A Neutron Streaming Problem to Test Rattlesnake Methods for TREAT

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Presented by Javier Ortensi, Ph.D., P.E. R&D Scientist Nuclear Analysis and Design Idaho National Laboratory





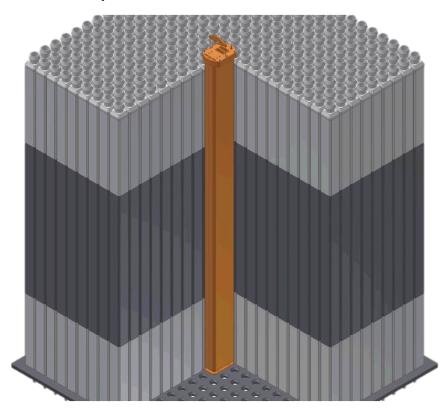
Outline

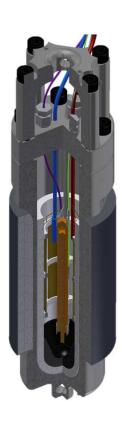
- Introduction / Motivation
- Codes
- Cross Section Preparation Process
- Methods
 - Superhomogenization
 - Calculation of tensor diffusion coefficients
- Test Problem Description
- Results
- Conclusion



Introduction / Motivation

- There are various regions in the Transient REActor Test (TREAT) facility core that contain voids, primarily in slotted elements and experiment vehicle.
- The slotted elements are positioned in front of the experiment region in order to provide a "field of view" of the experiment to the hodoscope.

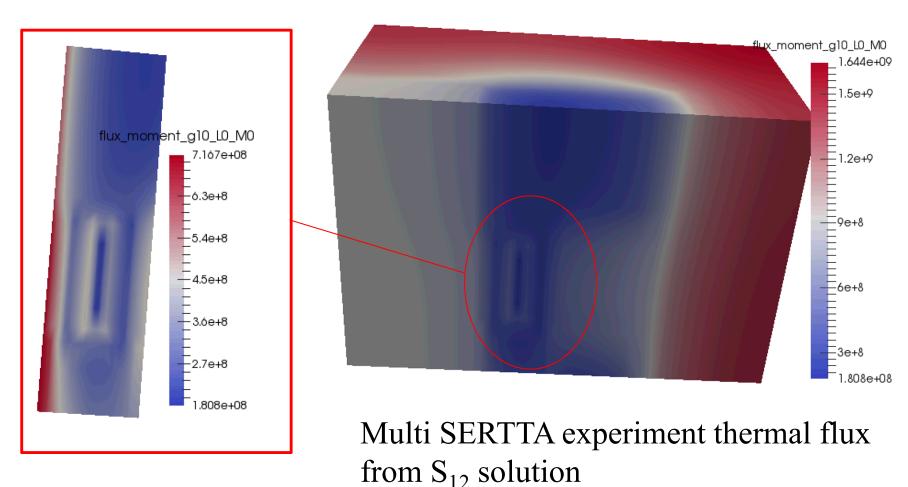






Introduction / Motivation

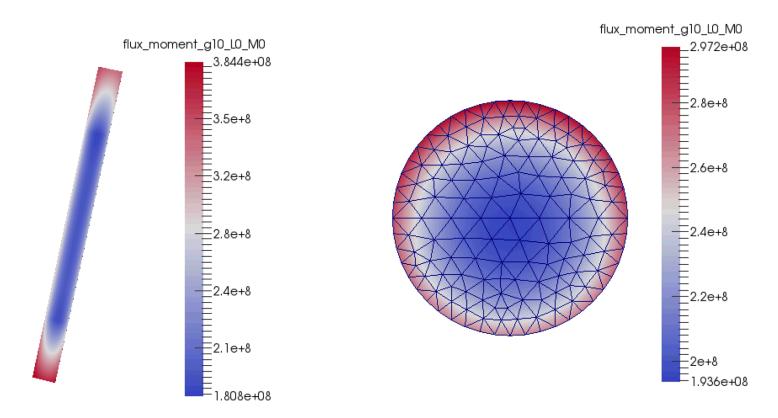
- Experiment location experiences significant flux gradients.
- Flux anisotropy might have important effects on experiments.





Introduction / Motivation

 Our goal is to provide modeling and simulation capability for experiment design and transient behavior.



Multi SERTTA experiment thermal flux from S_{12} solution



CODES

- Serpent Monte Carlo (v2.1.26)
 - Cross section preparation
 - Reference solution



- MOOSE based transport solver
- CFEM Diffusion, S_N , P_N
- Superhomogenization method
- Larsen-Trahan tensor diffusion coefficient computation
- Coupled to BISON and Relap-7 (MAMMOTH)



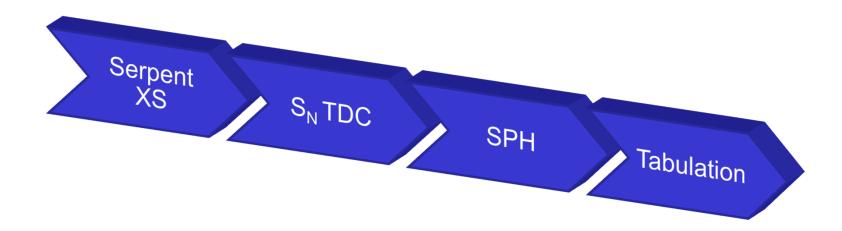






Cross Section Preparation

- Goal is to perform transient diffusion calculations when possible.
- Full core Monte Carlo to generate base cross sections.
 - Isotropic diffusion coefficient
- Full core S_N Larsen-Trahan source problem for tensor diffusion coefficients in void regions.
- SPH correction on coarse mesh as an equivalence procedure.





METHODS: Superhomogenization Procedure

- Cross section correction method for energy condensation and spatial homogenization.
- Reproduces the reaction rate and eigenvalue from a reference heterogeneous problem, but not the leakage.
- The SPH problem is a nonlinear problem usually solved with an iterative method, called SPH procedure:

$$\mu_{m,g} = \frac{\phi_{m,g}^{ref}}{\tilde{\phi}_{m,g}} \frac{\tilde{\phi}_{g}}{\tilde{\phi}_{g}^{ref}}$$

$$-\nabla \cdot \mu_{m}^{g} D_{m}^{g} \nabla \phi_{m}^{g} + \mu_{m}^{g} \Sigma_{r,m}^{g} \phi_{m}^{g} = \frac{\chi^{g}}{k_{eff}} \sum_{g'=1}^{G} \mu_{m}^{g'} \nu \Sigma_{f,m}^{g'} \phi_{m}^{g'} + \sum_{g'\neq 1}^{G} \mu_{m}^{g'} \Sigma_{s0,m}^{g' \to g} \phi_{m}^{g'}$$



METHODS: Nonlinear solve to the SPH problem

- SPH was implemented for diffusion, S_N, and P_N solvers.
- Two solver implementations:
 - Traditional SPH iteration
 - PJFNK-SPH solver (new approach)
- MOOSE's PJFNK solver
 - reduces SPH calculation time significantly,
 - can solve problems that were intractable such as reflectors and void boundary conditions,
 - might require updates to the initial guess to approach the radius of convergence of the Newton Method ("fee SPH iterations")

2145 coefficients	SPH iteration	PJFNK-SPH
# Iterations		11 (5 free)
Solve time (sec.)		113
Min. flux convergence	(not converged)	4.17E-9



Region Tensor Diffusion Coefficients (TDC)

- Need to define diffusion coefficient in near-void regions for TREAT.
- Selected Trahan's region-wise definition.
 - Define a tensor diffusion coefficient

$$\left[\underline{\underline{D}}\right]_{i,j} = \frac{1}{4\pi} \int_{4\pi} d\Omega_i \Omega_j f$$

Obtain f from auxiliary transport problem without scattering or fission

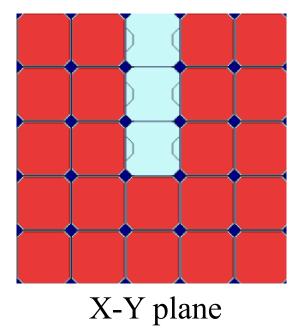
$$\vec{\Omega} \cdot \nabla f_g + \sum_{t,g} f_g \left(r, \vec{\Omega} \right) = 1$$

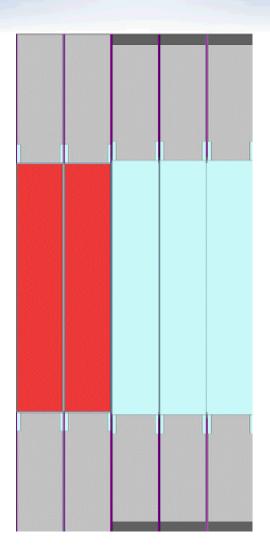
- Use one of the Rattlesnake's S_N transport solvers to solve the auxiliary problem:
 - 2nd order SAAF-S_N with void treatment
 - 1st order S_N



Simplified 5x5 TREAT model

- This 5x5 problem contains 3 slotted assemblies.
- 3 axial constant cross section regions in
 - fuel
 - each reflector
- 15 unique assemblies with cross sections.





Y-Z plane



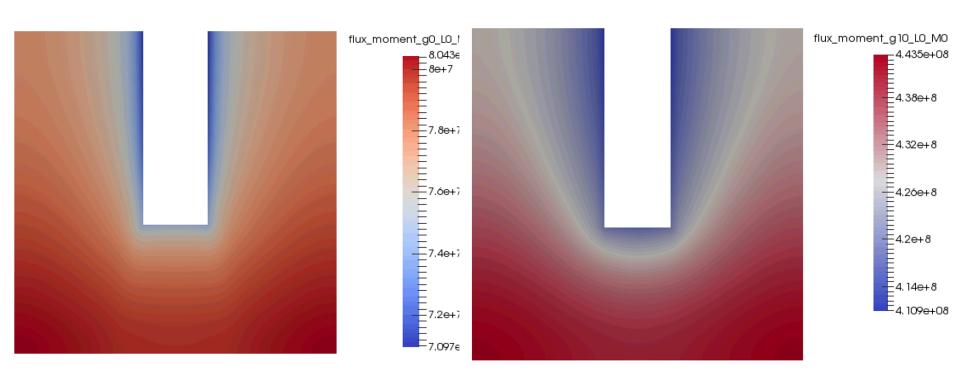
Serpent Results

- Serpent Run Setting
 - 1M particles/cycle
 - 50 inactive, 1000 active
- Cross section preparation in 11 and 4 coarse energy groups.
- Fission rate tally every 10 cm (axially) in fuel regions for each assembly.

k _{eff} (±pcm)	1.35124 (±1.7)
Source Rate	5.574x10 ¹² n/s
Absorption Rate	5.329x10 ¹² n/s
n Disappearance Rate	2.238x10 ¹² n/s
Fission Rate	3.091x10 ¹² n/s
Leakage Rate	2.450 x10 ¹¹ n/s

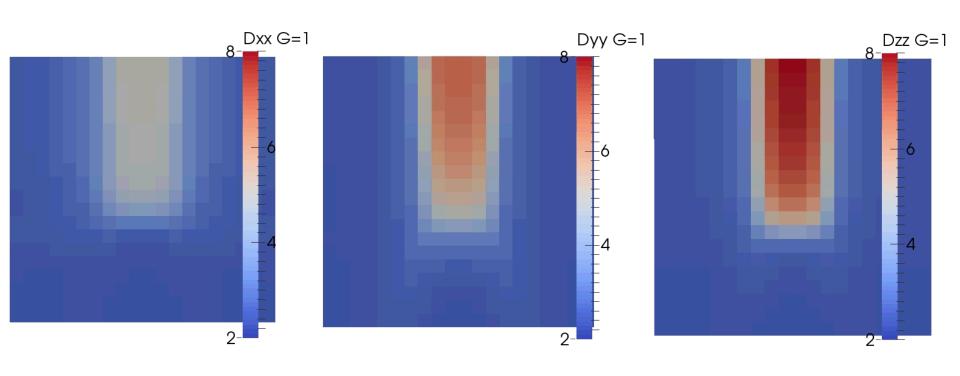


S₁₂ Solutions



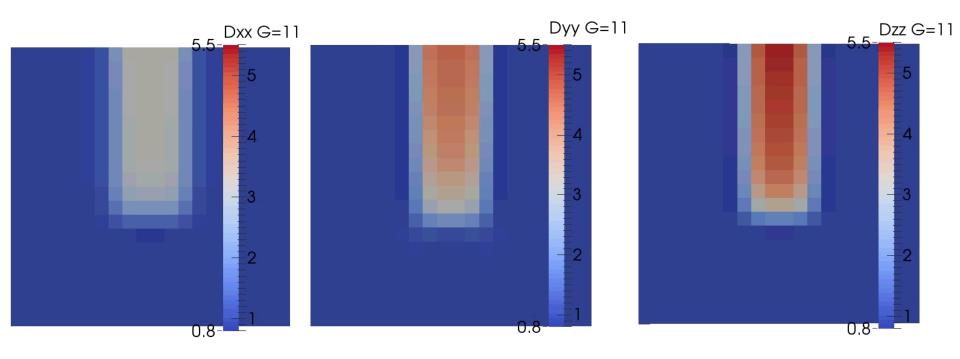


TDC in TREAT Slot (mid core) - Fast Group





TDC in TREAT Slot (mid core) - Thermal Group





Results 11 groups

Solver	k _{eff} (pcm)	Source Rate (% rel. diff.)	Absorption Rate (% rel. diff.)	Leakage Rate (% rel. diff.)
Diff.	1.33710 (-1046)	1.054	1.364	-5.671
S ₁₂	1.36511 (1026)	-1.020	-0.372	-15.08
Diff. SPH	1.35726 (445)	-0.447	0.025	-10.71
Diff. TDC	1.37227 (1556)	-1.536	-0.628	-21.26
Diff. TDC-SPH	1.35859 (544)	-0.545	0.039	-13.23

Solver	RMS [%]	Max. [%]	Min. [%]
Diff.	4.997	9.566	-6.362
S ₁₂	0.984	2.029	-1.270
Diff. SPH	1.744	3.309	-3.073
Diff. TDC	0.373	0.921	-0.932
Diff. TDC-SPH	0.661	1.434	-1.127



Results 4 groups

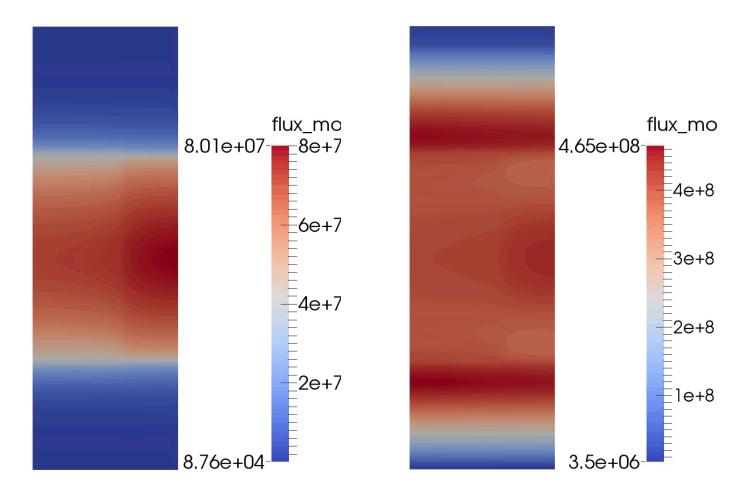
Solver	k _{eff} (pcm)	Source Rate (% rel. diff.)	Absorption Rate (% rel. diff.)	Leakage Rate (% rel. diff.)
Diff.	1.33462 (-1233)	1.242	1.451	-3.311
S ₁₂	1.36669 (1141)	-1.134	-0.592	-12.90
Diff. SPH	1.35767 (473)	-0.477	-0.008	-10.66
Diff. TDC	1.37157 (1502)	-1.403	-0.025	-31.33
Diff. TDC-SPH	1.35929 (593)	-0.595	-0.010	-13.31

Solver	RMS	Max.	Min.
Diff.	5.132	8.955	-6.382
S ₁₂	0.953	2.342	-1.125
Diff. SPH	1.637	3.153	-2.98
Diff. TDC	0.930	1.855	-1.716
Diff. TDC-SPH	0.848	2.030	-1.600



Flux Solutions

Fast and thermal flux solutions show small gradients in void.





Conclusions

- The TDC and SPH methods in Rattlesnake provide the means to improve the diffusion solutions in a calculation outside the traditional applicability of diffusion theory.
- The RMS differences with respect to the Monte Carlo reference are improved by a factor of 7.6 and the maximum difference is within 1.5% in 11 energy groups.
- The results in 4 energy groups confirm that coarser energy structures provide sufficient accuracy for most routine calculations when using appropriate corrections.
- SPH correction needs to be verified for transients with fully heterogeneous transport calculation to assess leakage errors.



QUESTIONS/COMMENTS to

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