

YRA poster session - July 25 2019

July 2019

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Prepared for the U.S. Department of Energy Under DOE Idaho Operations Office Contract DE-AC07-05ID14517



Pronghorn: A MOOSE Based TH Tool for Advanced Reactor Concepts

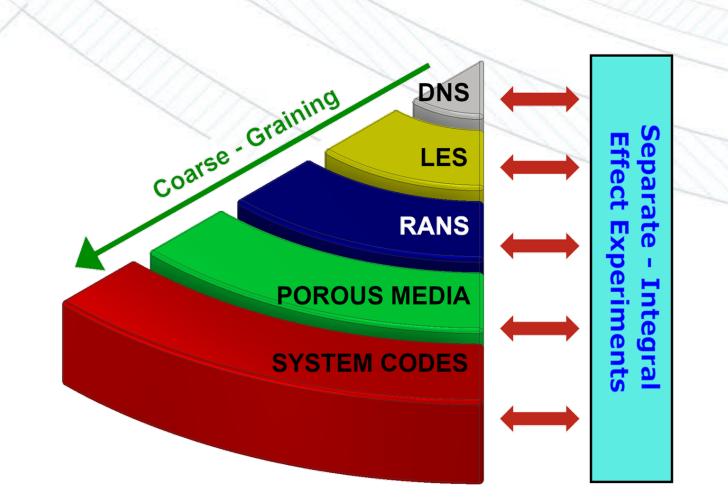
Final Edge of Poster

P. Balestra, S. Schunert, R. Carlsen, S. R. Sen, G. Strydom, R. C. Martineau Reactor Systems Design and Analysis, Nuclear Engineering Methods Development

Pronghorn history & activities



- NEK5000
- STARCCM+
- Pronghorn
- RELAP5-3D
- RELAP-7



Pronghorn under the hood

Governing Equations, Approach #1: Two-Phases with Compressible Flow Phase and a Stationary Solid Phase

$$\frac{\partial \alpha \rho}{\partial t} + \nabla \cdot (\alpha \rho \vec{u}) = 0$$

Balance of Momentum

$$\frac{\partial \alpha \rho \vec{u}}{\partial t} + \nabla \cdot \left[\alpha (\rho \vec{u} \otimes \vec{u} + p \mathbf{I}) \right] = p_i \nabla \alpha + \nabla \cdot (\alpha \mu_{eff} \nabla \vec{u}) + \alpha (1 - \alpha) K_m (\vec{u}_s - \vec{u})$$

Conservation of Total Energ

$$\frac{\partial \alpha \rho E}{\partial t} + \nabla \cdot (\alpha \rho \vec{u} H) = p_i \vec{u}_i \cdot \nabla \alpha - \nabla \cdot (\alpha \vec{q}) + \alpha \rho Q + \alpha (1 - \alpha) K_e(T_s - T) + \vec{u} \cdot (\alpha \rho \vec{g})$$

Solid Phase Energy Balance

$$(1 - \alpha)\rho_s c_{v,s} \frac{\partial T_s}{\partial t} = \nabla \cdot \left[(1 - \alpha)\vec{q}_s \right] + (1 - \alpha)\rho_s Q_s - \alpha (1 - \alpha)K_e(T_s - T)$$

Governing Equations, Approach #2: Thermally Expansive, Nearly Incompressible (liquid) Flow Phase and a Stationary Solid Phase

Conservation of Mass

$$\frac{\partial \alpha \rho}{\partial t} + \nabla \cdot (\alpha \rho \vec{u}) = 0$$

Balance of Momentum

$$\alpha \rho \frac{D\vec{u}}{Dt} = -\alpha \nabla p + \nabla \cdot (\mu_{eff} \alpha \nabla \vec{u}) - \alpha (1 - \alpha) K_m \vec{u} + \alpha \rho \vec{g}$$

Liquid Phase Energy Balance

$$\alpha \rho c_p(\frac{\partial T}{\partial t} + \nabla T \cdot \vec{u}) = (p - p_i)\vec{u} \cdot \nabla \alpha + \nabla \cdot (\alpha k_{eff} \nabla T) + \alpha \rho Q + \alpha (1 - \alpha) K_e(T_s - T)$$

Solid Phase Energy Balance

$$(1-\alpha)\rho_s c_{v,s} \frac{\partial T_s}{\partial t} = \nabla \cdot \left[(1-\alpha)\vec{q}_s \right] + (1-\alpha)\rho_s Q_s - \alpha (1-\alpha)K_e(T_s - T)$$

Legacy Governing Equations, Approach #3: Porous flow approximation. Reproduces legacy THERMIX approach.

Conservation of Mass

$$\epsilon \frac{\partial \rho}{\partial t} + \nabla \cdot \left[\frac{\epsilon^2}{W} \left(-\nabla P + \rho_f \vec{g} \right) \right] = 0$$

Balance Momentum

$$\epsilon \nabla P - \epsilon \rho_f \vec{g} + W \rho_f \vec{V} = 0$$

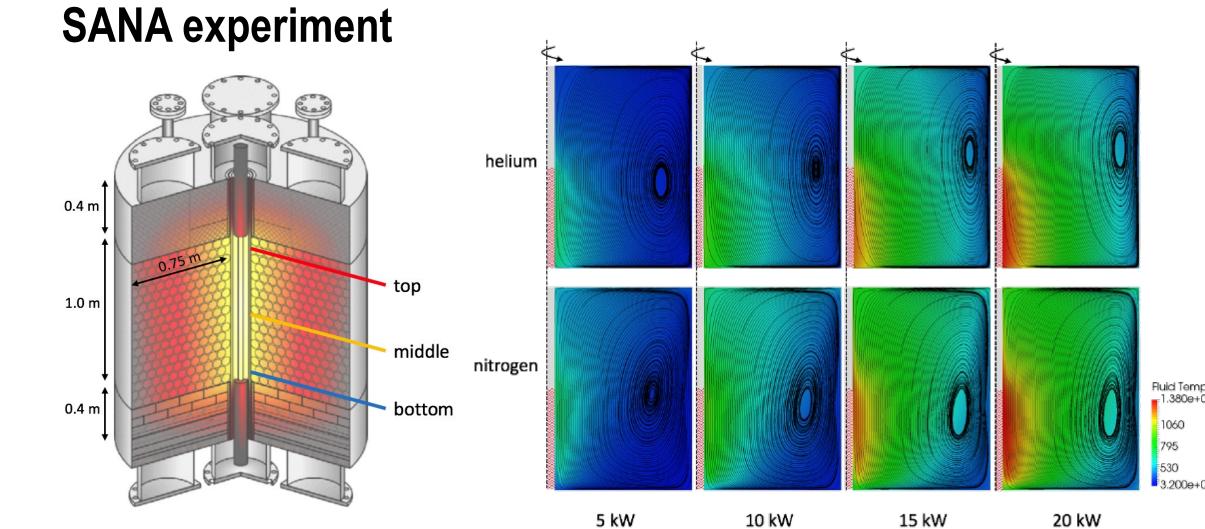
Liquid Phase Energy Balance

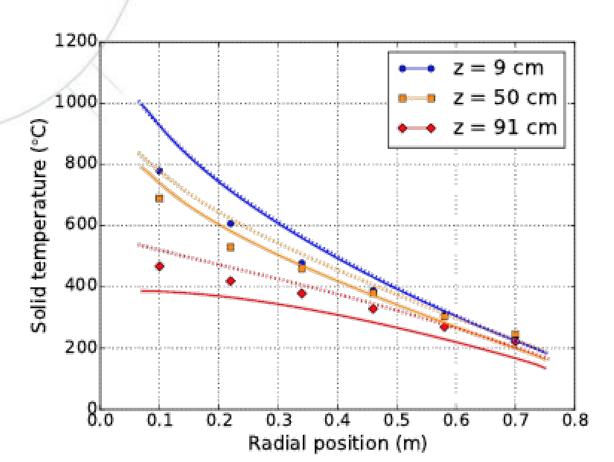
$$\epsilon \rho_f C_{p,f} \frac{\partial T_f}{\partial t} + \epsilon \rho_f C_{p,f} \vec{V} \cdot \nabla T_f - \nabla \cdot (\kappa_f \nabla T_f) + \alpha \left(T_f - T_s \right) + \dot{q}_f = 0$$

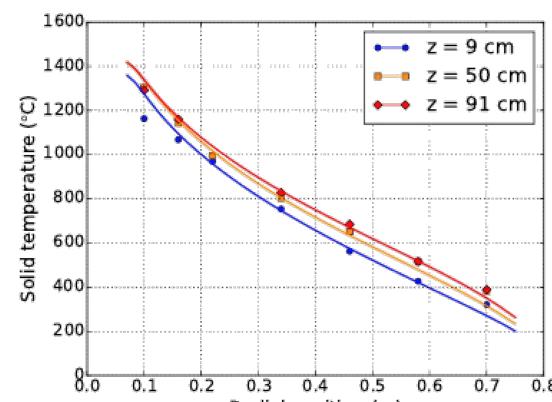
Solid Phase Energy Balance

$$(1 - \epsilon) \rho_s C_{p,s} \frac{\partial T_s}{\partial t} - \nabla \cdot (\kappa_s \nabla T_s) + \alpha (T_s - T_f) + \dot{q}_s = 0$$

Code Validation & Verification







PBMR-400 benchmark

