

# Refining Absorber Shroud Geometry to Maximize Power Output and Reduce Power Peaking in ATF Test Train

June 2024

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#### The Accident Tolerant Fuels (ATF) Program

- Initiated by DOE-NE following the 2011 Fukushima accident.
- Focused on developing nuclear fuels and claddings with enhanced accident tolerance.
- ATF definition: Fuels that can tolerate loss of active cooling in the reactor core for a considerably longer time period in comparison with the standard UO<sub>2</sub> – Zircaloy system.
- Potentially important attributes:
  - Reduced hydrogen generation (resulting from cladding oxidation),
  - Enhanced fission product retention under severe accident conditions,
  - Reduced cladding reaction with high-temperature steam, and
  - Improved fuel-cladding interaction for enhanced performance under extreme conditions.

# **Advanced Test Reactor (ATR)**

- One-of-a-kind pressurized water test reactor.
- ATR thermal power

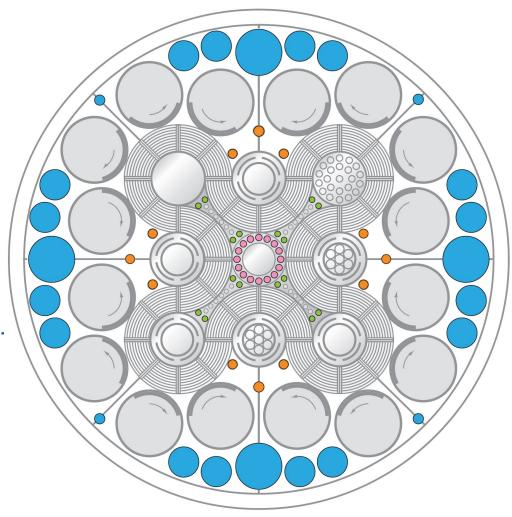
Maximum: 250 MW<sub>Th</sub>

Typical operation: 110 MW<sub>Th</sub>

- Regular cycles last approx. 60 days.
- Corner lobes can be independently operated at different power levels, making it possible to conduct multiple simultaneous experiments under different testing conditions.
- 77 test positions available.
- Peak flux in Center Flux Trap at 110 MW<sub>Th</sub>

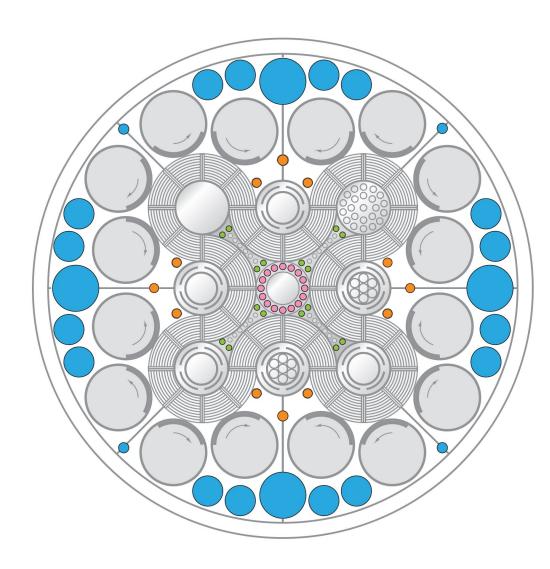
- Thermal:  $4.4 \times 10^{14}$  n/cm<sup>2</sup>-s

- Fast: 2.2×10<sup>14</sup> n/cm<sup>2</sup>-s



# **The ATF-2D Experiment**

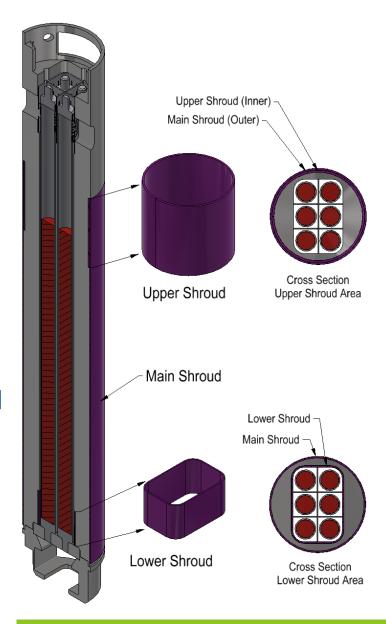
- ATF-2D is the latest experiment in the ATF series.
- Joint effort of the INL with industry partners (mainly fuel vendors).
- Irradiation in the ATR Center Flux Trap tentatively starting in June 2025.
- Closed loop with typical PWR conditions.
- Experiment design not yet finalized.



#### **Experiment Design**

4 holders (Zr or SS-316), vertically stacked in test train.

- Each holder houses 2×3 array of rodlets.
- Modeled rodlet dimensions
  - Fuel stack length: 17 cm
  - Pellet diameter: 8.2 mm and 9.5 mm.
- UO<sub>2</sub> fuel with varying enrichments, some Cr-doped. All modeled as UO<sub>2</sub> with 4.95% <sup>235</sup>U.
- Cladding materials: Zircaloy-4, SiC, FeCrAl, and M5 with and without coating. All modeled as Zirc-4 here.
- Upper, Main and Lower shrouds in each holder.



#### **Power Output and Profile Criteria**

#### Safety criterion:

1. Total fission power output of the entire test train ≤ 200 kW

Programmatic criteria (assuming max. 2 cm segments):

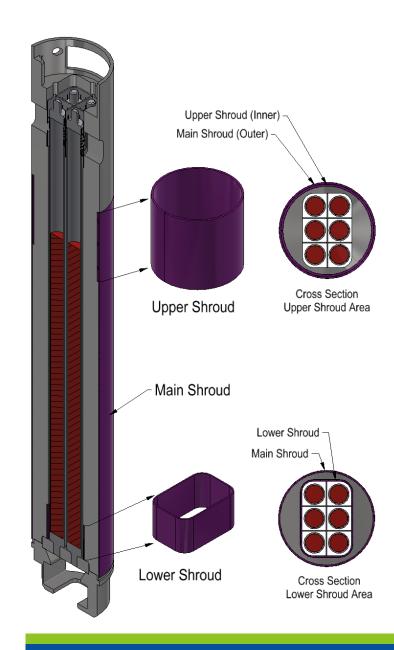
- 1. Max. LHGR in the top or bottom segment shall not exceed the LHGR of adjacent segments by more than 10%
- 2. The segment local-to-maximum fission heat rate shall be ≥ 70%
- 3. Max. LHGR for PWR pins shall be in the span 440-485 W/cm

#### **Calculations**

- MCNP 6.2 used for neutron transport and reaction rates.
- MCNP tally results (per particle) normalized to absolute neutron fluxes and reaction rates based on
  - average neutrons per fission,
  - average energy per fission,
  - total core power, and
  - power split between the five ATR lobes.
- Calculations performed using INL's High Performance Computing systems.

# **Shroud Design #1 and #2**

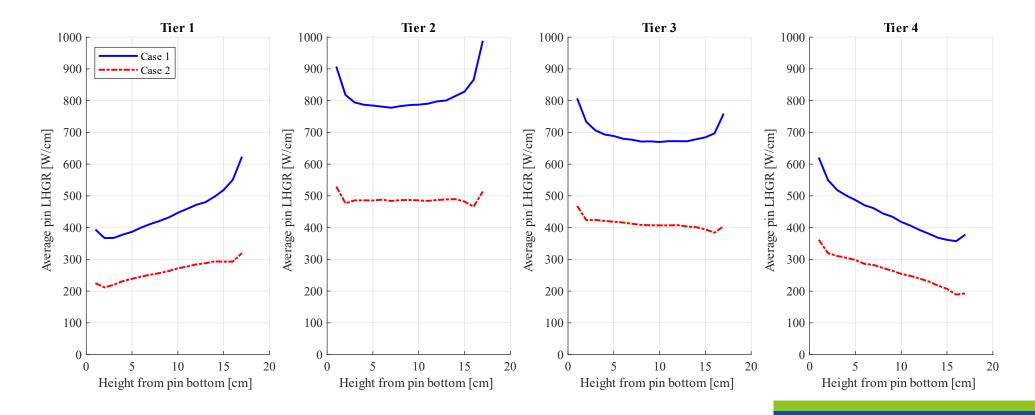
- Case 1: Zirconium only
  - Baseline
  - Thickness for Upper, Main, and Lower shrouds: 36 mil, 28 mil, and 26 mil.
  - All holders modeled as Zr.
- Case 2: Hafnium only
  - Same thicknesses



# **Shroud Design #1 and #2**

• Case 1: Zirconium only Total power: 279 kW (< 200 kW)

• Case 2: Hafnium only Avg. LHGR reduction ~60%

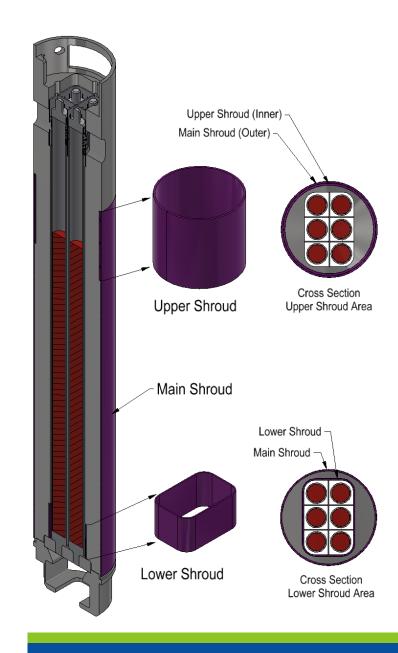


#### **Shroud Design #3**

- Case 3: Hafnium/zirconium combined
  - Most shrouds made from Hf.
  - Shrouds at top/bottom of test train made from Zr

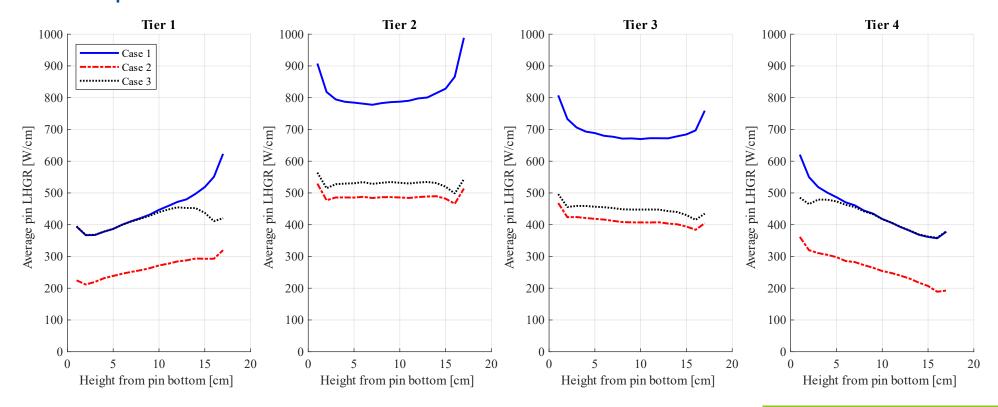
	Lower	Main	
Tier	shroud	shroud	shroud
1 (bottom)	Zr	Zr	Hf
2	Hf	Hf	Hf
3	Hf	Hf	Hf
4 (top)	Hf	Zr	Zr

 Main shroud thickness for Tiers 2 and 3 reduced to 20 mil.



# **Shroud Design #3**

- Case 3: Hafnium/zirconium combined
  - Tiers 1 and 4 somewhat flattened.
  - Total power: 211 kW



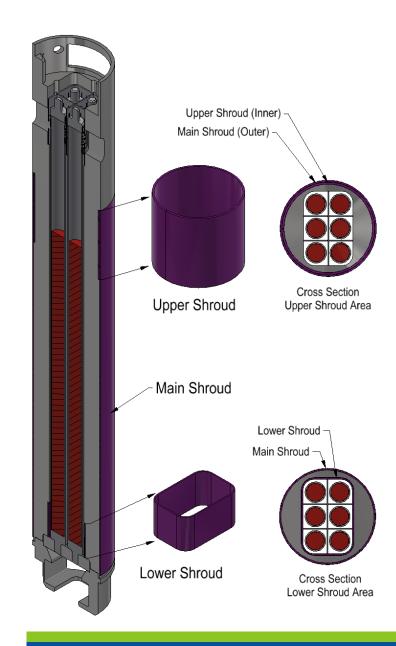
# **Shroud Design #4 and #5**

#### Case 4: Split Main shrouds

 Like Case #3 but Tiers 1 and 4 Main shrouds split in half. Hafnium closest to axial core center plane, zirconium away from center plane.

#### Case 5: Hafnium disks

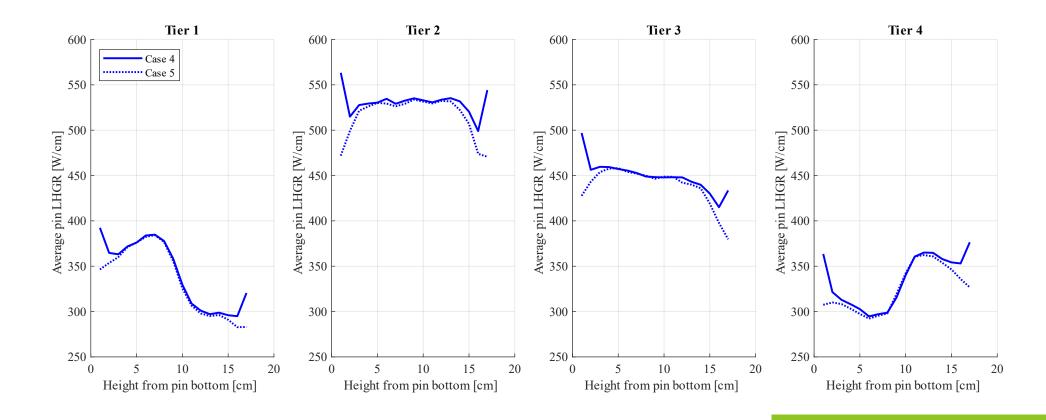
 Like Case #4 but has 1/16-inch hafnium disks at both the top and bottom of every fuel stack.



# **Shroud Design #4 and #5**

- Case 4: Split Main shrouds
- Case 5: Hafnium disks

T1 and T4 have too much Hf – not flat! End-effects suppressed



# **Shroud Design #6 and #7**

- Case 6: Final configuration, no hafnium disks
  - Thinner shrouds in T1 & T4
  - T2 holder modeled as stainless steel
  - Used in preliminary safety evaluations

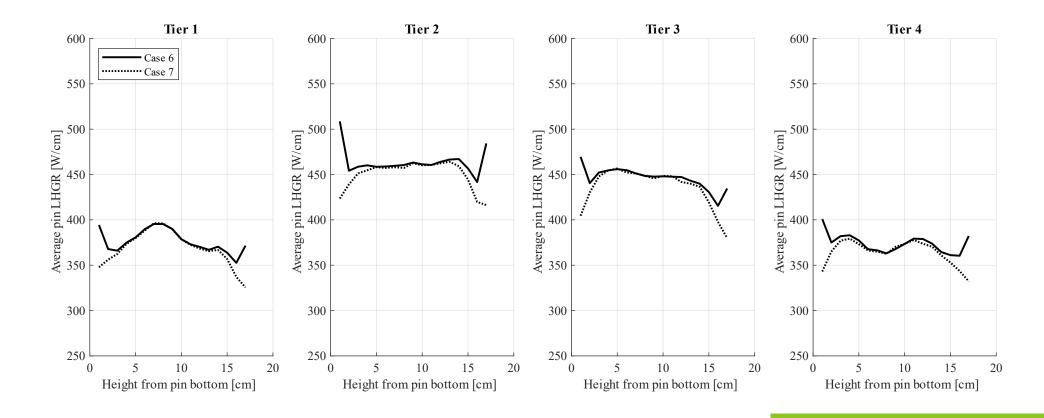
	Lower shroud		Main shroud, bottom		Main shroud, top		Upper shroud	
Tier	Material	Thickness	Material	Thickness	Material	Thickness	Material	Thickness
1 (bottom)	Zr	26 mil	Zr	10 mil	Hf	10 mil	Hf	36 mil
2	Hf	26 mil	Hf	20 mil	Hf	20 mil	Hf	36 mil
3	Hf	36 mil	Hf	20 mil	Hf	20 mil	Hf	26 mil
4 (top)	Hf	36 mil	Hf	10 mil	Zr	10 mil	Zr	26 mil

- Case 7: Final configuration with hafnium disks
  - Used in preliminary programmatic evaluations

# **Shroud Design #6 and #7**

- Case 6: Final configuration, no hafnium disks
- Case 7: Final configuration with hafnium disks

Total power: 193 kW All requirements met!



#### **Future Work to Prepare for Irradiation**

#### Establish final design

- Based on customer requests and INL's analyses
- May require multiple iterations
- Model a conservative safety case and a best-estimate case

#### Calculations to ensure requirements met:

- Total fission power
- Programmatic LHGR requirements
- Reactivity worths (experiment vs. backup, and multiple accident scenarios)
- 3-cycle projection calculations, incl. decay heat and radioactivity source terms
- Driver fuel axial perturbation
- Thermal and structural analyses downstream from neutronics calculations
- etc.



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