

#### Systems Level Fuel Cycle Modeling in TMAP8 - A Demonstration

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# Systems Level Fuel Cycle Modeling in TMAP8 - A Demonstration

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**Pacific Basin** Nuclear Conference

**Systems Level Fuel Cycle** Modeling in TMAP8 – A **Demonstration** 

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# Fuel Cycle Model

$$\frac{dI_1}{dt} = \Lambda \dot{N} + (1 - \eta_2) \frac{I_2}{\tau_2} - \frac{I_1}{\tau_1} - \frac{I_1 \varepsilon_1}{\tau_1} - I_1 \lambda$$
$$\frac{dI_2}{dt} = (1 - f_{1-5}) \frac{I_1}{\tau_1} - \frac{I_2}{\tau_2} - \frac{I_2 \varepsilon_2}{\tau_2} - I_2$$

System Name	System number d	$\frac{I_{13}}{dt} = f_{p-3} \frac{\dot{N}^{-}}{\eta_{e} f_{b}} + f_{5-3} (1 - f_{5-6}) (1 - f_{5-10}) \frac{I_{5}}{\tau_{5}} + f_{6-3} (1 - \eta_{6}) \frac{I_{6}}{\tau_{6}} - \frac{I_{3}}{\tau_{2}} - \frac{I_{3} \varepsilon_{3}}{\tau_{2}} - I_{3}$
Breeding zone	1	$ au_f  au_f  au_b$
Tritium Extraction System	$\frac{dI_4}{dt} = f_{p-4} - \frac{dI_4}{dt}$	$\frac{\dot{N}^{-}}{\eta_{\epsilon}f_{b}} + (1 - f_{5-3})(1 - f_{5-6})(1 - f_{5-10})\frac{I_{5}}{\tau_{5}} + (1 - f_{6-3})(1 - \eta_{6})\frac{I_{6}}{\tau_{6}} - \frac{I_{4}}{\tau_{4}} - \frac{I_{4}\epsilon_{4}}{\tau_{4}} - I_{4}$
First Wall	3	17.0
Divertor	4	$\frac{dI_5}{dt} = f_{1-5} \frac{I_1}{\tau_1} + \frac{I_3}{\tau_2} + \frac{I_4}{\tau_4} - \frac{I_5}{\tau_5} - \frac{I_5 \varepsilon_5}{\tau_5} - I_5$
Heat Exchanger	5	
Coolant Purification System	6	$\frac{dI_6}{dt} = f_{5-6}(1 - f_{5-10})\frac{I_5}{\tau_5} - \frac{I_6}{\tau_6} - \frac{I_6\varepsilon_6}{\tau_6} - I_6$
Vacuum Pump	7	$\frac{dI_7}{dt} = \left(1 - \eta_f f_b - f_{p-3} - f_{p-4}\right) \frac{\dot{N}^-}{\eta_f f_b} - \frac{I_7}{\tau_7} - \frac{I_7 \varepsilon_7}{\tau_7} - I_7$
Fuel Clean-up	8	$\frac{1}{dt} = (1 - \eta_f I_b - I_{p-3} - I_{p-4}) \frac{1}{\eta_f f_b} - \frac{1}{\tau_7} - \frac{1}{\tau_7} - \frac{1}{\tau_7}$
Isotope Separation System	9	$\frac{dI_8}{dt} = \frac{I_7}{T_7} - \frac{I_8}{T_8} - \frac{I_8 \varepsilon_8}{T_8} - I_8$
Exhaust and Water Detritiation System	10	$\frac{dI_9}{dt} = (1 - f_{8-11}) \frac{I_8}{T_9} + \frac{I_{10}}{T_{10}} + \eta_2 \frac{I_2}{T_2} + \eta_6 \frac{I_6}{T_6} - \frac{I_9 \varepsilon_9}{T_9} - \frac{I_9}{T_9} - I_9$
Storage and Management	11	$\frac{dI_{10}}{dt} = f_{5-10} \frac{I_5}{\tau_5} + f_{9-10} \frac{I_9}{\tau_9} - \frac{I_{10}}{\tau_{10}} - \frac{I_{10} \varepsilon_{10}}{\tau_{10}} - I_{10}$
		$\frac{dI_{11}}{dt} = f_{8-11} \frac{I_8}{\tau_8} + (1 - f_{9-10}) \frac{I_9}{\tau_9} - \frac{\dot{N}^-}{\eta_f f_b} - I_{11}$

## Sample Code – Equation 1

```
\frac{dI_{1}}{dt} = \left(MN^{-1} + (1 - \eta \eta) \frac{I_{2}^{-1} - I_{1}^{-1}}{\tau \tau_{2}} - I_{1}^{-1} \lambda \right) = 0
[ScalarKernels]
[11]
  # Breeding Zone
  type = ParsedODEKernel
  expression = '-(tritium_burn_rate * TBR + (1 - TES_efficiency)*T_02_TES/residence2 - T_01_BZ/residence1 -
T 01 BZ*epsilon1/residence1 - T 01 BZ*tdecay)'
  variable = 'T 01 BZ'
  coupled variables = 'T 02 TES'
  postprocessors = 'TBR tritium burn rate TES efficiency residence1 residence2 tdecay epsilon1'
 [|1t]
  type = ODETimeDerivative
  variable = T 01 BZ
```



### Comparison with Abdou 2021

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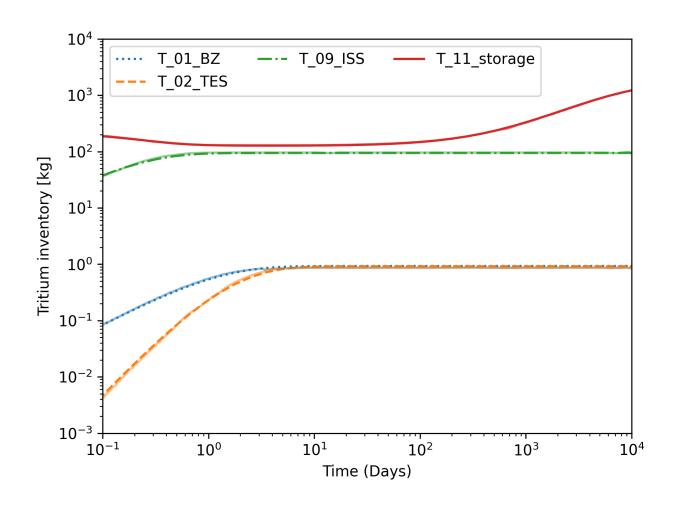
residence7 (т7) 1 s

residence8 (т8) 1 s

residence9 (т9) 14400 s

TBR ( $\Lambda$ ) 1.9247

Initial value for T\_11\_storage 225.4215 kg







#### **Possibilities**

- Able to substitute sub-applications at varying levels of model sophistication
  - Heat exchanger
  - Tritium extraction system
  - Blanket
- Feedback between systems possible through this model
- TMAP8 can be incorporated with other MOOSE-based FEM tools to accommodate more advanced physics
- Example problem publicly available example online https://mooseframework.inl.gov/TMAP8/examples/fuel\_cycle/index.html

