders 115.48 [degrees]  W3D4 * Position of shim cylinders 93.52 [degrees]  N1D2 * Position of shim cylinders 93.52 [degrees]  N1D2 * Reactor process water inlet temperature 113.16 [°F]	TPQ2		Thermal power for quadrant 2	29.52	MW
TPSM * Thermal power - sum  TPTO * Thermal power - total  REG1 * Position of regulating rod 1  REG2 * Position of regulating rod 2  N3D4 * Position of shim cylinders  E1D2 * Position of shim cylinders  E3D4 * Position of shim cylinders  E3D4 * Position of shim cylinders  E3D4 * Position of shim cylinders  S3D4 * Position of shim cylinders  S3D4 * Position of shim cylinders  W1D2 * Position of shim cylinders  W3D4 * Position of shim cylinders  W3D5 [degrees]  W3D6 * Position of shim cylinders  W3D7 * Position of shim cylinders  W3D6 * Position of shim cylinders  W3D7 * Position of shim cylinders  W3D7 * Position of shim cylinders  W3D8 * Position of shim cylinders  W3D9 * Position of shim cylinders  W3D6 * Position of shim cylinders  W3D7 * Position of shim cylinders  W3D7 * Position of shim cylinders  W3D8 * P	TPQ3		Thermal power for quadrant 3	32.54	MW
TPTO * Thermal power - total 112.88 MW  REG1 * Position of regulating rod 1 28.65 [in]  REG2 * Position of regulating rod 2 47.73 [in]  N3D4 * Position of shim cylinders 88.50 [degrees]  E1D2 * Position of shim cylinders 92.98 [degrees]  E3D4 * Position of shim cylinders 92.98 [degrees]  S1D2 * Position of shim cylinders 92.98 [degrees]  S3D4 * Position of shim cylinders 115.48 [degrees]  W1D2 * Position of shim cylinders 115.48 [degrees]  W3D4 * Position of shim cylinders 93.52 [degrees]  N1D2 * Position of shim cylinders 93.52 [degrees]  N1D2 * Reactor process water inlet temperature 113.16 [°F]	TPQ4		Thermal power for quadrant 4	29.21	MW
TPTO * Thermal power - total 112.88 MW  REG1 * Position of regulating rod 1 28.65 [in]  REG2 * Position of regulating rod 2 47.73 [in]  N3D4 * Position of shim cylinders 88.50 [degrees]  E1D2 * Position of shim cylinders 92.98 [degrees]  E3D4 * Position of shim cylinders 92.98 [degrees]  S1D2 * Position of shim cylinders 92.98 [degrees]  S3D4 * Position of shim cylinders 115.48 [degrees]  W1D2 * Position of shim cylinders 115.48 [degrees]  W3D4 * Position of shim cylinders 93.52 [degrees]  N1D2 * Position of shim cylinders 93.52 [degrees]  N1D2 * Reactor process water inlet temperature 113.16 [°F]	TPSM	*	Thermal power - sum	113.77	MW
REG2* Position of regulating rod 247.73 [in]N3D4* Position of shim cylinders88.50 [degrees]E1D2* Position of shim cylinders88.50 [degrees]E3D4* Position of shim cylinders92.98 [degrees]S1D2* Position of shim cylinders92.98 [degrees]S3D4* Position of shim cylinders115.48 [degrees]W1D2* Position of shim cylinders115.48 [degrees]W3D4* Position of shim cylinders93.52 [degrees]N1D2* Position of shim cylinders93.52 [degrees]PCIT* Reactor process water inlet temperature113.16 [°F]	TPTO	*		112.88	MW
REG2*Position of regulating rod 247.73[in]N3D4*Position of shim cylinders88.50[degrees]E1D2*Position of shim cylinders88.50[degrees]E3D4*Position of shim cylinders92.98[degrees]S1D2*Position of shim cylinders92.98[degrees]S3D4*Position of shim cylinders115.48[degrees]W1D2*Position of shim cylinders115.48[degrees]W3D4*Position of shim cylinders93.52[degrees]N1D2*Position of shim cylinders93.52[degrees]PCIT*Reactor process water inlet temperature113.16[°F]	REG1	*	Position of regulating rod 1	28.65	[in]
N3D4*Position of shim cylinders88.50[degrees]E1D2*Position of shim cylinders88.50[degrees]E3D4*Position of shim cylinders92.98[degrees]S1D2*Position of shim cylinders92.98[degrees]S3D4*Position of shim cylinders115.48[degrees]W1D2*Position of shim cylinders115.48[degrees]W3D4*Position of shim cylinders93.52[degrees]N1D2*Position of shim cylinders93.52[degrees]PCIT*Reactor process water inlet temperature113.16[°F]	REG2	*	Position of regulating rod 2	47.73	[in]
E3D4*Position of shim cylinders92.98[degrees]S1D2*Position of shim cylinders92.98[degrees]S3D4*Position of shim cylinders115.48[degrees]W1D2*Position of shim cylinders115.48[degrees]W3D4*Position of shim cylinders93.52[degrees]N1D2*Position of shim cylinders93.52[degrees]PCIT*Reactor process water inlet temperature113.16[°F]	N3D4	*	Position of shim cylinders	88.50	[degrees]
S1D2* Position of shim cylinders92.98 [degrees]S3D4* Position of shim cylinders115.48 [degrees]W1D2* Position of shim cylinders115.48 [degrees]W3D4* Position of shim cylinders93.52 [degrees]N1D2* Position of shim cylinders93.52 [degrees]PCIT* Reactor process water inlet temperature113.16 [°F]	E1D2	*	Position of shim cylinders	88.50	[degrees]
S3D4*Position of shim cylinders115.48[degrees]W1D2*Position of shim cylinders115.48[degrees]W3D4*Position of shim cylinders93.52[degrees]N1D2*Position of shim cylinders93.52[degrees]PCIT*Reactor process water inlet temperature113.16[°F]	E3D4	*	· ·	92.98	
S3D4*Position of shim cylinders115.48[degrees]W1D2*Position of shim cylinders115.48[degrees]W3D4*Position of shim cylinders93.52[degrees]N1D2*Position of shim cylinders93.52[degrees]PCIT*Reactor process water inlet temperature113.16[°F]	S1D2	*	Position of shim cylinders	92.98	[degrees]
W1D2*Position of shim cylinders115.48[degrees]W3D4*Position of shim cylinders93.52[degrees]N1D2*Position of shim cylinders93.52[degrees]PCIT*Reactor process water inlet temperature113.16[°F]	S3D4	*	Position of shim cylinders	115.48	
W3D4*Position of shim cylinders93.52[degrees]N1D2*Position of shim cylinders93.52[degrees]PCIT*Reactor process water inlet temperature113.16[°F]		*	· · · · · · · · · · · · · · · · · · ·		
N1D2       *       Position of shim cylinders       93.52       [degrees]         PCIT       *       Reactor process water inlet temperature       113.16       [°F]		*	· · · · · · · · · · · · · · · · · · ·		
PCIT * Reactor process water inlet temperature 113.16 [°F]		*	· · · · · · · · · · · · · · · · · · ·		
1 1 1		*	· · · · · · · · · · · · · · · · · · ·		
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	PCOT		Reactor process water outlet temperature	130.56	[°F]

Table 14. (continued).

14010 1 11	(continuea).			
			Example of	
	Captured		Raw Data from	
	by		6-18-	
Variable	NDMAS	Description	08:00:00:28	Units
RPWF	*	Reactor process water flow	43.70	
NERL	*	Position of NE neck shims (note 1)	100000	[-]
SERL	*	Position of SE neck shims (note 1)	111300	[-]
SWRL	*	Position of SW neck shims (note 1)	111210	[-]
NWRL	*	Position of NW neck shims (note 1)	111100	[-]
SROD		Safety rod limit switch status (note 2)		[-]
RDAS		Bit pattern sent by RDAS	5.00	[-]
CSUM		Checksum sent by RDAS	13048.00	[-]
RDCD		RDAS normal or abnormal (note 3)	0.00	[-]
RDTD		RDAS (DAC or DAN) transmitting data (note 4)	1.00	[-]
N16D	*	N16 system - normal or calibrate (note 5)	0.00	[-]
OSCD		OSC indication - normal or error (bad drums are	0.00	[-]
		indicated as zero) (note 6)		
WPMD		Water power calculator in use—system 1 or 2 (note 7)	0.00	[-]
SPRD		System power constraint	0.00	

1. Neck shim rod limit status:

Rods 1 to 6 are presented by six characters left to right. Leading zeros are omitted.

- 1 = Inserted 0 = Withdrawn
- 3 = Reg Rod # 1 (SE) 2 = Reg Rod # 2 (SW)
- 2. Safety rod limit status:

Rods N-E-SE-S-SW-W are presented by six characters left to right. Leading zeros are omitted.

- 1 =Inserted 0 =Withdrawn
- 9 = Both or neither limit switch
- 3. RDCD RDAS status (0 = Normal, 1 = Abnormal)
- 4. RDTD RDAS system transmitting data (0 = DAC, 1 = DAN)
- 5. N16D N16 system status (0 = Normal, 1 = Calibrate)
- 6. OSCD Outer shim cylinders (0 = Normal, 1 = Error)
- 7. WPMD Water power calculator (0 = System one, 1 = System two)
- 8. SPRD System power constraint (0 = Constrained, 1 = Unconstrained)

# 6.2 ATR Data Processing within NDMAS

Data processing and storage within NDMAS occurs via the following process shown in Figure 13. After raw ATR data files each covering one day of measurements are placed in folders on the FSISC1 server (AGR Data folder), those files are copied to an NDMAS server location devoted to raw data storage. A batch file is then run to update the NDMAS-maintained list of relevant file names in that directory, from which new file names will be processed. A SAS Enterprise Guide project entitled 'Update or build ATR dataset.egp' subsequently reads the new data files and assembles the data into a single SAS dataset, which represents the primary source for ATR data within NDMAS. Those data are averaged to 5-minute intervals to match the interval used for fuel irradiation monitoring and then stored in the NDMAS SQL database. Processing and storage in NDMAS occurs approximately once per week so that generally, numerous data files are processed and entered as a single package.

### Raw ATR operating conditions data:

FSISC server location:

 \FSISC1\Projects\AGRData\reactor data\RP daily Daily file names

• 'd'followed by date in 'yyyy-mm-dd' format

#### ATR operating conditions processing steps:

- 1) Copy new file folders from FSISC1 server to:
  - \\Sasngnp\NGNP\NGNP\_Data\AGR-1\reactor data\RP daily
- 2) FROM NDMAS directory, 'Vault\_PushPull'
  - 1) Run batch file 'update.bat'
    - Creates/updates the list of relevant file names to be processed
  - 2) Run Enterprise Guide Project file 'Update or build ATR dataset.egp' to construct SAS dataset for new data
    - Builds/appends all new data as SAS dataset
    - Pushes new data to SQL\_NDMAS (NDMAS vault)
    - Checks that vault data is correctly entered
  - 3) Update log file 'Irradiation capture-push instructions and log.doc'
  - 4) Run Enterprise Guide Project file '<u>Vault tests.egp</u>' and examine any failed data
  - 5) Resolve failed data as necessary
  - 6) Run Enterprise Guide Project file 'Combine\_Irrad\_ATR\_FPMS.egp' to populate N\_MART directory with new SAS data sets and cubes containing updated irradiation data

Figure 13. Raw ATR operating conditions data and processing steps.

Data processing includes the following error checks to ensure that the data are accurately captured:

- Dates are checked for proper syntax and chronology.
- Data are checked for duplicated measurement times with conflicting variable values.
- Completed SAS datasets are visually inspected and compared against the raw data files.
- A MST is assigned to each measurement that corrects for the switching between MST and MDT that occurs in the raw data. The switch to MDT leads to repeated measurement times with different variable values, while the switch to standard time leads to a gap in measurement times. The process of detecting the MDT shifts is not fully automated, because the changes are not always made at the correct date and time. The data is manually checked to find MDT shifts on dates/times that do not correspond with national shift time.
- The process of entering each data packages is recorded in an electronic log with appropriate notes about any problems or corrections encountered. After being entered into the NDMAS SQL database, each data package is compared to the SAS dataset from which it was built to ensure that the data were correctly stored. Results are stored in the electronic log "ATR capture-push instructions and log.doc."
- ATR parameters that reflect internal testing of the ATR system are used to identify potential problems
  with data from instruments or systems being tested. Lobe powers, for example, can fluctuate during
  calibration of the N16 system. The calibration system status indicators can thus be used to eliminate
  those data from datasets used for neutronics or other analyses.

## 6.3 ATR Data Qualification

NDMAS conducts routine error testing on collected ATR data, but ATR operating conditions data are qualified by the quality control procedures of the ATR, not by the VHTR program or NDMAS. Technical Specifications for nuclear power plants define operational limits and conditions as a way to assure that the plant operates safely and in a manner that is consistent with the assumptions made in the plant safety analysis. Plant Technical Specifications are strictly followed during all stages of plant operation, and operating conditions monitoring data are collected from the plant to demonstrate compliance. BEA operates ATR for DOE under the *Price-Anderson Amendments Act*, which indemnifies DOE contractors from costs related to public liability for operating a nuclear facility. However, DOE is required to take enforcement actions against indemnified contractors for violations of nuclear safety requirements; that is, for operating the reactor outside the Technical Specifications. Data collected to monitor ATR operating conditions are used to demonstrate that the reactor is operating within the Technical Specifications, These data are collected within a well documented QA program compliant with NQA-1 requirements following well documented procedures. Audits, BEA management oversight, and DOE oversight ensure that data collected to demonstrate compliance with ATR Technical Specifications meet the QA and measurement requirements for monitoring ATR. NGNP accepts that the ATR data meet requirements based on the ATR data qualification program and does not take additional actions to qualify reactor operating conditions data. ATR data are read from raw files, captured into the NDMAS vault, and verified for capture.

# 6.4 ATR Data Problems and Resolution

During the early cycles of the AGR-1 experiment, NDMAS obtained ATR data from informal records of NGNP technical personnel, rather than directly from the ATR data recording system, and in several different file formats and with different parameter lists. To provide the highest-integrity record of ATR data, and to use, rather than reproduce, time-averaging and other data integration features of the ATR data collection system, it is recommended that NDMAS have a direct link to archived data of the ATR system and its qualification status records.

As with AGR-1 fuel irradiation monitoring data, ATR data are collected with a local date/time stamp that periodically shifts to MDT at times not always consistent with official times for those changes. To provide a consistent time/record for all data sets, it is recommended that the ATR also maintain a MST or other standard-time date/time stamp for all records.

# 7. NEUTRONICS AND THERMAL SIMULATION DATA

# 7.1 Description of the Data Stream

The neutronics and thermal (N&T) data stream consists of daily and end-of-cycle (EOC) physics model simulation data of AGR-1 fuel performance and experimental component conditions. The response variables stored within NDMAS are grouped by simulation analysis type and data generator (i.e., modeler) as shown in Table 15. Two types of simulation data are stored for fission power, burnup, and fast neutron fluence: (1) EOC "as-run" calculations from Lillo and Chang (2009), and (2) daily calculations for each of 144 fuel compact cells. Other simulation data stored in NDMAS include daily heating rates for 22 capsule components, daily simulated fuel temperatures (averaged by compact, stack, and capsule), simulated thermocouple temperatures, and simulated radionuclide inventories (in progress).

Table 15. Neutronics and thermal simulation data being stored in NDMAS.

Variable Name	Description					
(1) End-of-Cycle MCNP and ORIGEN2 simulations for each compact cell (complete)						
FD	Fuel fission power density (W/cm <sup>3</sup> )					
FIMA	ORIGEN2 Simulation Fuel burnup at cycle end date (%FIMA)					
FLUENCE	MCNP Simulation Fast neutron fluence (E>0.18 MeV) at cycle end date $(x10^{20} \text{ n/cm}^2)$					
(2) Daily MCNP	and ORIGEN2 simulations for each compact cell (complete)					
FD_D	Total fission heat (MW)					
FIMA_D	Fuel burnup (%FIMA)					
FLUENCE_D	Fast neutron fluence (n/cm <sup>2</sup> )					
(3) Daily simulati	ons of 22 component heat rates for each capsule (W/cm³) (in progress)					
• •	JS simulations of fuel temperatures averaged by compact, stack, and capsule; simulated temperatures by capsule (°C) (in progress)					
SFT_AVE	Average fuel temperature					
SFT_MIN	Minimum fuel temperature					
SFT_MAX	Maximum fuel temperature					
SFT_TA_AVE	Time-averaged Average fuel temperature					
SFT_TA_MIN	Time-averaged Minimum fuel temperature					
SFT_TA_MAX	Time-averaged Maximum fuel temperature					
STC_[1,2,3,4,5]	STC_[1,2,3,4,5] Thermocouple temperature for capsules 1–5					
(5) End of cycle/experiment radionuclide inventories (in progress)						

# 7.2 Data Processing within NDMAS

The following source data files have been received from the data generators (e.g., modelers):

- AGR1 Final Fuel AsRun Summary thru 145A.xls (1/22/2010 transmittal date) includes EOC As-Run simulations for FD, FIMA, and FLUENCE
- \\Sterb\_Hawkes\_Heat\cycle #\Heat\ cycle #\_fiss.day# daily ASCII files for FD\_D (1/26/2010 transmittal date).
- \\Sterbentz\_FFluences\combo.[cycle #].output daily ASCII files for FLUENCE\_D (2/3/2010 transmittal date).

- Daily files for FIMA D (Date/time)
- Master Output AGR DailyCalcs.xls (Date/time) includes component heat rates [(3) in Table 15], simulated fuel and thermocouple temperatures [(4) in Table 15]
- AGR1 EFPD.xls includes effective power days (2/4/2010 transmittal date).

All source data files are stored within NDMAS in the location: "\\Sasngnp\\NGNP\\NGNP\_Data\\AGR-1\\." These files are captured and processed within NDMAS using the steps shown in Figure 14.

#### **N&T Raw Data:**

- Raw data files received from data generators are stored in \\Sasngnp\NGNP\NGNP Data\AGR-1\:
  - AGR1 Final Fuel AsRun Summary thru 145A.xls
  - Master Output AGR DailyCalcs.xls
  - Sterbentz FFluences\ combo.[cycle #].output
  - Sterb Hawkes Heat\cycle #\Heat\ cycle # fiss.day#
- Use Matlab codes to extract and reorganize Sterbentz's FD\_D and FLUENCE\_D data from multiple raw data files, lineup Sterbentz's time steps with Hawkes's date and save the combined excel spreadsheets in \\Sasngnp\\NGNP\\NGNP\_Data\\AGR-1\\\\begin{array}{c} before importing into SAS data sets:
  - o AGR Temp Fission Gamma.xls for FD D
  - o AGR\_FF\_STERB\_day.xls for FLUENCE\_D



#### **N&T SAS Data Sets:**

\\Sasngnp\NGNP\NDMAS Version 1.1\\Neutronics\_Thermal\:

- Upload Neut\_Temp to data\_table.egp: SAS processing
  - Import data from excel spreadsheets
  - Transpose data to make a tall table with one response value per line
  - Assign predefined response variable name, label, and description to each response value
  - Define component name for each response value (AGR-1 experiment, Capsule, Stack, Compact, or Compact cell) according to predefined component list "usv Neutronics Components"
  - Get component ID based on its name from the list "Exp comp"
  - Get response variable ID based on response variable name from the list "Response\_Var\_Attrib"
  - The following intermediate SAS datasets are stored in the N\_Depot library for inspection before pushing into the vault:
  - AGR1\_NEUTRONIC\_DATA for EOC As-Run simulations for FD, FIMA, and FLUENCE
  - AGR1 FASTFLUENCE STERB for daily FLUENCE D
  - o AGR1SIM FUEL HEAT for daily FD D
  - o AGR1 SIM TEMPERATURE for simulated fuel and thermocouple temperatures
  - o AGR1\_EFPD for effective power days

Figure 14. N&T data processing schematic.

Most of N&T data sets represent model predictions at each of 144 fuel compact cells (or modeling "nodes") counting from the top down with cells 1–48 in Stack 1, 49–96 in Stack 3, and 97–144 in Stack 2. The cell numbering scheme relative to the physical compact loading "level" within a capsule is shown in Figure 15. The SAS E-Guide processing listed in Figure 14 links the model output cell numbers to the

fuel compact name, capsule, stack, and loading level so that the modeling results can be linked to individual compact fabrication specifications as listed in Appendix A.

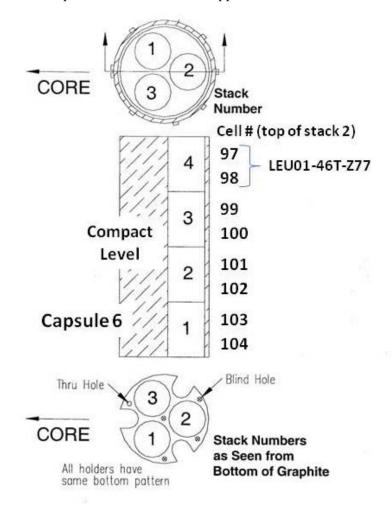


Figure 15. NDMAS links the modeling cell number to compact stack, loading levels, and lot names (shown here for top of stack 2).

## 7.3 Data Qualification

The neutronics and thermal data are physics model predictions that cannot be rigorously validated (except perhaps through post irradiation examination of the modeled components). Therefore, for this data stream, NDMAS data qualification consists only of capture testing to ensure the data stored in the database are identical to the raw data files loaded into the database, and documentation of the modeling analyses in approved reports (e.g., ECARs) produced by the data generators (e.g., Lilo and Chang 2009). Model reports for most of these data are still in progress.

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# Appendix A

NDMAS Database Join for Compacts and Modeling Cells

# Appendix A NDMAS Database Join for Compacts and Modeling Cells

Stack_Name	Compact_Name	Туре	Level	Compact-Cell	Cell
Capsule_6_Stack_1	LEU01-46T-Z53	Baseline	4	LEU01-46T-Z53-N1	1
Capsule_6_Stack_1	LEU01-46T-Z53	Baseline	4	LEU01-46T-Z53-N2	2
Capsule_6_Stack_1	LEU01-46T-Z49	Baseline	3	LEU01-46T-Z49-N1	3
Capsule_6_Stack_1	LEU01-46T-Z49	Baseline	3	LEU01-46T-Z49-N2	4
Capsule_6_Stack_1	LEU01-46T-Z33	Baseline	2	LEU01-46T-Z33-N1	5
Capsule_6_Stack_1	LEU01-46T-Z33	Baseline	2	LEU01-46T-Z33-N2	6
Capsule_6_Stack_1	LEU01-46T-Z32	Baseline	1	LEU01-46T-Z32-N1	7
Capsule_6_Stack_1	LEU01-46T-Z32	Baseline	1	LEU01-46T-Z32-N2	8
Capsule_5_Stack_1	LEU01-47T-Z79	Variant1	4	LEU01-47T-Z79-N1	9
Capsule_5_Stack_1	LEU01-47T-Z79	Variant1	4	LEU01-47T-Z79-N2	10
Capsule_5_Stack_1	LEU01-47T-Z23	Variant1	3	LEU01-47T-Z23-N1	11
Capsule_5_Stack_1	LEU01-47T-Z23	Variant1	3	LEU01-47T-Z23-N2	12
Capsule_5_Stack_1	LEU01-47T-Z13	Variant1	2	LEU01-47T-Z13-N1	13
Capsule_5_Stack_1	LEU01-47T-Z13	Variant1	2	LEU01-47T-Z13-N2	14
Capsule_5_Stack_1	LEU01-47T-Z08	Variant1	1	LEU01-47T-Z08-N1	15
Capsule_5_Stack_1	LEU01-47T-Z08	Variant1	1	LEU01-47T-Z08-N2	16
Capsule_4_Stack_1	LEU01-49T-Z72	Variant3	4	LEU01-49T-Z72-N1	17
Capsule_4_Stack_1	LEU01-49T-Z72	Variant3	4	LEU01-49T-Z72-N2	18
Capsule_4_Stack_1	LEU01-49T-Z68	Variant3	3	LEU01-49T-Z68-N1	19
Capsule_4_Stack_1	LEU01-49T-Z68	Variant3	3	LEU01-49T-Z68-N2	20
Capsule_4_Stack_1	LEU01-49T-Z64	Variant3	2	LEU01-49T-Z64-N1	21
Capsule_4_Stack_1	LEU01-49T-Z64	Variant3	2	LEU01-49T-Z64-N2	22
Capsule_4_Stack_1	LEU01-49T-Z58	Variant3	1	LEU01-49T-Z58-N1	23
Capsule_4_Stack_1	LEU01-49T-Z58	Variant3	1	LEU01-49T-Z58-N2	24
Capsule_3_Stack_1	LEU01-46T-Z65	Baseline	4	LEU01-46T-Z65-N1	25
Capsule_3_Stack_1	LEU01-46T-Z65	Baseline	4	LEU01-46T-Z65-N2	26
Capsule_3_Stack_1	LEU01-46T-Z39	Baseline	3	LEU01-46T-Z39-N1	27
Capsule_3_Stack_1	LEU01-46T-Z39	Baseline	3	LEU01-46T-Z39-N2	28
Capsule_3_Stack_1	LEU01-46T-Z24	Baseline	2	LEU01-46T-Z24-N1	29
Capsule_3_Stack_1	LEU01-46T-Z24	Baseline	2	LEU01-46T-Z24-N2	30
Capsule_3_Stack_1	LEU01-46T-Z23	Baseline	1	LEU01-46T-Z23-N1	31
Capsule_3_Stack_1	LEU01-46T-Z23	Baseline	1	LEU01-46T-Z23-N2	32
Capsule_2_Stack_1	LEU01-48T-Z56	Variant2	4	LEU01-48T-Z56-N1	33
Capsule_2_Stack_1	LEU01-48T-Z56	Variant2	4	LEU01-48T-Z56-N2	34
Capsule_2_Stack_1	LEU01-48T-Z03	Variant2	3	LEU01-48T-Z03-N1	35
Capsule_2_Stack_1	LEU01-48T-Z03	Variant2	3	LEU01-48T-Z03-N2	36
Capsule_2_Stack_1	LEU01-48T-Z43	Variant2	2	LEU01-48T-Z43-N1	37
Capsule_2_Stack_1	LEU01-48T-Z43	Variant2	2	LEU01-48T-Z43-N2	38

Stack_Name	Compact_Name	Туре	Level	Compact-Cell	Cell
Capsule_2_Stack_1	LEU01-48T-Z27	Variant2	1	LEU01-48T-Z27-N1	39
Capsule_2_Stack_1	LEU01-48T-Z27	Variant2	1	LEU01-48T-Z27-N2	40
Capsule_1_Stack_1	LEU01-49T-Z77	Variant3	4	LEU01-49T-Z77-N1	41
Capsule_1_Stack_1	LEU01-49T-Z77	Variant3	4	LEU01-49T-Z77-N2	42
Capsule_1_Stack_1	LEU01-49T-Z02	Variant3	3	LEU01-49T-Z02-N1	43
Capsule_1_Stack_1	LEU01-49T-Z02	Variant3	3	LEU01-49T-Z02-N2	44
Capsule_1_Stack_1	LEU01-49T-Z54	Variant3	2	LEU01-49T-Z54-N1	45
Capsule_1_Stack_1	LEU01-49T-Z54	Variant3	2	LEU01-49T-Z54-N2	46
Capsule_1_Stack_1	LEU01-49T-Z69	Variant3	1	LEU01-49T-Z69-N1	47
Capsule_1_Stack_1	LEU01-49T-Z69	Variant3	1	LEU01-49T-Z69-N2	48
Capsule_6_Stack_3	LEU01-46T-Z76	Baseline	4	LEU01-46T-Z76-N1	49
Capsule_6_Stack_3	LEU01-46T-Z76	Baseline	4	LEU01-46T-Z76-N2	50
Capsule_6_Stack_3	LEU01-46T-Z34	Baseline	3	LEU01-46T-Z34-N1	51
Capsule_6_Stack_3	LEU01-46T-Z34	Baseline	3	LEU01-46T-Z34-N2	52
Capsule_6_Stack_3	LEU01-46T-Z30	Baseline	2	LEU01-46T-Z30-N1	53
Capsule_6_Stack_3	LEU01-46T-Z30	Baseline	2	LEU01-46T-Z30-N2	54
Capsule_6_Stack_3	LEU01-46T-Z14	Baseline	1	LEU01-46T-Z14-N1	55
Capsule_6_Stack_3	LEU01-46T-Z14	Baseline	1	LEU01-46T-Z14-N2	56
Capsule_5_Stack_3	LEU01-47T-Z72	Variant1	4	LEU01-47T-Z72-N1	57
Capsule_5_Stack_3	LEU01-47T-Z72	Variant1	4	LEU01-47T-Z72-N2	58
Capsule_5_Stack_3	LEU01-47T-Z71	Variant1	3	LEU01-47T-Z71-N1	59
Capsule_5_Stack_3	LEU01-47T-Z71	Variant1	3	LEU01-47T-Z71-N2	60
Capsule_5_Stack_3	LEU01-47T-Z65	Variant1	2	LEU01-47T-Z65-N1	61
Capsule_5_Stack_3	LEU01-47T-Z65	Variant1	2	LEU01-47T-Z65-N2	62
Capsule_5_Stack_3	LEU01-47T-Z55	Variant1	1	LEU01-47T-Z55-N1	63
Capsule_5_Stack_3	LEU01-47T-Z55	Variant1	1	LEU01-47T-Z55-N2	64
Capsule_4_Stack_3	LEU01-49T-Z20	Variant3	4	LEU01-49T-Z20-N1	65
Capsule_4_Stack_3	LEU01-49T-Z20	Variant3	4	LEU01-49T-Z20-N2	66
Capsule_4_Stack_3	LEU01-49T-Z36	Variant3	3	LEU01-49T-Z36-N1	67
Capsule_4_Stack_3	LEU01-49T-Z36	Variant3	3	LEU01-49T-Z36-N2	68
Capsule_4_Stack_3	LEU01-49T-Z17	Variant3	2	LEU01-49T-Z17-N1	69
Capsule_4_Stack_3	LEU01-49T-Z17	Variant3	2	LEU01-49T-Z17-N2	70
Capsule_4_Stack_3	LEU01-49T-Z14	Variant3	1	LEU01-49T-Z14-N1	71
Capsule_4_Stack_3	LEU01-49T-Z14	Variant3	1	LEU01-49T-Z14-N2	72
Capsule_3_Stack_3	LEU01-46T-Z79	Baseline	4	LEU01-46T-Z79-N1	73
Capsule_3_Stack_3	LEU01-46T-Z79	Baseline	4	LEU01-46T-Z79-N2	74
Capsule_3_Stack_3	LEU01-46T-Z56	Baseline	3	LEU01-46T-Z56-N1	75
Capsule_3_Stack_3	LEU01-46T-Z56	Baseline	3	LEU01-46T-Z56-N2	76
Capsule_3_Stack_3	LEU01-46T-Z55	Baseline	2	LEU01-46T-Z55-N1	77
Capsule_3_Stack_3	LEU01-46T-Z55	Baseline	2	LEU01-46T-Z55-N2	78
Capsule_3_Stack_3	LEU01-46T-Z17	Baseline	1	LEU01-46T-Z17-N1	79
Capsule_3_Stack_3	LEU01-46T-Z17	Baseline	1	LEU01-46T-Z17-N2	80

Stack_Name	Compact_Name	Туре	Level	Compact-Cell	Cell
Capsule_2_Stack_3	LEU01-48T-Z67	Variant2	4	LEU01-48T-Z67-N1	81
Capsule_2_Stack_3	LEU01-48T-Z67	Variant2	4	LEU01-48T-Z67-N2	82
Capsule_2_Stack_3	LEU01-48T-Z66	Variant2	3	LEU01-48T-Z66-N1	83
Capsule_2_Stack_3	LEU01-48T-Z66	Variant2	3	LEU01-48T-Z66-N2	84
Capsule_2_Stack_3	LEU01-48T-Z63	Variant2	2	LEU01-48T-Z63-N1	85
Capsule_2_Stack_3	LEU01-48T-Z63	Variant2	2	LEU01-48T-Z63-N2	86
Capsule_2_Stack_3	LEU01-48T-Z58	Variant2	1	LEU01-48T-Z58-N1	87
Capsule_2_Stack_3	LEU01-48T-Z58	Variant2	1	LEU01-48T-Z58-N2	88
Capsule_1_Stack_3	LEU01-49T-Z52	Variant3	4	LEU01-49T-Z52-N1	89
Capsule_1_Stack_3	LEU01-49T-Z52	Variant3	4	LEU01-49T-Z52-N2	90
Capsule_1_Stack_3	LEU01-49T-Z49	Variant3	3	LEU01-49T-Z49-N1	91
Capsule_1_Stack_3	LEU01-49T-Z49	Variant3	3	LEU01-49T-Z49-N2	92
Capsule_1_Stack_3	LEU01-49T-Z34	Variant3	2	LEU01-49T-Z34-N1	93
Capsule_1_Stack_3	LEU01-49T-Z34	Variant3	2	LEU01-49T-Z34-N2	94
Capsule_1_Stack_3	LEU01-49T-Z33	Variant3	1	LEU01-49T-Z33-N1	95
Capsule_1_Stack_3	LEU01-49T-Z33	Variant3	1	LEU01-49T-Z33-N2	96
Capsule_6_Stack_2	LEU01-46T-Z77	Baseline	4	LEU01-46T-Z77-N1	97
Capsule_6_Stack_2	LEU01-46T-Z77	Baseline	4	LEU01-46T-Z77-N2	98
Capsule_6_Stack_2	LEU01-46T-Z69	Baseline	3	LEU01-46T-Z69-N1	99
Capsule_6_Stack_2	LEU01-46T-Z69	Baseline	3	LEU01-46T-Z69-N2	100
Capsule_6_Stack_2	LEU01-46T-Z09	Baseline	2	LEU01-46T-Z09-N1	101
Capsule_6_Stack_2	LEU01-46T-Z09	Baseline	2	LEU01-46T-Z09-N2	102
Capsule_6_Stack_2	LEU01-46T-Z07	Baseline	1	LEU01-46T-Z07-N1	103
Capsule_6_Stack_2	LEU01-46T-Z07	Baseline	1	LEU01-46T-Z07-N2	104
Capsule_5_Stack_2	LEU01-47T-Z74	Variant1	4	LEU01-47T-Z74-N1	105
Capsule_5_Stack_2	LEU01-47T-Z74	Variant1	4	LEU01-47T-Z74-N2	106
Capsule_5_Stack_2	LEU01-47T-Z66	Variant1	3	LEU01-47T-Z66-N1	107
Capsule_5_Stack_2	LEU01-47T-Z66	Variant1	3	LEU01-47T-Z66-N2	108
Capsule_5_Stack_2	LEU01-47T-Z56	Variant1	2	LEU01-47T-Z56-N1	109
Capsule_5_Stack_2	LEU01-47T-Z56	Variant1	2	LEU01-47T-Z56-N2	110
Capsule_5_Stack_2	LEU01-47T-Z07	Variant1	1	LEU01-47T-Z07-N1	111
Capsule_5_Stack_2	LEU01-47T-Z07	Variant1	1	LEU01-47T-Z07-N2	112
Capsule_4_Stack_2	LEU01-49T-Z38	Variant3	4	LEU01-49T-Z38-N1	113
Capsule_4_Stack_2	LEU01-49T-Z38	Variant3	4	LEU01-49T-Z38-N2	114
Capsule_4_Stack_2	LEU01-49T-Z44	Variant3	3	LEU01-49T-Z44-N1	115
Capsule_4_Stack_2	LEU01-49T-Z44	Variant3	3	LEU01-49T-Z44-N2	116
Capsule_4_Stack_2	LEU01-49T-Z76	Variant3	2	LEU01-49T-Z76-N1	117
Capsule_4_Stack_2	LEU01-49T-Z76	Variant3	2	LEU01-49T-Z76-N2	118
Capsule_4_Stack_2	LEU01-49T-Z73	Variant3	1	LEU01-49T-Z73-N1	119
Capsule_4_Stack_2	LEU01-49T-Z73	Variant3	1	LEU01-49T-Z73-N2	120
Capsule_3_Stack_2	LEU01-46T-Z44	Baseline	4	LEU01-46T-Z44-N1	121
Capsule_3_Stack_2	LEU01-46T-Z44	Baseline	4	LEU01-46T-Z44-N2	122

Stack_Name	Compact_Name	Туре	Level	Compact-Cell	Cell
Capsule_3_Stack_2	LEU01-46T-Z36	Baseline	3	LEU01-46T-Z36-N1	123
Capsule_3_Stack_2	LEU01-46T-Z36	Baseline	3	LEU01-46T-Z36-N2	124
Capsule_3_Stack_2	LEU01-46T-Z15	Baseline	2	LEU01-46T-Z15-N1	125
Capsule_3_Stack_2	LEU01-46T-Z15	Baseline	2	LEU01-46T-Z15-N2	126
Capsule_3_Stack_2	LEU01-46T-Z12	Baseline	1	LEU01-46T-Z12-N1	127
Capsule_3_Stack_2	LEU01-46T-Z12	Baseline	1	LEU01-46T-Z12-N2	128
Capsule_2_Stack_2	LEU01-48T-Z44	Variant2	4	LEU01-48T-Z44-N1	129
Capsule_2_Stack_2	LEU01-48T-Z44	Variant2	4	LEU01-48T-Z44-N2	130
Capsule_2_Stack_2	LEU01-48T-Z38	Variant2	3	LEU01-48T-Z38-N1	131
Capsule_2_Stack_2	LEU01-48T-Z38	Variant2	3	LEU01-48T-Z38-N2	132
Capsule_2_Stack_2	LEU01-48T-Z20	Variant2	2	LEU01-48T-Z20-N1	133
Capsule_2_Stack_2	LEU01-48T-Z20	Variant2	2	LEU01-48T-Z20-N2	134
Capsule_2_Stack_2	LEU01-48T-Z15	Variant2	1	LEU01-48T-Z15-N1	135
Capsule_2_Stack_2	LEU01-48T-Z15	Variant2	1	LEU01-48T-Z15-N2	136
Capsule_1_Stack_2	LEU01-49T-Z28	Variant3	4	LEU01-49T-Z28-N1	137
Capsule_1_Stack_2	LEU01-49T-Z28	Variant3	4	LEU01-49T-Z28-N2	138
Capsule_1_Stack_2	LEU01-49T-Z19	Variant3	3	LEU01-49T-Z19-N1	139
Capsule_1_Stack_2	LEU01-49T-Z19	Variant3	3	LEU01-49T-Z19-N2	140
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