

DDE-MURR Status Report of Conceptual Design Activities

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Abstract

The Design Demonstration Experiment for the University of Missouri Research Reactor (DDE-MURR) is intended to facilitate Low Enriched Uranium (LEU) conversion of the MURR by demonstrating the performance and fabrication of the LEU fuel element design through an irradiation test in a 200mm channel at the Belgium Reactor 2 (BR2). Revision 0 of this report was prepared at the end of government fiscal year 2012 when most of the resources for furthering DDE design work were expected to be postponed. Hence, the conceptual design efforts were summarized to provide the status of key objectives, notable results, and provisions for future design work. Revision 1 of this report was prepared at the end of fiscal year 2013 in order to include results from a neutronic study performed by BR2, to incorporate further details that had been achieved in the engineering sketches of the irradiation devices, and to provide an update of the DDE-MURR campaign in relation to program objectives and opportunities for its eventual irradiation. These updates were purposed to bring the DDE-MURR conceptual design to level of maturity similar to that of the other two DDE efforts (DDE-MITR and DDE-NBSR). This report demonstrates that the DDE-MURR design effort is well on the path to producing a suitable irradiation experiment, but also puts forth several recommendations in order to facilitate success of the irradiation campaign.

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1. Introduction

The National Nuclear Security Agency Global Threat Reduction Initiative Convert (GTRI-Convert) program employs the High Power Research Reactor (HPRR) Fuel Development (FD) pillar to facilitate maturation of Low Enriched Uranium (LEU) fuel technology in order to enable conversion of High Power Research Reactors (HPRR) to these fuels. The HPRR-FD pillar has overseen design, fabrication, irradiation, and examination of numerous tests on small to medium sized specimens containing these fuels. To enable three HPRR conversions, including the Massachusetts Institutes of Technology Reactor (MITR), University of Missouri Research Reactor (MURR), and National Bureau of Standard Reactor (NBSR), the FD pillar is currently focused on qualification of the “Base Monolithic Design”. The Base Monolithic Design consists of uranium-10 wt% molybdenum alloy (U-10Mo) in the form of a monolithic foil, with thin zirconium interlayers, clad in aluminum by hot isostatic press as seen in Figure 1. ^{[1][2][3][4]}

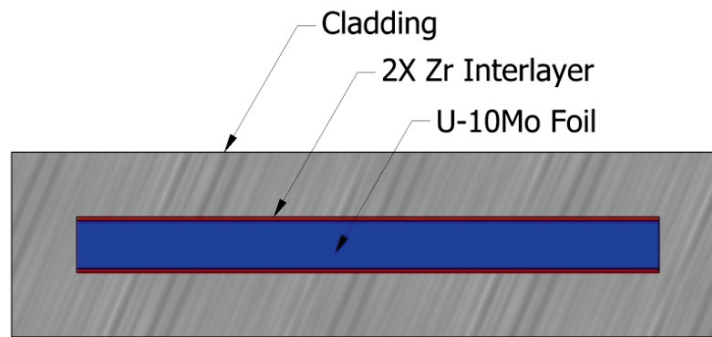


Figure 1: Base Monolithic Design

The licensing basis of the three aforementioned HPRR's restricts them from testing lead test elements of their respective LEU fuel element designs ^[5]. In lieu of the lead test assembly methodology, one Design Demonstration Experiment (DDE) for each of the three NRC licensed reactors will be irradiated elsewhere using prototypic fuel plate geometries under prototypic conditions. Execution of the DDE campaign will represent a significant level of technological maturity will be subject to applicable quality assurance requirements of ASME NQA-1 Parts I and II ^[6].

1.1 Objectives

While absolute prototypic conditions may not be achievable in any reactor except the one for which the LEU element is designed, the DDE campaign is intended to accomplish several critical functions. The following list constitutes the core goals for the DDE campaign:

- **Confirm Performance** under stringent prototypic parameters (e.g. heat flux, fission density)
- **Show Resistance** to worrisome failure modes (e.g. fission gradients, thin-clad structural stability)
- **Demonstrate Fabrication** by producing the plates/elements as demonstration products ^[7]
- **Give Confidence** in the LEU fuel designs prior to conversion

1.2 MURR Reactor Description

The MURR is a multi-disciplinary research and education facility providing a broad range of analytical and irradiation services. The MURR is a pressurized reactor which is both cooled and moderated by light water. The reactor core assembly is located eccentrically within a cylindrically-shaped, aluminum-lined pool as seen in Figure 2. The fuel region has a fixed geometry consisting of eight fuel elements having identical physical dimensions placed vertically around an annulus in between two cylindrical aluminum reactor pressure vessels ^[8].

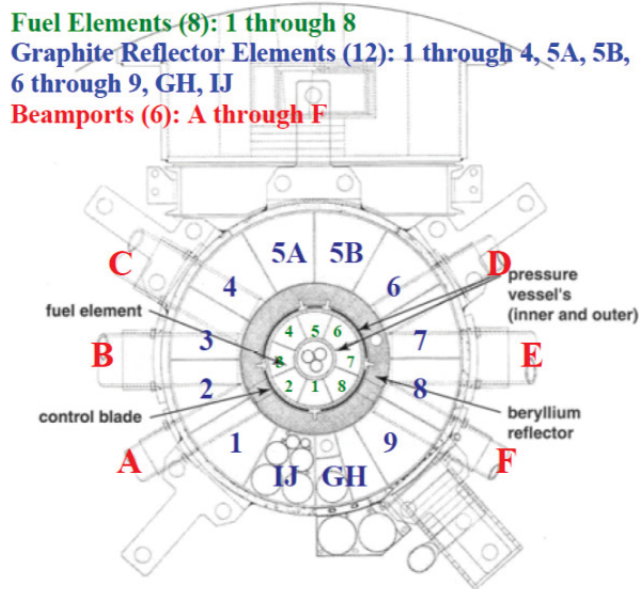


Figure 2: MURR Core Layout (reference [8])

2. Design Inputs

MURR critical geometry and irradiation parameters were established based on forthcoming conversion analyses provided by the GTRI-Convert Reactor Conversion (RC) pillar. The LEU fuel assembly will be comprised of 23 circumferential plates as seen in Figure 3. Nominal LEU fuel plate dimensions can be seen in Figure 4, Figure 5, Figure 6, and Table 1. Irradiation parameters are summarized in Table 2.



Figure 3: LEU MURR Fuel Element Design

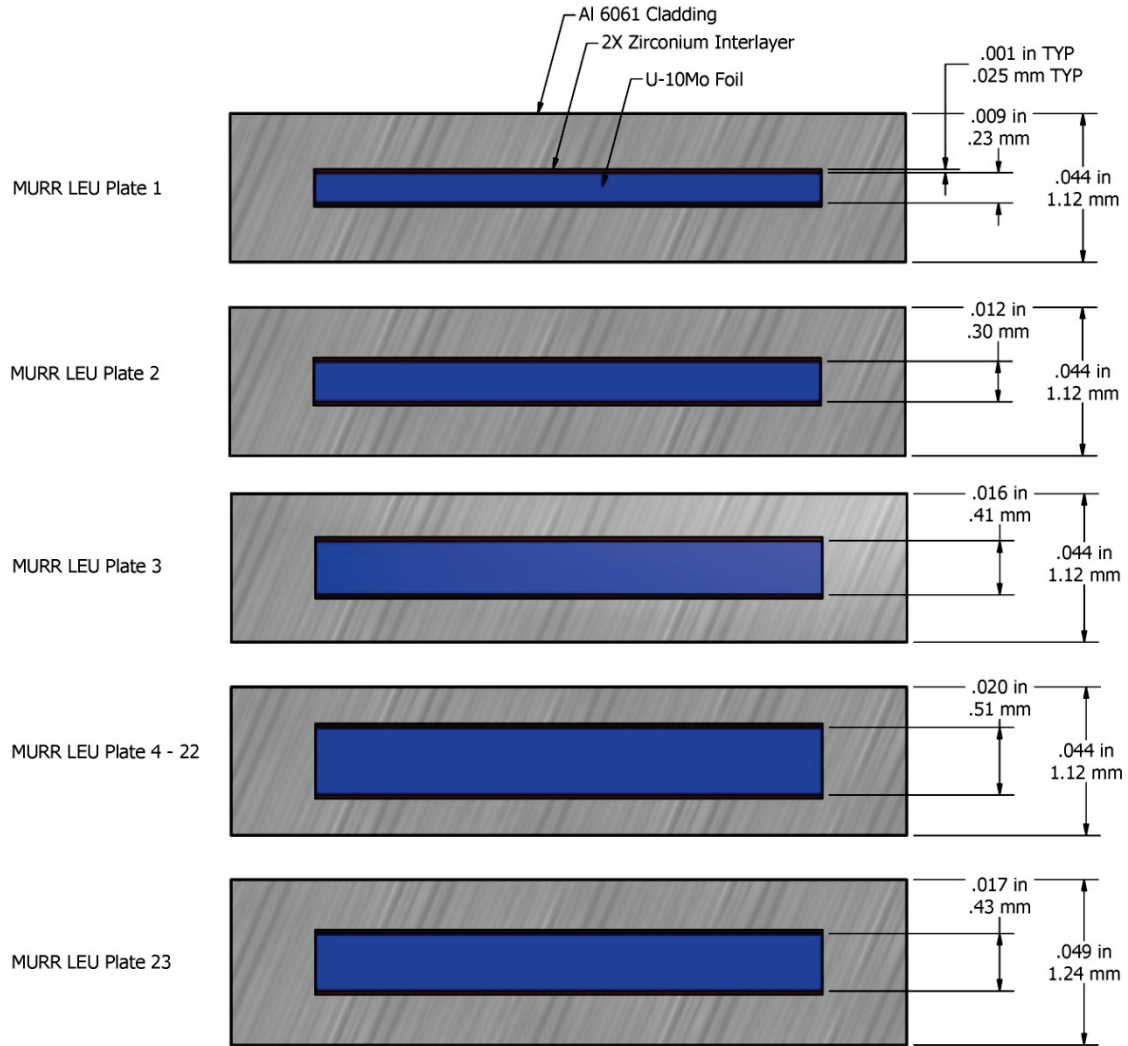


Figure 4: MURR LEU Fuel Plate Nominal Cross Sections

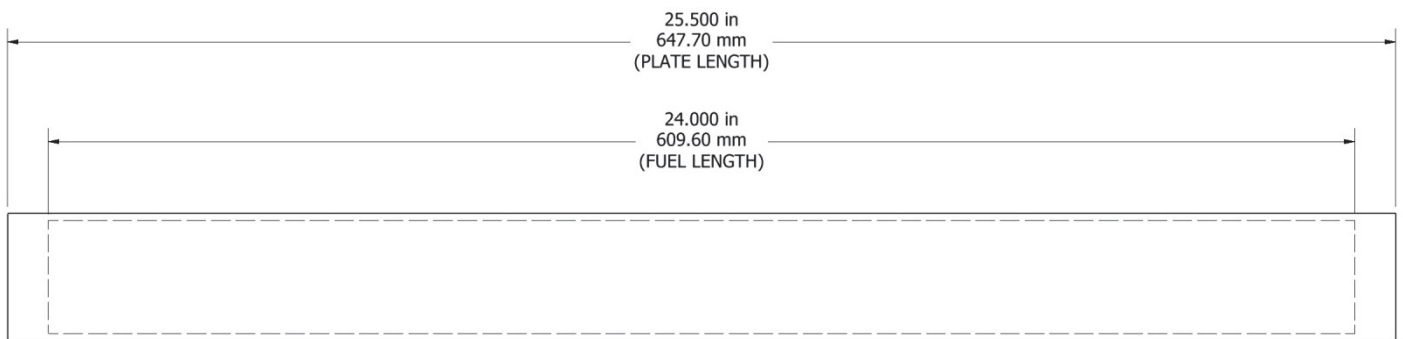


Figure 5: MURR LEU Fuel Plate Nominal Lengths

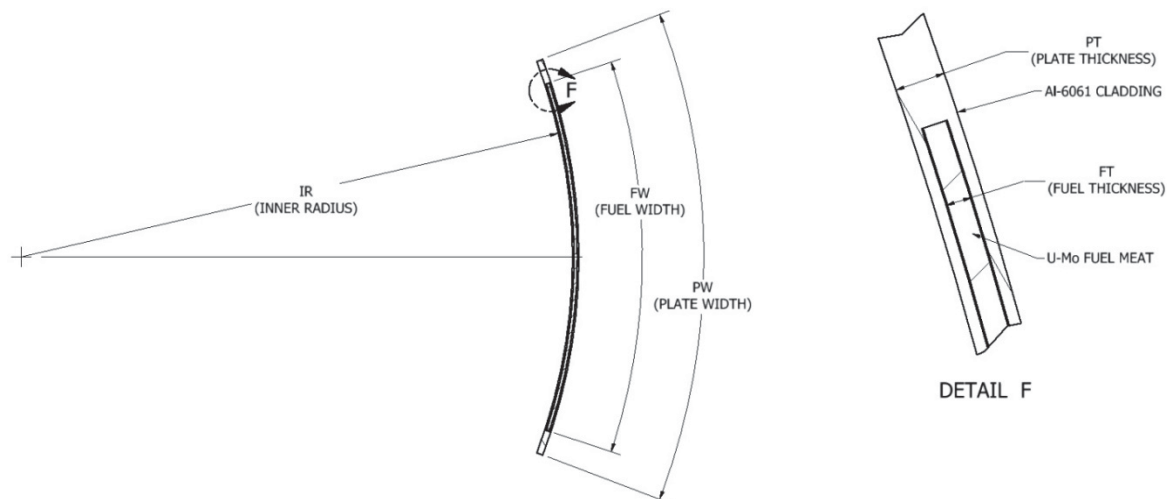


Figure 6: MURR LEU Fuel Plate Widths and Radii Sketch (see Table 1)

Table 1: MURR LEU Fuel Plate Nominal Dimensions

Plate	Inner Radius		Fuel Width		Plate Width		Plate Thickness		Fuel Thickness	
	in	mm	in	mm	in	mm	in	mm	in	mm
1	2.7555	69.99	1.690	42.93	1.980	50.29	0.044	1.12	0.009	0.23
2	2.8925	73.47	1.797	45.64	2.087	53.01	0.044	1.12	0.012	0.30
3	3.0295	76.95	1.905	48.39	2.195	55.75	0.044	1.12	0.016	0.41
4	3.1665	80.43	2.012	51.10	2.302	58.47	0.044	1.12	0.020	0.51
5	3.3035	83.91	2.120	53.85	2.410	61.21	0.044	1.12	0.020	0.51
6	3.4395	87.36	2.227	56.57	2.517	63.93	0.044	1.12	0.020	0.51
7	3.5755	90.82	2.334	59.28	2.624	66.65	0.044	1.12	0.020	0.51
8	3.7115	94.27	2.440	61.98	2.730	69.34	0.044	1.12	0.020	0.51
9	3.8475	97.73	2.547	64.69	2.837	72.06	0.044	1.12	0.020	0.51
10	3.9835	101.18	2.654	67.41	2.944	74.78	0.044	1.12	0.020	0.51
11	4.1195	104.64	2.761	70.13	3.051	77.50	0.044	1.12	0.020	0.51
12	4.2555	108.09	2.868	72.85	3.158	80.21	0.044	1.12	0.020	0.51
13	4.3915	111.54	2.974	75.54	3.264	82.91	0.044	1.12	0.020	0.51
14	4.5275	115.00	3.081	78.26	3.371	85.62	0.044	1.12	0.020	0.51
15	4.6635	118.45	3.188	80.98	3.478	88.34	0.044	1.12	0.020	0.51
16	4.7995	121.91	3.295	83.69	3.585	91.06	0.044	1.12	0.020	0.51
17	4.9355	125.36	3.402	86.41	3.692	93.78	0.044	1.12	0.020	0.51
18	5.0715	128.82	3.508	89.10	3.798	96.47	0.044	1.12	0.020	0.51
19	5.2075	132.27	3.615	91.82	3.905	99.19	0.044	1.12	0.020	0.51
20	5.3445	135.75	3.723	94.56	4.013	101.93	0.044	1.12	0.020	0.51
21	5.4815	139.23	3.830	97.28	4.120	104.65	0.044	1.12	0.020	0.51
22	5.6185	142.71	3.938	100.03	4.228	107.39	0.044	1.12	0.020	0.51
23	5.7555	146.19	4.048	102.82	4.338	110.19	0.049	1.24	0.017	0.43

Table 2: MURR Operating Conditions and Reactor Parameters

Parameter	LEU Core Nominal	DDE Target
Average Coolant Velocity (m/s) ^[9]	7.0	~7.0
Beginning of Life Element Power (MW) ^[9]	1.58	>1.58
Peak Local Heat Flux (W/cm ²) ^[9]	215*	>215
Peak Plate Surface Temp (°C) ^[10]	114	~114
Peak Fuel Meat Centerline Temp (°C) ^[10]	140	~140
Peak Fission Density (fissions/cc) ^[9]	4.0 E+21 [†]	>4.0 E+21

* Peak local heat flux occurs on plate 23

† Peak fission density occurs in plate 1

While the above geometries and parameters were subject to change, they were assumed based on the best information available at the onset of the DDE-MURR effort and were used for scoping analysis activities. A formalized submission of the experiment's critical characteristics was requested from the RC pillar with the intent of including these, among other requirements, in a Functional and Operational Requirements (F&OR) document. Receipt of this submittal was delayed. As a result, the above parameters were also assumed as the key inputs for the FY12 conceptual design work. The F&OR document was not approved as a final document, but the draft document is included in this report for reference purposes and can be seen in Appendix A.

The DDE-MURR critical characteristics submittal was eventually received at the end of FY12 ^[11]. This submittal was consistent with the assumptions made for FY12 conceptual design as displayed in Table 2. This information, in combination with sketches of the irradiation vehicle, was provided to BR2 as input to the FY13 conceptual physics analysis as shown in Appendix B. Incidentally, efforts in FY-13 pertaining to the MiniPlate-1 (MP-1) experiment design received a similar submittal from the RC pillar and MURR with regards to design environment and irradiation conditions ^[12]. These were not included as input to the DDE-MURR conceptual analysis in FY13, but are shown in Table 3. These showed slightly elevated BOL heat rates and slightly decreased EOL burnups compared to the inputs assumed for the FY13 conceptual analysis. Formalization of the F&OR document should reconcile which of these are most pertinent for DDE-MURR during future detailed design efforts.

Table 3: MP-1 MURR Design Inputs

Reactor	Plate	Plate Thickness, cm (inch)	U-Mo Thickness, cm (inch)	Peak BOL Power (kW/cc)	Peak BOL Heat Flux (W/cm ²)	Peak EOL Burnup (fis/cc)	Peak Fuel Temp (°C)	Peak Surface Temp (°C)
MURR	1	0.112 (0.044)	0.023 (0.009)	15.8	181*	3.37E+21	118	105
	22	0.112 (0.044)	0.051 (0.020)	7.1*	181	2.07E+21	147	106
	23	0.124 (0.049)	0.043 (0.017)	10.4*	226	2.59E+21	139	116

* Power value calculated from reported heat flux using meat thickness or vice-versa

2.1 Alternatives and Selection

Several irradiation locations were considered and it was determined that DDE-MURR would be best suited for irradiation in one of the 200mm “H” positions of the Belgium Reactor 2 (BR2). This is documented elsewhere ^[13].

3. Design Status

A detailed accounting of the design chronology to date can be found in Appendix C. The following sections present the technical outcomes of these efforts.

3.1 FY12 Experiment Design and Physics Analysis

This section provides a summary of the experiment design and physics analysis performed up to the end of FY12. Section 3.2 provides an update to these based on the work performed in FY13. The DDE-MURR experiment was designed to accommodate a full size MURR fuel element in accordance with the objective to irradiate prototypic plate geometry. This geometry could fit within a 200mm channel in the BR2. In order to accommodate international shipping considerations, design options such as >20% fuel meat enrichment were not explored as a means of tailoring the fission rates within the experiment design. Constituent compositions of the LEU fuel plates can be seen in Table 4.

Table 4: DDE-MURR Nominal Plate Volumes and Masses

Plate	Constituent Volumes			Constituents Masses					
	Fuel Core	Interlayer	Cladding	Fuel Core				Interlayer	Cladding
	U-Mo Volume (cm ³)	Zr Volume (cm ³)	Al-6061 Volume (cm ³)	U-Mo Mass (g)	Total U Mass (g)	U-235 Mass (g)	Mo Mass (g)	Zr Mass (g)	Al-6061 Mass (g)
1	5.98	1.33	29.09	101.81	91.63	18.10	10.18	8.68	78.55
2	8.48	1.41	28.48	144.34	129.91	25.66	14.43	9.23	76.89
3	11.99	1.50	26.87	204.03	183.62	36.27	20.40	9.78	72.55
4	15.83	1.58	24.92	269.36	242.42	47.88	26.94	10.33	67.27
5	16.68	1.67	25.97	283.82	255.43	50.45	28.38	10.89	70.11
6	17.52	1.75	27.01	298.14	268.33	52.99	29.81	11.44	72.93
7	18.36	1.84	28.05	312.47	281.22	55.54	31.25	11.99	75.74
8	19.19	1.92	29.08	326.66	293.99	58.06	32.67	12.53	78.52
9	20.03	2.00	30.12	340.98	306.88	60.61	34.10	13.08	81.34
10	20.88	2.09	31.17	355.31	319.78	63.16	35.53	13.63	84.15
11	21.72	2.17	32.21	369.63	332.67	65.70	36.96	14.18	86.96
12	22.56	2.26	33.25	383.96	345.56	68.25	38.40	14.73	89.77
13	23.39	2.34	34.28	398.15	358.33	70.77	39.81	15.28	92.56
14	24.23	2.42	35.32	412.47	371.22	73.32	41.25	15.83	95.37
15	25.08	2.51	36.36	426.80	384.12	75.86	42.68	16.37	98.18
16	25.92	2.59	37.41	441.12	397.01	78.41	44.11	16.92	100.99
17	26.76	2.68	38.45	455.45	409.90	80.96	45.54	17.47	103.81
18	27.59	2.76	39.48	469.64	422.67	83.48	46.96	18.02	106.59
19	28.43	2.84	40.52	483.96	435.56	86.02	48.40	18.57	109.40
20	29.28	2.93	41.57	498.42	448.58	88.59	49.84	19.12	112.24
21	30.13	3.01	42.61	512.74	461.47	91.14	51.27	19.67	115.05
22	30.98	3.10	43.66	527.20	474.48	93.71	52.72	20.23	117.89
23	27.06	3.18	58.57	460.64	414.58	81.88	46.06	20.79	158.15
Mass Totals (g)				8477.08	7629.37	1506.80	847.71	338.78	2145.04

Physics analysis of a 20% enriched DDE-MURR design in a peripheral (i.e. not center) 200mm “H” channel, combined with BR2’s “flexible” core loading schemes, showed that prototypic fission rates were achievable in the BR2. The physics analysis assumed the experiment to be fixtured within two aluminum “plugs”, the larger outer plug containing an eccentric hole for the smaller inner plug with the inner plug containing a cavity for the DDE-MURR element. This was evaluated in the BR2 H5, H4, and H3 channels as seen in Figure 7.

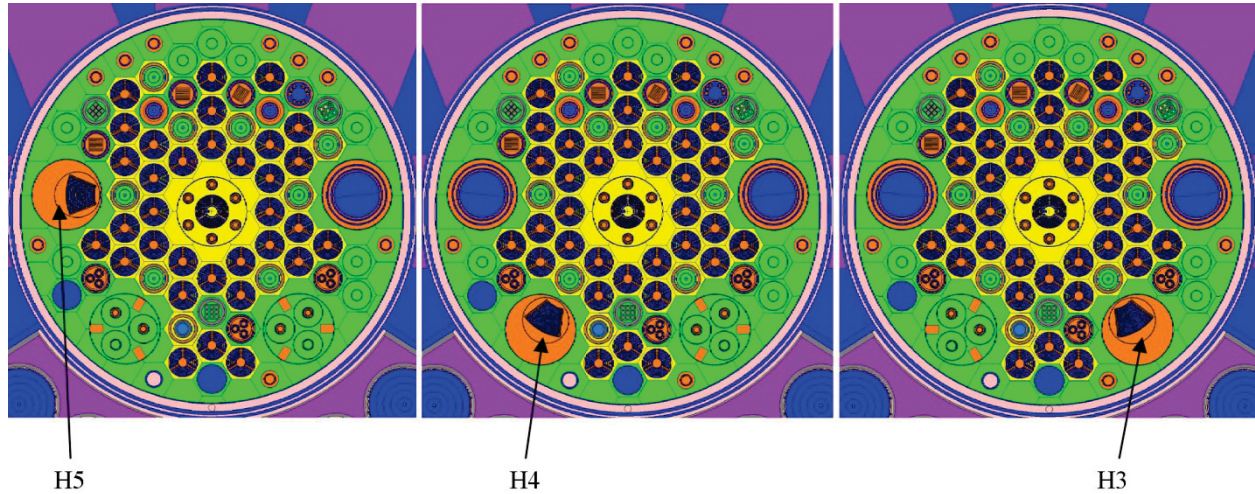


Figure 7: DDE-MURR in Various 200mm H Channels

The target peak heat flux for DDE-MURR was 215 W/cm^2 occurring on plate 23. MCNPX was used to model and evaluate these configurations^[14] and showed a peak Beginning of Life (BOL) heat flux of 238 W/cm^2 , 211 W/cm^2 , and 219 W/cm^2 in the H5, H4, and H3 channels, respectively. A final determination regarding which H channel to use was not made during this phase of the design, but all seemed to be fair matches for the MURR heat flux. This determination should be made when the future DDE-MURR and BR2 schedules become more mature and will likely include considerations of other BR2 irradiation users.

These calculations included axially and azimuthally resolved cells to account for edge peaking. Unlike the projected LEU MURR design, however, these peaks occurred on those plates with full-thickness fuel which were nearest the core center (i.e. plates 3 and 4). In general, the plate-to-plate power profiles exhibited more suppressed powers on the trailing plates than would be expected in the LEU MURR design as seen in Figure 8 and Figure 9.

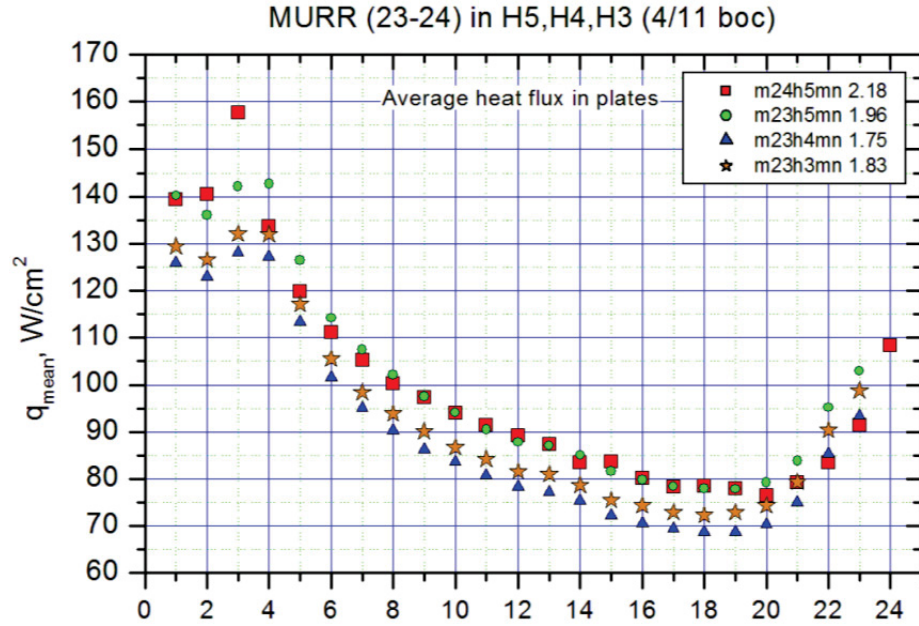


Figure 8: DDE-MURR Plate-to-Plate Average BOL Heat Flux Plot with Plate 1 Leading (LEU 24 plate design also plotted in red)

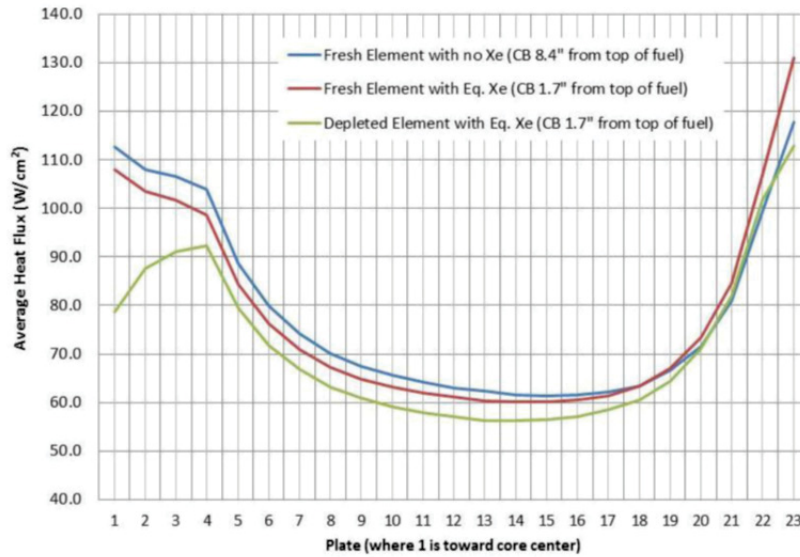


Figure 9: MURR Plate-to-Plate Average Heat Flux Plot (reference [11])

These behaviors are due to inherent differences in the spatial distribution of the thermal flux profiles within the MURR and BR2 reactors. However, design options which include cycle-to-cycle 180° rotation of the DDE-MURR inner plug were suggested in order to orient plate 23 as the “leading” plate during some cycles to achieve peak heat fluxes targets on the correct plate, while orienting plate 1 as the “leading” plate during other cycles in order to achieve peak fission density targets on the correct plate. These should be investigated in greater detail in the future.

While detailed depletion analyses were not performed, an assumption of linearly decreasing plate fission rates estimated achievement of the fission density goal ($4.0\text{E}+21$ fissions/cc in plate 1) in ~130 full power days where plate 1 is configured nearest the core center for every cycle. Alternating rotational schemes,

while not yet investigated in detail, would somewhat extend the time required to achieve this goal in plate 1 as they would orient plate 1 furthest from the core center during some cycles, but would likely induce a more prototypic plate-to-plate burnup profile in the final irradiated element.

More detailed thermal hydraulic analyses and structural evaluations were not accomplished during this phase of the design. The intent was to design an irradiation vehicle which throttles flowrates to match those of the project LEU MURR core. This design feature was thought to require additional thermal analysis for flow coastdown and reversal in the BR2. Irradiation vehicle and CGP design efforts were also undertaken. These are summarized in sections 3.3 and 3.4.

3.2 FY13 Experiment Design and Physics Analysis

An effort was undertaken in FY13 to mature the design of DDE-MURR to be comparable to that of the other DDE's as described in preceding sections. This effort primarily saw more detailed conceptual evaluations of the neutronic configurations possible for DDE-MURR. These cases focused on achieving the experimental conditions as described in section 2. The calculations were performed by personnel at the BR2 facility in accordance with the inputs as shown in Appendix B. These calculations evaluated achieving experimental conditions with a model that simulated the neutronically significant characteristics of the irradiation hardware design and further explored irradiation design options and experimental configurations in an attempt to better achieve experimental conditions. Two geometric configurations were addressed including the concentric design (represent current vehicle design) and the eccentric design option as illustrated in Figure 10. Other parameters included BR2 reactor power, external plug material, and rotational/axial placement within the core. ^[15]

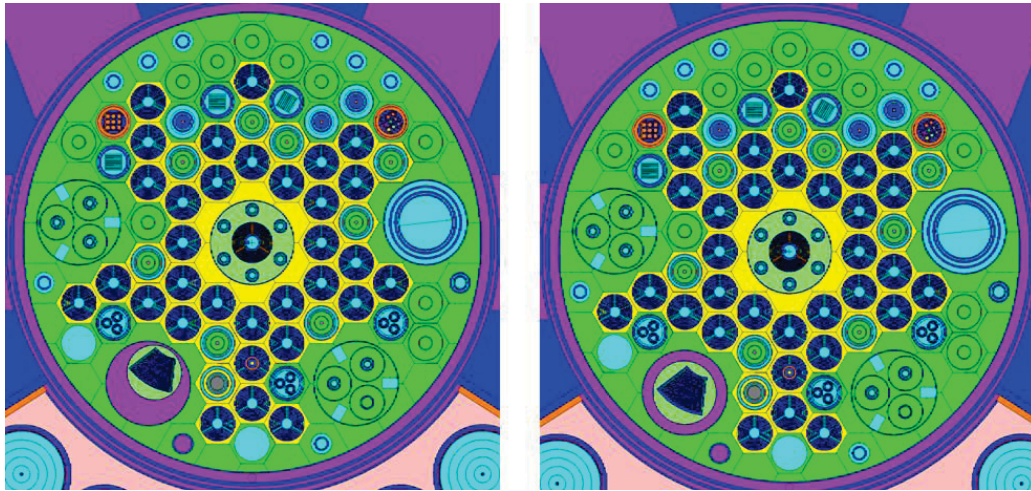


Figure 10: DDE-MURR Geometric Configurations, 0° rotation displayed (eccentric-left, concentric-right) ^[15]

The BOL results of several cases can be seen below in Table 5. Target conditions in Table 5 came from reference [9], case 1-12 results came from reference [15], case 13 & 14 results were interpolated from cases 11 & 12, and case 15 results were roughly approximated by scaling case 14 with “rotation effect factors” derived from case 5 / case 2.

Table 5: BOL Physics Results

Case	Xe	BR2 Power (MW)	Axial Offset	Plug Config.	Inner Plug Rotation (0° = plate 1 towards core center)	Int Plug	Ext Plug	DDE-MURR Element	Plate 1	Plate 23
									Max (W/cm ²)	Max (W/cm ²)
Target								1.58	147	193
1	BOC, No Xe	54	0	Eccentric	0°	AlMgSi1	AlMgSi1	1.65	186	160
2	BOC, Eq. Xe	54	0	Eccentric	0°	AlMgSi1	AlMgSi1	1.49	179	149
3	BOC, Eq. Xe	54	-10cm	Eccentric	0°	AlMgSi1	AlMgSi1	1.55	182	158
4	BOC, Eq. Xe	54	0	Eccentric	0°	AlMgSi1	Be	2.02	242	227
5	BOC, Eq. Xe	54	0	Eccentric	180°	AlMgSi1	AlMgSi1	1.44	72	221
6	BOC, Eq. Xe	54	0	Eccentric	180°	AlMgSi1	Be	1.96	122	297
7	BOC, No Xe	51	0	Eccentric	0°	AlMgSi1	AlMgSi1	1.69	176	164
8	BOC, Eq. Xe	51	0	Eccentric	0°	AlMgSi1	AlMgSi1	1.53	162	147
9	BOC, Eq. Xe	51	0	Eccentric	0°	AlMgSi1	Be	2.07	225	241
10	BOC, Eq. Xe	51	0	Eccentric	0°	Be	AlMgSi1	1.75	202	166
11	BOC, Eq. Xe	51	0	Concentric	0°	Al 6061	AlMgSi1	1.27	127	124
12	BOC, Eq. Xe	65	0	Concentric	0°	Al 6061	AlMgSi1	1.61	160	158
13	BOC, Eq. Xe	60	0	Concentric	0°	Al 6061	AlMgSi1	1.49	148	146
14	BOC, Eq. Xe	54	0	Concentric	0°	Al 6061	AlMgSi1	1.34	134	131
15	BOC, Eq. Xe	54	0	Concentric	180°	Al 6061	AlMgSi1	1.30	54	195

The above results demonstrated that no ideal configuration exists which simultaneously mimics the MURR's prototypic BOL plate-to-plate power profiles as indicated most prominently by the outermost plates 1 and 23. However, cases 13 and 15 suggested that an aluminum-based concentric irradiation vehicle can meet plate 1 power targets when plate 1 is closest to the core center (0° rotation) while the BR2 power is ~60 MW, and that plate 23 power targets can be met when the same vehicle is oriented at 180° while BR2 power is ~54 MW. These two configurations cannot be accomplished simultaneously and would need to be alternated in some fashion from cycle to cycle in order to achieve a proper plate-to-plate burnup profile throughout the element. This approach would exhibit a high-low alternating power history for these exterior plates, giving way to a longer total irradiation time to accomplish burnup targets.

Conversely, approaches such as case 4 and case 9 suggested that the both the plate 1 and 23 target powers could be exceeded simultaneously through the use of eccentric plugs and slightly-poisoned beryllium plug material. This design would offer the advantage of achieving burnup targets in less irradiation time, but would also pose the notable disadvantages of far exceeding plate 1 powers and requiring a more complex irradiation vehicle designs which makes use of Beryllium-based materials. At the time that rev 1 of this design report was written, no concept could be definitively recommended since the distinguishing design trade-offs pertained to schedule constraints; which were not mature enough to be formalized as design requirements. Hence, both options are considered viable and should receive further evaluation in future design work.

These analyses demonstrated that the azimuthal profile (i.e. edge peaking) is influenced by the 180° orientation configuration resulting in an elevated fission rates in the central azimuthal regions as displayed in Figure 11. These analyses further demonstrated that a 10 cm shift in the axial positioning of the DDE-MURR fuel assembly can shift the axial peak region by about that same distance.

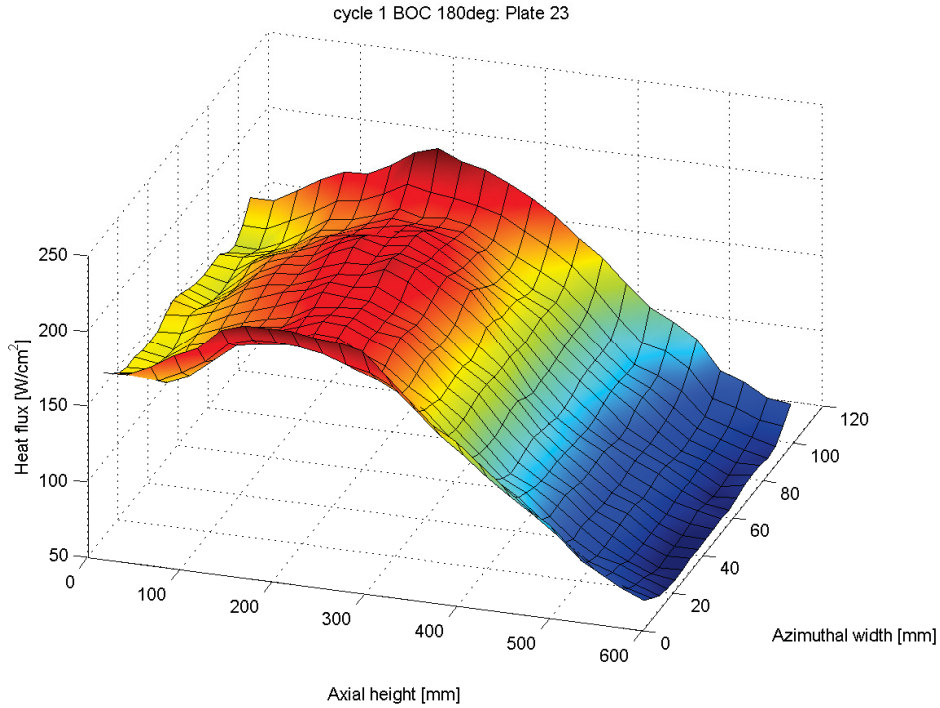


Figure 11: Plate 23 Heat Flux Profile (180° Rotation)

Lastly, these analyses considered the detailed depletion analyses of the DDE-MURR element within the eccentric aluminum plug vehicle design. These results indicated that the burnup target of $>4.0\text{E}21$ fis/cc in plate 1 can be achieved in as few as five BR2 cycles (~ 126 full power days) at a reactor power of 51 MW where the vehicle is oriented at 0° for all five cycles. These results also showed that the peak burnup in plate 23 would achieve $2.5\text{E}21$ fis/cc. The peak burnup in plate 23 was not included as a design requirement for these FY13 physics analyses, but in light of the later-received MP-1 input MURR conditions ^[12] it appeared that this DDE-MURR experiment configuration fell short of the plate 23 predicted burnup of $2.59\text{E}21$ fis/cc while exceeding the same value for plate 1 of $3.37\text{E}21$ fis/cc as display above in Table 3. This result was not surprising as the 0° configuration was expected to exhibit a tilted plate-to-plate power profile, with less power in the trailing plates such as plate 23, when compared to that of the actual MURR as illustrated in Figure 12. This result demonstrates that occasional 180° rotation of the DDE-MURR test vehicle or use of slightly-poisoned Beryllium plug material may be needed to achieve a more representative plate-to-plate burnup distribution. These options should receive more detailed treatment in future design efforts.

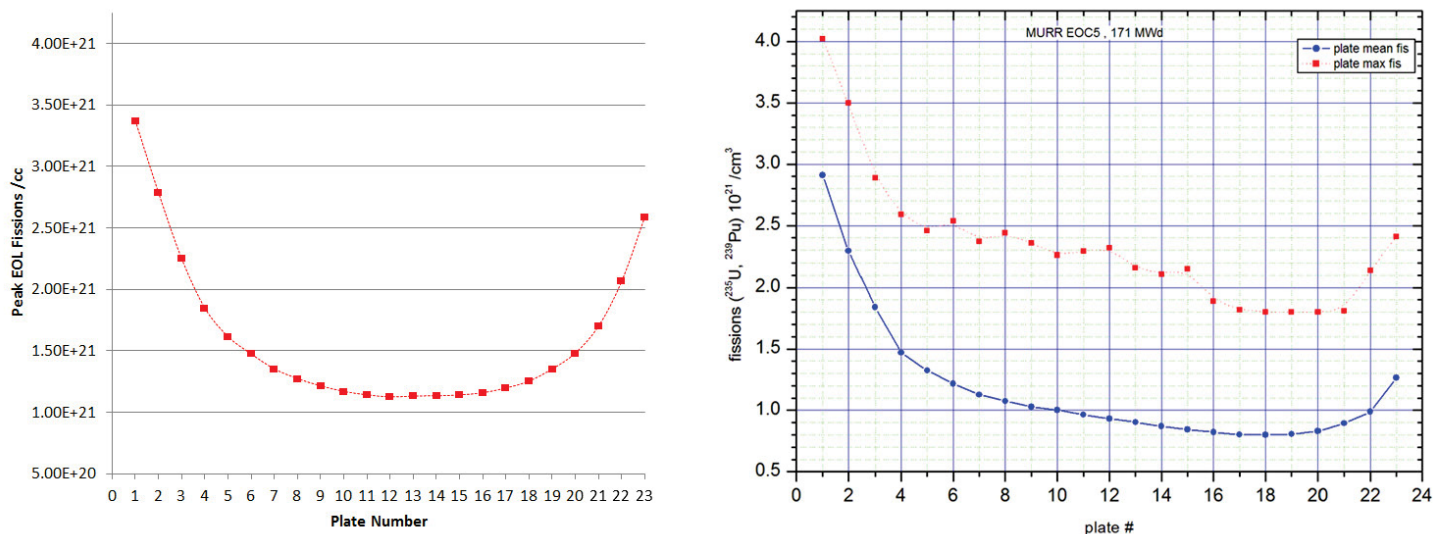


Figure 12: EOL Burnup Predictions, Left: MURR MP-1 Input Predictions^[12], Right: DDE-MURR 5 Cycle BR2 Predictions (red points represent local plate peaks)

3.3 Irradiation Assembly Design

Functional and Operational Requirements document FOR-118 was initiated to capture the requirements for the DDE-MURR hardware designs (see Appendix A). Detailed irradiation assembly design information can be found in Appendix D. This design incorporated the requirements to be irradiated in the BR2 reactor and was designed with the following fundamental features, see also Figure 13:

- **BR2 Outer Pressure Boundary:** This outer tube is approximately 7.7 m (25.5 feet) long and slightly smaller than the 200mm diameter of the BR2 H position irradiation tube. The boundary tube incorporates an upper lifting bail and lower catcher. The catcher will contain the fuel if there is a meltdown condition. The irradiation zone contains the vehicle portion which is comprised primarily of aluminum and serves the purpose of holding the fuel element and displacing water between the cylindrical channel and element. The eccentric inner plug concept, as seen in Figure 7, was not investigated during this initial concept generation.
- **The Irradiation Vehicle:** The irradiation vehicle is approximately 26 inches (660mm) in length and 6 inches (150mm) diameter. It is designed to contain the MURR LEU 23 plate fuel during the irradiation process. This portion includes orientation slots at 90° to facilitate alternate orientation schemes as discussed in section 3.1 (e.g. 180° cycle-to-cycle rotation).
- **The E-FUTURE style Grapple:** This grapple is designed to provide the irradiation vehicle's handling interface. The grapple will also have the typical MURR End Box attached so that it will be part of the irradiation process but will be removed after placement in the Channel Gap Probe basket.
- **Upper Sealing Plug:** This plug seals the reactor channels during the irradiation process. This design also allows the entire assembly to be lifted out or for removal of just the irradiation vehicle with the BR2 lift bail.

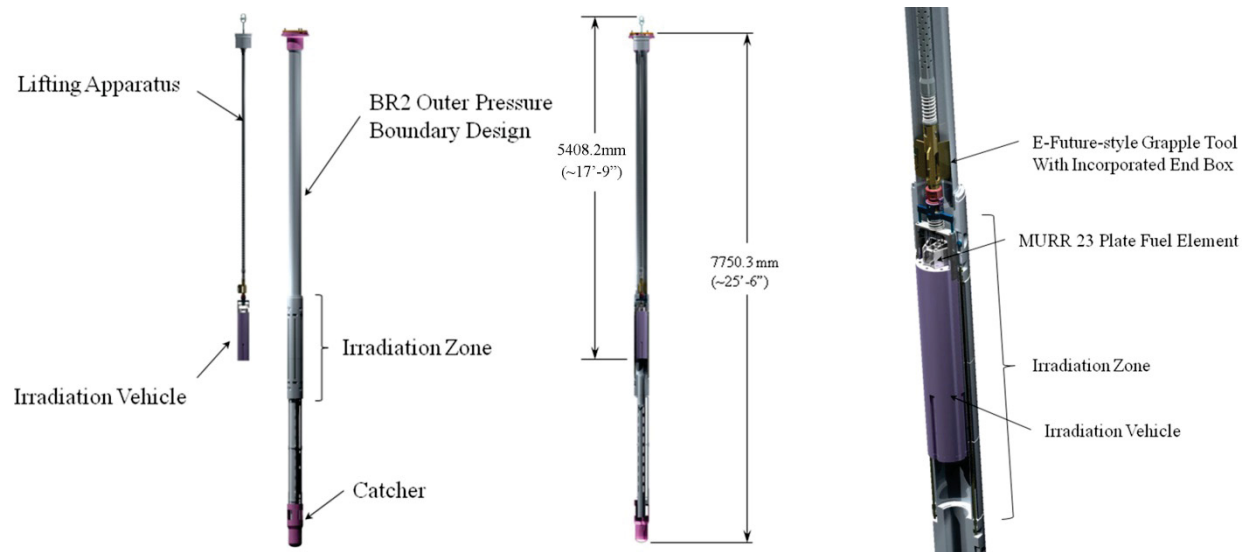


Figure 13: DDE-MURR Irradiation Assembly Concept

3.4 Channel Gap Probe Design

Functional and Operational Requirements document FOR-118 was initiated to capture the requirements for the DDE-MURR hardware designs (see Appendix A). More-detailed Channel Gap Probe (CGP) design information can be found in Appendix E. The CGP measurements taken before, during, and after irradiation are key to the DDE-MURR mission. As BR2 did not have this capability existing, a BR2-specific CGP design was conceptualized with the following key features (see also Figure 14):

- **Basket Frame Assembly:** This outer frame is approximately 16 feet (4.9m) long and 2 feet by 2 feet (0.6m by 0.6m). It holds the Irradiation Vehicle that contains the DDE-MURR fuel element. It mates with the probe frame using alignment pins corresponding to the E-Future grapple. The basket Frame Assembly stays in the canal for the entire fuel irradiation campaign.
- **CGP to Fuel Alignment Assembly –** This assembly consists of a plate that is 2 feet by 2 feet (0.6m by 0.6m) and a precisely located guide block (mimics the fuel shape) that aligns the fuel to the above Channel Gap Probe using alignment pins. This Guide Block aids the operators in inserting the probe in the correct spot without damage to the delicate probe.
- **The Channel Gap Probe (CGP) Frame:** This frame is approximately 16 feet (4.9m) long and 2 feet by 2 feet (0.6m by 0.6m). This frame mates with the Basket Frame Assembly using the CGP to Fuel Alignment Assembly. The framework is removed from the canal following the completion of each fuel gap measurement.
- **Probe movements:** The probe is approximately 0.5 inch (12 mm) wide, 0.05 inch (1.2 mm) thick, and 4 feet (1200 mm) in length. The probe is capable of being moved in the X and Y planes, up and down (Z), and rotated about the Z-axis. A system of gears enables these movements.
- **Calibration Block:** The probe passes through a calibration block before insertion into the MURR fuel to ensure consistent and accurate measurements.

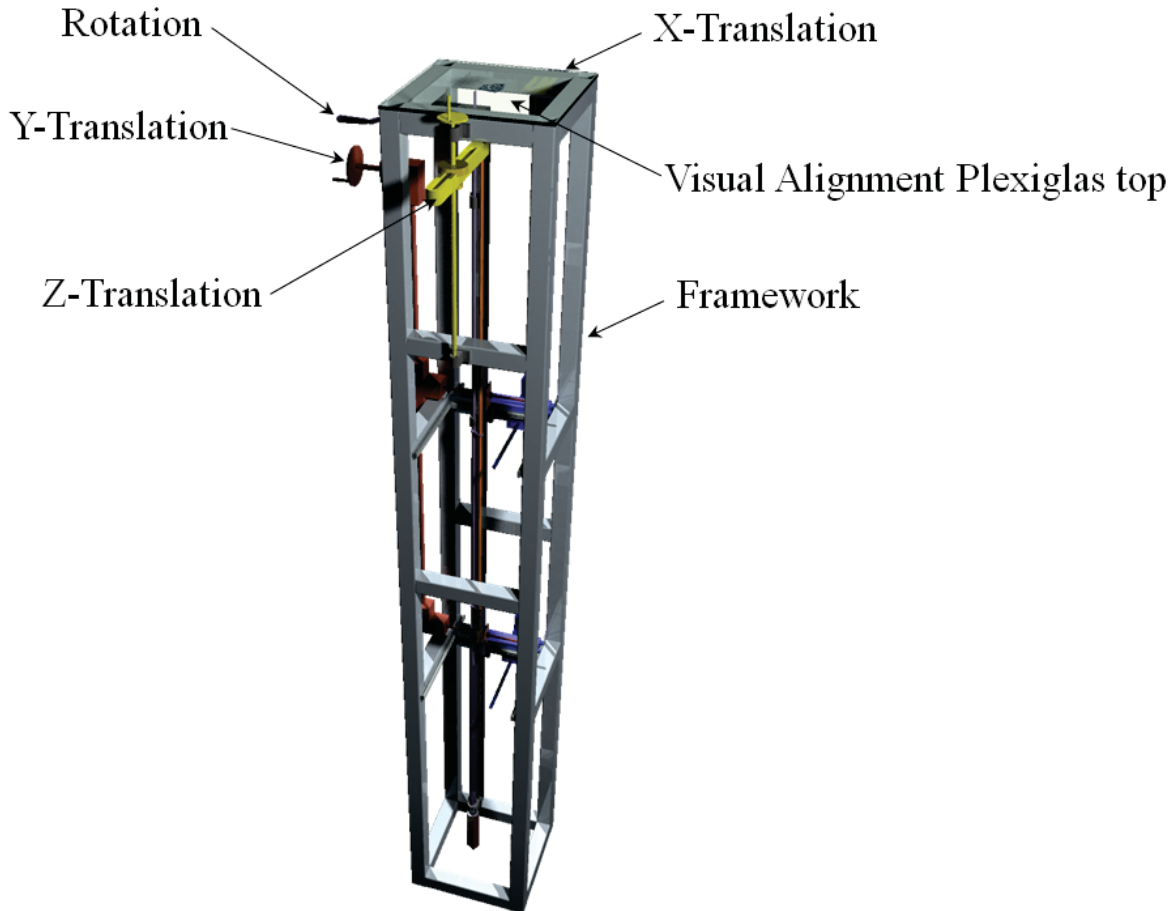


Figure 14: BR2 Channel Gap Probe

The following items need further design consideration in regard to the Channel Gap Probe design:

- Interface with the Irradiation Vehicle: Both designs need to incorporate alignment features for both in the reactor and in the CGP. Alignment pins have been designed generally, but actual length, position, and shape need to be looked at more closely.
- Guide Block: The Guide Block is an intricately machined part that matches the nominal dimensions of the MURR fuel. There will need to be tapered features incorporated into the design so that it will give alignment of the CGP to the fuel assembly.
- Probe: This probe has a T-shaped feature at the top side that allows the probe to be slid through a support channel. Whether this probe and channel system will work as assumed needs further investigation.
- The CGP shows the probe being able to move in 4 directions as described in above. The mechanisms and functionality of these concepts needs to be developed more so that the probe can be precisely located over the guide block repeatedly.
- Basket Frame Assembly attachment to the wall of the BR2 Reactor also needs development.

3.5 Fuel Specifications

Draft specifications were produced for the DDE-MURR U-Mo coupons and fuel element and can be seen in Appendix F. These specifications represent a design maturity level commensurate with conceptual

design only and are considered to be inadequately mature for fabrication of final DDE products. The element specification corresponds with fuel element assembly drawing 603455, as seen in Appendix G. This element drawing represents the in-progress drawing for the actual LEU MURR design. While the final DDE-MURR element drawing may differ slightly (e.g. end box attachment design) and eventually require a distinct drawing, this drawing was used for the conceptual design specification work.

These specifications were based, to the level possible, upon a quality control and quality assurance requirements in existing specifications. The chemical and isotopic requirements of U-Mo materials were based upon existing standards for HEU metal ^[15], Y-12 specifications for LEU metal ^[16] and LEU-Mo ^[17], ASTM standards for LEU-metal ^[18], and U-Mo foil specifications for the RERTR-FE campaign ^[19]. These were tabulated and the appropriate compositional limits were selected. Equivalent Boron Content (EBC) limits were derived by comparing the sum total max EBC of each plate constituent in the existing HEU designs to the proposed EBC limit for U-Mo. These limits were compared to historical analyses of U-Mo materials. These tabulations, calculations, and comparisons can be found in the Coupon Specification Composition Worksheet as denoted in Table 6 of section 5.2.

The composition and isotopic limits explained above were specified based primarily on existing requirements and equivalency to currently accepted designs and/or standards. Consequently, these limits represent a proposed base for nuclear safety and LEU reactor operation of the MITR, MURR, and NBSR, but do not represent any requirements that the manufacturer wish to impose in order to facilitate greater yield rates or ease in fabrication. Intermediate product specifications ^[20], sampling plans, manufacturing procedures, etc. should be incorporated into the DDE coupon specifications, or related documents, as their effects on fabrication processes becomes known during the FFC pillar's ongoing fabrication studies.

Like the coupon specifications, DDE element specifications were based, to the level possible, on existing specifications and standards. Specifically, the MITR HEU ^[21] element and MURR HEU ^[22] element specifications were chosen as "templates" to work from. These were selected based on their succinct structure and experience base with the fuel procurement group at the INL who currently procures HEU fuel elements for MURR. This was intended to facilitate one of the core DDE goals to demonstrate fabrication by providing a prototypic procurement structure.

Other specification adaptations include differences innate to the MURR LEU design such as the plate/element U-235 limits based on a 23 plate 20% enriched design and boehmite prefilm treatment. Requirements that were based on upon the precedent HEU dispersion fuel (e.g. stray fuel particles and provisions for "dogbones") were eliminated or modified. Additional inspections and requirements which pertain to the monolithic base fuel design and respective fabrication process are also included such as bend testing of clad croppings and zirconium interlayer thickness inspection. Finally, some specification adaptations were necessary based on the DDE's end use such as referencing to the MURR as the "stakeholder" rather than the "user".

Developments in FY13 prompted the creation of a group of experts within the project whom are considered the "design authority" with immediate responsibility for a U-Mo plate generic product specification ^[23] and eventual responsibility for facilitating the final reactor element specifications. This group should engage with the future design work to mature the DDE specifications.

4. Future Recommendations

4.1 Hardware Design Recommendations

The following items need further design consideration in regard to the Irradiation Vehicle:

- Interface with the Channel Gap Probe: Both designs need to incorporate alignment features for both in the reactor and in the CGP. Alignment pins have been designed generally, but actual length, position, and shape need to be looked at more closely.
- The irradiation vehicle needs to be modified to include flow inlet and outlet path features with input from thermal calculations. This will also include design of the orifice at the bottom of the irradiation vehicle which needs to operate in normal and flow coastdown and reversal conditions.
- The detailed E-Future Grapple design with removable end box is anticipated to be a difficult endeavor. Future investigations should include evaluations of simpler designs and their propensity to meet design requirements. This should include a detailed design work in regards to tolerance stack-up and the exterior coolant channel gap (i.e. channels 1 and 24) and their means of being determined/located within the irradiation vehicle.
- The detailed design of inner plug eccentricity in outer plug features is also anticipated to be a difficult endeavor. Future investigations should include evaluations “centered” design options and their propensity to meet design requirements.
- Detailed evaluations of the feasibility of simple instrumentation (e.g. thermocouples) in the irradiation test vehicle.

The following items need further design consideration in regard to the Channel Gap Probe:

- More detailed design and drafting of the irradiation vehicle and CGP should be accomplished as a continuation of the fruitful collaboration which is already in place with BR2 engineers. This also should include a channel gap probe sensor which can measure channel gap distance and water temperature concurrently.

Other design considerations should include:

- An effort intended to fabricate full-size mock-ups of the DDE-MURR irradiation assembly for the purpose of functional handling in the BR2 vessel, handling pools, channel gap probe, and other applicable handling evolutions should be commenced. This should substantially reduce the risk of hardware based failure in providing “hands-on” experience regarding fabrication of the hardware, ability to assemble underwater and perform channel gap measurements, and likelihood of damage during handling. Completion of this work is strongly recommended.
- Development of any special purpose tooling for handling such as storage buckets, handling tools, and fixturing. These should also be fabricated and handled in a prototypic effort as described above early enough in the design process to facilitate modifications if necessary. Storage buckets and similar fixtures should also endeavor to allow for natural circulation removal of decay heat.
- Design of a suitable location in the irradiation assembly and selection of an appropriate dosimetry material (e.g. flux wires) for the purpose of benchmarking cycle-to-cycle as-run depletion analysis in order to reduce the risk of “over-burning” or “under-shooting” the actual experiment during irradiation.

4.2 Analytic Recommendations

Several analytic efforts were not completed due cancellation of the FY13 scope for DDE-MURR. Their maturation is recommended for future efforts. These include:

- Upon ascertainment of a more mature design schedule and selection of the appropriate 200mm channel, a full suite of analyses should be performed and reviewed by the appropriate personnel.
 - Physics: 180° inner plug rotational scheme, detailed depletion, source term
 - Thermal: Flow coastdown and reversal analysis for throttled irradiation vehicle design, BR2 recommended that Argonne National Laboratory perform this based their familiarity with the BR2 coolant system.
 - Structural based on more mature inputs from the thermal analysis and all anticipated loading modes
- Further design analyses should include:
 - An analysis “round robin” where the DDE-MURR heat loads, flow rates, etc. would be provided to the RC team for input into their MURR LEU models and vice-versa for the purpose of comparing analytic results between the DDE-MURR and MURR LEU methods, models, codes, etc.
 - Since the DDE experiments, compared to previous HPRR-FD irradiations, have more specific fission density goals which must be confidently met prior to post irradiation shipment, as-built equivalent boron content of non-fueled components (e.g. aluminum stock used to fabricate the irradiation vehicle) should be investigated for its contribution to the final fission densities via physics analyses.
 - Fluid Structure Interaction (FSI) analysis performed in order to evaluate the risks for flow induced failure modes. This should be performed in conjunction with physical flow testing of dummy hardware. This flow testing should be performed far in advance of the final “acceptance” flow testing that BR2 must perform on the delivered final element and vehicle.
 - Analysis to determine the risk for an oxide spallation failure. Since the DDE-MURR experiment will reside in BR2 storage pools under decay heat conditions for greater lengths of time than previous HPRR-FD fuel development experiments these calculations should also consider including “pool-time”, if significant, in the oxide spallation analysis.
 - Analysis regarding fuel plate performance and its impact on potential failure modes. This should be done with the most pertinent tools, including multiphysics codes where applicable, to evaluate effect of fuel swelling, material properties evolution, fuel creep, thermal conductivity degradation, and other pertinent and predictable fuel performance phenomena.

4.3 Design and Engineering Process Recommendations

A Process Focused on Risk and Failure Modes

The DDE-MURR campaign is considered an engineering scale demonstration test with significant maturity in the technology life cycle. As such, this campaign constitutes less of a “scientific” interest compared to other GTRI-FD irradiations (e.g. RERTR and AFIP series tests) where fuel is often driven to extreme conditions in order to amplify fuel performance phenomena. Rather, DDE-MURR constitutes a demonstration of engineering design scale performance. As a result, the campaign is likely to have lower probability of scientific-scale type failures, but constitutes a large consequence of failure in precluding regulatory approval of reactor conversion.

Consequently, the campaign should be treated as a high risk effort and handled appropriately. This should include design efforts strongly focused on failure modes in regards to concept generation, analysis, evaluations, design reviews, and other pertinent arenas. Furthermore, project management strategies should work to this end through use of campaign-focused risk management plans and an emphasis on stable funding in order to foster design team continuity and propensity to identify failure modes. In this regard, stable “modest” funding should be considered superior to sporadic “aggressive” funding.

A Process Founded in Structured Design-Phases

In the context of the original assumptions, the DDE-MURR design concept is a sound strategy. However, some of the original schedule assumptions have already been invalidated. Combined with the possibilities of a redefined base fuel design (driven largely by emergent PIE results), the potential for design modifications of the proposed final LEU conversion element, and prospective design modifications based on forthcoming FFC fabrication studies, it is apparent that the existing DDE-MURR design concept should be evaluated and updated for their applicability at such time as the design work is recommenced. This should include:

- Final approval of the rev 0 Functional and Operational Requirements document with the Critical Characteristics and more detailed campaign mission requirements incorporated
- More detailed hardware design work, as described in section 4.1, with production of detailed engineering drawings
- Updating and final approval of rev 0 Experiment Control Plan complete with plan details regarding design control, quality level determination, and quality assurance measures for the overall design campaign.
- Producing a detailed DDE-MURR schedule, project execution plan, and other deliverables needed for project management. As the experience and knowledge base of key personnel from the BR2 facility were crucial in commencing this work these planning bases should include provisions for on-site collaboration with the BR2.
- Evaluate, in the context of the new schedule constraints, the severity of the risk that BR2 operation will be terminated prior to DDE-MURR completion and identify, if needed, a suitable back-up plan and irradiation location.
- Performance of a conceptual design evaluation with key stakeholders from the GTRI-Convert program to ensure that the concept is appropriately engineered to meet the campaign objectives

- Approval of the conceptual design package by the BR2's Committee for Examination of Experiments (CEE)

Completion of the conceptual design work should give way to completion of the more detailed preliminary work per the experiment control plan and should include the following recommendations:

- Completion and approval of the Technical and Functional Requirements with updating of the F&OR as needed
- Flow testing of a physical mock-up irradiation assembly combined with FSI structural analysis to experimentally determine flowrates and potential for flow induced failure modes. This flow testing should be performed far in advance of the final "acceptance" flow testing that BR2 must perform on the delivered final element and vehicle.
- Functional handling and operation of a physical mock-up irradiation assembly in BR2 facility. These should verify that the assembly can be manipulated underwater through all expected handling evolutions including characterization in the channel gap probe.
- Performance of the full suite of safety analyses required for physics, thermal, structural, and oxide growth/spallation calculations
- Receipt of the official Technical Tolerances submittal and finalization of the coupon and element specifications
- PIE design activities
- Evaluation of the emerging design in the context of potential failure modes and effects
- Performance of a preliminary design evaluation with key stakeholders from the GTRI-Convert program to ensure that the concept is appropriately engineered to meet the campaign objectives
- Approval of the preliminary design package by the CEE

Completion of the preliminary design work should give way to completion of final design per the experiment control plan and should include the following recommendations:

- Finalization of all engineering deliverables
- Fabrication of the final DDE-MURR irradiation vehicle hardware, fuel element, CGP, and ancillary tools/fixtures with the appropriate quality assurance measures and incorporation of any as-built features, if needed, into the original engineering deliverables
- Compilation and approval of the final design and analyses package for the CEE
- Performance of a final design evaluation with key stakeholders from the GTRI-Convert program to ensure that the concept is appropriately engineered to meet the campaign objectives

5. Provisions for Future Work

5.1 Design Team

The following personnel made up the INL portion of the DDE-MURR conceptual design team:

- Bruce Nielson – Experiment Manager
- Nicolas Woolstenhulme – Irradiation Design Lead

- Michael Sprenger – Irradiation Assembly Designer
- Greg Housley – Channel Gap Probe Designer

Additionally, a communication plan was compiled in collaboration with BR2. This provides personnel functions and contact information of the RC, FD, and BR2 team member. This is available in the location shown in section 5.2.

5.2 Document Location

The following items were produced during this design campaign and, at the time this report was prepared, were stored as seen in Table 6.

Table 6: Document Location

Item	Status	Location
DDE Design Status Report Nov 2011	Final rev 0	INL external report INL/EXT-11-23991
Fuel Element Drawings	Draft INL drawing 603455	Appendix G of this report CAD and solid model files reside with ATR Experiment Drafting and are stored on their server
Irradiation Vehicle and CGP Solid Models	In-Progress	Original model files stored in Windchill database management system Exported model on DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
Experiment Control Plan	Draft	DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
Fuel Specifications	Draft, awaiting Technical Tolerances submittal and Preliminary Design work	Appendix F of this report DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
Coupon Specification Composition Worksheet	In-process worksheet “Origin of DDE Coupon Spec Limits.xlsx”	DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
F&OR	Draft	Appendix A of this report DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
Critical Characteristics Submittal	Final Received	DDE design file path

		(\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
Technical Tolerances Submittal	Not yet received Requested information outlined in experiment control plan	n/a
DDE-MURR presentation given at BR2 initial meeting “Irradiation Characteristics of MURR LEU Fuel Design” ^[9]	Received	DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
Physics analysis report “DDE-MURR assembly: Provisional heat fluxes in channels H5, H4, H3” ^[14]	Received	DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
DDE-MURR Communication Plan	Living Document	DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
INL/BR2 action item list from June 2012 on-site visit	Living Document	DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
BR2 FY13 Physics Analysis Report ^[15]	Received	DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)
FY13 CGP and Irradiation Vehicle CAD drawings	Conceptual	DDE design file path (\\fserob1\projects\rertr\Design Demonstration Experiments\DDE-MURR)

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Functional and Operational Requirements

DDE-MURR Irradiation in the BR2



The INL is a U.S. Department of Energy National Laboratory
operated by Battelle Energy Alliance.

Appendix A (Draft F&OR)

Idaho National Laboratory

DDE-MURR IRRADIATION IN THE BR2	Identifier:	FOR- 118	Page: 2 of 12
	Revision:	0 (DRAFT)	
	Effective Date:	XX/XX/XX	

Applicability: Laboratory-wide	Functional and Operational Requirements	eCR Number: XXXXXX
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Management System: Engineering

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Appendix A (Draft F&OR)

Idaho National Laboratory

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1. INTRODUCTION

1.1 Description of Engineering Task

This engineering task will facilitate maturation of Low Enriched Uranium (LEU) fuel technology in order to enable conversion of High Power Research Reactors. To enable conversion of the University of Missouri Research Reactor (MURR), whose licensing basis restricts them from testing lead test elements of its LEU fuel element design ^[1], a Design Demonstration Experiment (DDE) will be irradiated elsewhere using prototypic fuel plate geometries under prototypic conditions (i.e. “end use application” in a “design environment” ^[2]) in lieu of the lead test element methodology. MURR intends to convert using the Base Monolithic Design which consists of uranium-10 wt% molybdenum alloy (U-10Mo) in the form of a monolithic foil, with thin zirconium interlayers, clad in aluminum by hot isostatic press as seen in Figure 1. ^{[3] [4] [5]}

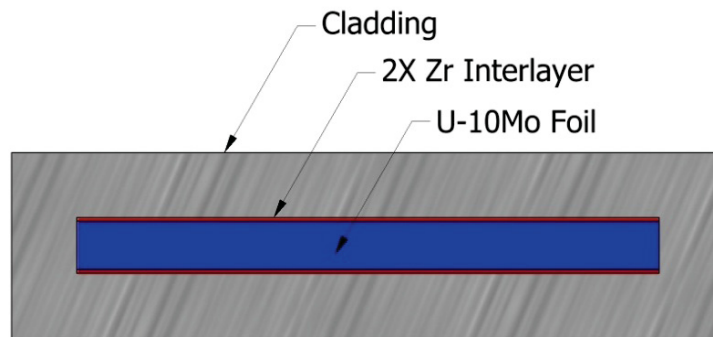


Figure 1: Base Monolithic Design

1.2 Description of the End-Use for the Engineered Item or Activity

The following list constitutes the core goals for the DDE campaign:

- Confirm Performance under stringent prototypic parameters (e.g. heat flux, fission density)
- Show Resistance to worrisome failure modes (e.g. fission gradients, thin-clad structural stability)
- Demonstrate Fabrication by producing the plates/elements as demonstration products ^[6]
- Give Confidence in the LEU fuel design prior to conversion

This design is intended for irradiation in the Belgium Reactor 2 (BR2) and channel gap measurements in the BR2 pool area (hereafter referred to as pool). The majority of the scientific information gathered is planned to occur in Post Irradiation Examination (PIE) activities at the BR2 Facility.

Appendix A (Draft F&OR)

Idaho National Laboratory

DDE-MURR IRRADIATION IN THE BR2	Identifier:	FOR- 118	Page: 4 of 12
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2. OVERVIEW

2.1 Ownership of the F&OR

This F&OR is owned by the Irradiation Testing Lead for the Global Threat Reduction Initiative-Convert (GTRI-Convert) Fuel Development (FD) program. The GTRI-Convert program experiment working group is also responsible for identification of the requirements found in this document.

2.2 End-User of Engineered Item or Activity

End users of this design will include:

- Fuel Fabrication Capability (FFC) pillar fabrication group
- FD characterization group
- BR2 operations
- LHMA post irradiation examination (PIE) group
- Channel gap probe user team
- INL experiment design and analysis group
- MURR stakeholders (who will submit the final data to the Nuclear Regulatory Commission as part of the licensing request to operate with LEU fuel)

3. ENGINEERING INPUTS

3.1 Functional Requirements

- 3.1.1 The DDE-MURR experiment shall be designed to irradiate fuel specimens which include prototypic MURR LEU fuel plate geometry under representative irradiation conditions as defined in the DDE-MURR experiment critical characteristics in Appendix A.
- 3.1.2 The DDE-MURR experiment shall be designed with features which enable irradiation in BR2 for several irradiation cycles.
- 3.1.3 The DDE-MURR experiment shall be designed with fuel plate coolant channel gaps which can be characterized via the channel gap probe.
- 3.1.4 The DDE-MURR experiment should be designed to accommodate dosimeters to enable cycle to cycle as-run benchmarking of burn-up analysis.
- 3.1.5 The DDE-MURR experiment shall be designed to be easily removable and re-installable in the BR2 during routine outages.

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- 3.1.6 The DDE-MURR experiment shall fit within existing fresh and spent fuel shipping containers.
- 3.1.7 The DDE-MURR experiment shall be designed to be characterized by channel gap probe before irradiation, between each cycle (during outage) and after irradiation.
- 3.1.8 The DDE-MURR experiment shall be designed to mitigate the risk of fuel plate damage (e.g. scratches).
- 3.1.9 DDE-MURR components and other extra-reactor handling equipment shall be designed to allow decay heat removal via low-impedance free-convection pathways.
- 3.1.10 The DDE-MURR element side plates of the experiment must enable the fabricator (i.e. Babcock and Wilcox) to “swage” the fuel plates.

3.2 Operational Requirements

- 3.2.1 The DDE-MURR element shall be designed to provide adequate flow and cooling during flow coastdown and reversal conditions.
- 3.2.2 The DDE-MURR experiment shall be designed so that moving part interfaces resist binding, galling, galvanic corrosion, and other phenomena which may cause the assembly to be inoperable.
- 3.2.3 The DDE-MURR experiment shall be designed to be disassembled at the LHMA hot cell facility with minimal redesign of PIE equipment and risk of damaging the fuel plate specimens.
- 3.2.4 The DDE-MURR experiment shall be designed to be capable of 180 degree rotation of the element following each irradiation cycle.
- 3.2.5 The DDE-MURR experiment shall be designed so that duplicate components can be identified with unique features (e.g. identification markings) that are present in locations where the risk for damage or obliteration of such features is minimized.
- 3.2.6 The DDE-MURR experiment shall be easy to handle remotely and must be very robust to mitigate unintended separation of components in the reactor.
- 3.2.7 All materials shall meet BR2 primary coolant system requirements.
- 3.2.8 The DDE-MURR experiment shall be designed for in-core service lifetime of at least ## BR2 cycles

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- 3.2.9 The DDE-MURR experiment shall be designed to allow decay removal adequate to prevent melting of the aluminum cladding in the event that the irradiated assembly is dropped horizontal in water during handling.
- 3.2.10 The DDE-MURR experiment shall minimize the use of difficult or high risk welds, especially thin-to-thick section or small throat aluminum welds.
- 3.2.11 The DDE-MURR experiment shall be designed to provide structural integrity through use of simple and robust components which remain intact during irradiation/handling and alleviate the risk of damaging the fuel plate specimens.
- 3.2.12 The DDE-MURR experiment shall be designed so that the position of the fuel plate specimens/element and all other components remains fixed during reactor operation.
- 3.2.13 The DDE-MURR irradiation test assemblies shall allow for test element fabrication/assembly at the commercial facilities within the fabrication process to be established by the FFC pillar.
- 3.2.14 The DDE-MURR irradiation test assemblies shall allow for non-fueled hardware fabrication/assembly at the commercial facilities within the existing capabilities of facilities at the INL complex.
- 3.2.15 The DDE-MURR irradiation test assemblies shall be designed so that no more than two operators and two handling tools are required concurrently for a given handling evolution (e.g. vessel to pool transport, channel gap examination, reconfiguration, etc.).
- 3.2.16 The DDE-MURR channel gap probe shall be designed to be removable from the pool and stored on the deck or rack.
- 3.2.17 The DDE-MURR irradiation test assemblies shall be designed to facilitate timely accomplishment of outage work so that the specimen extraction, characterizations, and experiment reconfiguration, for one irradiation assembly, can be accomplishment in one normal working day.
- 3.2.18 The DDE-MURR channel gap probe shall be designed to move in 3 directions: radial, linear, and up and down.
- 3.2.19 The DDE-MURR channel gap probe shall be designed to include cameras to aid in alignment and insertion of probe.
- 3.2.20 The DDE-MURR channel gap probe shall be designed to always have a minimum of 3 meters of water coverage over MURR fuel.

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- 3.2.21 The DDE-MURR channel gap probe shall be designed to include a guide block or alignment fixture that will aid the operator in inserting the probe into the MURR fuel.

3.3 Owner Specified Technical Requirements

- 3.3.1 The DDE-MURR experiment should be designed to minimize the acquisition of additional PIE equipment by accommodating with the existing fabrication and PIE infrastructure at the LHMA (e.g. machine tools, PIE measurement bench, etc.).
- 3.3.2 The DDE-MURR irradiation test assemblies shall be designed to satisfy all BR2 safety requirements and to prohibit operational failure modes. The specific requirements relating to this shall be recorded in a Technical and Functional Requirements (TFR) document.

3.4 Supporting Information

3.4.1 Quality Level of Engineered Item or Activity

Those activities needed to perform this engineering task for which graded application is applicable include:

- Calculations and Analysis – QLX per QLD#XXXX rev 0
- Design Control – QLX per QLD#XXXX rev 0
- Configuration Management – QLX per QLD#XXXX rev 0
- Material Acquisitions – QLX per QLD#XXXX rev 0
- Fabrication – QLX per QLD#XXXX rev 0

3.4.2 Need for Configuration Management

Configuration management shall be needed for this engineering activity.

3.4.3 Sensitive Information

This engineering activity is not expected to include or produce information of a sensitive nature.

3.4.4 Need for Engineering Change Control

Engineering change control shall be needed for this engineering activity.

3.4.5 Level of Verification Needed

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The engineering deliverables associated with this design shall be verified by way of design review per the applicable INL procedure. Additionally, the GTRI-Convert program experiment working group will review the design and ensure that it is adequately engineered to meet the programmatic experiment objectives. These design reviews shall each take place upon completion of the conceptual, preliminary, and final design phases of the DDE-MURR experimental campaign.

3.4.6 Technical Integrator

The technical integrator is the Experiment Manager for the DDE-MURR irradiation campaign.

4. REFERENCES

- [1] M.K. Meyer and R.B. Nielsen, “Utilization of the Center Flux Trap for Irradiation During Cycles 157A – 160B”, draft white paper 11/17/11.
- [2] “Applying Quality Assurance Requirements to Research and Development Activities”, rev 3, 8/12/2010, INL Document LWP-13016.
- [3] N.E. Woolstenhulme, D.M. Wachs, and M.K. Meyer, “Design and Testing of Prototypic Elements Containing Monolithic Fuel”, Proceedings of the RERTR-2011 International Conference, Santiago Chile, October 23-27, 2011.
- [4] D.M. Wachs, “RERTR Fuel Development and Qualification Plan”, rev 5, 07/05/2011, INL external report INL/EXT-05-01017.
- [5] A.B. Robinson et al., “Irradiation Performance of U-Mo Alloy Based ‘Monolithic’ Plate-Type Fuel – Design Selection”, INL external report INL/EXT-09-16807, Aug. 2009.
- [6] D.E. Burkes, “Overview of the GTRI Fuel Fabrication Capability (FFC) Project”, presentation given at High Power Research Reactor Working Group Meeting, Cambridge Massachusetts, July 26-27, 2011.

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Appendix A

Critical Characteristics Submittal for DDE-MURR

J. Stevens
RC National Technical Lead

Date

C. McKibben
MURR Director

Date

E. Wilson
RC Analysis Lead

Date

Introduction

The University of Missouri Research Reactor (MURR) is slated for conversion to Low Enriched Uranium (LEU) using a monolithic Uranium Molybdenum (U-Mo) alloy base fuel design which is currently under development by the Fuel Development (FD) pillar of the Agency Global Threat Reduction Initiative Convert (GTRI-Convert) program. The MURR licensing basis restricts them from testing their own LEU lead test elements. Consequently, a Design Demonstration Experiment campaign (DDE-MURR) will be performed with irradiation of MURR prototypic LEU fuel plates/assemblies in the Best Reactor 2 (BR2) located in Belgium in the chosen H position.

As set forth in INL document PLN-4060, the DDE-MURR campaign will be executed primarily by the FD pillar. Scoping design and feasibility studies have shown that this irradiation campaign can likely achieve the experiment objectives. The FD pillar is ready to enter a formalized engineering process, beginning with conceptual design, and requires further explication of experiment objectives from the Reactor Conversion (RC) pillar of the GTRI-Convert program. This submittal is referred to as the Critical Characteristics of the experiment. The sections below constitute submittal of the requested Critical Characteristics.

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Nominal Fuel Element Design

Table 1: Nominal Element Characteristics

Plates Per Element	Interior Channel Spacing

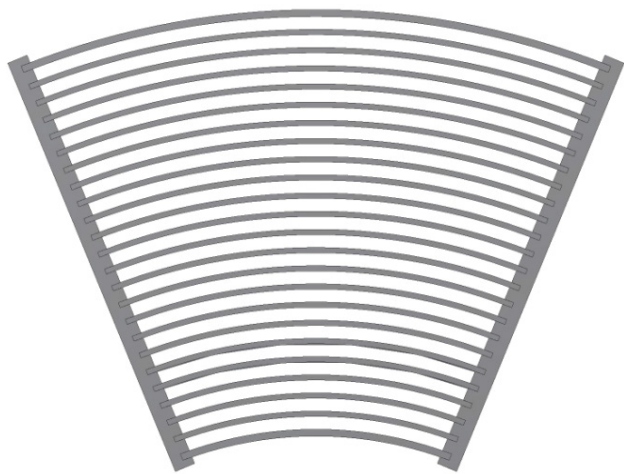


Table 2: Nominal Plate Dimensions

Plate Number	Plate Length	Plate Width	Plate Total Thickness	Plate Radius	Fuel Length	Fuel Width	Fuel Thickness (U-Mo)

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Table 3: Plate Constituents

Plate Number	U-Mo Mass	U-235 Mass	Zr Mass	Al-6061 Mass
##				
##				
##				
##				
##				
##				
##				
##				
##				
##				
##				
##				
##				
##				
##				
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##				
##				
##				

Target Irradiation Conditions

Table 4: Key Irradiation Parameters

Parameter	Value
Coolant Velocity	
Peak Local Heat Flux	
Peak Plate Surface Temp	
Peak Fuel Meat Centerline Temp	
Target Fission Density (total fissions from all isotopes)	

Fuel plate 2D heat flux maps for the peak case were obtained. For the hottest plate, results can be seen in Table 5. In order to give refined results each fuel meat was analyzed with ## and ## cells in the transverse and axial directions, respectively.

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Table 5: Fuel Plate Heat Flux (W/cm2)

Plate Number ##		Cell Transverse Location (from edge of fuel meat)									
		##	##	##	##	##	##	##	##	##	##
Cell Axial Location (from top of fuel meat)	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##
	##	##	##	##	##	##	##	##	##	##	##

The normal NBSR LEU fuel cycle is expected to consist of ## cycles of approximately ## full power days each. The peak conditions noted above are expected to occur at ##. Beginning and end of life heat fluxes are expected to be ## and ##, respectively. More detailed 2D heat flux maps for time steps of interest can be seen

Discussion

It is acknowledged that the above Critical Characteristics were produced as part of a suite of ongoing analyses, design, and development activities lead by the RC pillar. While these Critical Characteristics may be subject to change, they represent the best known data at this time and are the most appropriate design inputs for proceeding with the conceptual design of DDE-NBSR. Any future changes to the Critical Characteristics will be communicated in follow-on submittals.

Appendix B (FY13 Physics Analysis Inputs)

DDE-MURR Physics Analysis Inputs - March 2013

This document contains information regarding the features of nuclear significance for the DDE-MURR conceptual design produced during 2012. Please use this information to build physics models for the further analysis. If there are any discrepancies or questions feel free to contact Bruce Nielson, Nick Woolstenhulme, or Greg Housley.

Primary objectives of this analysis:

- Produce neutronic analysis results using the design produced during conceptual design (

Appendix B (FY13 Physics Analysis Inputs)

- Table 1, Figure 1 through Figure 8)
 - Match MURR conversion analysis ^[1] fuel meat mesh: Each plate with 24 equal length axial zones and 9 equal width azimuthal zones (azimuthal zone width varies based on plate width type 1-23)
- Further investigate BR2 core load and experiment position (H3, H4, or H5) best suited to achieving the following conditions ^[2]
 - Peak local heat flux $>215 \text{ W/cm}^2$, on plate 23
 - Peak fission density $>4.0\text{E}+21$ fissions/cc, in plate 1
 - Approximate plate-to-plate power profile (see Figure 1), further investigate the effect of 180 degree test vehicle rotation between BR2 cycles

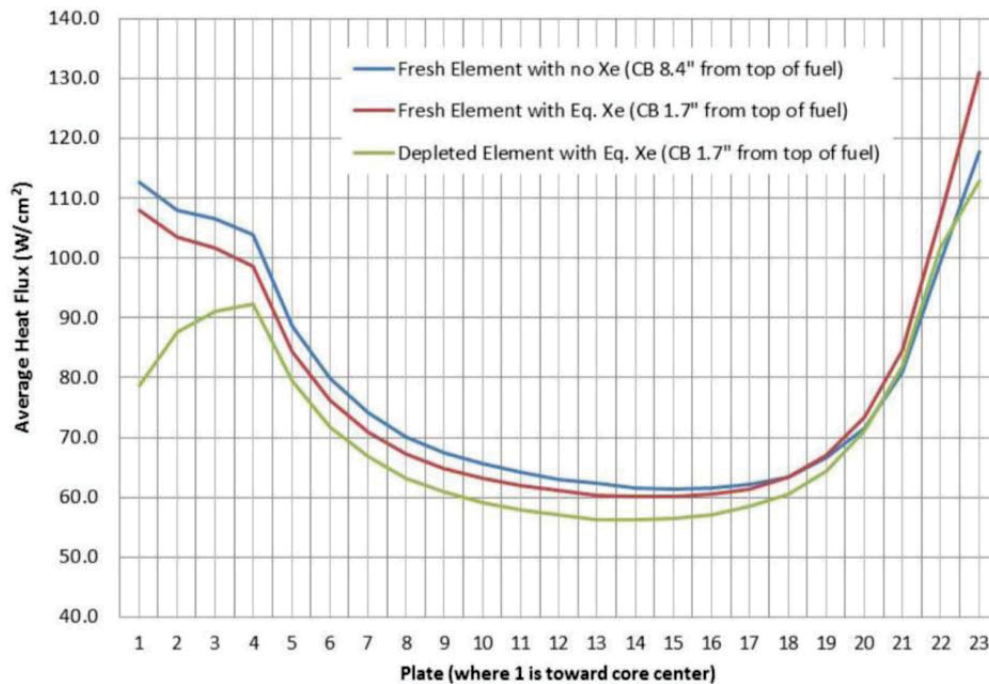


Figure 1: Plate to Plate Power Profile ^[1]

Appendix B (FY13 Physics Analysis Inputs)

Table 1: DDE-MURR Nominal Plate Volumes and Masses

Plate	Constituent Volumes			Constituents Masses					
	Fuel Core	Interlayer	Cladding	Fuel Core				Interlayer	Cladding
	U-Mo Volume (cm3)	Zr Volume (cm3)	Al-6061 Volume (cm3)	U-Mo Mass (g)	Total U Mass (g)	U-235 Mass (g)	Mo Mass (g)	Zr Mass (g)	Al-6061 Mass (g)
1	5.98	1.33	29.09	101.81	91.63	18.10	10.18	8.68	78.55
2	8.48	1.41	28.48	144.34	129.91	25.66	14.43	9.23	76.89
3	11.99	1.50	26.87	204.03	183.62	36.27	20.40	9.78	72.55
4	15.83	1.58	24.92	269.36	242.42	47.88	26.94	10.33	67.27
5	16.68	1.67	25.97	283.82	255.43	50.45	28.38	10.89	70.11
6	17.52	1.75	27.01	298.14	268.33	52.99	29.81	11.44	72.93
7	18.36	1.84	28.05	312.47	281.22	55.54	31.25	11.99	75.74
8	19.19	1.92	29.08	326.66	293.99	58.06	32.67	12.53	78.52
9	20.03	2.00	30.12	340.98	306.88	60.61	34.10	13.08	81.34
10	20.88	2.09	31.17	355.31	319.78	63.16	35.53	13.63	84.15
11	21.72	2.17	32.21	369.63	332.67	65.70	36.96	14.18	86.96
12	22.56	2.26	33.25	383.96	345.56	68.25	38.40	14.73	89.77
13	23.39	2.34	34.28	398.15	358.33	70.77	39.81	15.28	92.56
14	24.23	2.42	35.32	412.47	371.22	73.32	41.25	15.83	95.37
15	25.08	2.51	36.36	426.80	384.12	75.86	42.68	16.37	98.18
16	25.92	2.59	37.41	441.12	397.01	78.41	44.11	16.92	100.99
17	26.76	2.68	38.45	455.45	409.90	80.96	45.54	17.47	103.81
18	27.59	2.76	39.48	469.64	422.67	83.48	46.96	18.02	106.59
19	28.43	2.84	40.52	483.96	435.56	86.02	48.40	18.57	109.40
20	29.28	2.93	41.57	498.42	448.58	88.59	49.84	19.12	112.24
21	30.13	3.01	42.61	512.74	461.47	91.14	51.27	19.67	115.05
22	30.98	3.10	43.66	527.20	474.48	93.71	52.72	20.23	117.89
23	27.06	3.18	58.57	460.64	414.58	81.88	46.06	20.79	158.15
Mass Totals (g)				8477.08	7629.37	1506.80	847.71	338.78	2145.04

Isotopic composition of the fuel meat is specified in Table 2 (taken from Appendix B of reference [2]).

Table 2: Isotopic Specification

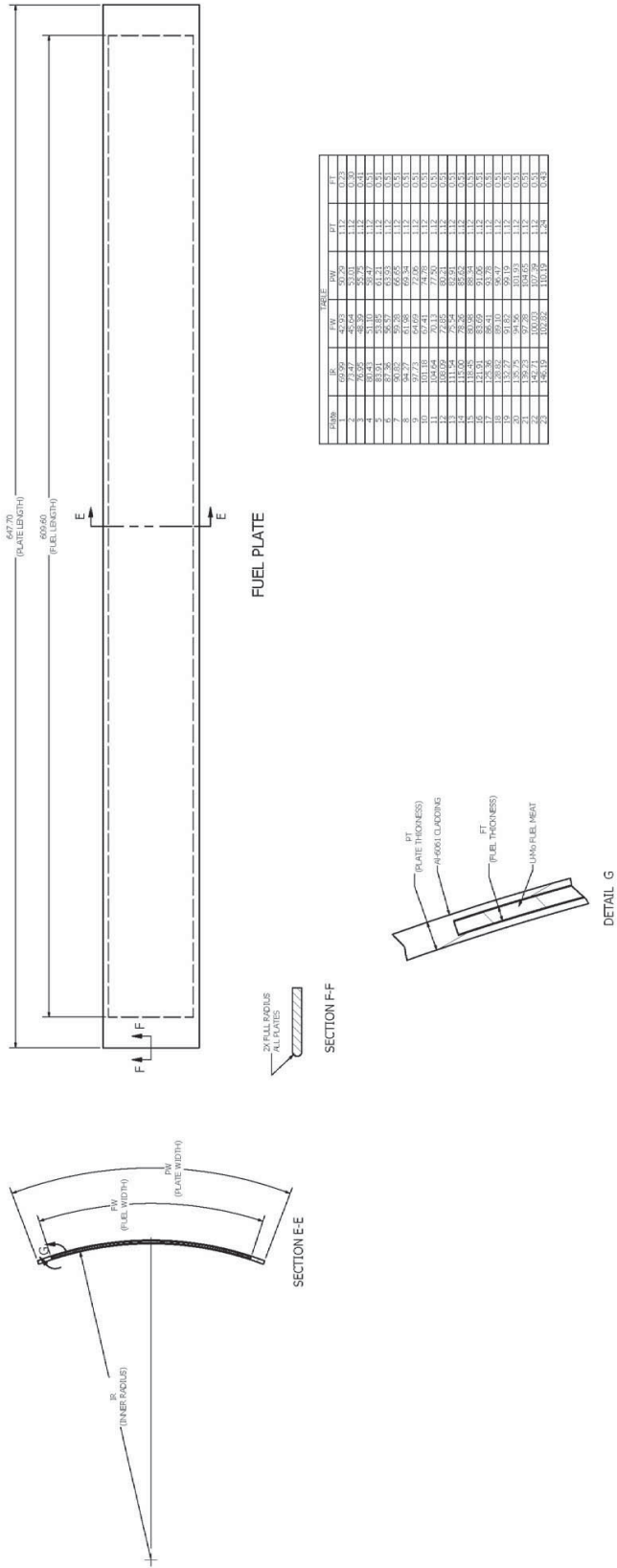
Element	Symbol	Units	Limit
U-232	U-232	μg/gU	≤ 0.002
U-234	U-234	wt%U	≤ 0.260%
U-235	U-235	wt%U	19.75% +0.20% -0.30%
U-236	U-236	μg/gU	≤ 4600
Trans-U (Alpha)	TRU	Bq/gU-Mo	≤ 250.0
Fission Products	Gamma	Bq/gU-Mo	≤ 600.0

Appendix B (FY13 Physics Analysis Inputs)

References:

- [1] J. Stillman et al., “Conceptual Design Parameters for MURR LEU U-Mo Fuel Conversion Design Demonstration Experiment”, ANL/RERTR/TM-12-38, pre-print edition September 2012.
- [2] N.E. Woolstenhulme et al., “DDE-MURR Status Report of Conceptual Design Activities”, INL/EXT-12-27078, September 2012.

Appendix B (FY13 Physics Analysis Inputs)



DDE-MURR
ALL DIMENSIONS IN MM

Figure 3

Appendix B (FY13 Physics Analysis Inputs)

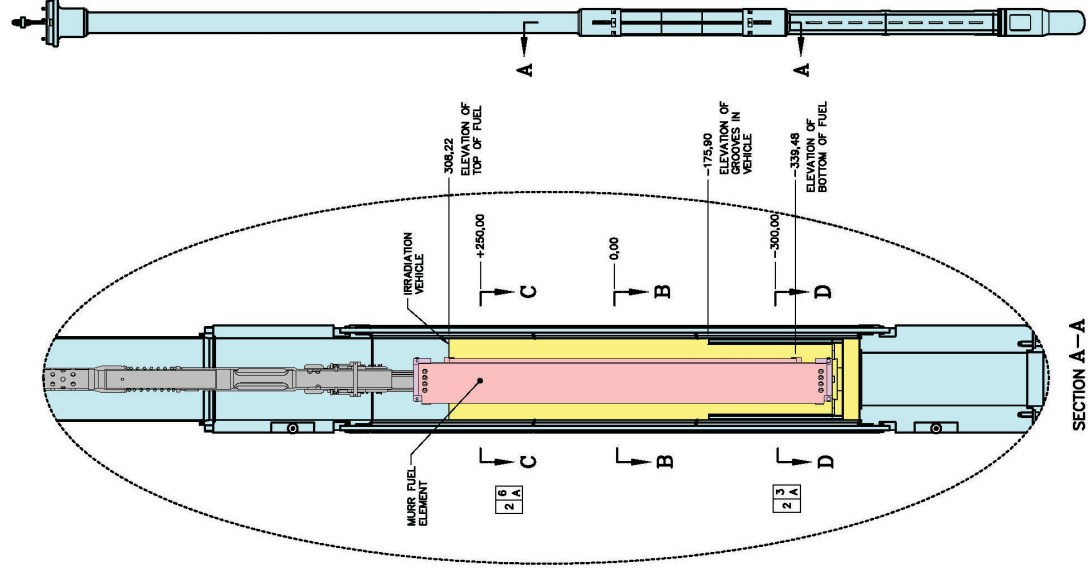


Figure 4

Appendix B (FY13 Physics Analysis Inputs)

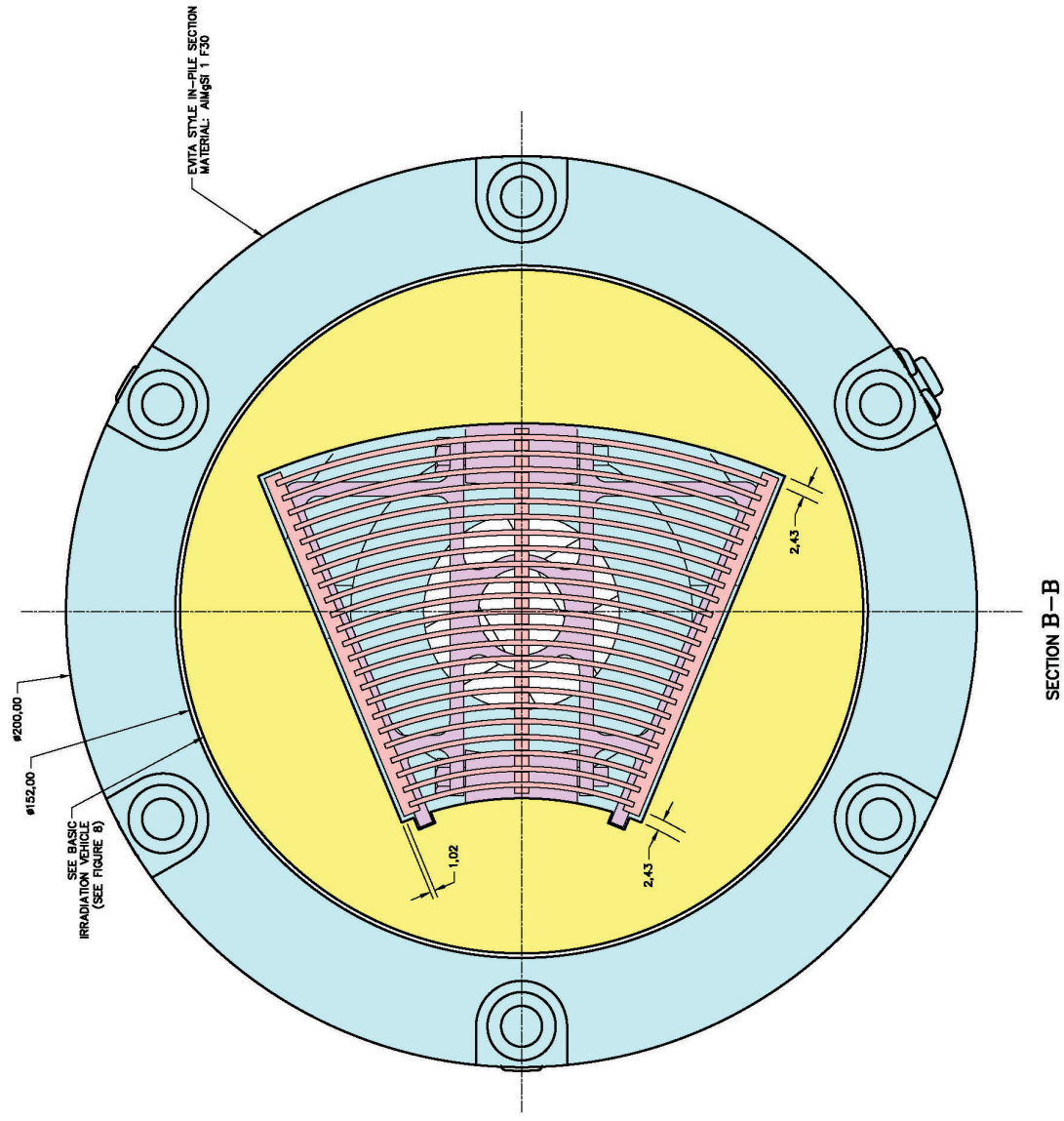


Figure 5

Appendix B (FY13 Physics Analysis Inputs)

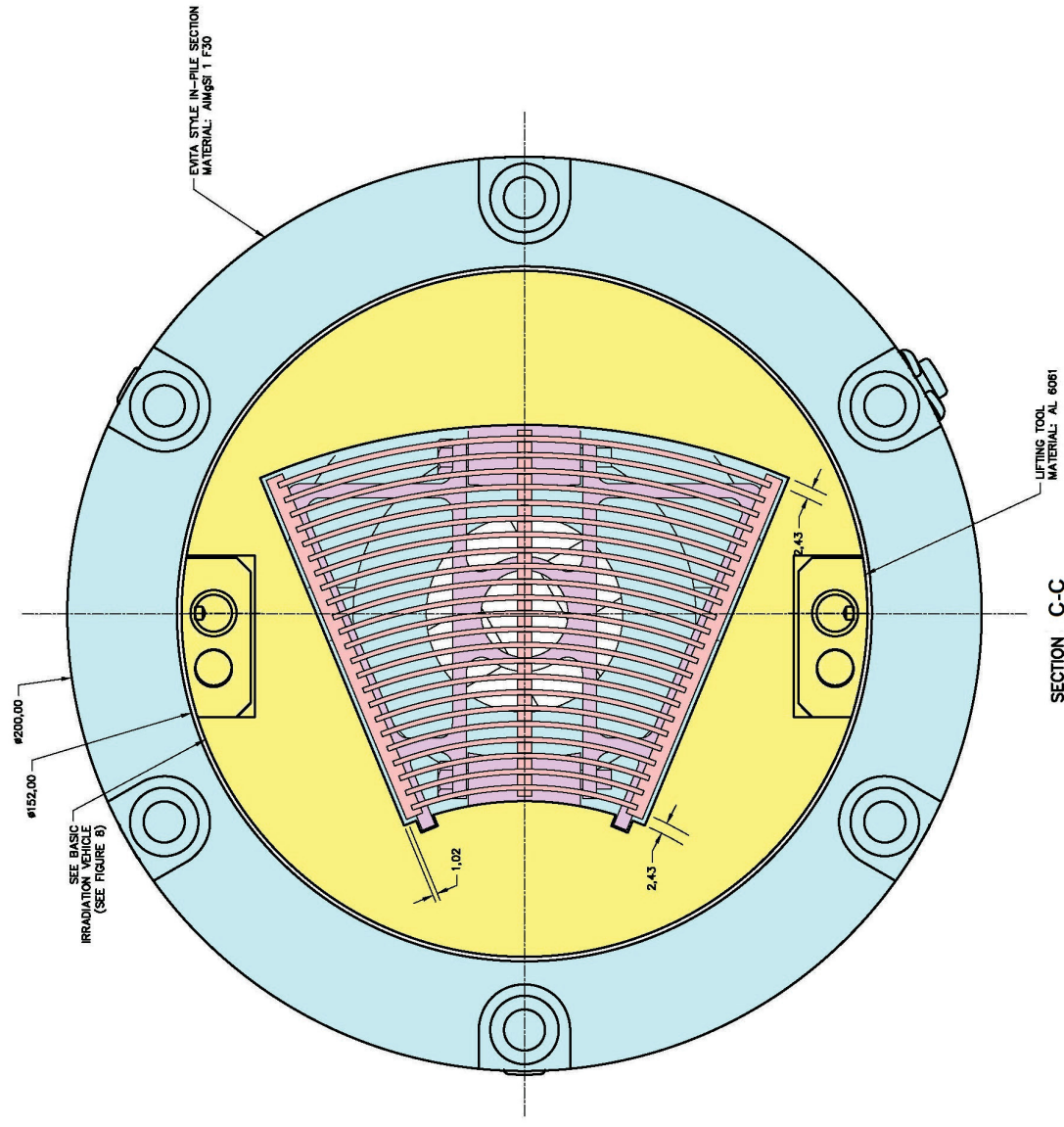


Figure 6

Appendix B (FY13 Physics Analysis Inputs)

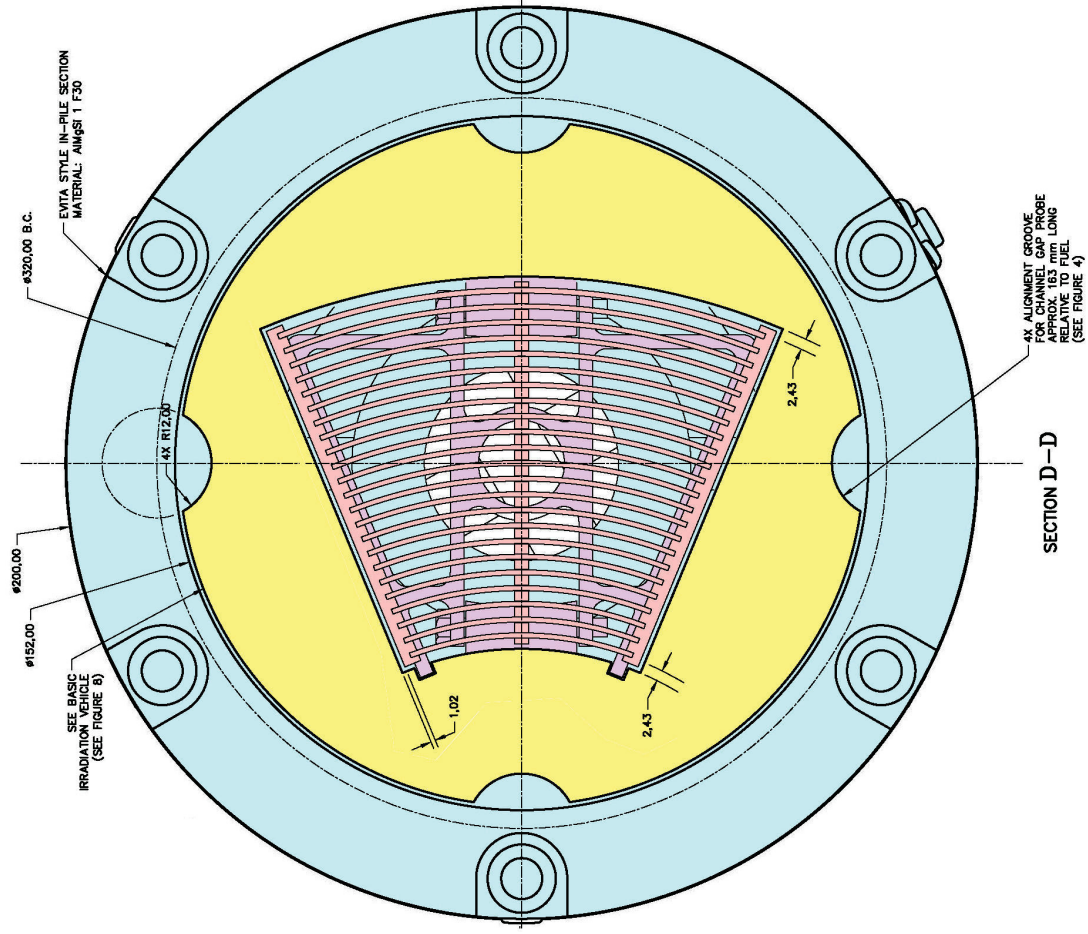
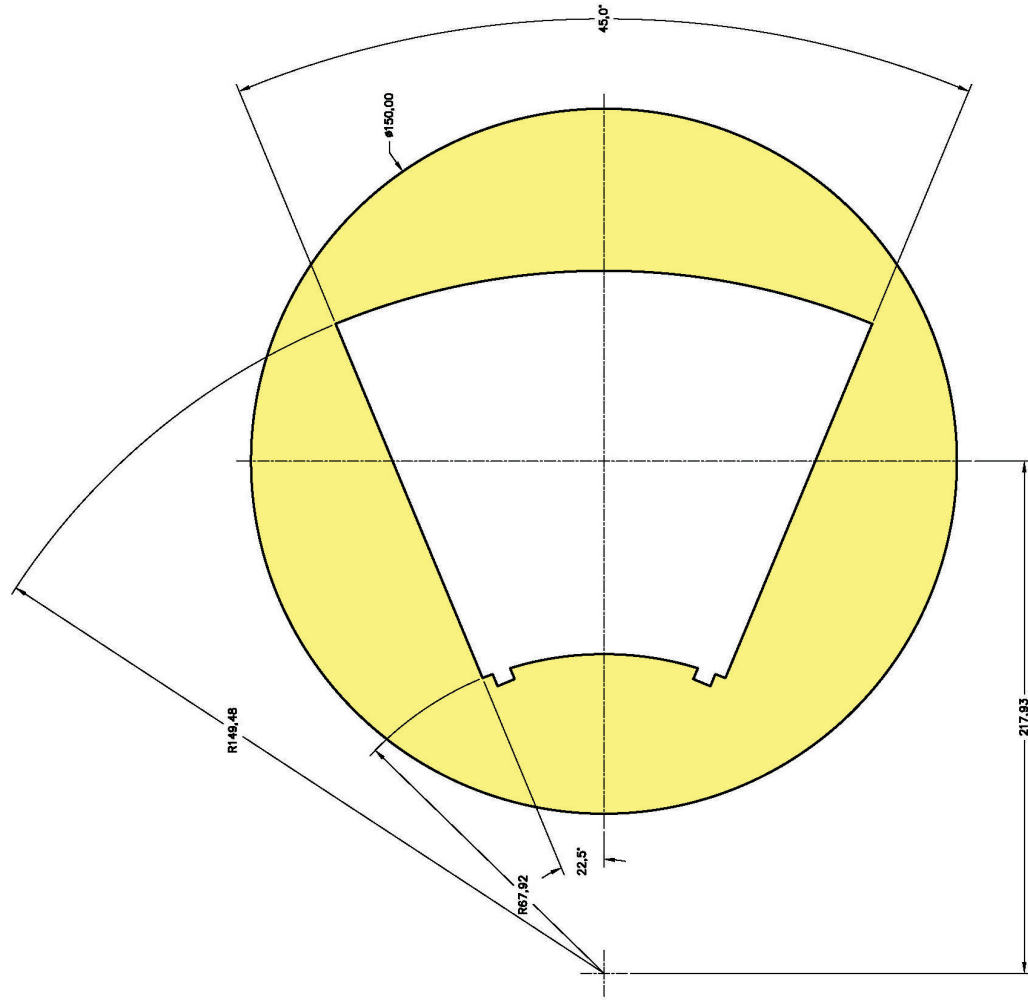


Figure 7

Appendix B (FY13 Physics Analysis Inputs)



BASIC IRRADIATION VEHICLE
MATERIAL: AL 6061

Figure 8

Appendix C (Design Chronology)

The DDE design effort was commenced in mid-2010 for three distinct campaigns; one for each MITR, MURR, and NBSR. This was premised around the original proposal to irradiate each in an Advanced Test Reactor (ATR) Medium I position. As a result, the efforts primarily concerned designing an experiment, consisting of LEU fuel meat, which would fit in to the Medium I position geometry, which can accommodate just over three inches of useable test geometry with the existing liner cans removedⁱ, while meeting the ATR TSR requirement of <365g U-235 per experiment positionⁱⁱ.

Resources for designers and analysts were difficult to ascertain until the effort was better funded in Fiscal Year 2011 (FY11). It was at this point that analysts identified that the low fluence of ATR I positions gave fission rates which failed to approach the irradiation conditions of each reactor. Budget cuts in March of 2011 caused suspension of further investigations until June of that year when a small budget was allocated to evaluate DDE designs with increased fuel meat enrichment (i.e. HEU). While scoping analysis indicated that HEU fuel meat could give fission rates representative of the MITR, these efforts were unsuccessful for the DDE-MURR and DDE-NBSR experiments. As a result, alternate experiment positions were evaluated and one of the 200mm “H” positions of the Belgium Reactor 2 (BR2) was selected for DDE-MURRⁱⁱⁱ.

The DDE work languished somewhat due to inadequate funding in FY11, but was revived in FY12 with meaningful funding and allocation of personnel. This is the general timeframe when the conceptual design work is considered to have been commenced. Design efforts for DDE-MITR and DDE-NBSR (both planned for irradiation in ATR) were aggressive in early FY12 in order to accommodate an HPRR conversion schedule which would require completion of these DDE’s irradiation around 2015 while DDE-MURR represented a different schedule strategy due to irradiation in BR2. Efforts were undertaken to mature this schedule in collaboration with BR2 personnel. Experiment plans were drafted and called for formal submission of the aforementioned Critical Characteristics, as well as another set of inputs referred to as the Technical Tolerances, from the RC pillar in mid FY12. These were intended to facilitate further design work and production of specifications for the DDE U-Mo coupons and fuel elements. This planning effort also identified the need for design and engineering of a new Channel Gap Probe (CGP) to be installed at BR2 to support characterization of the DDE-MURR element coolant channels before, during, and after irradiation. INL held regular conference calls with key personnel from the RC and Fuel Fabrication Capability (FFC) pillars as well as representatives from the each reactor in order to define experiment parameters, discuss design options, and foster communication between the design team and stakeholders.

Formal submission of both the Critical Characteristics and Technical Tolerances was postponed due to re-prioritization of GTRI-Convert personnel resources which was caused, to some extent, caused by emergent PIE blister threshold results from the RERTR-12 and AFIP-4 campaigns^{iv}. These prompted reduction of the DDE funding level in mid FY12 with the intent to complete less design work than originally intended. Regardless, the aforementioned specifications were produced for each DDE design, but are considered to be inadequately mature for fabrication of final DDE products and are included in Appendices C and D for reference purposes. While these were not required as INL milestones as were the same for DDE-MITR and DDE-NBSR, completion of the DDE-MURR draft specifications was undertaken in the interest of good documentation as it only required minimal modification of those produced for the other DDE campaigns.

Due to difficulties in arranging onsite meetings (i.e. at BR2), which eventually proved to be paramount in defining the scope, schedule, roles, and responsibilities of both GTRI and BR2 personnel, the status of the DDE-MURR design work trailed that of DDE-MITR and DDE-NBSR slightly. However, the DDE-MURR conceptual design work saw meaningful acceleration in the second half of FY12. Personnel from the RC pillar were instrumental in providing the majority of the needed information, prior to official submittal of the Critical Characteristics document in late FY12, in a detailed presentation on the emergent MURR “CD-35” design with the new 23 plate LEU element geometric scheme and the corresponding irradiation conditions^v. This material was presented at the initial BR2 onsite meeting in April of 2012 and

Appendix C (Design Chronology)

enabled BR2 personnel to proceed with more detail physics analysis^{vi}. The initial onsite meeting also revealed that BR2 did not have adequate personnel to support the design of the irradiation vehicle and CGP and requested that INL provide design, engineering, drafting, and fabrication services in this regard. A second design meeting with BR2 in June of 2012 saw significant maturation of the design needs and preferred concepts for the irradiation vehicle and CGP.

Toward the latter end of FY12 several factors drove a new HPRR conversion schedule to be proposed. This invalidated some the original DDE design assumptions, particularly those pertaining to schedule constraints, and also gave way to a suspension of DDE-related funding in FY13. As a result, the DDE design team endeavored to use the remaining FY12 resources to finalize a few important activities and document the results in preparation for a hiatus in DDE design work; resulting in the preparation of this document. However, funding overruns in another project which shared the DDE control account forced abandonment of some critical DDE design activities. These, in combination with the already trailing design work, gave way to a conceptual design status that was not considered entirely complete at the time that rev 0 of this report was prepared.

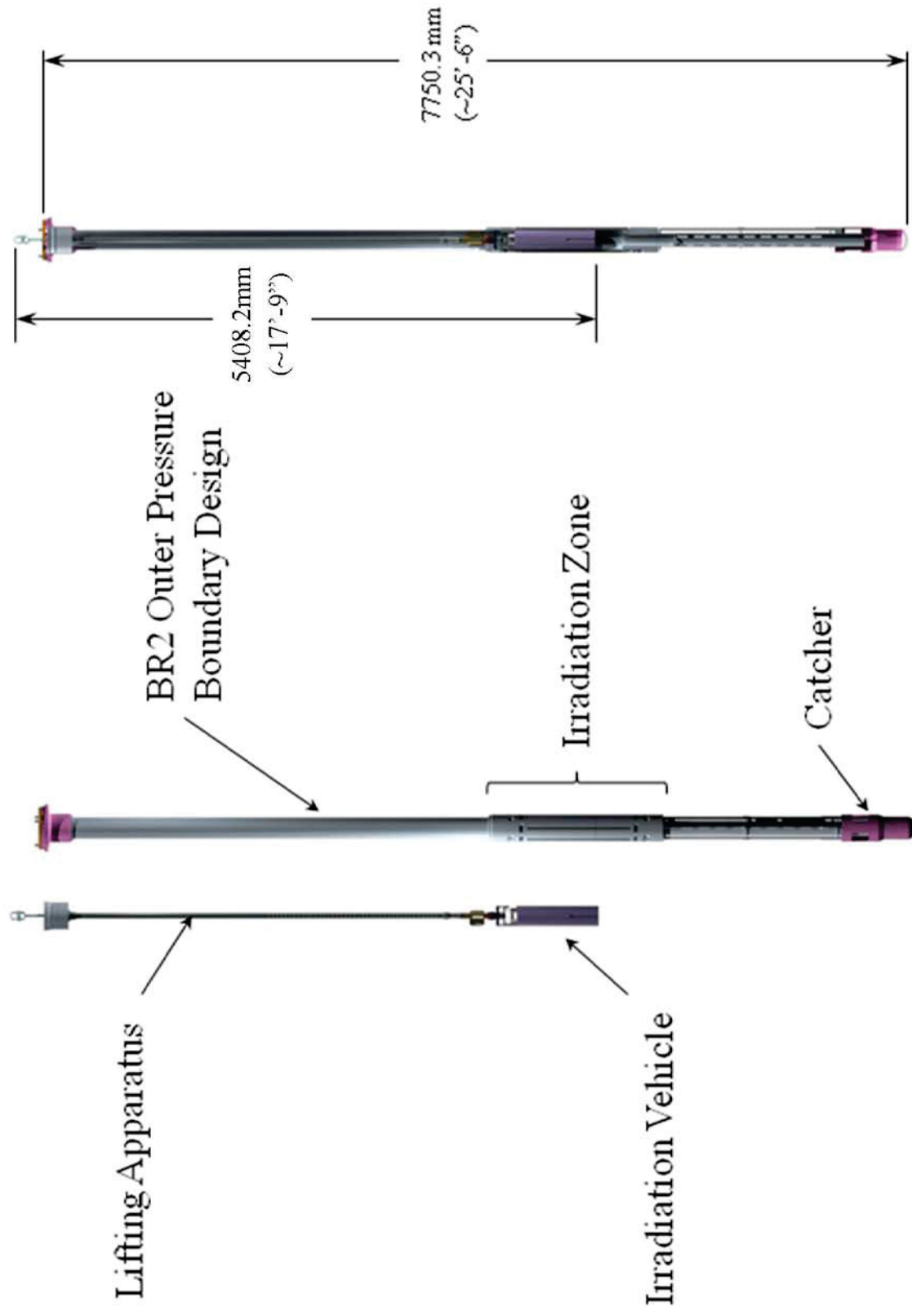
FY12 funds that had been committed to a BR2 contract for more detailed neutronic analysis carried execution of such into FY13. Hence, a small allocation was given to the INL to provide input and interface with BR2's neutronic analysts during execution of this contract. Another small allocation of FY12 carryover funds for RC's involvement in DDE-MURR became available to support related work in FY13 at the INL. It was determined that these resources should be devoted to interfacing with BR2 during the contracted analysis, bringing DDE-MURR up to a similar level of design maturity as the other two DDE's^{vii, viii} by producing engineering sketches of the irradiation vehicle and channel gap probe, and updating this report to reflect these developments. Although the effort in FY13 served to mature the DDE-MURR concept somewhat, several recommendations, concerns, risk, and incomplete activities still existed.

References for this Appendix

- i. INL Drawing 419609, "ATR Beryllium Reflector Blocks Mark IV", 7-11-1984.
- ii. INL Document TSR-186, "ATR Complex-ATR Nuclear Safety Basis - Technical Safety Requirements".
- iii. J.C. McKibben, et. al, "Progress Made on the University of Missouri Research Reactor HEU to LEU Fuel Conversion Feasibility Study", proceedings of the RERTR-2007 International Conference, Prague, Czech Republic, Sep 23-27, 2007.
- iv. INL External Report INL/EXT-12-26500, "Investigation Of The Cause Of Low Blister Threshold Temperatures In The RERTR-12 And AFIP-4 Experiments", rev 0, 06/28/2012.
- v. J. Stevens to N. Woolstenhulme, "MURR DDE Critocal [*sic*] Characteristics ppt from BR2 Visit", email 5/9/2012, attachment "Stevens_MURR_DDE_Element_Requirements_120417rev1.ppt"
- vi. V. Kuzminov to S. Van Dyck and E. Koonen, "DDE-MURR assembly: Provisional heat fluxes in channels H5, H4, H3", technical note 06/18/2012.
- vii. N.E. Woolstenhulme, R.B. Nielson, J.D. Wiest, J.W. Nielsen, G.A. Roth, and S.D. Snow, "DDE-MITR Status Report of Conceptual Design Activities", rev 0, September 2012, INL/EXT-12-27077.
- viii. N.E. Woolstenhulme, R.B. Nielson, B.P. Durtschi, C.R. Glass, G.A. Roth, and D.T. Clark, "DDE-NBSR Status Report of Conceptual Design Activities", rev 0, September 2012, INL/EXT-12-27079.

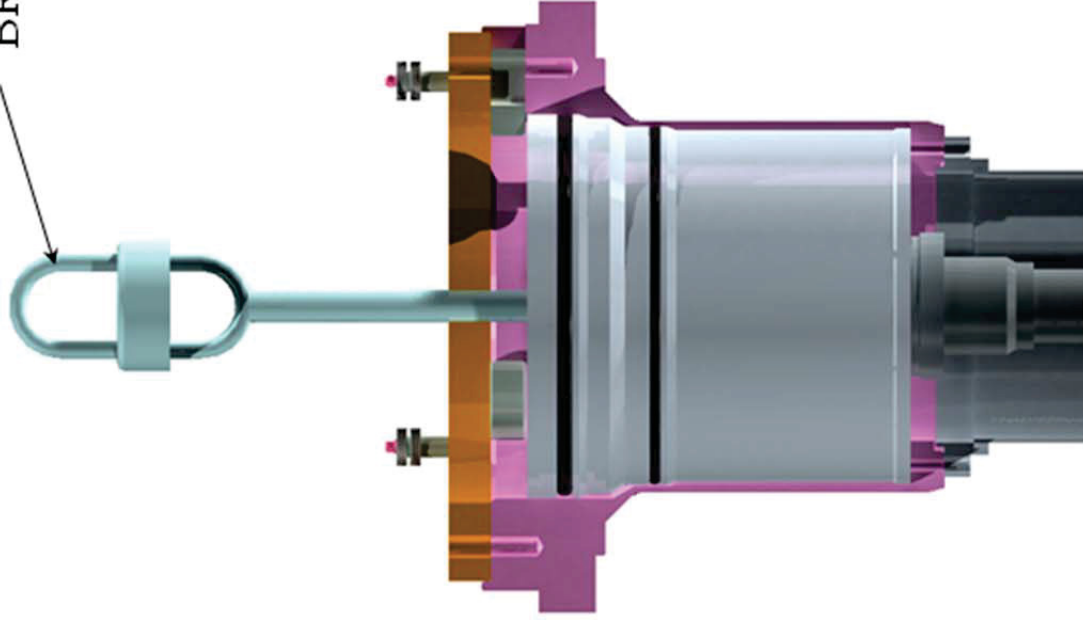
Appendix D (Irradiation Vehicle Design)

DDE-MURR Irradiation Vehicle and Outer Pressure Boundary

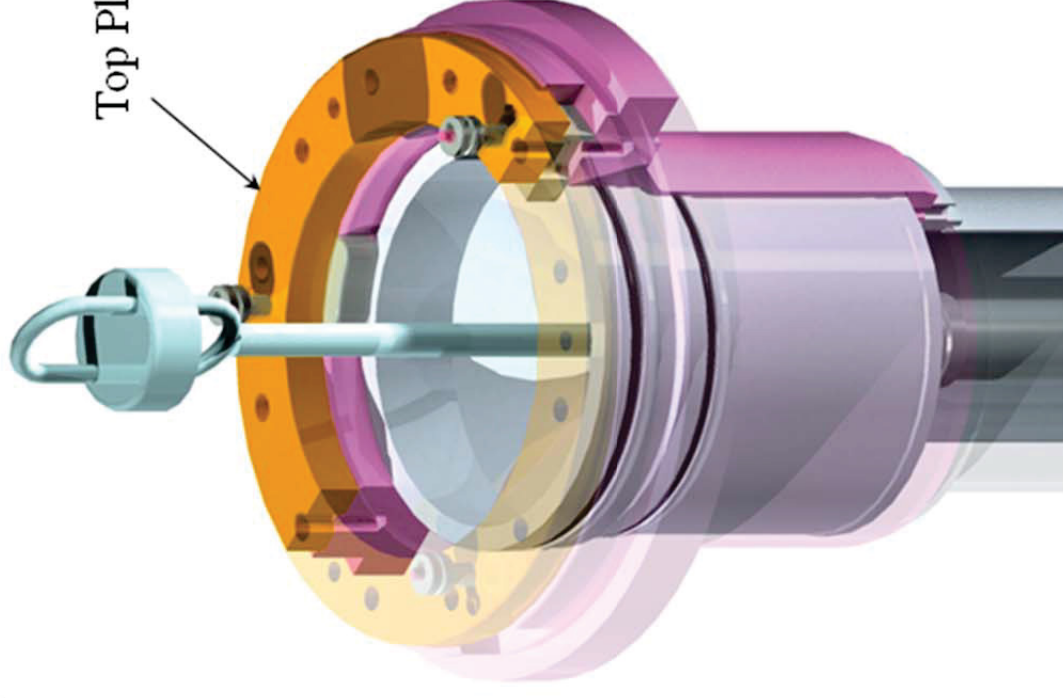


DDE-MURR BR2 Experiment Top View

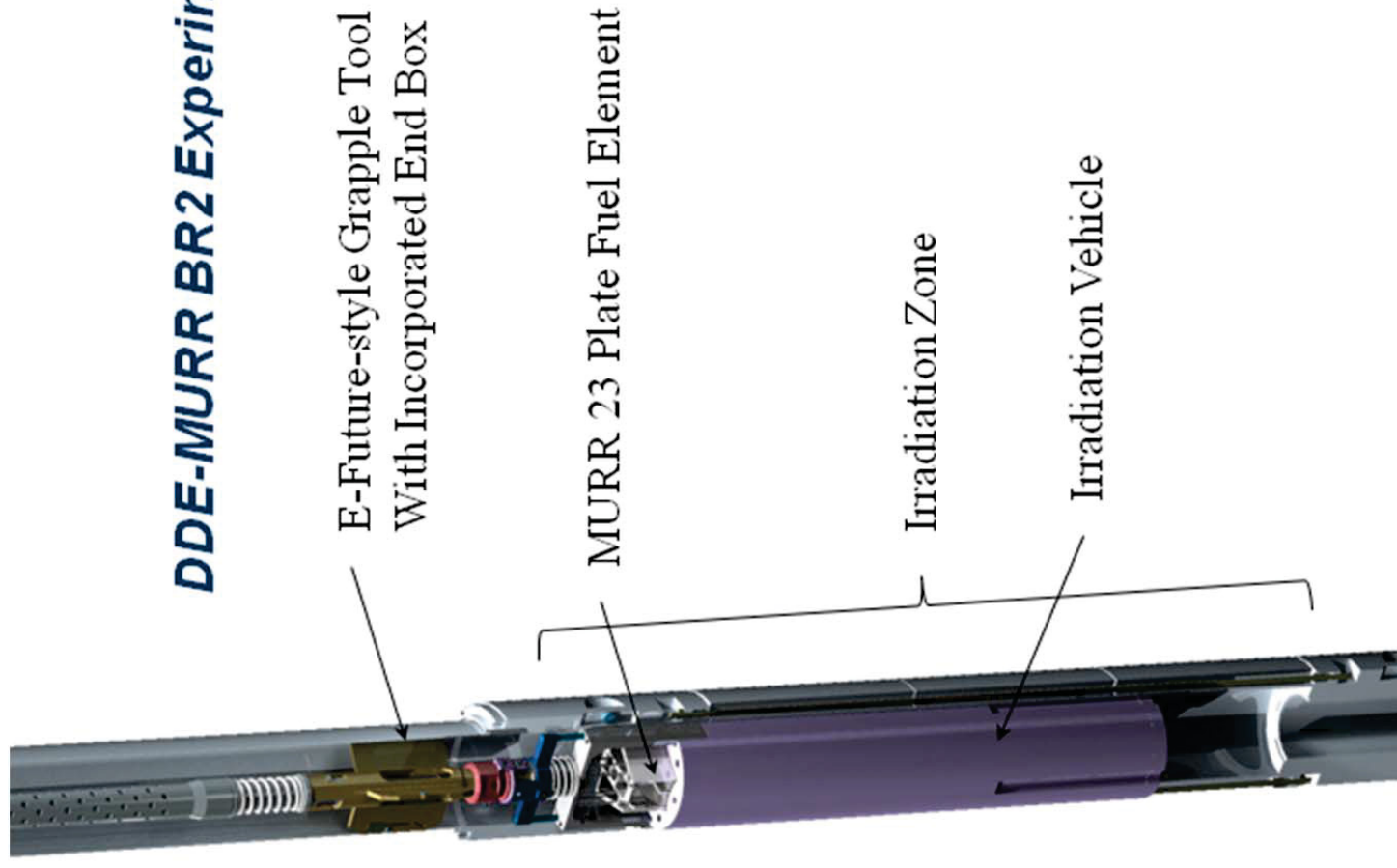
BR2 Lift Bail



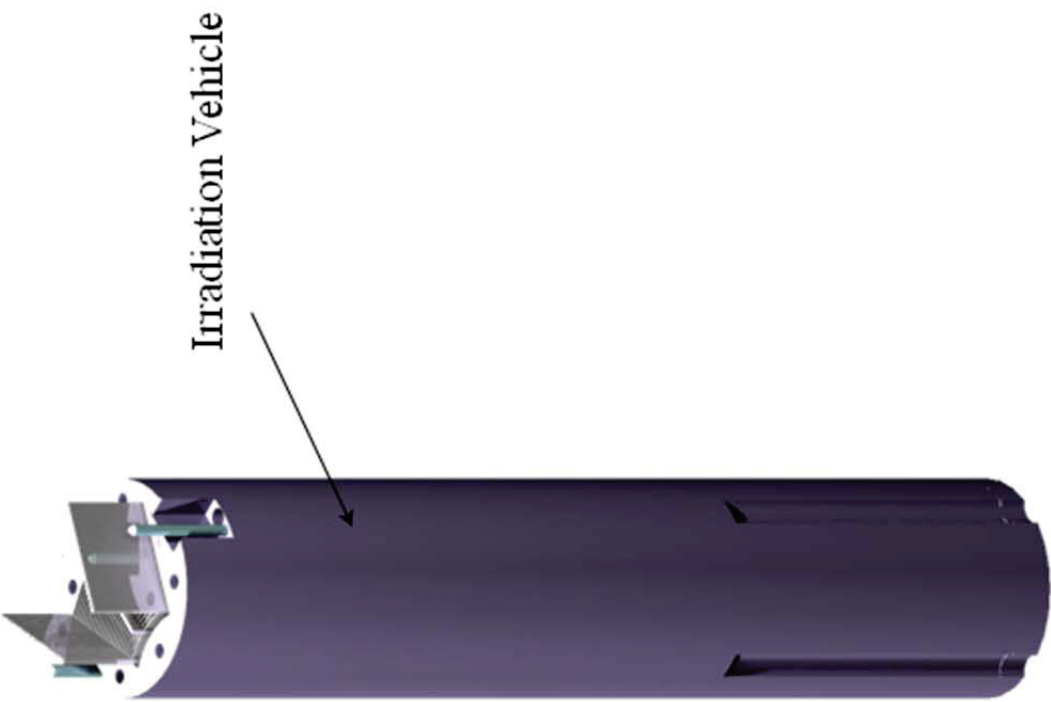
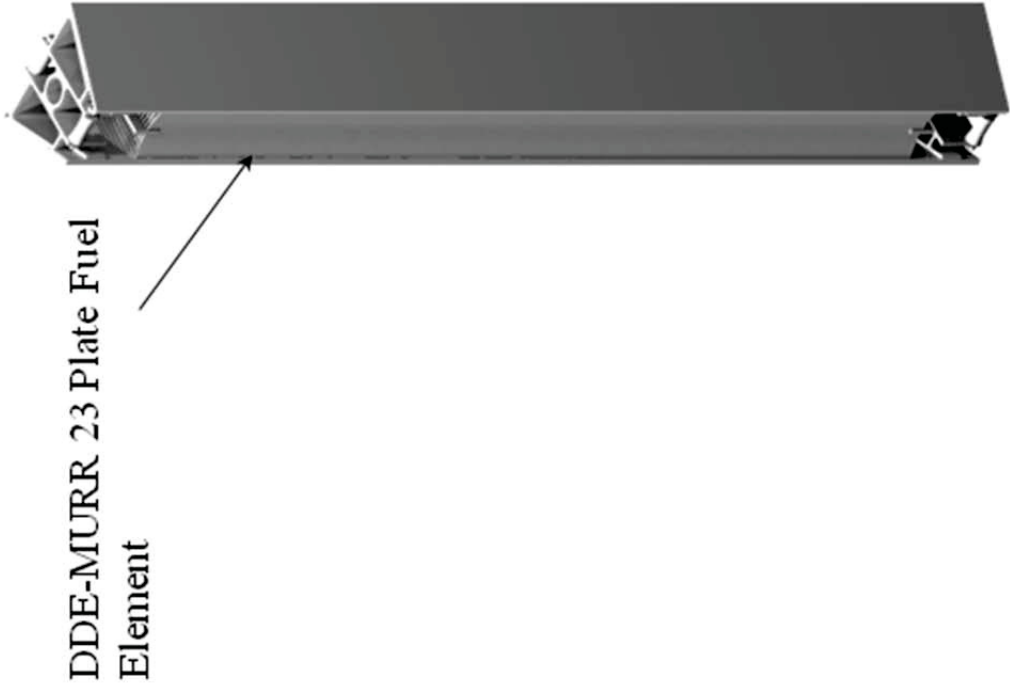
Top Plug



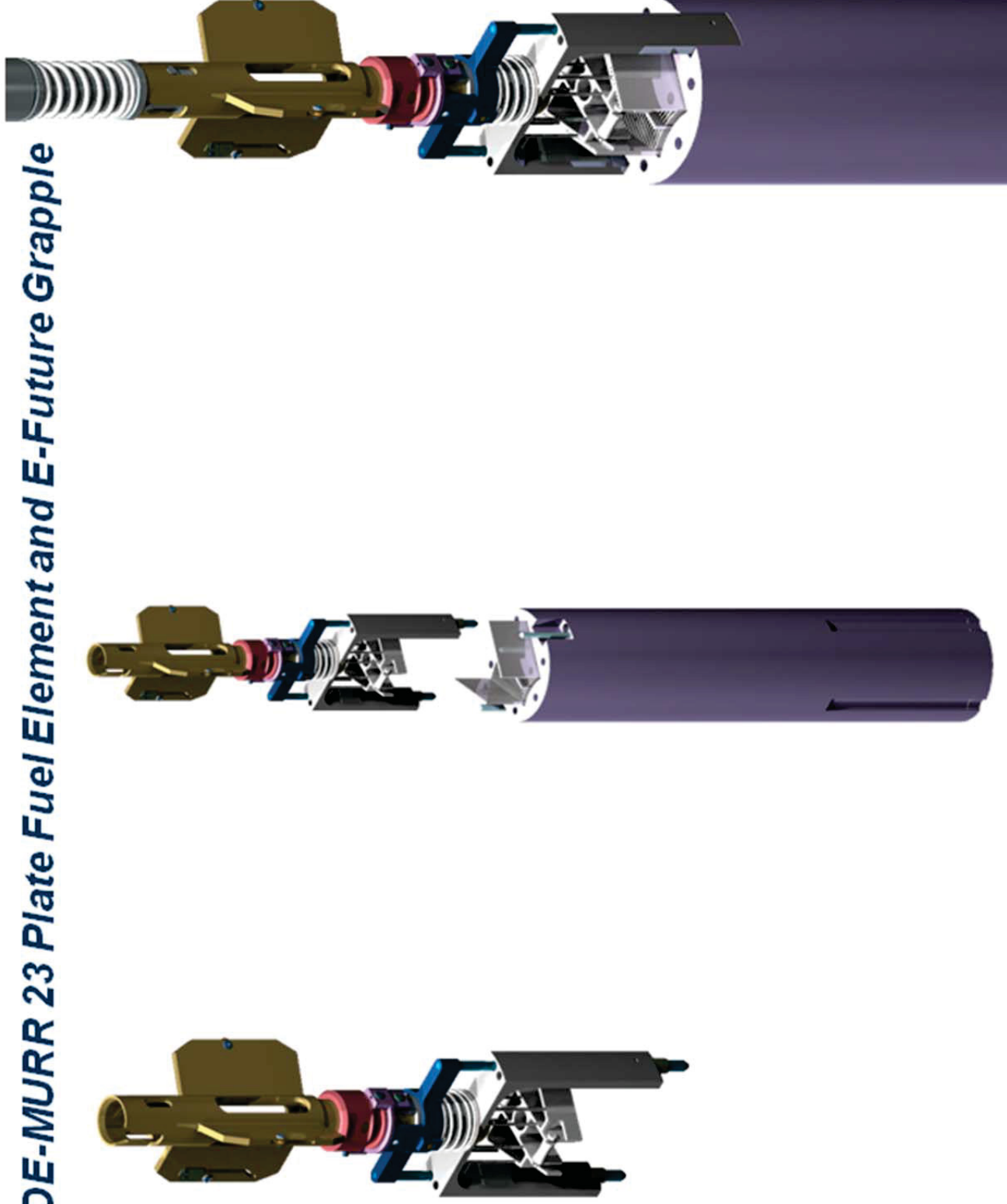
DDE-MURR BR2 Experiment



DDE-MURR 23 Plate Fuel Element

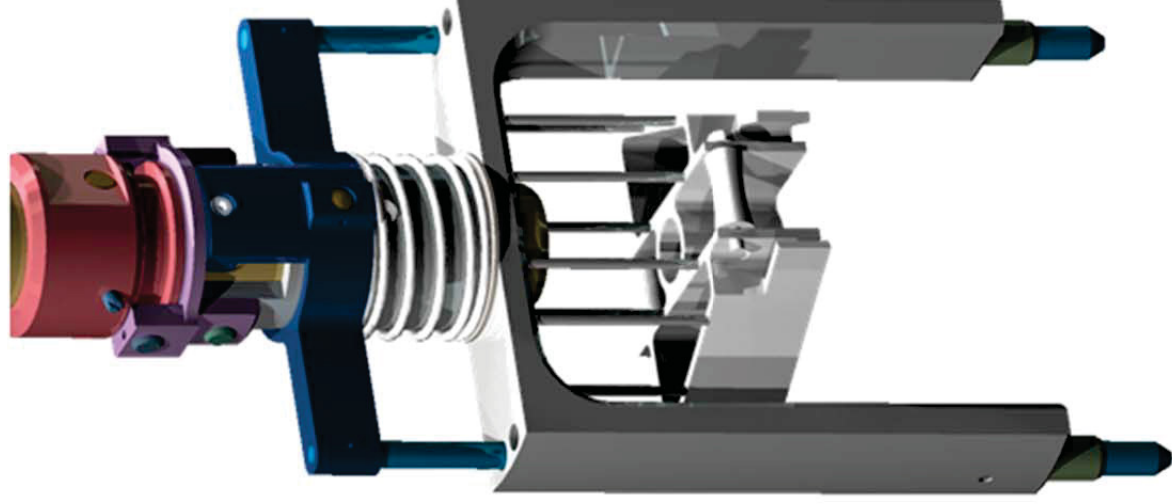


DDE-MURR 23 Plate Fuel Element and E-Future Grapple



Appendix D (Irradiation Vehicle Design)

E-Future Grapple Modified to Hold MURR End Box



[illegible][illegible]

SKETCH
IN CONCEPT DESIGN
STAGE. DO NOT USE
FOR FABRICATION

-1 ASSEMBLY
SCALE: 1/20

-2 ASSEMBLY
SCALE: 1/2

12 SEE DETAIL
13 SEE DETAIL

15 SEE DETAIL
18 SEE DETAIL
19 SEE DETAIL

-5 ASSEMBLY
SCALE: 1/2

12 DETAIL
SCALE: 1/2

13 DETAIL
SCALE: 1/2

15 DETAIL
SCALE: 1/1

18 DETAIL
SCALE: 1/1

19 DETAIL
SCALE: 1/1

SKETCH
IN CONCEPT DESIGN
STAGE. DO NOT USE
FOR FABRICATION

-2 ASSEMBLY
SCALE: 1/2

SCALE: 1/2"

13 DETAIL
SCALE: 1/2

16 DETAIL
SCALE: 1/1

19 DETAIL
SCALE: 4/1

18 DETAIL
SCALE: 1/2"

-5 ASSEMBLY
SCALE: 1/2"

SIZE	CASE CODE	INDEX CODE NUMBER		DWG-781442
D 01MF3	540 9999	CL	Q381	

1
2

2

4

9

7

[illegible][illegible]

[illegible]

-3 ASSEMBLY
SCALE: 1/2

ISOMETRIC VIEW
NOT TO SCALE
FOR INFORMATION ONLY

ISOMETRIC VIEW
NOT TO SCALE
FOR INFORMATION ONLY



7
2 C
5
SEE ASSEMBLY

5
2 B
17
SEE DETAIL

16 2X
SIDE DETAIL

2 2
2 D

2X 15
SEE DETAIL

5
ASSEMBLY

SEE DETAIL

16 2X

24

2X 15
SEE DETAIL

SIZE	CASE CODE	INDEX CODE NUMBER	REV
D	01MF3	AREA TYPE CL OBS 540 9999 43 081	DWG-781442
SCALE: NOTED		SHEET	3

-3 ASSEMBLY
SCALE: 1/2

-4 ASSEMBLY
SCALE: 1/2

ISOMETRIC VIEW
NOT TO SCALE
FOR INFORMATION ONLY

ISOMETRIC VIEW
NOT TO SCALE
FOR INFORMATION ONLY



7
2 C

5
SEE ASSEMBLY

5
2 B

17
SEE DETAIL

16 2X
SEE DETAIL

2 2
2 D

2X 15
SEE DETAIL

5
ASSEMBLY

SEE DETAIL

16 2X

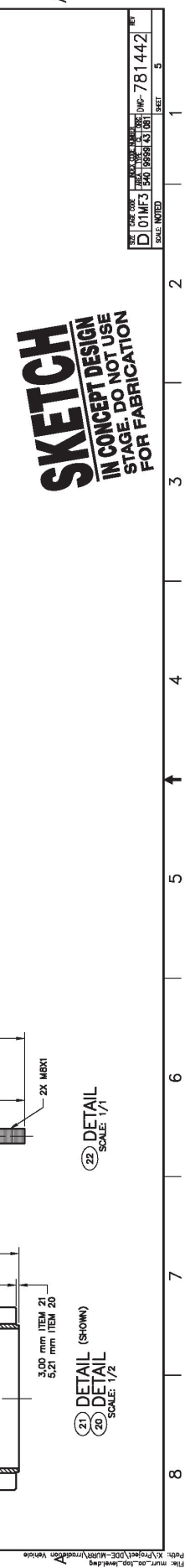
24

2X 15
SEE DETAIL

SIZE	CASE CODE	INDEX CODE NUMBER	REV
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		540 9999 43 081	DWG-781442
SCALE: NOTED			SHEET 3

-3 ASSEMBLY
SCALE: 1/2

8 7 6 5 4 3 2 1



88

1

mm X 45°

**IN CONCEPT DESIGN
STAGE. DO NOT USE
FOR FABRICATION**

-1 ASSEMBLY
SCALE: 1/2

1
2
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6
7
8



SKETCH
IN CONCEPT DESIGN
STAGE. DO NOT USE
FOR FABRICATION

3 DETAIL
SCALE: 1/2

4 DETAIL
SCALE: 1/2

-1 ASSEMBLY
SCALE: 1/16

REV	DATE	BY	CHK	APP	DESCRIPTION
1	07/29/13	11:10 AM			Initial Design

SKETCH
IN CONCEPT DESIGN
STAGE. DO NOT USE
FOR FABRICATION

-1 ASSEMBLY
SCALE: 1/8

-2 ASSEMBLY
SCALE: 1/4

VIEW A-A
SCALE: 1/2

(10) DETAIL
SCALE: 1/1

REV	DESCRIPTION	REVISIONS	DATE
1			

REV	DESCRIPTION	REVISIONS	DATE
1			

6	SCREW, SOC HD CAP, MB X 10 mm LG	SST	13
12			12
11			11
10	PIPE, #15mm O.D. X #12mm I.D.		10
9	VARIOUS PPE AND CAP		9
8	BAR, OR PLATE		8
7	BAR OR PLATE		7
6	LOWER END GUIDE RING		6
5	LOWER END TOP FLANGE		5
4	LOWER END SUPPORT TUBE		4
3			3
2	FIN SECTION ASSEMBLY		2
1	ASSEMBLY		1

REV	DESCRIPTION	REVISIONS	DATE
1			

6	SCREW, SOC HD CAP, MB X 10 mm LG	SST	13
12			12
11			11
10	PIPE, #15mm O.D. X #12mm I.D.		10
9	VARIOUS PPE AND CAP		9
8	BAR, OR PLATE		8
7	BAR OR PLATE		7
6	LOWER END GUIDE RING		6
5	LOWER END TOP FLANGE		5
4	LOWER END SUPPORT TUBE		4
3			3
2	FIN SECTION ASSEMBLY		2
1	ASSEMBLY		1

REV	DESCRIPTION	REVISIONS	DATE
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6	SCREW, SOC HD CAP, MB X 10 mm LG	SST	13
12			12
11			11
10	PIPE, #15mm O.D. X #12mm I.D.		10
9	VARIOUS PPE AND CAP		9
8	BAR, OR PLATE		8
7	BAR OR PLATE		7
6	LOWER END GUIDE RING		6
5	LOWER END TOP FLANGE		5
4	LOWER END SUPPORT TUBE		4
3			3
2	FIN SECTION ASSEMBLY		2
1	ASSEMBLY		1

REV	DESCRIPTION	REVISIONS	DATE
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6	SCREW, SOC HD CAP, MB X 10 mm LG	SST	13
12			12
11			11
10	PIPE, #15mm O.D. X #12mm I.D.		10
9	VARIOUS PPE AND CAP		9
8	BAR, OR PLATE		8
7	BAR OR PLATE		7
6	LOWER END GUIDE RING		6
5	LOWER END TOP FLANGE		5
4	LOWER END SUPPORT TUBE		4
3			3
2	FIN SECTION ASSEMBLY		2
1	ASSEMBLY		1

REV	DESCRIPTION	REVISIONS	DATE
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12			12
11			11
10	PIPE, #15mm O.D. X #12mm I.D.		10
9	VARIOUS PPE AND CAP		9
8	BAR, OR PLATE		8
7	BAR OR PLATE		7
6	LOWER END GUIDE RING		6
5	LOWER END TOP FLANGE		5
4	LOWER END SUPPORT TUBE		4
3			3
2	FIN SECTION ASSEMBLY		2
1	ASSEMBLY		1

REV	DESCRIPTION	REVISIONS	DATE
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6	SCREW, SOC HD CAP, MB X 10 mm LG	SST	13
12			12
11			11
10	PIPE, #15mm O.D. X #12mm I.D.		10
9	VARIOUS PPE AND CAP		9
8	BAR, OR PLATE		8
7	BAR OR PLATE		7
6	LOWER END GUIDE RING		6
5	LOWER END TOP FLANGE		5
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3			3
2	FIN SECTION ASSEMBLY		2
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REV	DESCRIPTION	REVISIONS	DATE
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6	SCREW, SOC HD CAP, MB X 10 mm LG	SST	13
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11			11
10	PIPE, #15mm O.D. X #12mm I.D.		10
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8	BAR, OR PLATE		8
7	BAR OR PLATE		7
6	LOWER END GUIDE RING		6
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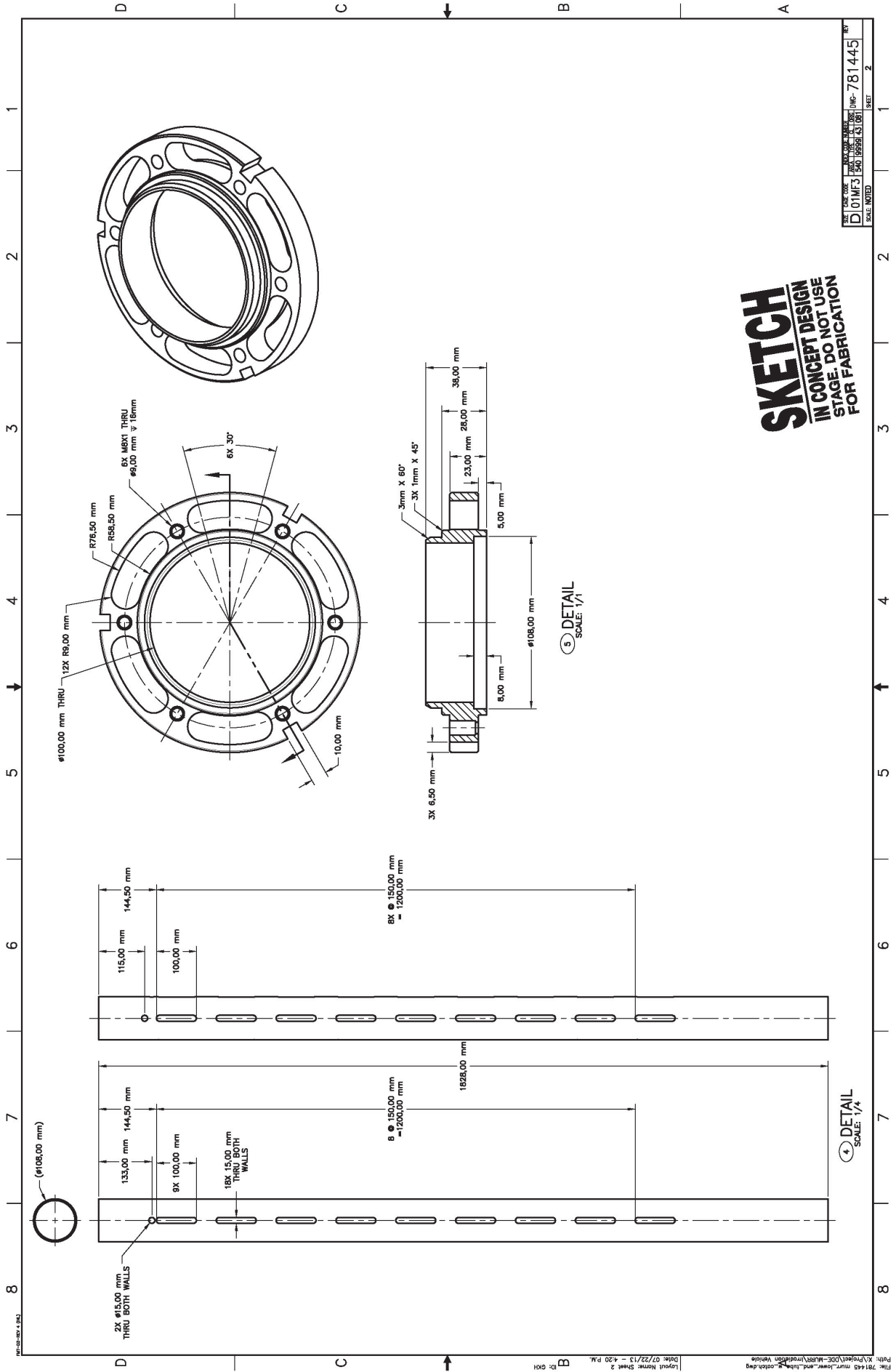
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8	BAR, OR PLATE		8
7	BAR OR PLATE		7
6	LOWER END GUIDE RING		6
5	LOWER END TOP FLANGE		5
4	LOWER END SUPPORT TUBE		4
3			3
2	FIN SECTION ASSEMBLY		2
1	ASSEMBLY		1

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						12	
						11	
2	-10			CROSS PIPE	PIPE, #15mm O.D. X #12mm I.D.	10	
1	-8			CATCH	VARIOUS PPE AND CAP	9	
3	-8			FIN	BAR, OR PLATE	8	
1	-7			LOWER END ATTACH-TO-CATCH	BAR OR PLATE	7	
1	-8			LOWER END GUIDE RING	PLATE, 10mm THK	6	
1	-5			LOWER END TOP FLANGE	PLATE, 38mm THK	5	
1	-4			LOWER END SUPPORT TUBE	TUBE, #108 O.D. X #100 I.D.	4	
						3	
	-2			FIN SECTION ASSEMBLY		2	
	-1			ASSEMBLY		1	
-2	-1						
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SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							
DIMENSIONS: 3 ± .1							
FINISHES: 100% ZN							
EFFECTIVE DATE: 10/1/00							
FOR REVIEW/APPROVAL SIGNATURES							
SEE CDP NO.							
SCALE: 1" = 10'							
NOTES:							
FOR SCALE BAR:							
DRAWN BY: J. DODLEY							
CHECKED BY: J. DODLEY							
DESIGNED BY: J. DODLEY							
SURFACE FINISHES: 100% ZN							
DIMENSIONS AND TOLERANCES							
TOLERANCES: 3 ± .1							

Appendix D (Irradiation Vehicle Design)



[illegible]

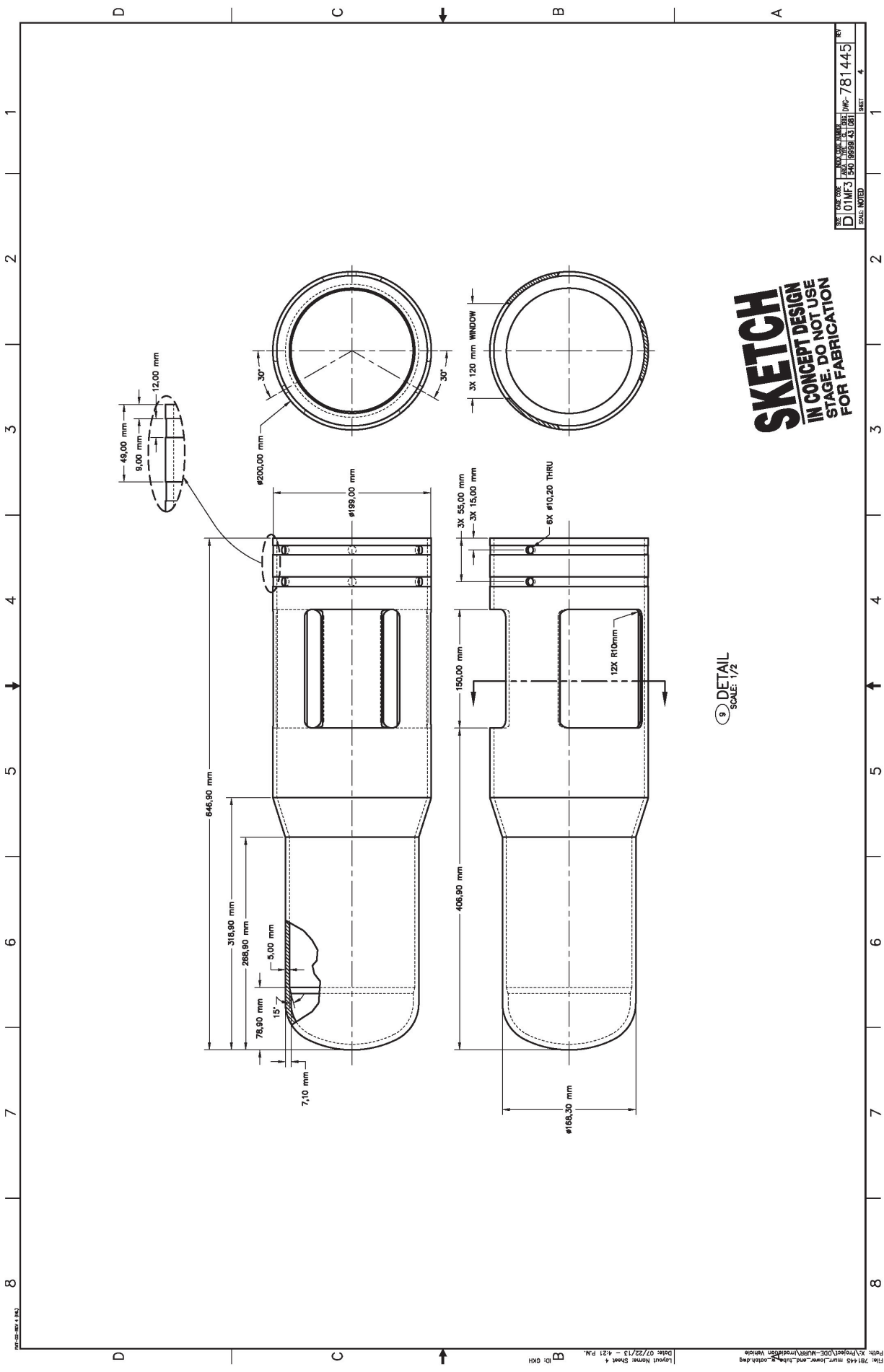
⑦ DETAIL
SCALE: 1/1

8 DETAIL
SCALE: 1/1

6 DETAIL
SCALE: 1/1

SIZE	CAGE CODE	NADCAP CODE NUMBER		REV
D	01MF3	AREA	TYPE Q. LOSS	
		540	99999	01G-781445
SCALE NOTED				3

Appendix D (Irradiation Vehicle Design)



FILE	DATE	BY	CHKD	DATE	BY	CHKD	DATE	BY	CHKD
D 01 MF3	1540	1555	1555	1555	1555	1555	1555	1555	1555
DATE NOTED									1

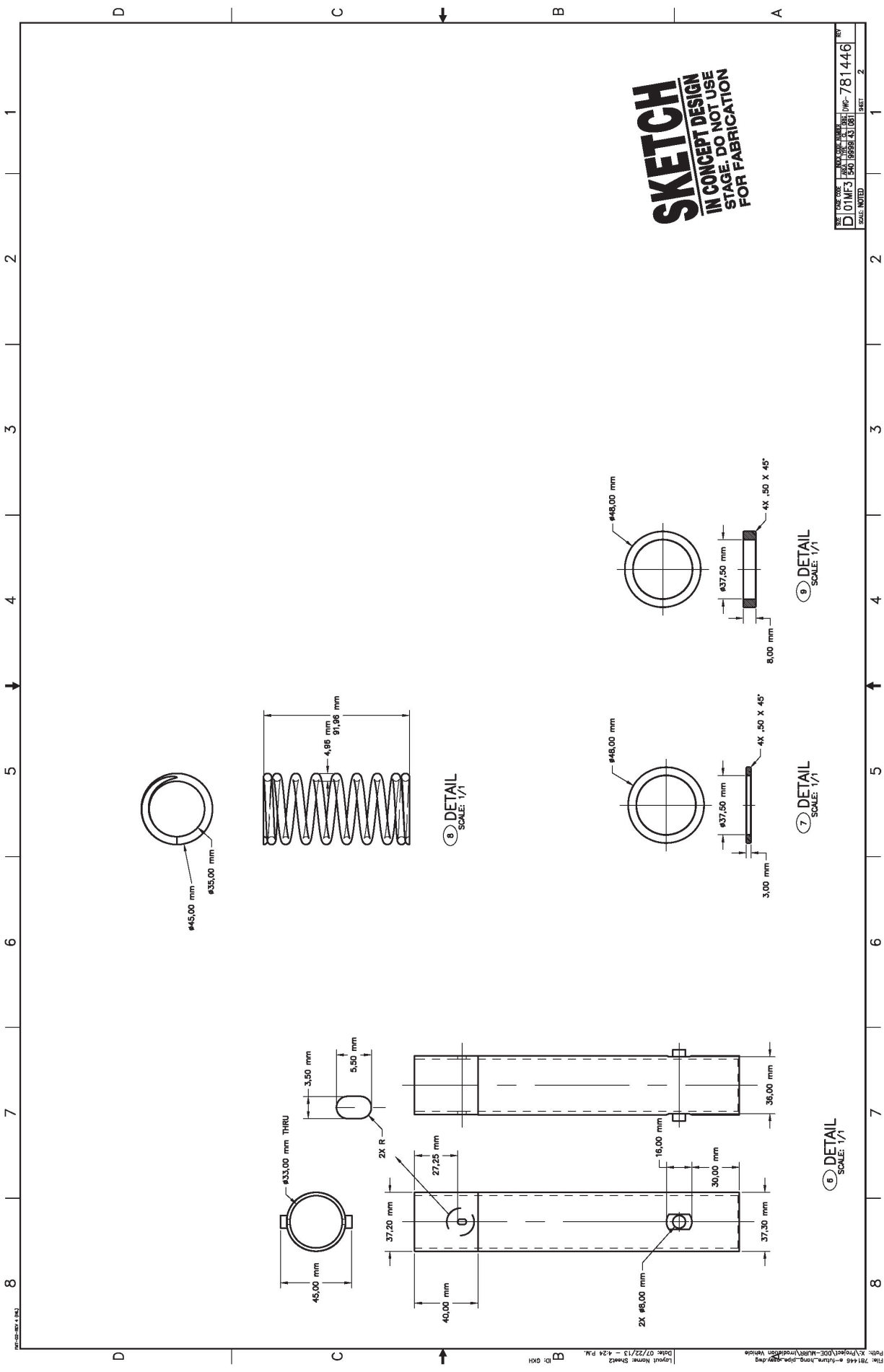
[illegible]

-1 ASSEMBLY
SCALE: 1/2

1	-8	LOWER SUPPORT RING	9		
1	-8	SPRING	8		
1	-7	TOP SUPPORT RING	7		
1	-6	COUPLING	6		
1	-5	ATTACHING FLANGE	5		
1	-4	TOP FLANGE	4		
1	-3	PERFORATED PIPE	3		
1	-1	ASSEMBLY	2		
-2	-1	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL SPECIFICATION OR VENDOR NAME	ITEM NO.
QTY REQD					
PARTS LIST					
MEASUREMENTS AND TOLERANCES PER CASE 11416 AND STD-1001 REPT DORS G. HADLEY					
DESIGN SERVICE DRAWINGS BY DRAWING NO. 11416-1					
DIMENSIONS AND TOLERANCES DIMENSIONS IN INCHES TOLERANCES FINISHES COATINGS PAINTS MATERIALS FABRICATIONS TREATMENTS SPECIAL REQUIREMENTS NOTES REVISIONS APPROVALS SIGNATURES DATE EFFECTIVE DATE SCALE NOTED					
DDE-MURR IRRADIATION PIGGLE E-FUTURE STYLE TRAP PIPE ASSEMBLY					
SINL Idaho National Laboratory					
SHEET NO. 781446 OF 2					

[illegible]

Appendix D (Irradiation Vehicle Design)



WHEN ITEM 13 IS PUSHED DOWN, IT CAUSES BEARING (ITEM 29) TO PUSH OUT AND PREVENTS ITEM BEING LIFTED FROM DETACHING

ISOMETRIC VIEW
FOR CLARITY ONLY
NOT TO SCALE

UNLOCKED

LOCKED

FUNCTIONALITY VIEWS
FOR CLARITY ONLY
NOT TO SCALE

1 ASSEMBLY
SCALE: 1/2

ITEM NO.	DESCRIPTION	MATERIAL SPECIFICATION OR VENDOR NAME
6	BALL BEARING, 62/250	SST
2	SCREW, SDC HO CAP, M4 X 6	SST
1	80015A33	SPRING PLUNGER
3	80857A110	EXTERNAL RETAINING RING, 46mm, SST
26		MCMASTER-CARR
25		MCMASTER-CARR
24		
1	600455-29	DEC-MURR END FITTING
23		
1	-22	WEAR PIN
2	-21	CONNECTION PIN
2	-20	COUPLING PIN
3	-19	WHEEL
3	-18	AXLE
2	-17	GUIDE PIN
2	-16	RATCHET PIN
1	-15	GUIDE PLATE
2	-14	BEARING HOUSING
2	-13	LOOK ROD
1	-12	BOTTOM RING
1	-11	CONNECTING RING
1	-10	FORK
1	-8	SUPPORT RING
1	-8	UNLOCKING RING
1	-7	TUBE WITHOUT FEATURES
1	-6	FIN SECTION TUBE
1	-5	FLEXIBLE FIN
1	-4	NON FLEXIBLE FIN
	-2	FIN SECTION ASSEMBLY
	-1	ASSEMBLY

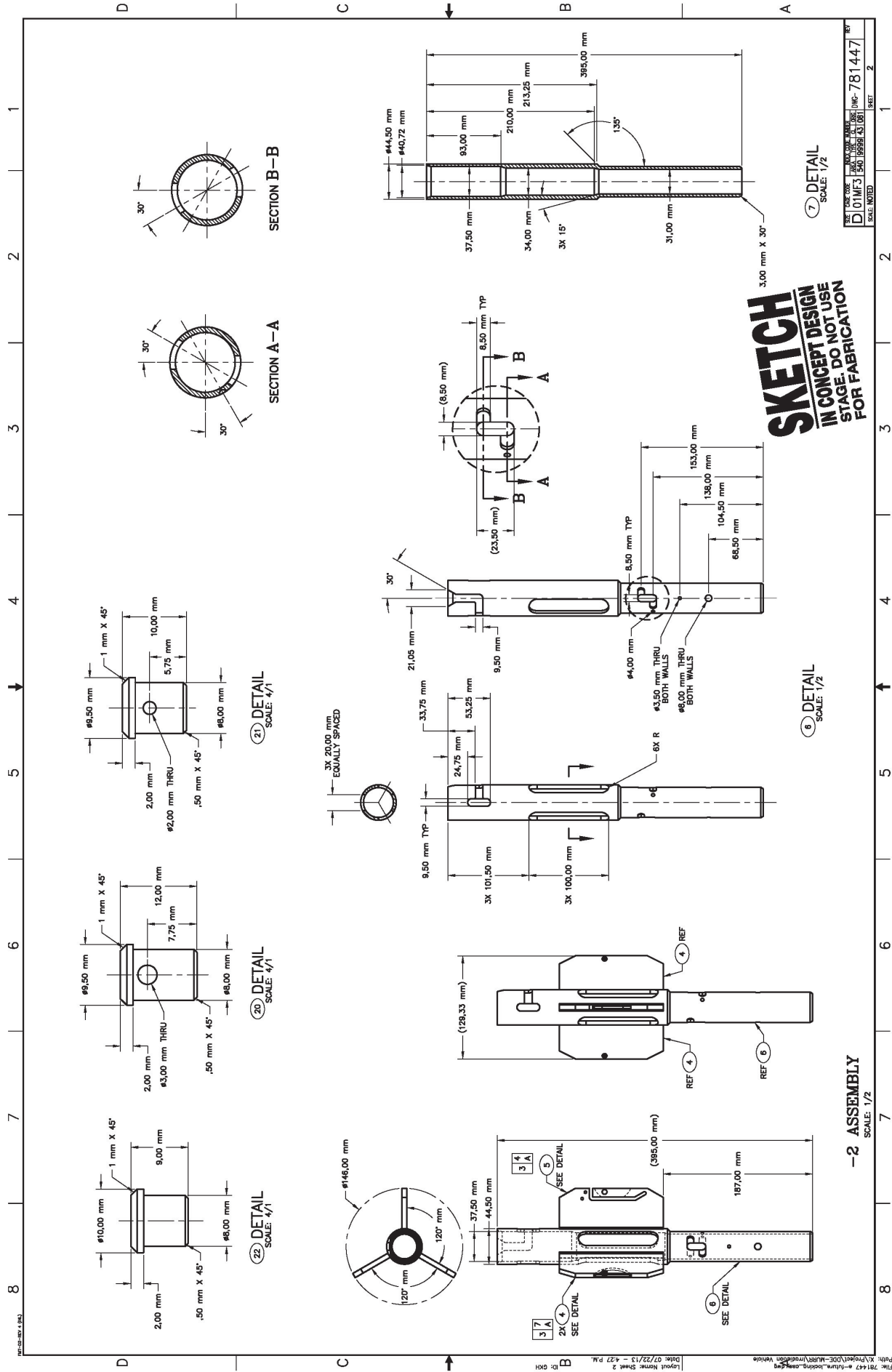
—1 ASSEMBLY
SCALE: 1/2

6		BALL BEARING, #2520		SST	20
2		SOREN, SOC HD CMC, 1/4" X 8		SST	28
1	85015A33	SPRING PLUMBER		MAWMASTER-CARR	27
3	90857A110	EXTERNAL RETAINING RING, 1/40mm, SST		MAWMASTER-CARR	26
					25
1	603445-29	DOE-MUIRE END FITTING			24
					23
1	-22	WEAR PIN		SST	22
2	-21	CONNECTION PIN		SST	21
2	-20	COUPLING PIN		SST	20
3	-19	WHEEL		SST	19
3	-18	AXLE		SST	18
2	-17	GUIDE PIN		SST	17
2	-16	ROOT PIN		BAR	16
1	-15	GUIDE PLATE		SHEET	15
2	-14	BEARING HOUSING		BAR	14
2	-13	LOCK ROD		BAR	13
1	-12	BOTTOM RING		BAR	12
1	-11	CONNECTING RING		BAR	11
1	-10	FORK		PLATE	10
1	-9	SUPPORT RING		PLATE	9
1	-8	UNLOCKING RING		BAR, #45 mm	8
	-7	TUBE WITHOUT FEATURES		BAR, #45 mm	7
1	-6	FIN SECTION TUBE		MADE FROM ITEM 7	6
1	-5	FLEXIBLE FIN		PLATE, 1/4mm THK	5
1	-4	NON FLEXIBLE FIN		PLATE, 1/4mm THK	4
					3
	-2	FIN SECTION ASSEMBLY			2
	-1	ASSEMBLY			1
QTY REQD	-2 -1	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL, SPECIFICATION OR REFERENCE NAME	ITEM NO.

[illegible]

DATE	11/10/2000	1	0
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Appendix D (Irradiation Vehicle Design)

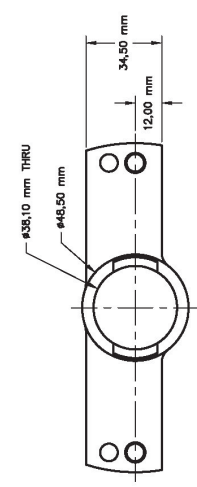


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D: 01MF3
DATE: 07/22/13
SCALE: 1/2
SHEET: 2

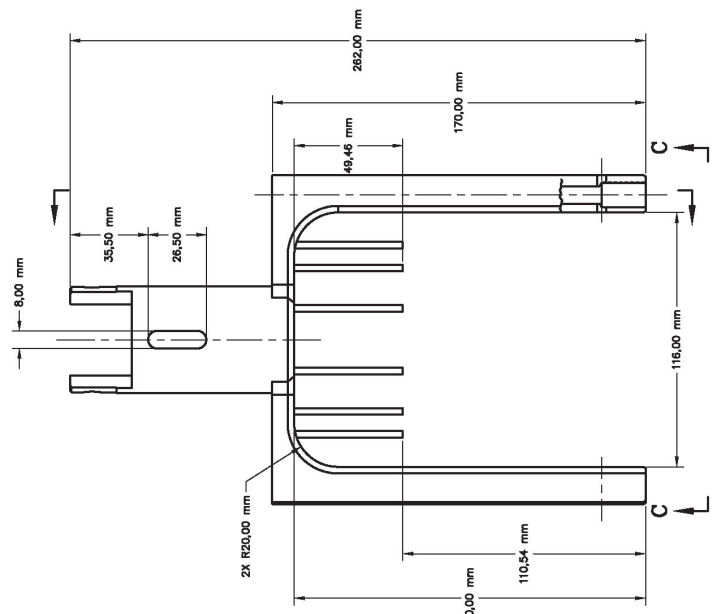
781447 - Irradiation Vehicle Design
D: 01MF3
DATE: 07/22/13
SCALE: 1/2
SHEET: 2

[illegible]

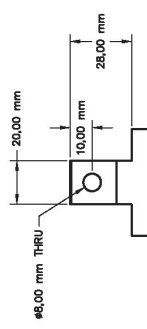
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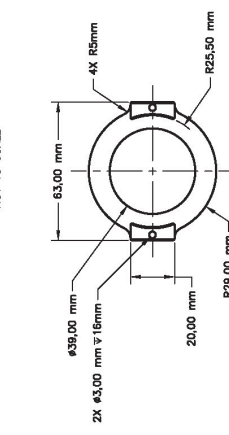
SECTION C-C
SCALE: 1/1



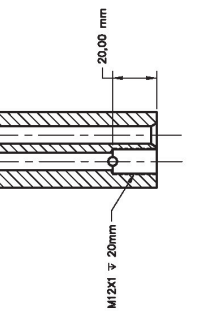
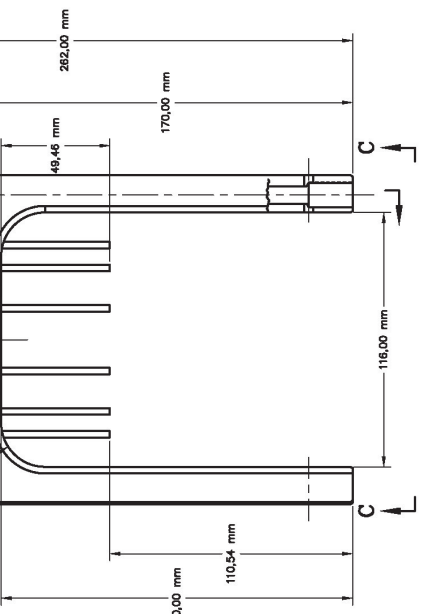
10 DETAIL
SCALE: 1/1



ISOMETRIC VIEW
FOR CLARITY ONLY
NOT TO SCALE



ISOMETRIC VIEW
FOR CLARITY ONLY
NOT TO SCALE



11 DETAIL
SCALE: 1/1

SIZE	CAGE CODE	NDC CODE NUMBER		REV
D	01MF3	AREA	TYPE	Q. ORDER
		540	9958	43 081
SCALE NOTED				SHEET 5

[illegible]

1	5	ALIGNMENT PIN	BAR
2	5	VEHICLE BASE	PLATE
3	3	VEHICLE BODY	BAR
4	2		
5	1	ASSEMBLY	
6			
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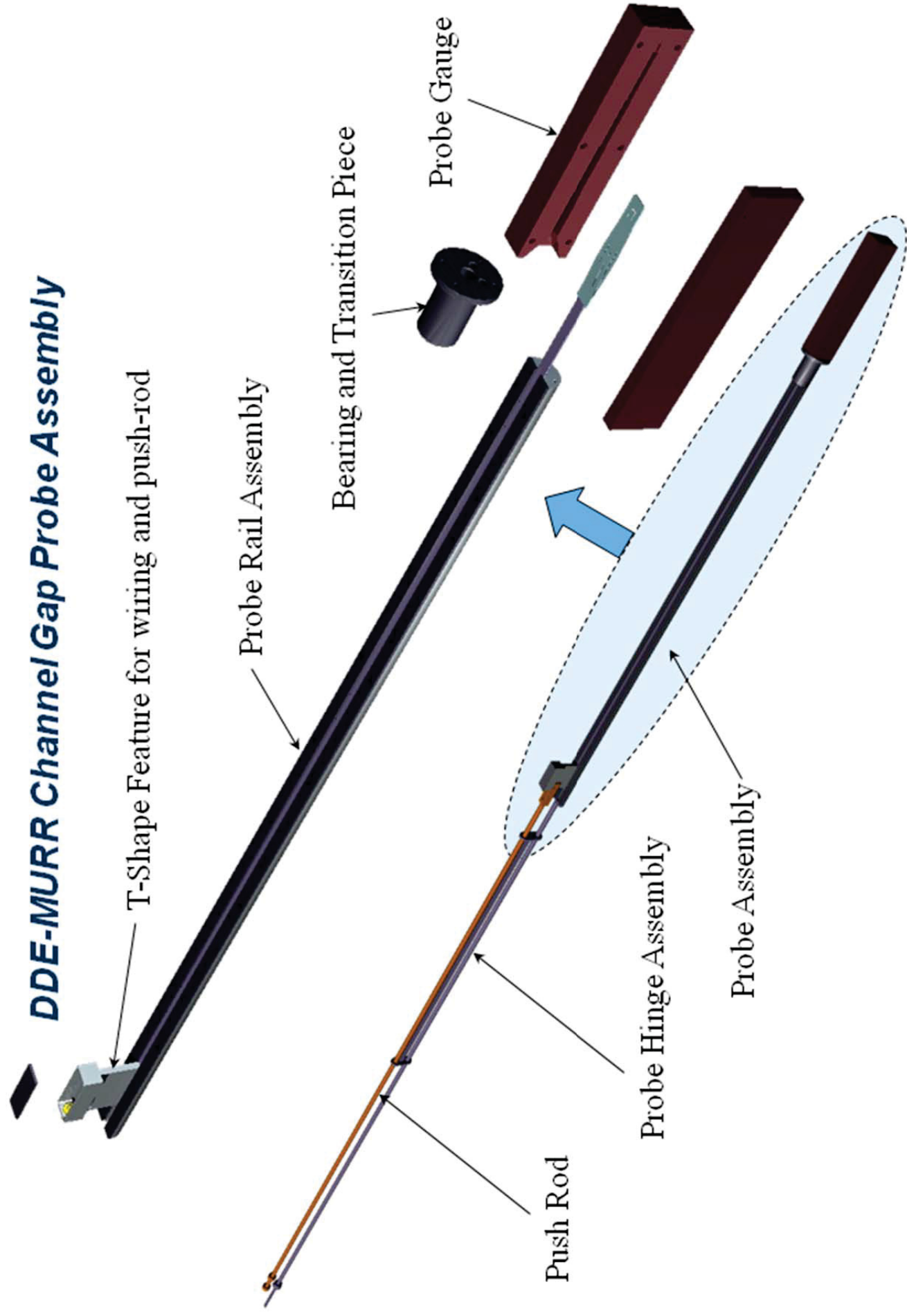
SKETCH
IN CONCEPT DESIGN
STAGE. DO NOT USE
FOR FABRICATION

-1 ASSEMBLY
SCALE: 1/2

8	7	6	5	4	3	2	1
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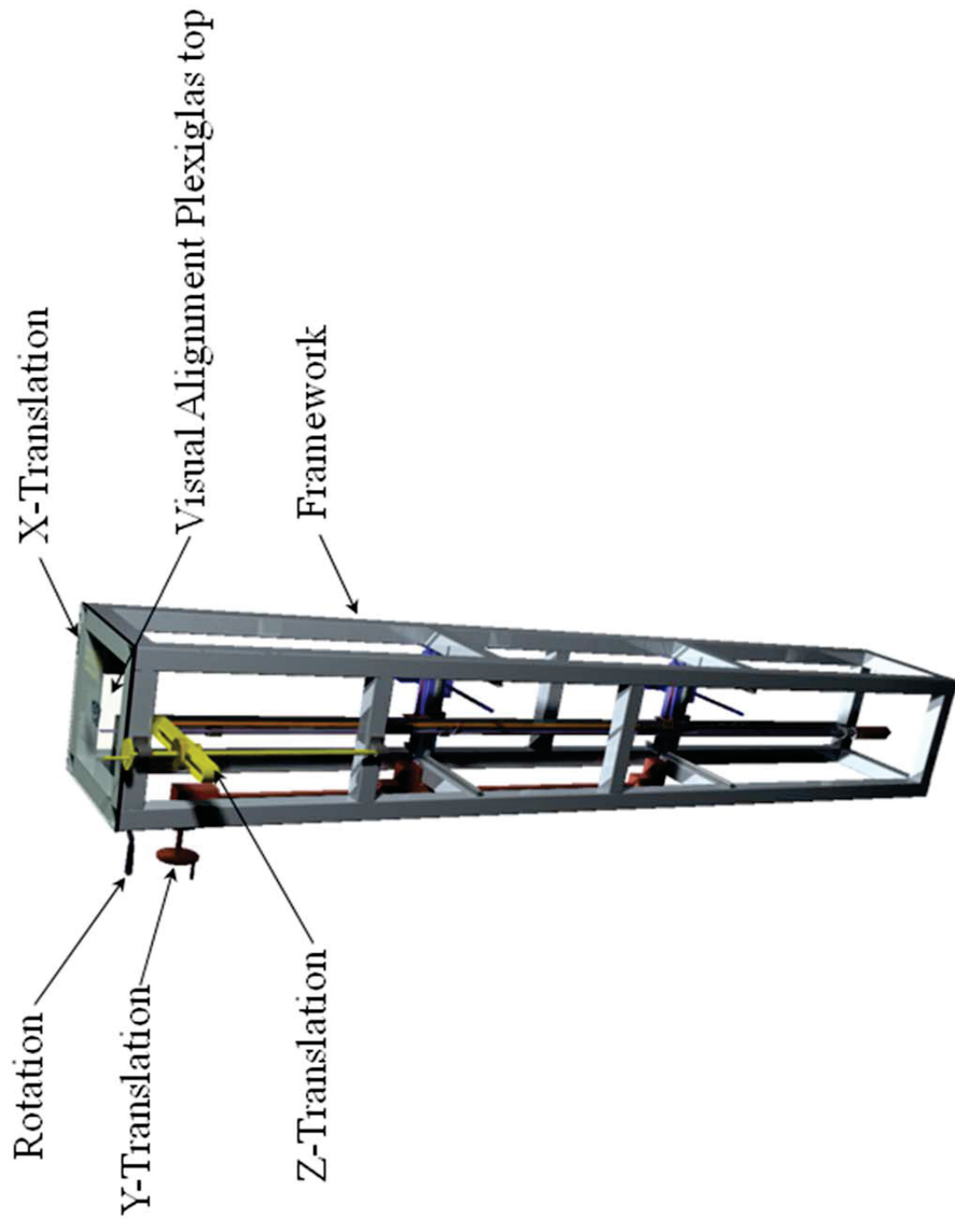


Appendix E (Channel Gap Probe Design)



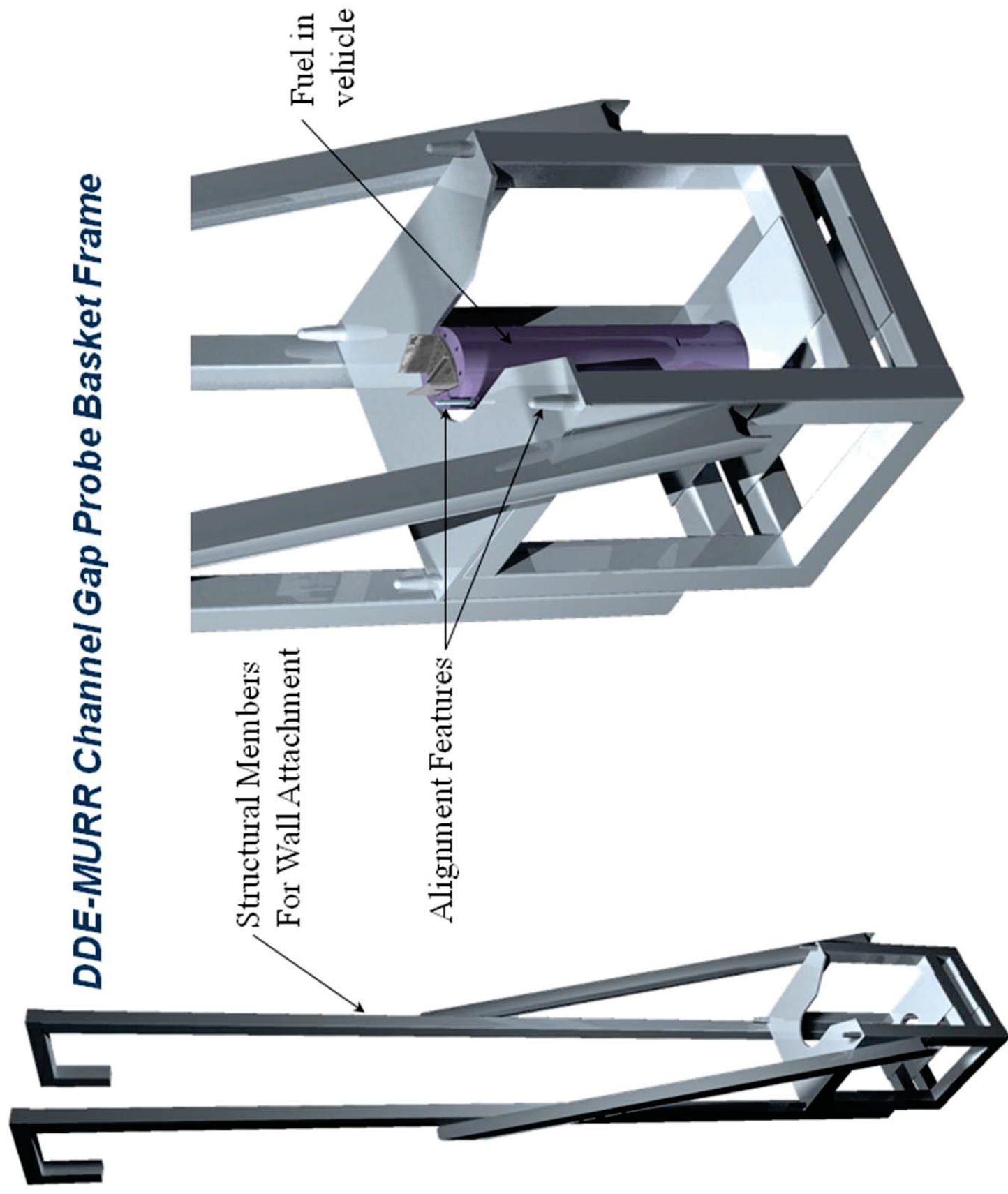
Appendix E (Channel Gap Probe Design)

DDE-MURR Channel Gap Probe

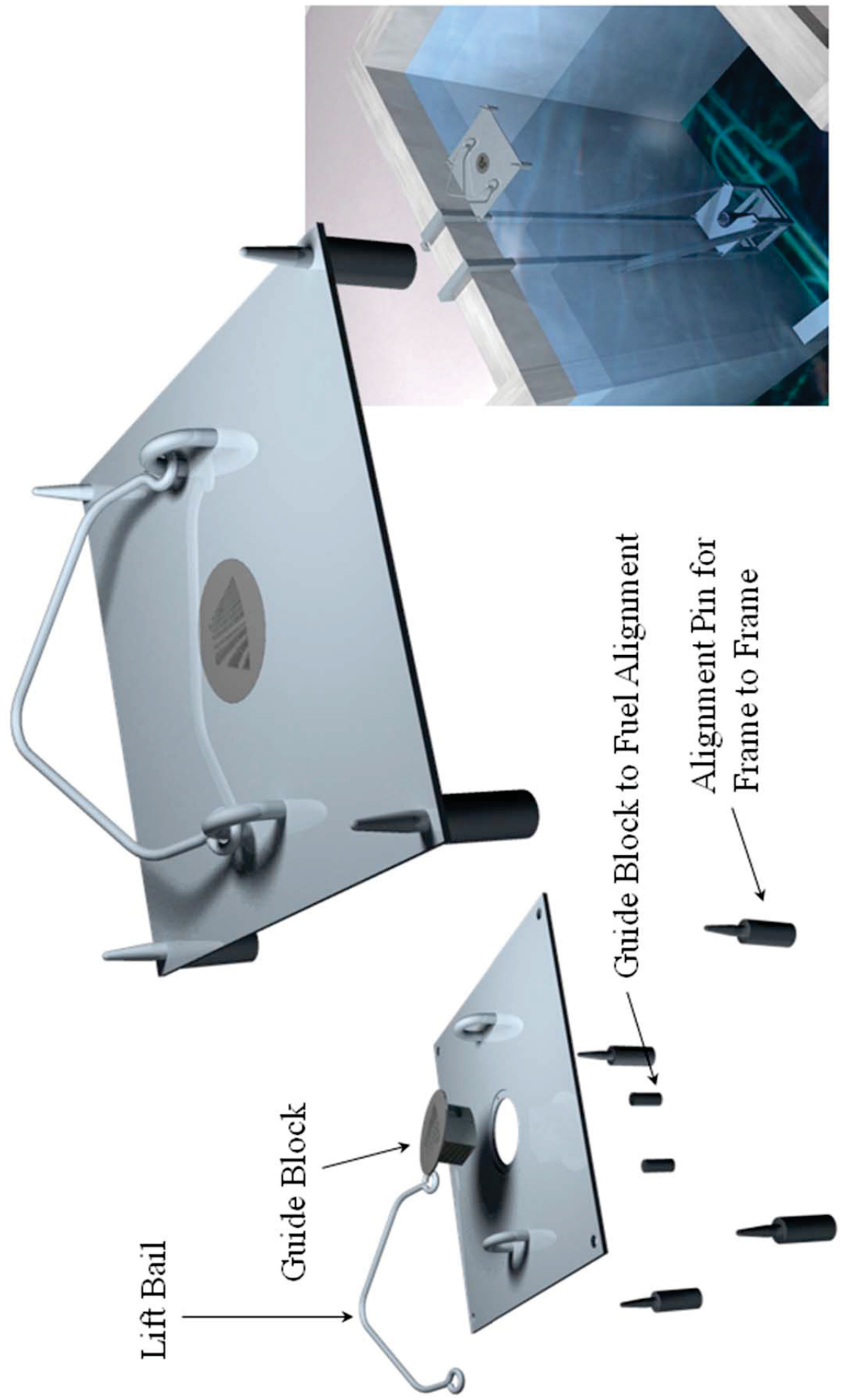


Appendix E (Channel Gap Probe Design)

DDE-MURR Channel Gap Probe Basket Frame

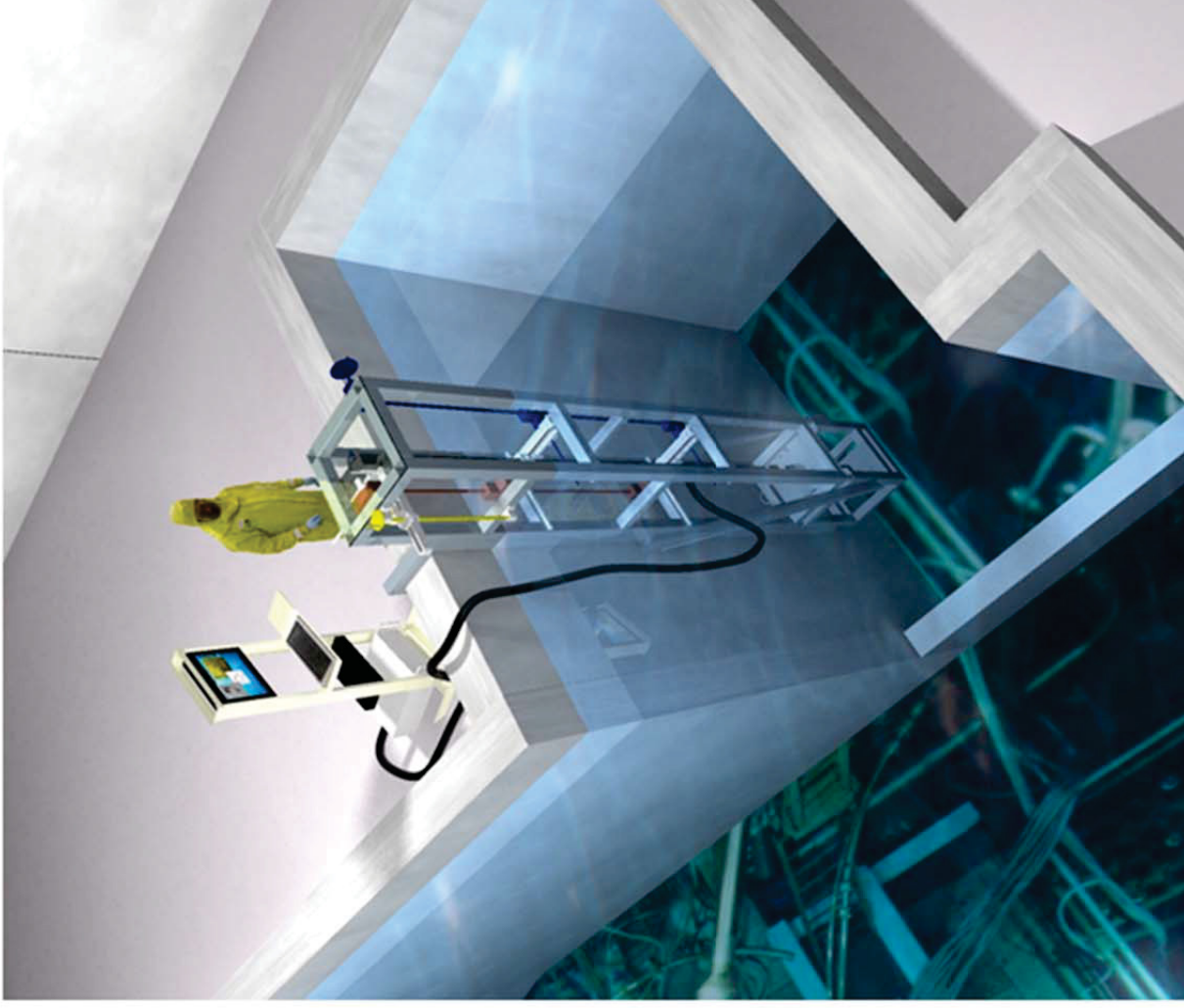


DDE-MURR Channel Gap Probe to Fuel Alignment Fixture



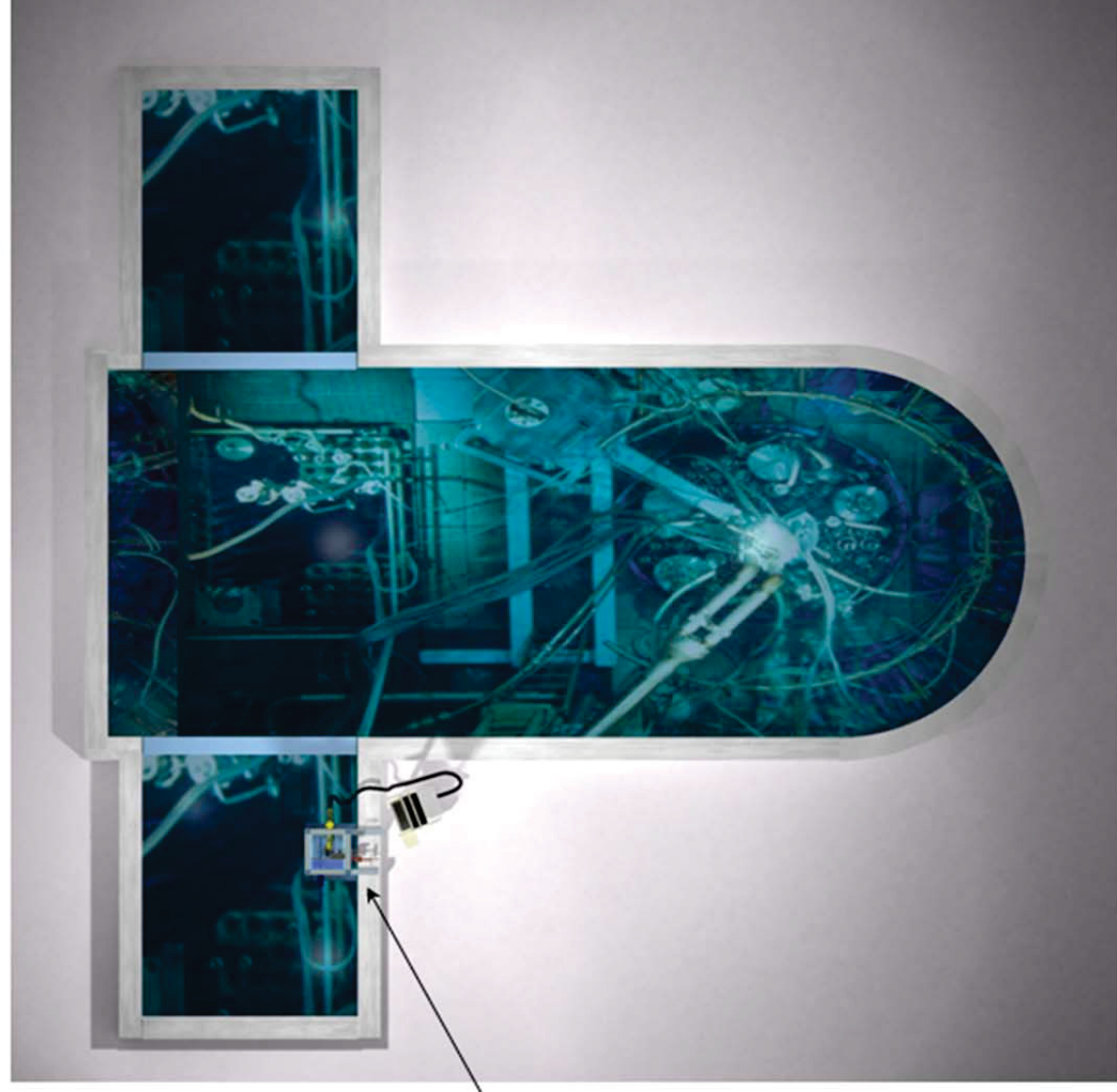
Appendix E (Channel Gap Probe Design)

DDE-MURR Channel Gap Probe



Appendix E (Channel Gap Probe Design)

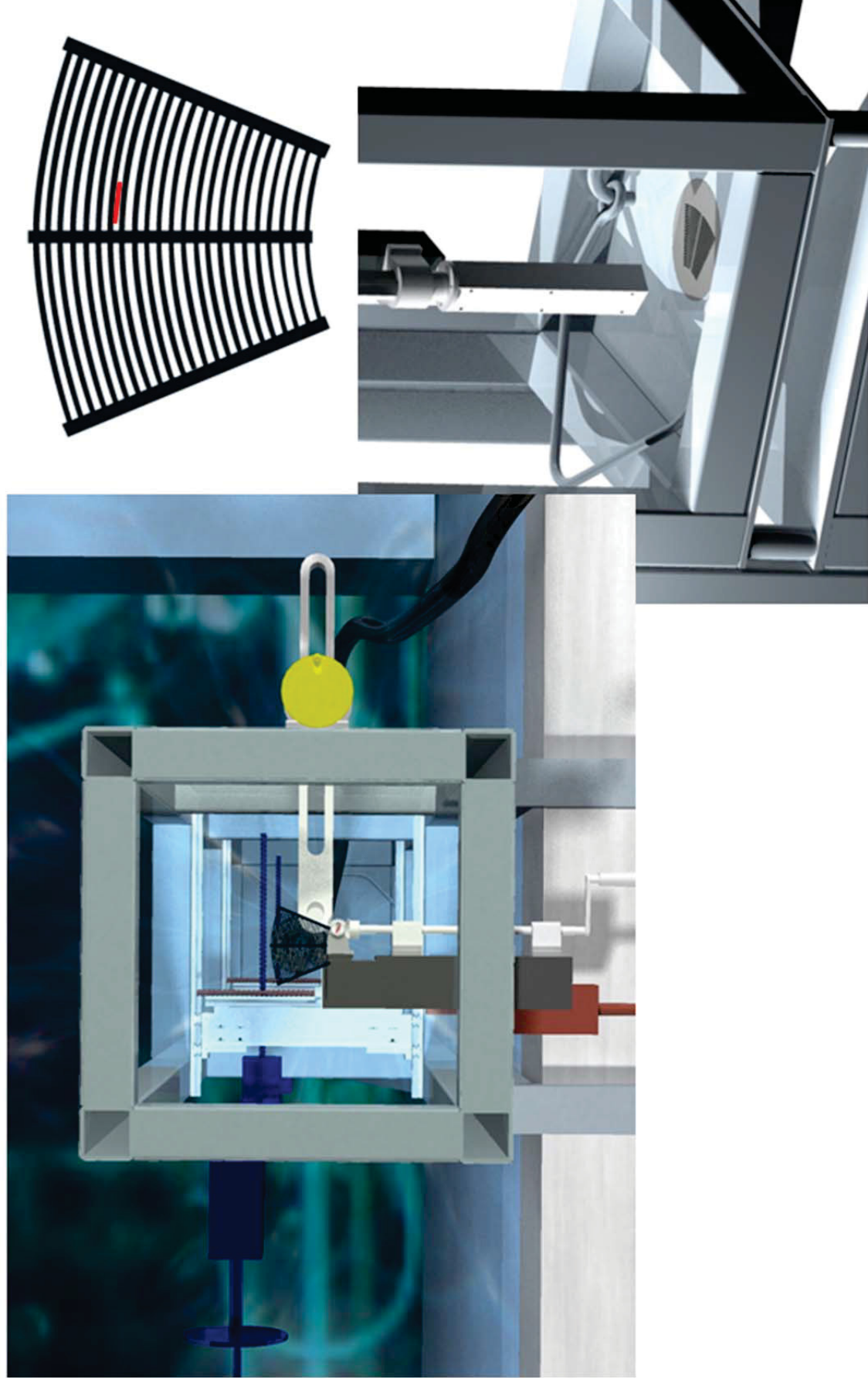
DDE-MURR Channel Gap Probe at BR2



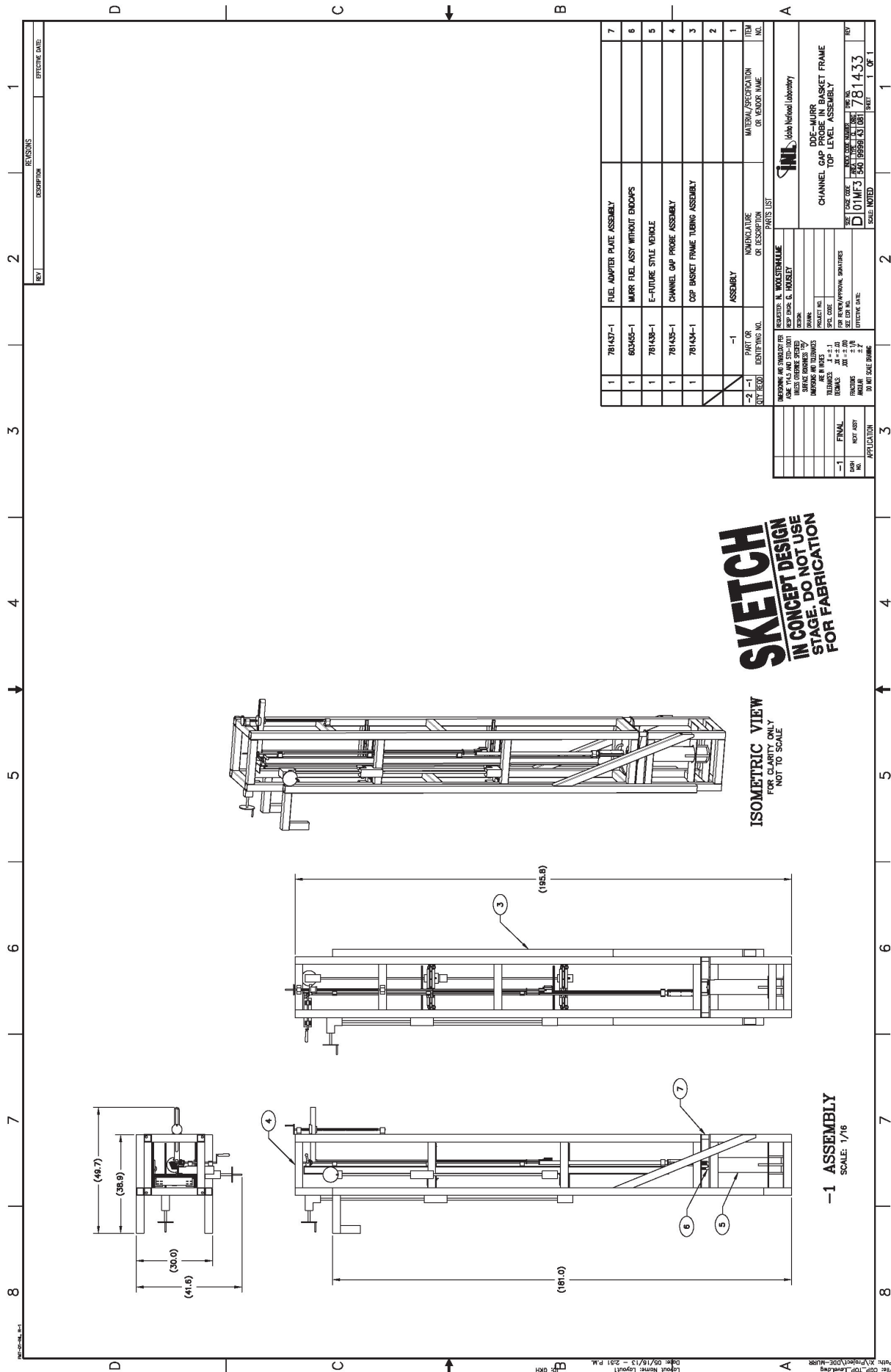
Approximate Location of
Channel Gap Probe at
BR2

Appendix E (Channel Gap Probe Design)

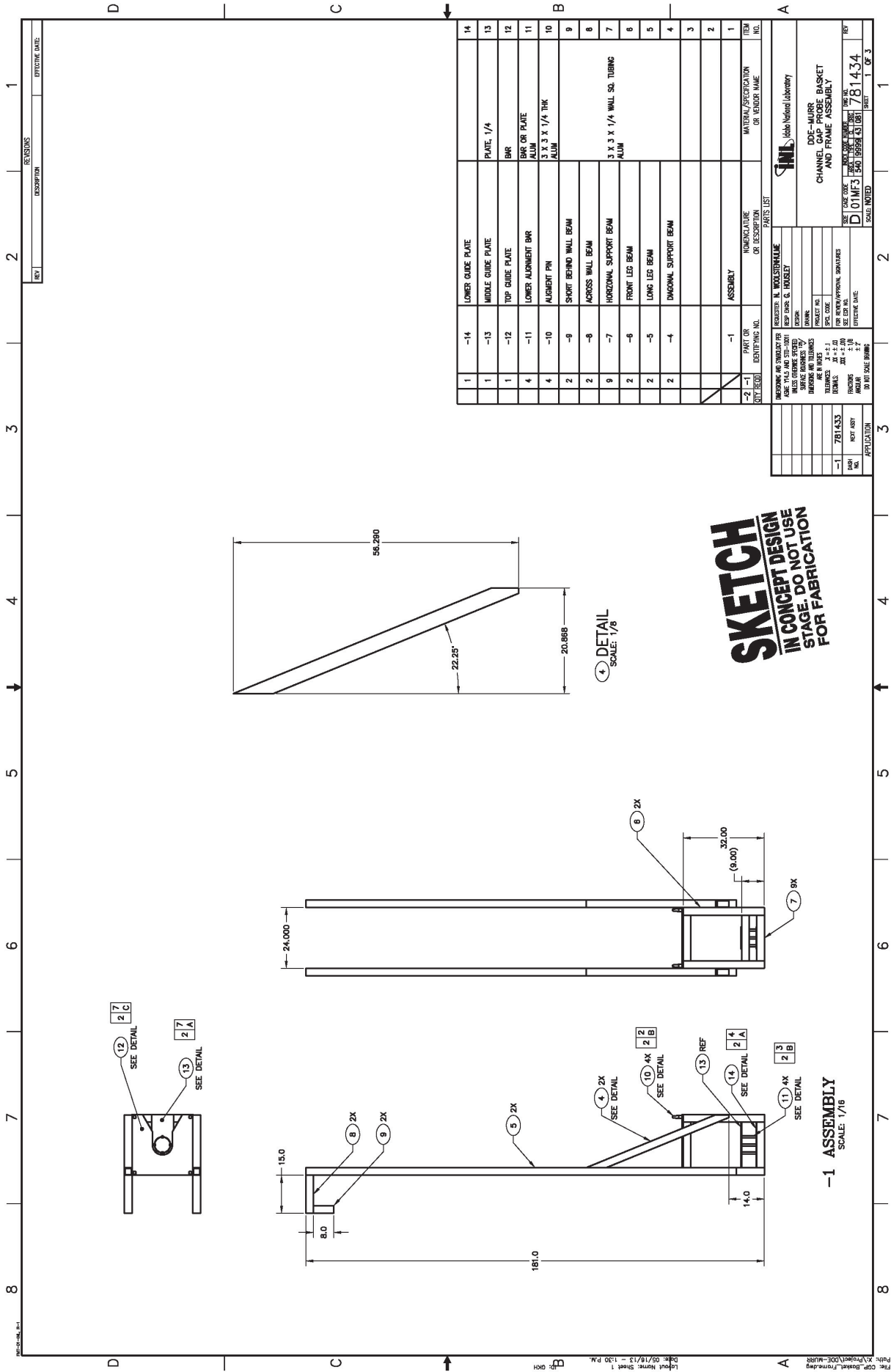
DDE-MURR Channel Gap Probe Visual Alignment Feature



Appendix E (Channel Gap Probe Design)



Appendix E (Channel Gap Probe Design)

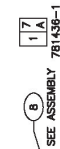


8 7 6 5 4 3 2 1



SIZE	CAGE CODE	INDEX CODE NUMBER		REV
D	01MF3	JAN	CL	006
		540	9999	43 081
SCALE: NOTED		SHEET		2
		DWG-		781434

3



-1 ASSEMBLY
SCALE: 1/16

2015

[illegible]

ISOMETRIC VIEW
FOR INFORMATION ONLY
NOT TO SCALE

-2 ASSEMBLY
SCALE: 1/16

SIZE	NAME CODE	INDEX CODE	INDEX	KEY
D	01MF3	540 9999	43 081	01G-781435
SCALE: NOTED				SHEET 2

[illegible]

—5 ASSEMBLY
SCALE: 1/4"

ISOMETRIC VIEW
FOR INFORMATION ONLY
NOT TO SCALE

—6 ASSEMBLY
SCALE: 1/2

SIZE	CAGE CODE	INDEX CODE NUMBER				DWC-781435	REV
D	01MF3	AREA	TYPE	CL	LOG		
		540	9999	43	081		
SCALE: NONE						QEST	3

-1 ASSEMBLY
SCALE 1/16

SKETCH
IN CONCEPT DESIGN
STAGE. DO NOT USE
FOR FABRICATION

REV	DESCRIPTION	EFFECTIVE DATE
1	ISSUED FOR FABRICATION	05/15/13

REV	DESCRIPTION	EFFECTIVE DATE
1	ISSUED FOR FABRICATION	05/15/13

ISOMETRIC VIEW
FOR INFORMATION ONLY
NOT TO SCALE

—1 ASSEMBLY
SCALE: 1/16

				-28	CALIBRATION BLOCK END PLATE ALUM.	BK OR PLATE, 3/4" THK ALUM.	26
	2			-27	CALIBRATION BLOCK STEP PLATE ALUM.	BK OR PLATE, 3/4" THK ALUM.	27
		2	SAMI-5-20		BEVEL GEAR	KENDUP OR OTHER	26
		2	IYAWIC-JAOWO		CARRIAGE, INTERNAL V	PACIFIC BEARING COMPANY	25
		1	-24		CHANNEL MAIN STRUCTURAL HOLER	CHANNEL, 3 X 1.75	24
		1	-23		RHIT ANGLE LEG OF FRAME	ANGLE, 3 X 3 X 1/4"	23
		5	-22		BELLOW BLOCK / BEARING	NUT SELECTED	22
		1	-21		PUSH ROD	BKS #1/2"	21
	1		-20		ROTATING PUSH BAR INCHIE WITH INDICATOR	BKS #1/2"	20
	1		-19		ROTATING PUSH BAR RECTANGULAR REAM ALUM	BKS, 1/2" X 1/4"	19
	1		-18		ROTATING PUSH BAR BOTTOM END PLATE	BK OR PLATE, 1/4" THK ALUM	18
	2		-17		ROTATING PUSH BAR SUPPORT PLATE	BK OR PLATE, 1/4" THK ALUM	17
		1	-16		PROBE END FOUTINE WITH ULTRA-SOUNDS	ONCE TO BE SUPPLIED BY IRL PERSONNEL (RECENTLY LET GO)	16
			-15		PROBE WIRE COVER	THIN SHEET SS	15
		1	-14		PROBE MAN BODY	SS THIN SHEET	14
		1	-13		PROBE ELECTRICAL COVER PLATE	BK OR PLATE, 1" THK ALUM	13
		1	-12		PROBE ELECTRICAL JUNCTION BOX	BK OR PLATE, 1" THK ALUM	12
		1	-11		PROBE T-SWAPPE TRISH PIECE	BK OR PLATE, 1" THK ALUM	11
		2	-10		SLIDE RAIL COVER	BK OR PLATE, 1/8" THK ALUM	10
		1	-8		SLIDE RAIL END-Piece	BKS #2-50 ALUM	9
		1	-8		SEMI-CIRCULAR SLICE RAIL	BKS #1-50 ALUM	8
		1	-7		ROTATING PUSH BKR ASSEMBLY		7
		1	-6		PROBE ROTATION HANDLE ASSEMBLY		6
		1	-5		CALIBRATION BLOCK ASSEMBLY		5
		1	-4		PHORE BODY ASSEMBLY		4
		1	-3		SLIDING PROBE ASSEMBLY		3
		1	-2		ROTATABLE AND SLIDING PROBE ASSEMBLY		2
			-1		ASSEMBLY		1
			-1		FART OF IDENTIFYING NO. NOT KNOWN	MATERIAL SPECIFICATION OR DONOR NAME	ITEM NO.
	-7	-6	-5	-4	-3	-2	-1

[illegible]

[illegible]

[illegible]

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[illegible]

8	1	-8	HOOF FOR HANDLE	BKS #50	
7	1	-7	LEFT HANDLE	BKS #50	
6	1	-6	MAIN ADAPTER PLATE	PLATE ALUM	
5	1	-5	MURS FUEL CHANNEL CAP ALIGNER	BKS #400	
4	2	-4	LOWER ALIGNMENT PIN	ALUM #150	
3	4	-3	LARGE ALIGNMENT PIN	BKS #100	
2				ALUM	
1			ASSEMBLY		
ITEM NO.	-2	-1	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL SPECIFICATION OR BRAND NAME
QTY REQ'D					

[illegible]

Technical drawing of a mechanical part, likely a fuel nozzle or injector, showing multiple views and dimensions. The drawing includes a top view (A), a side view (B), a cross-section (C), and a detail view (D). Dimensions are provided in inches and millimeters. The drawing is labeled "SKETCH IN CONCEPT DESIGN STAGE. DO NOT USE FOR FABRICATION".

Top View (A): Shows the overall dimensions of the part. The total width is 24.00 inches, and the total height is 22.047 inches. The central circular feature has a diameter of 4.724 inches. The distance from the center to the outer edge is 5.354 inches. The distance from the center to the bottom edge is 12.00 inches. The distance from the center to the side edge is 22.047 inches. The distance from the center to the top edge is 22.047 inches. The distance from the center to the bottom edge is 12.00 inches. The distance from the center to the side edge is 22.047 inches. The distance from the center to the top edge is 22.047 inches.

Side View (B): Shows the profile of the part. The total height is 24.00 inches. The distance from the top edge to the center of the circular feature is 12.00 inches. The distance from the center of the circular feature to the bottom edge is 12.00 inches. The distance from the center of the circular feature to the side edge is 22.047 inches. The distance from the center of the circular feature to the top edge is 22.047 inches.

Cross-Section (C): Shows the internal structure of the part. The central circular feature has a diameter of 4.724 inches. The distance from the center to the outer edge is 5.354 inches. The distance from the center to the bottom edge is 12.00 inches. The distance from the center to the side edge is 22.047 inches. The distance from the center to the top edge is 22.047 inches.

Detail View (D): Shows a close-up of the central circular feature. The diameter is 4.724 inches. The distance from the center to the outer edge is 5.354 inches. The distance from the center to the bottom edge is 12.00 inches. The distance from the center to the side edge is 22.047 inches. The distance from the center to the top edge is 22.047 inches.

SKETCH IN CONCEPT DESIGN STAGE. DO NOT USE FOR FABRICATION

SKETCH
IN CONCEPT DESIGN
STAGE. DO NOT USE
FOR FABRICATION

5 DETAIL
SCALE: 1/1

6 DETAIL
SCALE: 1/2"

SIZE	CAGE CODE	NAD CODE NUMBER		DWG-781437	REV
D 01MF3		AREA	TYPE CL. QRE		
		540	9999 43 081	9-SET	2
SCALE: NOTED					

Specification

Specification for U-Mo Coupons for DDE-MURR



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1. SUMMARY

This specification defines the requirements for *U-Mo* (see def.) Coupons for use in production of fuel plates for the Design Demonstration Experiment (DDE) for the Missouri University Research Reactor (MURR).

2. APPLICABLE CODES, PROCEDURES, AND REFERENCES

Applicable portions of the following documents as defined herein, form a part of this specification. Where there is a conflict between the document cited and its latest revision, the supplier shall notify the Purchaser of the conflict and use the latest revision in effect unless otherwise directed by the Purchaser.

2.1 Standards and Specifications

ASTM C1233-03	Standard Practice for Determining Equivalent Boron Content of Nuclear Materials
SPC-1314	Specification for DDE-MURR Fuel Elements

3. TECHNICAL REQUIREMENTS

3.1 Isotopic Composition

The uranium isotopic composition shall be within the limits shown in Table 1.

Table 1: Isotopic Composition

Element	Symbol	Units	Limit
U-232	U-232	μg/gU	≤ 0.002
U-234	U-234	wt%U	≤ 0.260%
U-235	U-235	wt%U	19.75% +0.20% -0.30%
U-236	U-236	μg/gU	≤ 4600
Trans-U (Alpha) ¹	TRU	Bq/gU-Mo	≤ 250.0
Fission Products ²	Gamma	Bq/gU-Mo	≤ 600.0

¹ The "Alpha activity" reflects measured *transuranium* elements to include: Americium 241, Curium 243/244, Neptunium 237, Plutonium 238, and Plutonium 239/240.

² Only those isotopes with a mass number less than 200 shall be considered fission products. Fission product activity levels which are false positive due to gamma photopeak interference may be excluded.

3.2 Chemical Composition

The composition of the LEU-Mo material shall be uranium alloyed with molybdenum (nominally 10 wt% Mo). Molybdenum content shall be no less than 9.00% and no greater than 11.00% by weight. Total weight percent uranium shall be reported. Chemical composition and impurities shall be determined on each Lot of material and shall be within the limits in Table 2.

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Table 2: Chemical composition and impurities of the alloyed material

Element	Symbol	Units	Limit	EBC Factor
Aluminum	Al	μg/gU-Mo	≤ 150	0.0000
Beryllium	Be	μg/gU-Mo	≤ 10.0	0.0000
Boron	B	μg/gU-Mo	≤ 3.0	1.0000
Cadmium	Cd	μg/gU-Mo	≤ 5.0	0.3172
Calcium	Ca	μg/gU-Mo	≤ 100.0	0.0002
Carbon	C	μg/gU-Mo	≤ 725.0	0.0000
Chromium	Cr	μg/gU-Mo	≤ 50.0	0.0008
Cobalt	Co	μg/gU-Mo	≤ 10.0	0.0089
Copper	Cu	μg/gU-Mo	≤ 50.0	0.0008
Dysprosium	Dy	μg/gU-Mo	≤ 5.0	0.0818
Erbium	Er	μg/gU-Mo	≤ 100.0	0.0135
Europium	Eu	μg/gU-Mo	≤ 2.0	0.4250
Gadolinium	Gd	μg/gU-Mo	≤ 1.0	4.3991
Iron	Fe	μg/gU-Mo	≤ 250.0	0.0006
Lead	Pb	μg/gU-Mo	≤ 10.0	0.0000
Lithium	Li	μg/gU-Mo	≤ 10.0	0.1439
Magnesium	Mg	μg/gU-Mo	≤ 50.0	0.0000
Manganese	Mn	μg/gU-Mo	≤ 50.0	0.0034
Nickel	Ni	μg/gU-Mo	≤ 100.0	0.0011
Phosphorus	P	μg/gU-Mo	≤ 100.0	0.0000
Samarium	Sm	μg/gU-Mo	≤ 3.0	0.5336
Silicon	Si	μg/gU-Mo	≤ 250.0	0.0000
Sodium	Na	μg/gU-Mo	≤ 25.0	0.0003
Tin	Sn	μg/gU-Mo	≤ 100.0	0.0000
Tungsten	W	μg/gU-Mo	≤ 100.0	0.0014
Vanadium	V	μg/gU-Mo	≤ 30.0	0.0014
Zirconium	Zr	μg/gU-Mo	≤ 250.0	0.0000
Total Impurities ¹		μg/gU-Mo	≤ 1500	
Equivalent Boron Content ^{2, 3}		μg/gU-Mo	≤ 10.0	

¹ Total Impurities includes all unlisted elements; remainder shall be U-Mo.

² EBC Factors are taken from ASTM C1233-03, "Standard Practice for Determining Equivalent Boron Contents of Nuclear Materials." EBC calculation will include: Boron, Cadmium, Dysprosium, Europium, Gadolinium, Lithium, and Samarium. Other EBC factors are provided for information purposes only.

³ The limit on EBC may restrict some elements to lower values than shown in the table above.

3.3 Equivalent Boron Content

The EBC shall be calculated in accordance with ASTM C1233, "Standard Practice for Determining Equivalent Boron Contents of Nuclear Materials". The individual μg/gU-Mo impurity limits shall not be exceeded except as allowed in Section 3.4. The total impurities (μg/gU-Mo) and EBC shall not exceed the limits shown in Table 2.

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3.4 Out-of-Limits Condition

An out-of-limits condition for Table 2 elements is acceptable for a maximum of two elements not to exceed 10% of the limit established in Table 2 provided the EBC and total impurities limits are not exceeded.

3.5 Product Form

U-Mo shall be provided in the form of a Coupon meeting the dimensional requirements of Figure 1. The dimensions L, W, and T as well as quantity of Coupons will be specified by the Purchaser in a purchase order or similar contractual document.

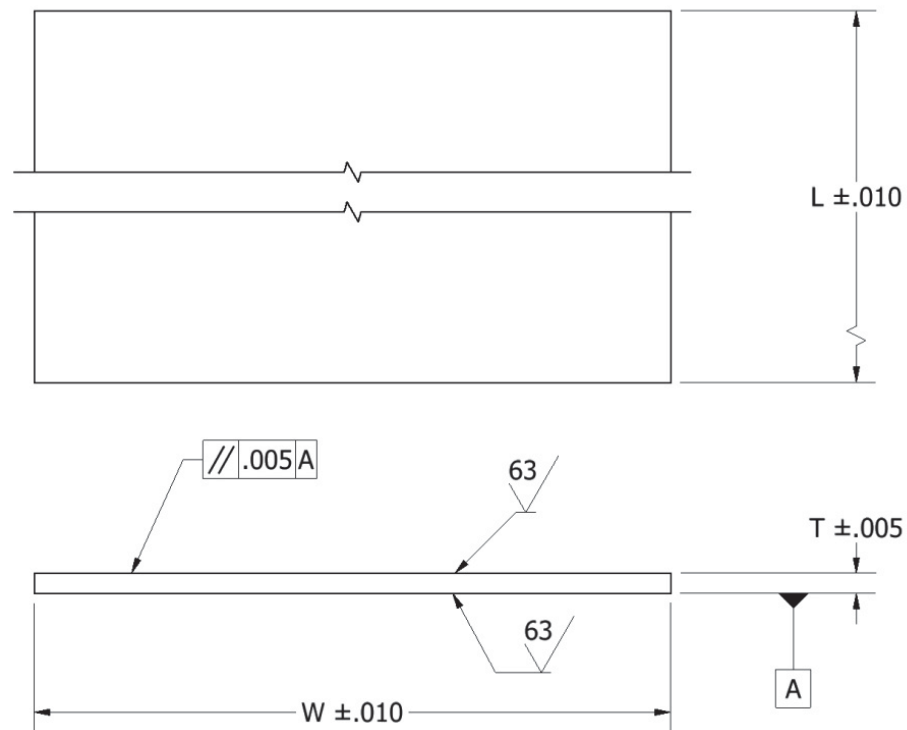


Figure 1: Coupon Dimensional Tolerances

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3.6 Defects

Every Coupon shall be visually examined for surface defects. Each coupon surface shall be found free the following:

- Visible inclusions greater than 0.063 in any dimension
- Surface scratches and cracks greater than 0.003 in. in depth or 0.25 in. in length
- Surface pores greater than 0.063 in. in any dimension, except depth, which shall not exceed 0.031 in.

One randomly selected Coupon per Lot shall be examined by radiography and evaluated against the above criteria. Radiography parameters shall produce images of sufficient quality to identify the types of defects and rejection criteria as above.

3.7 Cleanliness

There shall be no volatiles, oil, grease, particulate, or other foreign materials on the surfaces of finished Coupons.

4. QUALITY ASSURANCE

The supplier shall document, implement, and maintain a quality program in compliance with Title 10, Code of Federal Regulations, Part 830.120, "Quality Assurance".

4.1 Supplier Responsibility

The supplier shall be responsible for performing all tests and inspections required for the product form provided prior to shipment of the material. The results of all tests shall be recorded as quantitative data and furnished to the Fabricator as stipulated by Section 6.1.1.

4.2 Sampling

Each Lot of U-Mo shall be sampled and tested in accordance with the requirements of this specification and a purchaser approved sampling plan.

4.3 Acceptance Tests

The following tests shall be conducted on all Lots of U-Mo.

4.3.1 Isotopic Composition

The isotopic composition of each Lot of uranium alloy shall be determined by mass spectrographic analysis or equivalent method. The

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isotopic concentration shall be in conformance with Section 3.1. Isotopic composition of total uranium content shall be calculated by difference or equivalent method.

4.3.2 Chemical Composition

The chemical composition and impurities shall be determined on each Lot of material. The results shall be in conformance with Section 0.

4.4 Source Inspection

The supplier shall facilitate access to Purchaser-assigned quality assurance and/or technical representative(s) sufficient to provide the information necessary to verify and accept the product per the requirements of this specification.

5. PACKAGING AND SHIPPING

5.1 Packaging

Packaging and shipping containers shall comply with DOE and NRC Regulations in effect at the time of delivery.

6. NOTES

6.1 Definitions

- 6.1.1 *Certification Package*. A written and signed document from the supplier which certifies that the material described thereon complies with this specification and provides results of tests performed
- 6.1.2 *Coupon*. A thick rectangular product form intended to be reduced to final foil thickness by rolling
- 6.1.3 *Fabricator*. The primary entity selected by the Purchaser to use the U-Mo coupons to fabricate fuel plates
- 6.1.4 *Lot*. A group of pieces handled as a unit or material traceable to a common processing step
- 6.1.5 *Purchaser*. Idaho National Laboratory
- 6.1.6 *Supplier*. The primary entity selected by the Purchaser to supply the U-Mo coupons
- 6.1.7 *U-Mo*. A binary alloy comprised of uranium and molybdenum

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6.2 Quality Verification Test Results

A Certification Package shall be provided for each shipment or group of shipments. Certifications shall be signed by project quality engineer or equivalent. Three (3) copies of the Certified Test Results (see Section 4.1) and certification as required above shall be provided to the fuel plate fabricator and one (1) copy to the Purchaser at time of shipment. Also one (1) copy should accompany the shipment or be provided to the receiver at time of shipment. The Certification Package shall include the following:

- 6.2.1 A statement that the material meets the requirements contained in this specification
- 6.2.2 A list of Coupon identification numbers and total Coupon, U-Mo alloy, uranium, and isotope masses

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Specification

Specification for DDE-MURR Fuel Elements



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1. SCOPE

1.1 Introduction

This Specification details the materials, components, testing, inspection, and Quality Control requirements for the fabrication of Fuel Elements for the Design Demonstration Experiment (DDE) representing the Missouri University Research Reactor (MURR) low enriched uranium fuel design. DDE-MURR Fuel Elements are designed for irradiation in the Belgium Reactor 2 (BR-2) in Mol, Belgium. If there appears to be any conflict between parts of this Specification, such as its referenced drawings and standards, the Purchaser and Stakeholder shall be notified for resolution.

1.2 Definitions

For the purpose of this Specification, the following terms are identified:

- 1.2.1 *Cladding*. The aluminum bonded to the Fuel Meat
- 1.2.2 *Controlled Work Area*. A work area to which access of personnel, tools, and materials is limited and physically controlled. Temporary enclosures may be used where adjacent activities produce contamination which is detrimental to the job
- 1.2.3 *Coupon*. A thick rectangular product form intended to be reduced to final foil thickness by rolling
- 1.2.4 *Development*. A determination of processes, equipment, and parameters required to produce a product in compliance with this Specification
- 1.2.5 *Failure*. A condition where the Manufacturing Process appears to be out of control or damage to Fuel Plates or Fuel Elements or breakdown of equipment causes delays and/or excessive cost
- 1.2.6 *Fuel Meat*. The uranium bearing region of each Fuel Plate
- 1.2.7 *Fuel Element*. An assembly of Fuel Plates and hardware components
- 1.2.8 *Fuel Plate*. The Fuel Meat complete with aluminum Cladding
- 1.2.9 *Hot Isostatic Press (HIP)*. Fabrication process which bonds Cladding to Monolithic foils by subjecting un-bonded Fuel Plate materials to a high pressure and temperature

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- 1.2.10 *In-Process Controls*. Inspection and tests made during Production to ensure that the Manufacturing processes, equipment, and personnel are producing a product meeting specified requirements
- 1.2.11 *Interlayer*. Thin zirconium layer applied to the surface of Monolithic foils
- 1.2.12 *Lot*. A group of pieces handled as a unit or material traceable to a common processing step
- 1.2.13 *Manufacturing*. All fabrication, assembly, test, inspection, and Quality Control processes
- 1.2.14 *Monolithic*. Fuel type composed of a metallic alloy in the form of a foil.
- 1.2.15 *Production*. That phase of the program, following Qualification, during which the product is in Manufacture
- 1.2.16 *Purchaser*. Idaho National Laboratory
- 1.2.17 *Qualification*. A documented demonstration approved by the Purchaser that the Manufacturing processes, equipment, and personnel can produce a product in compliance with this Specification
- 1.2.18 *Quality Control*. The sampling plans, inspections, and tests required during Production to assure that the product is in compliance with this Specification
- 1.2.19 *Rejection*. Refusal of acceptance of materials, parts, components, or assembly products as part of the contract requirements of this program because of noncompliance with this Specification
- 1.2.20 *Requalification*. A demonstration that a single, or group of Manufacturing processes, equipment, and personnel can produce a product in compliance with this Specification after the original Qualification has been completed and becomes invalid
- 1.2.21 *Specification*. All parts and attachments of this document, its references, drawings, and standards, as may be modified from time to time by contractual document
- 1.2.22 *Stakeholder*. Missouri University Research Reactor
- 1.2.23 *Subtier Supplier*. Any vendor selected by the Supplier to furnish materials, services, or manufactured parts to the Supplier

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1.2.24 *Supplier*. The primary vendor selected by INL to Manufacture the product

1.2.25 *U-Mo*. A binary alloy comprised of uranium and molybdenum

2. APPLICABLE DOCUMENTS

2.1 Applicable Standards

The applicable portions of the following documents, as defined herein, form a part of this Specification. Where there is a conflict between the documents cited and the latest revision, thereof, the Supplier shall notify the Purchaser of the conflict and use the latest revision unless otherwise directed by the Purchaser.

2.1.1 National Codes and Standards

MIL-C-45662	Calibration System Requirements
-------------	---------------------------------

2.1.2 American Society for Testing and Materials (ASTM)

ASTM E 1742	Standard Practice for Radiograph Examination
ASTM E 8	Methods of Tension Testing of Metallic Materials
ASTM E 29-93a	Recommended Practice for Indicating Which Places of Figures are to be Considered Significant in Specified Limiting Values

2.1.3 American National Standards Institute (ANSI)

ANSI B46.1	Surface Texture
ANSI Y14.5	Dimensioning and Tolerancing for Engineering Drawings

2.1.4 American Society of Mechanical Engineers (ASME)

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ASME Boiler and Pressure Vessel Code Section V

ASME NQA-1 Quality Assurance Requirements for Nuclear Facility Applications

2.1.5 Idaho National Laboratory

STD-7022A Cleanliness Acceptance Levels for Nuclear or Non-Nuclear Service Components

SPC-1568 Specification for U-Mo Coupons for DDE-MURR

2.1.6 American Society for Nondestructive Test (ASNT)

SNT-TC-1A American Society For Nondestructive Testing (ASNT) Recommended Practice

2.1.1 Drawings (INL)

603455 MURR LEU Fuel Element Assembly

3. REQUIREMENTS

3.1 Records and Reports

3.1.1 Two (2) copies of the following data and records shall be supplied to the Purchaser for review and approval prior to fabrication of Fuel Elements. One (1) information copy shall be supplied to the Stakeholder by the Supplier.

3.1.1.1 All shop drawings of Fuel Element components and assemblies to be used in the fabrication of Fuel Elements

3.1.1.2 Integrated Manufacturing and Inspection Test Plan, submittal of Supplier route cards, operation procedures, drawings, and flow sheets may fulfill this requirement

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3.1.1.3 A detailed description as to the manner by which the Supplier proposes to assign Fuel Plate U-235 content, included in the description shall be sampling, analytical, and Quality Control procedures; a statement as to the estimated absolute accuracy of the assigned Fuel Plate and Fuel Element U-235 content

3.1.1.4 Qualification Package for Fuel Plate fabrication

3.1.2 Concurrent with or prior to the shipment of each Fuel Element the Supplier shall provide the Purchaser with the items in Section 6 of this Specification.

3.1.3 Two (2) copies of the following reports are required by this Specification:

3.1.3.1 Monthly Reports: A monthly report using Line of Balance, Program Evaluation and Review Technique (PERT), or similar reporting techniques which details program progress against a previously submitted schedule shall be provided by the Supplier to the Purchaser and Stakeholder by the fifteenth (15th) working day of each month.

3.1.3.2 Failure Notification: During Production, complete records shall be kept by the Supplier. In the event of a Failure, the time, nature, description, corrective action taken, and proposed further corrective action shall be reported to the Purchaser within five (5) working days after such Failure. An information copy shall be sent to the Stakeholder when process Failures are involved.

3.2 Manufacturing Procedures

All changes and modifications to programs, processes, procedures to be used to Manufacture the product shall be submitted to the Purchaser for review and approval prior to use. Information copies shall be provided to the Stakeholder. These shall include:

3.2.1 Supplier's Specifications for all materials used

3.2.2 Identification of Subtier Suppliers

3.2.3 Complete Development program, including material, process, equipment, and test procedures, Supplier submittal of the Qualification data package may fulfill this requirement

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- 3.2.4 All fabrication, assembly, cleaning, surface treating, handling, and demonstration procedures
- 3.2.5 All test, inspection, Production, and Quality Control procedures, including all nondestructive tests and standards
- 3.2.6 In-Process Controls, sampling programs, and procedures
- 3.2.7 Quality Control sampling program and procedures
- 3.2.8 All rework or repair programs and procedures
- 3.2.9 All final inspection, washing, packaging, storage, and shipping procedures
- 3.2.10 Manufacturing plan and inspection procedure for Fuel Plate and Fuel Element fabrication
- 3.2.11 The Supplier shall prepare and maintain written procedures also for radiograph test, ultrasonic test, visual examination, and personnel certification

3.3 Quality Assurance

The Supplier shall document, implement, and maintain a quality system in compliance with ASME NQA-1. Measurement equipment used for tests and inspection required in this section and in Section 5 shall be calibrated in conformance with Mil-C-45652. A description of the Quality Assurance Program and the procedures to maintain adequate control and quality shall be furnished to the Purchaser.

The Supplier shall permit the Purchaser to conduct pre-award and continuing evaluation of the Supplier's quality system. The Supplier shall be subject to Source Inspection by the Purchaser at the Supplier's facility and also at the Subtier Supplier's facility if deemed necessary. The Purchaser will identify hold points to the Supplier to be witnessed by the Purchaser's representative. The Purchaser's source inspection does not constitute final acceptance of the items. A Quality Supplier Release, which is approved by the source inspector, shall be required before shipment to the facility designated by the Purchaser.

Personnel performing NDE examinations, specifically radiographic, ultrasonic, and visual shall be certified to American Society for Nondestructive Testing (ASNT) Number SNT-TC-1A and certification documentation shall be made available to the purchaser.

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The Supplier is required to qualify the processes or portions of the process, or be exempt from same by written approval of the Purchaser. Only materials which comply with this Specification shall be used. Fuel Plate Qualification shall be satisfied by the fabrication of at least one Lot of consecutively produced Fuel Plates of each size having a yield of at least 65% acceptable Fuel Plates which meet the requirements of this Specification. The Lot size shall be determined by an agreement between the Purchaser and Supplier.

Fuel plates made prior to and during qualification runs that fail to meet the 65% yield requirements shall not be used in fabricating Fuel Elements without prior approval of the purchaser.

3.3.1 Operator Qualification: Operator Qualification shall be accomplished via an approved Supplier Internal Qualification program for the following operations:

3.3.1.1 Swaging

3.3.1.2 Final machining

In addition to the operations specified above, the Supplier shall also show evidence of the training and competency of those individuals who perform any of the following Fuel Element fabrication and inspection activities:

3.3.1.3 HIP pack assembly and preparation

3.3.1.4 Fuel Plate, Fuel Element, and component cleaning

3.3.1.5 Dimensional inspection of Fuel Plates, Fuel Elements, and subcomponents

3.3.1.6 Visual inspection of the Fuel Plates, Fuel Elements, subcomponents, and bend test specimens

3.3.1.7 Coolant channel gap dimensioning or probing

3.3.1.8 Radiography and inspection of Fuel Plate radiographs

3.3.1.9 Ultrasonic testing

3.3.1.10 Eddy current testing

The individuals performing these operations shall have specific requirements imposed on them that will demonstrate their knowledge

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and ability to perform their respective assignments. Documented evidence of the training of those individuals shall be maintained and shall be made available to the Purchaser upon request.

3.3.2 In-Process Controls: The Supplier shall establish a process control program whereby checks are made on the Fuel Plate Manufacturing processes, operational procedures, intermediate product characteristics, and equipment to demonstrate process stability during Production is at least equal to that demonstrated during Qualification. These In-Process Controls shall monitor, as a minimum, the following fuel plate characteristics:

3.3.2.1 Fuel Homogeneity

3.3.2.2 Fuel Configuration

3.3.2.3 Cladding Thickness

3.3.2.4 Internal defects and bond integrity

3.3.2.5 Surface finish and defects

3.3.2.6 Cleanliness

3.3.2.7 Dimensional

3.3.2.8 Swage joint pull tests

3.3.3 Requalification: The Supplier shall notify the Purchaser of any proposed process change. A changed process may not be used in Production until the Supplier has submitted the results and data of the Requalification effort to the Purchaser and received written approval to use the changed process in Production. The Supplier may be exempt from Requalification if the Supplier can demonstrate to the Purchaser by proof test or engineering explanation, and receives written approval from the Purchaser, that the proposed process change will not degrade the quality of the product.

3.4 Product Requirements

3.4.1 Fuel Meat: Fuel Meats shall be U-Mo Monolithic foils fabricated from U-Mo Coupons furnished per SPC-1567. U-Mo Monolithic foils shall have zirconium Interlayers bonded to the largest surfaces for which the nominal thickness is 0.001 inch each. Zirconium materials shall be at least 99.5% pure (metals basis excluding hafnium) with no greater than

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100ppm hafnium impurities. Zirconium materials shall be purchased with vendor certifications and shall be verified by independent laboratory analysis. During Qualification a minimum of one (1) randomly selected Monolithic foils of each thickness type shall be examined for Interlayer thickness per section 3.4.1.1. During Production a minimum of one (1) randomly selected Monolithic foil per 100 of each thickness type shall be examined for Interlayer thickness per section 3.4.1.1.

3.4.1.1 Interlayer Thickness: At least four (4) microscopic examinations per foil shall be evaluated for Interlayer thickness. Each side of the foil shall be represented by at least one (1) sample as in Figure 1. Samples shall be taken from those portions of the foil that are removed during final sizing. Each sample shall be sectioned, polished, and dimensional measurements shall be obtained at 50X minimum magnification. At least ten (10) thickness measurements shall be obtained for each of the two (2) Interlayers on each of the four (4) samples. The average of each set of ten (10) readings shall not be less than 0.0005 inch.

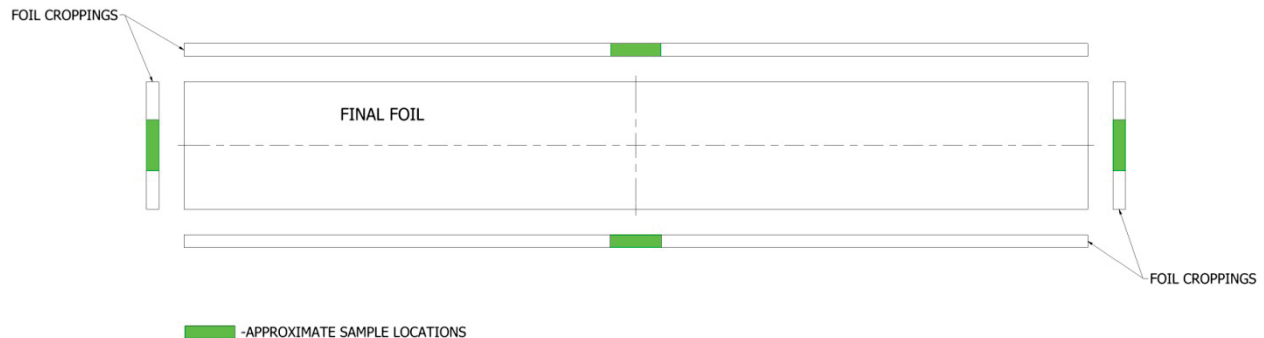


Figure 1: Foil Sample Locations

3.4.2 Fuel Plates

Fuel Loading: Each Fuel Plate shall be loaded to U-235 content limits per Table 1. Requirements for fuel loading shall be established in accordance with Section 3.1.1.3 by the Supplier subject to the approval of the Purchaser.

Table 1: Fuel Plate U-235 Loading

Fuel Plate	U-235 Nominal (g)	Tolerance ($\pm\%$)	U-235 Minimum (g)	U-235 Maximum (g)
1	18.10	11%	16.09	20.11
2	25.66	8.3%	23.52	27.80

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3	36.27	6.3%	34.00	38.53
4	47.88	5.0%	45.48	50.27
5	50.45	5.0%	47.93	52.97
6	52.99	5.0%	50.34	55.64
7	55.54	5.0%	52.76	58.32
8	58.06	5.0%	55.16	60.97
9	60.61	5.0%	57.58	63.64
10	63.16	5.0%	60.00	66.31
11	65.70	5.0%	62.42	68.99
12	68.25	5.0%	64.84	71.66
13	70.77	5.0%	67.23	74.31
14	73.32	5.0%	69.65	76.98
15	75.86	5.0%	72.07	79.66
16	78.41	5.0%	74.49	82.33
17	80.96	5.0%	76.91	85.00
18	83.48	5.0%	79.30	87.65
19	86.02	5.0%	81.72	90.33
20	88.59	5.0%	84.16	93.02
21	91.14	5.0%	86.58	95.70
22	93.71	5.0%	89.02	98.40
23	81.88	5.9%	77.06	86.70

3.4.2.1 Requirements for Radiography of Fuel Plates: A procedure shall be written by the Supplier to specify the details for achieving acceptable Fuel Plate radiographs. The procedure shall include the requirements given in this Specification and shall be approved by the Purchaser.

The voltage shall be at least 100 k.v.p with focal spot size of 5mm maximum. The distance between the focal point and the Fuel Plate shall be at least twice the length of the Fuel Plate. The focal point shall be centered laterally and longitudinally over the Fuel Plate or group of Fuel Plates. Any method(s) used to mitigate and/or correct for undercutting effects at Fuel Meat edges shall be documented in the procedure.

The image outline shall be clear and sharp; the film shall be free of runs, streaks, scratches, blurs, and cassette defects that will affect the area covered by the Fuel Plates.

Film density for fuel homogeneity radiographs, as read over the Fuel Meat region, shall provide densitometer readings of between 1.0 and 4.0.

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Density standard(s) shall be exposed simultaneously with each Fuel Plate.

The film shall be an extreme sensitivity, extra fine grain, high contrast, double emulsion, industrial X-ray type, (Kodak type M or equal) which is acceptable to the Purchaser. Development of the film shall be in accordance with the manufacturer's recommendation.

A system of identification of the film shall be provided by the Supplier which shall show as a minimum:

- 3.4.2.1.1 Fuel Plate Lot number
- 3.4.2.1.2 Fuel Plate serial number
- 3.4.2.1.3 Orientation of density standard
- 3.4.2.1.4 Density standard identification
- 3.4.2.1.5 Date of radiography

Fuel Homogeneity: Any one half (1/2) inch diameter area, at any location in the Fuel Meat shall not exceed the limit of a $\pm 15\%$ density standard.

Between the minimum and maximum permissible Fuel Meat length boundary, fuel underload condition shall not be evaluated.

- 3.4.2.2 Fuel Configuration: The outline of the Fuel Meat shall be within the largest and smallest areas as defined by dwg 603455 dimensions and their respective tolerances.

Compliance with Fuel Meat configuration requirements shall be by visual inspection of Fuel Plate radiographs of all Fuel Plates. Visual radiograph inspections shall be performed on a light table having a light range of 450-600 footcandles at the table surface and the area darkened to give a light range of 5-15 footcandles 18 inches above the light table with radiographic film in place on the table.

- 3.4.2.3 Cladding Thicknesses: All Fuel Plates shall be evaluated for Cladding thickness by UT and shall have a minimum Cladding thickness of 0.008 inches.

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- 3.4.2.4 Internal Defects and Bond Integrity: During Qualification all Fuel Plates shall be evaluated for bond integrity by UT and bend testing. During Production all Fuel Plates shall be evaluated for bond integrity by UT and one (1) Fuel Plate per Lot shall be evaluated by bend testing.

Any UT indications of debond, voids, blisters, or delaminations larger than 0.060 inches over the Fuel Meat or 0.120 inches outside the Fuel Meat area shall be cause for Rejection. A maximum of two (2) indications less than 0.060 inches in diameter are allowed in the Fuel Meat area provided they are more than 0.250 inches apart. A maximum of two (2) indications less than 0.120 inches in diameter are allowed in any edge or end clad area, outside the Fuel Meat area, provided they are not any closer than 0.050 inches to the edge or end of the Fuel Plate and no closer together than the major dimension of the largest indication.

Bend test samples shall be the portions of the Fuel Plate assembly adjacent to the final Fuel Plate which are removed from the assembly during final sizing of the Fuel Plate. Each sample shall be bent around a mandrel 90 degrees in one direction, returned to 0 degrees, then bent 90 degrees in the other direction, and returned to 0 degrees. The edges of the bend test specimen adjacent to the Fuel Plate shall then be visually examined, without magnification, for delamination. Any edge adjacent to the Fuel Plate showing visual delamination of the Cladding layers shall be cause for Rejection of the associated Fuel Plate. At least six (6) bend samples per Fuel Plate, including two (2) along each long side and one (1) along each short side, shall be tested and visually inspected to verify bonding.

- 3.4.2.5 Surface Finish and Defects: The finished Fuel Plates shall be free from pits, dents, scratches, and other areas of Cladding removed in excess of 0.003 inch deep.

Compliance with surface finish and defect requirements shall be established by 100% visual inspection without magnification of all Fuel Plates. An optical depth gage shall be used to evaluate questionable defects.

- 3.4.2.6 Dimensional: Fuel Plate outer dimensions shall be verified by inspection of three (3) Fuel Plates per Lot. If any of these three

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(3) is discrepant, the entire Lot shall be dimensionally inspected. All Dimensions shall apply at a temperature of 75° F \pm 5°F.

3.4.2.7 Identification: Each finished Fuel Plate shall be identified by a marking method approved by the Purchaser over the non-fueled region per dwg 603455 and shall not be in excess of 0.010 inch deep. Positive identification shall be maintained relative to the complete fabrication history including the Fuel Plate Lot, Monolithic foils, basic material Lots, U-Mo coupons, Manufacturing cycle, and Quality Control phases.

3.4.2.8 Storage: All Fuel Plates that have received final cleaning shall be contained in clean polyethylene containers or other containers approved by the Purchaser while awaiting final assembly, being transferred into storage, and being maintained in storage. Any material exposed to contamination shall be re-inspected to the requirements of Section 3.4.3.6.

3.4.3 Fuel Elements

3.4.3.1 Fuel Loading: Each Fuel Element shall contain 1439g \pm 14.4g U-235.

3.4.3.2 Mechanical Integrity: The Supplier shall assemble fuel plates to side plates by swaging. Mechanical integrity of swage joints shall be established by performing pull tests with care equivalent to performing tension tests as prescribed in ASTM E 8. Swaged joints between the Fuel Plates and side plates shall be able to withstand a load of not less than 150 pounds per linear inch of swage joint.

Pull test samples shall have matching geometry compared to the Fuel Elements except that they shall be 3.0 \pm 0.1 inch long and that the plate portions may be made from “blank” aluminum stock in lieu of fueled plates. Swaging of test specimens shall be interspersed in the normal Fuel Element swaging process without adjustment of the swaging parameters. The swage test specimen quantity, placement, type, and sequencing shall be sufficient to comprehensively represent each Fuel Element’s swaging operation in all of the following parameters:

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- 3.4.3.2.1 Fuel plate type including a sample plate 1, plate 23, and one plate each selected from each of the ranges plates 2-8, plates 9-15, and plates 16-22
- 3.4.3.2.2 Each side plate (left and right)
- 3.4.3.2.3 Three locations in the swage bed direction of travel (fore, middle, and aft)
- 3.4.3.2.4 Swaging sequence (both prior to and following swaging of the Fuel Element)
- 3.4.3.3 Identification: The side plate of each Fuel Element shall be identified as DDE-MURR as shown in drawing 603455.
- 3.4.3.4 Dimensional: Verification of all external dimensions of the Fuel Elements and all coolant channel gaps shall be by 100% inspection in accordance with INL drawing 603455. Final coolant channel gap dimensions shall be taken after the final Fuel Element assembly. The coolant channel gap dimensions shall be taken within the full length of each channel as measured half way between the combs and the side plates and by a procedure that provides digital dimensions. All dimensions of this Specification shall apply at a temperature of $75^{\circ}\text{F} \pm 5^{\circ}\text{F}$. Results of this inspection shall be submitted to the Purchaser and the User.
- 3.4.3.5 Surface Finish and Defects: Fuel Elements surfaces, which are not Fuel Plate surfaces, shall be free from pits, dents, scratches, and other removal of metal in excess of 0.015 inches deep and 0.180 inches in diameter.
- 3.4.3.6 Cleanliness and Surface Contamination: The Supplier's fabrication, assembly, and storage areas used for the Production of Fuel Elements and/or components shall conform to the requirements of a "Controlled Work Area" as defined in Paragraph 1.3.6 of STD-7022A. Cleanliness shall be in compliance with STD-7022A, paragraphs 1.1, 1.2.3, 3.1, 3.2-b, -d, -1, 3.3-d, -e, 4.1.3, 4.2, and 4.3. Freon shall not be used to clean Fuel Elements or components.

There shall be no foreign materials on the surfaces of the finished Fuel Plates or Fuel Elements. Use of graphite or organics for marking purposes is prohibited. The use of

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abrasives for cleaning the Fuel Plates or for any other purpose is prohibited, as is any procedure which removes aluminum from the surface of the finished Fuel Plates. Any corrosion products, dirt, scale, graphite, oil products, metal chips, finger prints, etc., shall be removed without violating minimum Cladding thickness. Degreasing agents shall be approved by the Purchaser. After degreasing, all surfaces, including all crevices shall be thoroughly rinsed with distilled water. Water marks that do not affect the mechanical integrity of the swage joints are allowed.

Fuel Plate and Fuel Element cleanliness requirements of shall be verified by visual inspection of 100% of the Fuel Plates and Fuel Elements and by In-Process Controls. The surfaces of each Fuel Plate and the completed Fuel Element shall be smeared and the smear counted for radioactive contamination. The alpha count shall be less than five (5) dpm per 100 cm² and the beta-gamma count shall be less than two hundred (200) dpm per 100 cm².

- 3.4.3.7 Fuel Element Surface Treatment: After Fuel Elements are final machined and inspected they shall be subjected to an environment that will cause an evenly distributed boehmite layer to form on all surfaces of the entire assembly. The treatment process shall be performed under controlled conditions, which shall require the Supplier to maintain a record of the thermal history of the autoclave. The records shall include heat charts of recorded time and temperature. The Supplier shall maintain documented evidence of the controls placed on the autoclave.

Each Fuel Element shall have a corresponding aluminum plate cropping, made from Fuel Plate end crops, placed near the Fuel Element during the boehmite formation process. The aluminum plate croppings shall be subjected to the same environment as the Fuel Elements and each aluminum plate cropping measured for boehmite thickness via Eddy current instrumentation. The average of these measurements shall not be less than less than 0.00006 inch or more than 0.0003 inch thickness.

Fuel Elements and aluminum plate croppings subjected to the boehmite formation process shall be carefully handled to preclude scratches, dents, and gouges that would cause removal of boehmite.

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3.4.3.8 Storage: All Fuel Elements that have received boehmite treatment shall be sealed in clean polyethylene containers or other containers approved by the Purchaser while being transferred into storage, maintained in storage, and prepared for packaging and shipment. Any material exposed to contamination shall be re-inspected according to the requirements of Section 3.4.3.6.

4. MATERIALS OF CONSTRUCTION

- 4.1 All items prepared for Fuel Element assembly shall be traceable to the raw material from which they were fabricated.
- 4.2 Prior to fabrication of Fuel Plates and Fuel Elements, the Supplier or an independent laboratory shall perform chemical analysis, and mechanical tests where applicable, on U-Mo alloys, zirconium Interlayer, side plates, end box, and Fuel Plate Cladding materials.

5. TEST AND INSPECTION REQUIREMENTS

5.1 Responsibility

Unless otherwise specified, the Supplier shall be responsible for the performance of all tests and inspections required prior to submission to the Purchaser of any Fuel Element for acceptance. The following tests and inspections, in addition to the ones listed in the various sections of the Specification, shall be performed by the Supplier to assure that the product quality is in accordance with the requirements of this Specification.

- 5.1.1 Materials: Compliance with material requirements shall be established by Supplier certification. A certification of chemical analysis or a certified Mill Test Report shall be supplied to the Purchaser for each Lot of material used in the fabrication of Fuel Elements. All materials shall be traceable to the Fuel Elements fabricated from these materials.

6. DELIVERY SUBMITTALS

- 6.1 Two (2) copies (except as noted) of the following data and records shall be sent previous to or concurrent with shipments to the Purchaser and one (1) copy shall be sent to the Stakeholder.
 - 6.1.1 Certification of product compliance to the requirements of this Specification to include any test data pertaining thereto

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- 6.1.2 Certification of material compliance to the requirement of this Specification to include any chemical and physical test results pertaining thereto
- 6.1.3 Dimensional Data as required by Section 3.4.2.6 and Section 3.4.3.4
- 6.1.4 Individual Fuel Plate uranium data including:
 - 6.1.4.1 Serial number with foil identification
 - 6.1.4.2 Foil weight
 - 6.1.4.3 Uranium content
 - 6.1.4.4 Total U-235 content
 - 6.1.4.5 Alpha contamination results
- 6.1.5 Individual Fuel Element Composition data including:
 - 6.1.5.1 Serial number of the Fuel Element
 - 6.1.5.2 Uranium content
 - 6.1.5.3 U-235 content
 - 6.1.5.4 Serial number of each Fuel Plate in the Fuel Element and the stacking order
- 6.1.6 Radiation smear count from Fuel Plate and Fuel Element exterior, as required by Section 3.4.3.6
- 6.1.7 Results of swage joint pull tests specified in Section 3.4.3.2
- 6.1.8 List of all applicable waivers and deviations and related Fuel Plates or Fuel Elements
- 6.1.9 Radiographs as specified in Section 0 and UT data as specified in Section 3.4.2.4 to be sent to the Purchaser

7. PACKAGING AND SHIPPING

- 7.1 Purchaser shall provide shipping containers which will protect the Fuel Elements from damage during shipment and which conform in all respects to the applicable regulations of the U.S. Department of Energy, of the U.S. Department of

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Transportation, and of any other agencies having jurisdiction over the shipment of radioactive materials.

- 7.2 The Supplier shall load the Fuel Elements into the shipping containers in a sealed polyethylene bag in a clean and dry condition free of extraneous materials.
- 7.3 The Supplier shall take all necessary precautions during packing to prevent damage to the Fuel Elements during shipment. Each container shall be provided with a tamper-proof seal. The container's loading and shipping documents shall be prepared in accordance with all applicable regulations.
- 7.4 The Supplier shall make arrangements for shipment to the facility designated by the Purchaser. Approval of shipping date shall be obtained from Purchaser prior to any shipment. The Supplier shall make the shipment per a prepared and maintained handling, packaging, and shipping procedure.

8. ACCEPTANCE INSPECTION

8.1 Acceptance Inspection

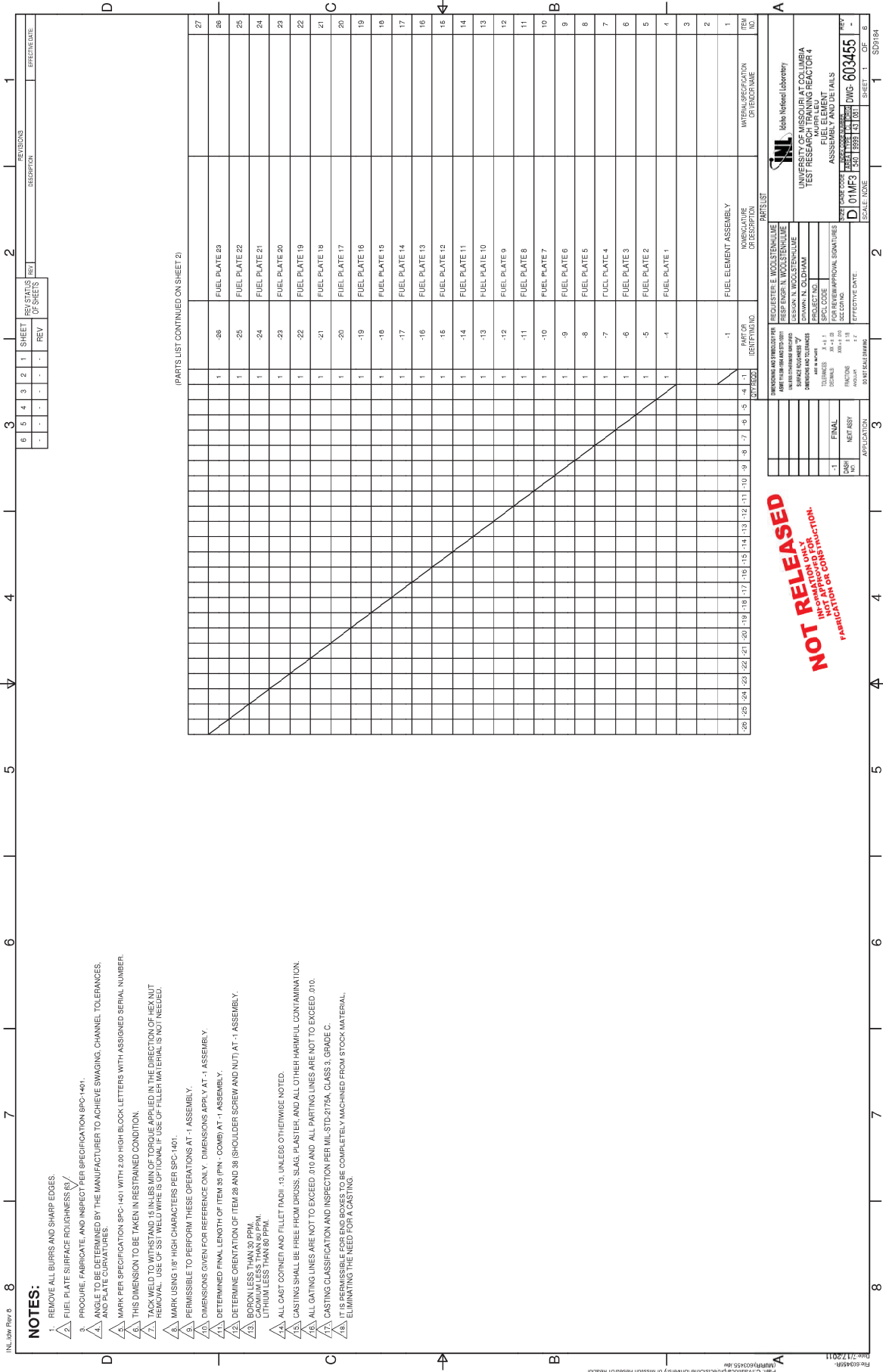
All materials, workmanship, and procedures shall be subject to inspection, examination, test, and Rejection by the Purchaser for noncompliance with the Specifications at any and all times during Manufacture, and at any and all places where such Manufacture is carried on. Final inspection and acceptance or Rejection will be made by the Purchaser at the Supplier's plant. The Purchaser shall have the right to reject any finished products for defects in workmanship, or defects in any of the materials comprising the finished product which otherwise fail to meet the Specification.

8.2 Deviation from Specifications

Notwithstanding other provisions of these Specifications, the Purchaser may, when requested in writing, waive certain minor deviations from requirements of the Specifications and drawings where the Failure to meet any specific requirement either alone or in combination with other Failures will not significantly reduce the efficiency or performance of the assembly. Acceptance of a Fuel Element by the Purchaser with deviations from the Specifications shall not be construed to mean the Purchaser approves or will approve similar deviations in Fuel Elements not yet delivered under the contract.

Deviations from design documents shall be documented on a change request form One (1) copy is to be sent to the Stakeholder concurrent to transmittal to the Purchaser.

Appendix G (Draft Element Drawings)



PARTS LIST CONTINUED											
QTY	PART OR IDENTIFYING NO.	DESCRIPTION OR REMARKS	REMARKS	QTY	PART OR IDENTIFYING NO.	DESCRIPTION OR REMARKS	REMARKS	QTY	PART OR IDENTIFYING NO.	DESCRIPTION OR REMARKS	REMARKS
4	4424	SHOULDER SCREW, SCH		4	4424	SHOULDER SCREW, SCH		4	4424	SHOULDER SCREW, SCH	
2	-29	END FITTING		2	-29	END FITTING		2	-29	END FITTING	
2	-30	OUT ROLLER		2	-30	OUT ROLLER		2	-30	OUT ROLLER	
2	-31	IN ROLLER		2	-31	IN ROLLER		2	-31	IN ROLLER	
1	-32	SIDE PLATE / 3		1	-32	SIDE PLATE / 3		1	-32	SIDE PLATE / 3	
1	-33	SIDE PLATE / 3		1	-33	SIDE PLATE / 3		1	-33	SIDE PLATE / 3	
2	-35	PIN - COMB		2	-35	PIN - COMB		2	-35	PIN - COMB	
2	-37	COMB		2	-37	COMB		2	-37	COMB	
4		NUT, HEX		4		NUT, HEX		4		NUT, HEX	
AR		WELD FILLER METAL		AR		WELD FILLER METAL		AR		WELD FILLER METAL	
16	CR2162-6-5	RIVET, 6016 X .0516 GR0P		16	CR2162-6-5	RIVET, 6016 X .0516 GR0P		16	CR2162-6-5	RIVET, 6016 X .0516 GR0P	
42		CLADDING / 3		42		CLADDING / 3		42		CLADDING / 3	
42		AL ALLOY 6061-T6 (RAW MATERIAL)		42		AL ALLOY 6061-T6 (RAW MATERIAL)		42		AL ALLOY 6061-T6 (RAW MATERIAL)	

42	AL 6061-T6 OR ASTM B209	AL ALLOY 6061-T6 (RAW MATERIAL)
41	TOWNSEND TEXTRON CORP. SANTA ANA, CA	AL 6061-T6 OR ASTM B209
40		ER312
39	AWG A5.9	300 SERIES SST
38		AL 6061-T6 OR ASTM B209 OR AL 6061-T651 OR ASTM B211 OR AL 6061-T6510
37		AL 6061-T6 OR ASTM B209 OR AL 6061-T651 OR ASTM B211 OR AL 6061-T6510
36		AL 6061-T6 OR ASTM B209 OR AL 6061-T651 OR ASTM B211 OR AL 6061-T6510
35		AL 6061-T6 OR ASTM B209 OR AL 6061-T651 OR ASTM B211 OR AL 6061-T6510
34		PLATE, 1/8" OR 1/4" OR 1/2" OR 3/4" OR 1" OR 1 1/2" OR 2" OR 3" OR 4" OR 6" OR 8" OR 10" OR 12" OR 14" OR 16" OR 18" OR 20" OR 24" OR 30" OR 36" OR 42" OR 48" OR 54" OR 60" OR 66" OR 72" OR 78" OR 84" OR 90" OR 96" OR 102" OR 108" OR 114" OR 120" OR 126" OR 132" OR 138" OR 144" OR 150" OR 156" OR 162" OR 168" OR 174" OR 180" OR 186" OR 192" OR 198" OR 204" OR 210" OR 216" OR 222" OR 228" OR 234" OR 240" OR 246" OR 252" OR 258" OR 264" OR 270" OR 276" OR 282" OR 288" OR 294" OR 300" OR 306" OR 312" OR 318" OR 324" OR 330" OR 336" OR 342" OR 348" OR 354" OR 360" OR 366" OR 372" OR 378" OR 384" OR 390" OR 396" OR 402" OR 408" OR 414" OR 420" OR 426" OR 432" OR 438" OR 444" OR 450" OR 456" OR 462" OR 468" OR 474" OR 480" OR 486" OR 492" OR 498" OR 504" OR 510" OR 516" OR 522" OR 528" OR 534" OR 540" OR 546" OR 552" OR 558" OR 564" OR 570" OR 576" OR 582" OR 588" OR 594" OR 600" OR 606" OR 612" OR 618" OR 624" OR 630" OR 636" OR 642" OR 648" OR 654" OR 660" OR 666" OR 672" OR 678" OR 684" OR 690" OR 696" OR 702" OR 708" OR 714" OR 720" OR 726" OR 732" OR 738" OR 744" OR 750" OR 756" OR 762" OR 768" OR 774" OR 780" OR 786" OR 792" OR 798" OR 804" OR 810" OR 816" OR 822" OR 828" OR 834" OR 840" OR 846" OR 852" OR 858" OR 864" OR 870" OR 876" OR 882" OR 888" OR 894" OR 900" OR 906" OR 912" OR 918" OR 924" OR 930" OR 936" OR 942" OR 948" OR 954" OR 960" OR 966" OR 972" OR 978" OR 984" OR 990" OR 996" OR 1002" OR 1008" OR 1014" OR 1020" OR 1026" OR 1032" OR 1038" OR 1044" OR 1050" OR 1056" OR 1062" OR 1068" OR 1074" OR 1080" OR 1086" OR 1092" OR 1098" OR 1104" OR 1110" OR 1116" OR 1122" OR 1128" OR 1134" OR 1140" OR 1146" OR 1152" OR 1158" OR 1164" OR 1170" OR 1176" OR 1182" OR 1188" OR 1194" OR 1200" OR 1206" OR 1212" OR 1218" OR 1224" OR 1230" OR 1236" OR 1242" OR 1248" OR 1254" OR 1260" OR 1266" OR 1272" OR 1278" OR 1284" OR 1290" OR 1296" OR 1302" OR 1308" OR 1314" OR 1320" OR 1326" OR 1332" OR 1338" OR 1344" OR 1350" OR 1356" OR 1362" OR 1368" OR 1374" OR 1380" OR 1386" OR 1392" OR 1398" OR 1404" OR 1410" OR 1416" OR 1422" OR 1428" OR 1434" OR 1440" OR 1446" OR 1452" OR 1458" OR 1464" OR 1470" OR 1476" OR 1482" OR 1488" OR 1494" OR 1500" OR 1506" OR 1512" OR 1518" OR 1524" OR 1530" OR 1536" OR 1542" OR 1548" OR 1554" OR 1560" OR 1566" OR 1572" OR 1578" OR 1584" OR 1590" OR 1596" OR 1602" OR 1608" OR 1614" OR 1620" OR 1626" OR 1632" OR 1638" OR 1644" OR 1650" OR 1656" OR 1662" OR 1668" OR 1674" OR 1680" OR 1686" OR 1692" OR 1698" OR 1704" OR 1710" OR 1716" OR 1722" OR 1728" OR 1734" OR 1740" OR 1746" OR 1752" OR 1758" OR 1764" OR 1770" OR 1776" OR 1782" OR 1788" OR 1794" OR 1800" OR 1806" OR 1812" OR 1818" OR 1824" OR 1830" OR 1836" OR 1842" OR 1848" OR 1854" OR 1860" OR 1866" OR 1872" OR

[illegible]

-1 ISOMETRIC
 DWG: 603455
 SHEET: 2
 SCALE: NONE
 DATE: 7/17/2011
 FILE: 603455.rvt

SECTION A-A
SCALE: 2:1

VIEW C
SCALE: 4:1

VIEW D
SCALE: 4:1

-1 ASSEMBLY
SCALE: 1:1

NOT RELEASED
INFORMATION ONLY
FOR APPROVAL OF FABRICATOR
FABRICATION OR CONSTRUCTION.

18X INSTALL ITEM 41 PER MANUFACTURER'S RECOMMENDATION. SEE DETAILS 32 & 33 FOR HOLE LOCATION PATTERN.
102
 Ø 108 THRU
 MAX. MACHINE ITEM 29 USING ITEMS 32 & 33 AS TEMPLATES.
 ENSURE THAT RIVET HEADS DO NOT CONTACT SURFACE OF ITEMS 32 & 33 (SIDE PLATES)

14X .002 & .008
 WATERSIDE RIVETS
 PLATES 19 THRU 23

14X .002 & .008
 WATERSIDE RIVETS
 PLATES 5 THRU 19

8X .002 & .008
 WATERSIDE RIVETS
 PLATES 19 THRU 23

32 SEE DETAIL
31 2X SEE DETAIL
30 2X SEE DETAIL
29 2X SEE DETAIL
28 4X
27 2X SEE DETAIL
26 REF
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2X 3.12
2X .355
2X .020
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SECTION A-A
SCALE: 2/1

VIEW D
SCALE: 4/1
4X

VIEW C
SCALE: 4/1

8X .093 ± .008
WATER GAP BETWEEN
PLATES 1 THRU 5 AND
PLATES 19 THRU 23

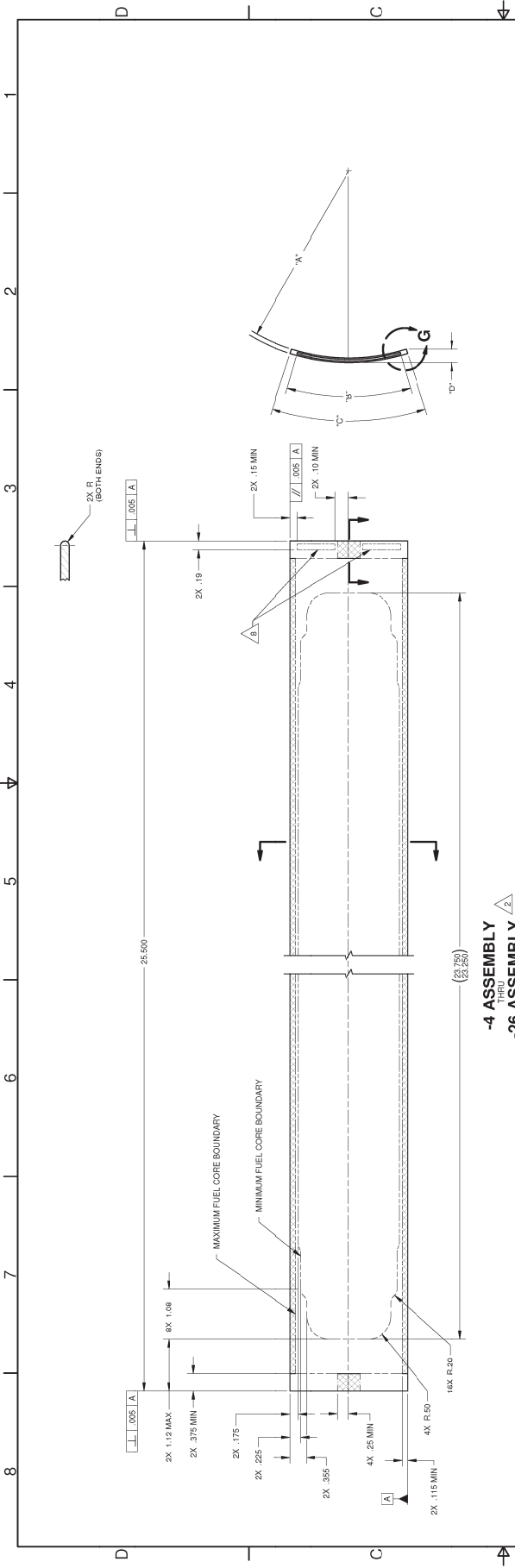
14X .092 ± .008
(WATER GAP BETWEEN
PLATES 5 THRU 19)

This technical drawing illustrates a mechanical assembly, likely a filter or separator, with the following components and details:

- Top View (A):** Shows the overall layout with dimensions 3,160 and 3,140. It features 24 slots (#1 to #24) with a spacing of 137 between slots 1 through 5. Slot #18 is specifically labeled. A note indicates that holes are permissible for drilling at assembly.
- Side View (B):** Shows the profile of the assembly with a total width of 3,200 and a thickness of 0.062.
- Detail 31 (SCALE: 2/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 32 (SCALE: 2/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 33 (SCALE: 2/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 34 (SCALE: 2/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 35 (SCALE: 2/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 36 (SCALE: 2/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 37 (SCALE: 4/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 38 (SCALE: 1/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 39 (SCALE: 2/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.
- Detail 40 (SCALE: 2/1):** A cross-sectional view of a slot showing a diameter of 0.192 thru 0.190, a width of 0.276, and a depth of 0.577.

[illegible]

Appendix G (Draft Element Drawings)



-4 ASSEMBLY
-26 ASSEMBLY

LEGEND
FUEL FREE AREA PER SPC-1401

FUEL PLATE DIMENSION TABLE Δ_{10}						
DASH NO.	"A"	"B"	"C"	"D"	"E"	"F"
-4	2.758	1.890	1.880	.214	.044	.009
-5	2.893	1.797	2.097	.225	.044	.012
-6	3.030	1.905	2.195	.235	.044	.016
-7	3.167	2.012	2.302	.245	.044	.020
-8	3.304	2.120	2.410	.255	.044	.020
-9	3.440	2.227	2.517	.265	.044	.020
-10	3.576	2.334	2.624	.275	.044	.020
-11	3.712	2.440	2.730	.285	.044	.020
-12	3.848	2.547	2.837	.297	.044	.020
-13	3.984	2.654	2.944	.307	.044	.020
-14	4.120	2.761	3.051	.317	.044	.020
-15	4.256	2.868	3.158	.328	.044	.020

FUEL PLATE DIMENSION TABLE (CONTINUED) Δ_{10}						
DASH NO.	"A"	"B"	"C"	"D"	"E"	"F"
-16	4.392	2.974	3.264	.338	.044	.020
-17	4.528	3.081	3.371	.348	.044	.020
-18	4.664	3.188	3.478	.359	.044	.020
-19	4.800	3.295	3.585	.369	.044	.020
-20	4.936	3.402	3.692	.379	.044	.020
-21	5.072	3.508	3.798	.389	.044	.020
-22	5.208	3.615	3.905	.400	.044	.020
-23	5.345	3.723	4.013	.410	.044	.020
-24	5.482	3.830	4.120	.421	.044	.020
-25	5.619	3.938	4.229	.431	.044	.020
-26	5.756	4.046	4.338	.446	.040	.017

