

Use of Flooding Probabilistic Risk Assessment

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Dr. Curtis Smith, Director Nuclear Safety and Regulatory Research Division Idaho National Laboratory



Outline of my talk today

- SDP related to flooding in US
- Door integrity tests at Idaho State University
- Smoothed Particle Hydrodynamics for external flooding
- NRC-INL Flood Barrier project

SDP related to flooding in US





SDP related to flooding in US NRC

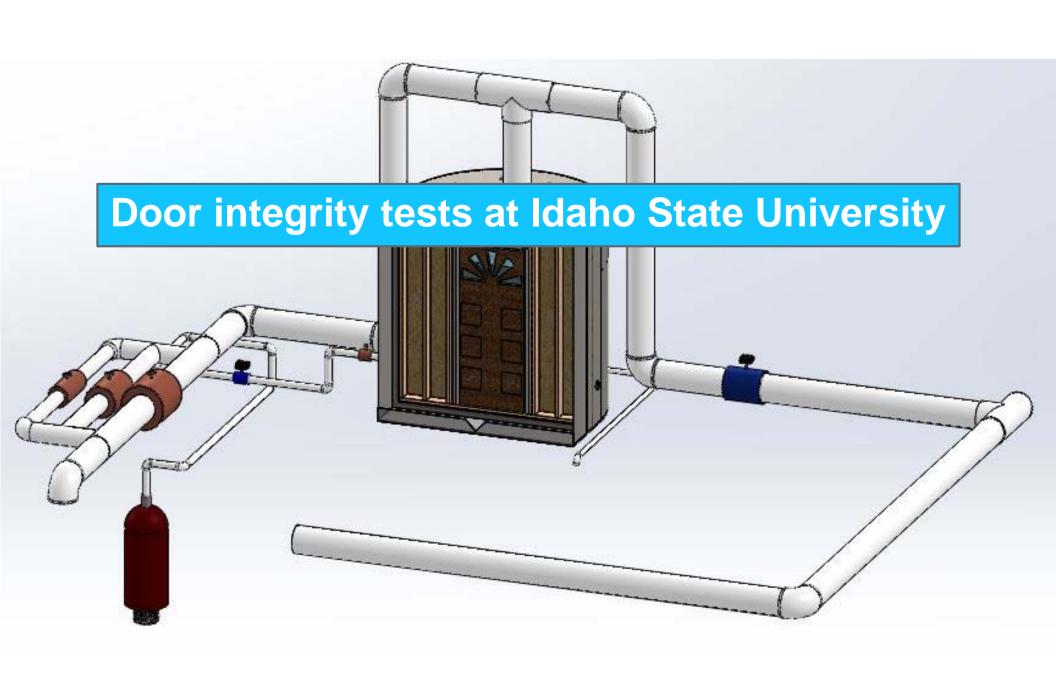
- Collected information from public NRC documents related to SDP for flooding
- NRC ROP includes determining safety significance of inspection findings through SDP
 - Specific hazards are evaluated → external flooding a challenge
 - Site-specific hazard that depends on geographical, meteorological, hydrological, and hydraulic information needed to characterize potential events relevant to the site
 - Limited data available to characterize PRA tools
- NRC technical guidance does exist
 - IMC 0609 Appendix A, Risk Assessment Standardization Project (RASP) handbooks
- Several events have been evaluated
- https://www.nrc.gov/docs/ML1515/ML15152A315.pdf
- Items that correlate back to application of PRA
 - Modeling of flooding sequences
 - Quantification of SSCs and flood protection that are credited in specific scenarios
 - Evaluation of operator manual actions outside the control room involving flood mitigation

NPP Site	Significance Determination	Reference
St. Lucie [†]	White	ML14294A466
Ginna	White	ML14107A080
Point Beach	White	ML13221A187
Monticello [†]	Yellow	ML13240A435
Dresden	White	ML13213A073
Three Mile	White	ML13042A277
Island		
Watts Bar*	White	ML13155A572
Watts Bar*	Yellow	ML13155A572
Sequoyah*	White	ML13155A560
Sequoyah*	White	ML13155A560



Examples of flood SDP

- Oconee Standby Shutdown Facility (ML14058A051)
 - Open penetration into SSF for two years
 - Opening below maximum flood height identified by licensee (5 feet)
 - Susceptible to up-stream dam failure
 - Independent analysis indicated 12 feet flood possible
 - Analysis indicated possible WHITE finding
- Fort Calhoun Flooding Strategy (ML15152A315)
 - January 2010, NRC identified inadequacies of buildings protection against floods
 - Site flood protection strategy may not be fully effective during scenarios
 - NRC determined that a "Yellow" finding was appropriate
 - Specific challenges associated with flooding after Fukushima were highlighted
 - Credit for hardening a facility prior to flood waters affecting the site
 - Assessing credit for limited available actions during a flood scenario based on timing availability (e.g., procuring additional equipment during or after the flood)
 - Consideration of information provided by licensee via qualitative IMC 0609 Appendix M approach in SDP was also evaluated and the finding was reaffirmed as "Yellow"





The Portal Evaluation Tank (PET)

- PET is a semi-cylindrical 7,500 liter capacity steel tank
- An opening environment of 2.4 x 2.4 m for installation
- PET is connected through 3 in. PVC pipe to a 5 Hp. submersible pump
 - Located inside a 30,000 liter water reservoir
- Instrumentation
 - Electronic flow meter
 - Ultrasonic sensor
 - Pressure transducer
 - Pressure Gauge



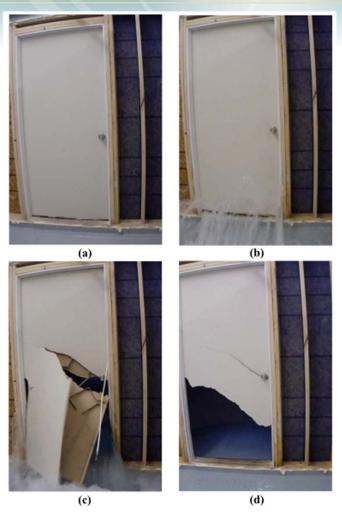




Flooding Fragility Experiments

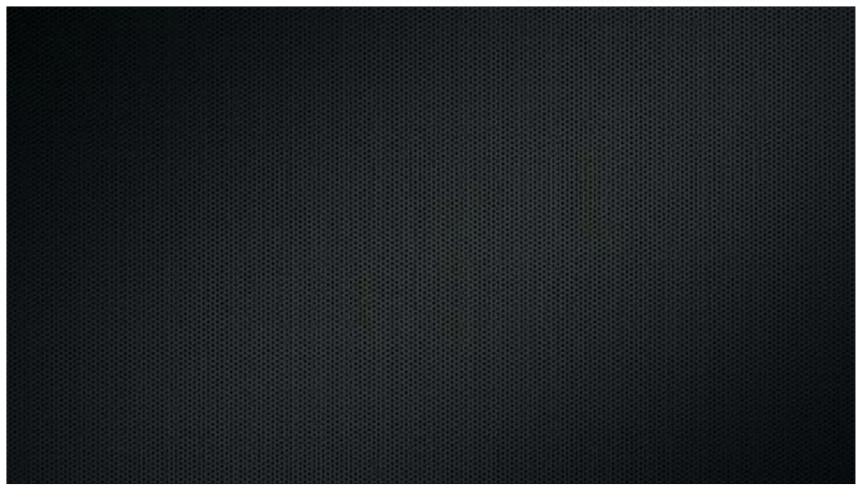
- A door frame was constructed using building code and decreased stud spacing
- Initial tests used hollow core doors and involved water rise until catastrophic failure occurred or leak rate equalization







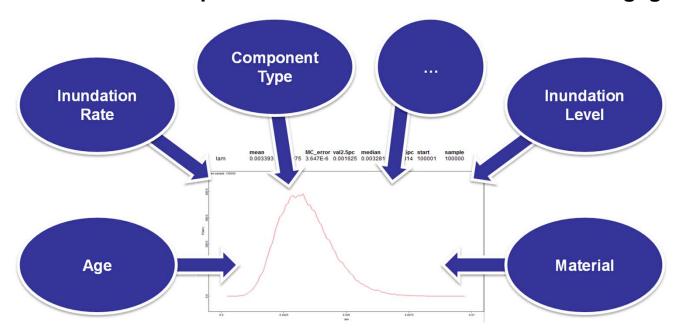
PET Video Demonstration





Flooding Bayesian Analysis

- One of the complications for the flooding fragility modeling is the variety of observable phenomena related to the flood itself
 - Some thought should be given to which factors might be the most important
- An advantage of the Bayesian quantification approach is parameters in the regression model associated with unimportant factors should be found to be negligible





Work Using PET Data

- Eight complete sets of data
 - Depth at failure or greatest depth achieved
 - Average flow rate
 - Average temperature
- Door failure when damage is permanent & leakage increases in a short time (1)
- Success when an equilibrium state is reached between the flow and leakage rate (0)

Also moved on to testing metal doors



Depth (in)	Flow Rate (gal/min)	Temp (°F.)	Failure
23.23	291.5	65.98	0
20.75	292.5	67.04	0
42.3	292.5	66.02	1
21.05	297	67.67	0
24.22	294.5	66.6	0
35.41	292.5	66.87	1
40.76	291	68.33	1
38.85	294	68.14	1

INL-EXT-18-45247 - Nuclear Power Plant Component Flooding Fragility Research





Example of Flooding Model

 The fragility model for this case looks at seven possibilities:

1.
$$logit(p) = int + aD + bF + cT$$

2.
$$logit(p) = int + aD$$

3.
$$logit(p) = int + bF$$

4.
$$logit(p) = int + cT$$

5.
$$logit(p) = int + aD + bF$$

6.
$$logit(p) = int + aD + cT$$

7.
$$logit(p) = int + bF + cT$$

```
#Flow Rate (F), Depth (D), and Temperature (T) Model
model {
for(i in 1:tests) {
         failure[i] \sim dbern(p[i])
         # Regression model
         logit(p[i]) \leftarrow int + a*flow[i] + b*depth[i] + c*temp[i]
         # failure.rep[i] ~ dbin(p[i], num.tested)
                                                       # Replicate values for model validation
         # diff.obs[i] <- pow(failure[i] - num.tested*p[i], 2)/(num.tested*p[i]*(1-p[i]))
         # diff.rep[i] <- pow(failure.rep[i] - num.tested*p[i], 2)/(num.tested*p[i]*(1-p[i]))
#chisq.obs <- sum(diff.obs[])
#chisq.rep <- sum(diff.rep[])
#p.value <- step(chisq.rep - chisq.obs)
# Prior distributions
int \sim dnorm(0, 0.0001)
a \sim dnorm(0, 0.001)
data
list(tests=8,
         flow = c(291.5,292.5,292.5,297,294.5,292.5,291,294),
         depth = c(23.23,20.75,42.3,21.05,24.22,35.41,40.76,38.85),
         temp = c(65.98,67.04,66.02,67.67,66.6,66.87,68.33,68.14),
         failure = c(0,0,1,0,0,1,1,1)
inits
list(int=0, a=0)
```



Results for the Cloglog equations

<u> </u>							
Parameter	Equ. 1	Equ. 2	Equ. 3	Equ. 4	Equ. 5	Equ. 6	Equ. 7
Intercept	10.84	-107.5	4.832	5.301	5.847	1.222	1.88
a (depth coeff)	47.88	3.705	-	-	45.31	35.61	-
b (flow rate coeff)	-10.84	-	-0.01814	-	-4.648	-	0.02401
c (temp coeff)	25.86	-	-	-0.08646	-	-15.89	-0.141
DIC	0.01568	0.2372	12.68	13.25	0.0174	0.0203	13.51

- Deviance Information Criterion (DIC) can be used to examine the relative fit of a model
 - Measure of relative goodness of fit
 - Smallest DIC indicates the best fitting model

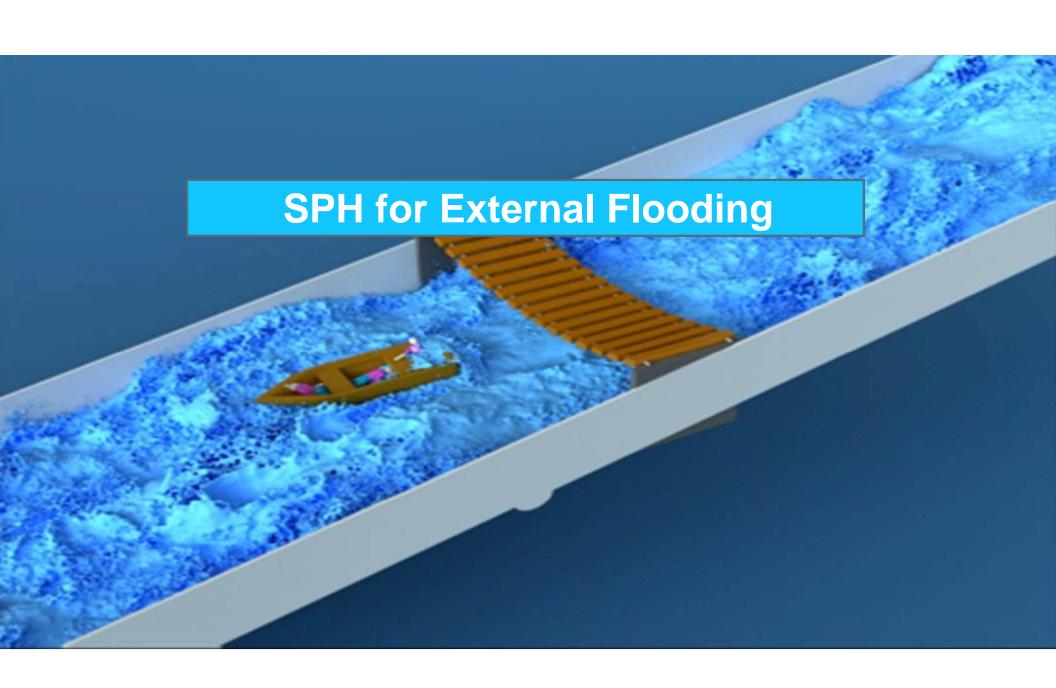


Pipe break tests

ISU also performed tests to better understand water spray for breaks in pipes



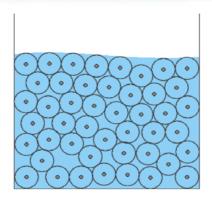


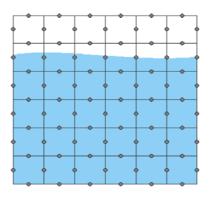




Smoothed Particle Hydrodynamics

- A way to simulate flooding scenarios is needed
- Smoothed Particle Hydrodynamics (SPH)
 - Particle based method
 - Originally developed for astrophysics applications in 1977
 - Later extended for fluid dynamic applications
- SPH allows for flooding scenarios to be simulated
 - Does not confine fluid to meshes
 - Allows for a natural flow to be modeled
- A reliable SPH code is needed
 - Compare to experimental results







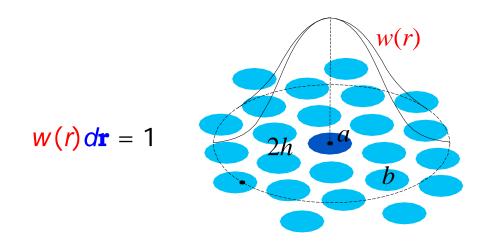
Introduction: SPH

- Particles
 - A particle is a minute fragment or quantity of matter'
- Usual meanings in science
 - Smallest constituents of matter (Standard Model)
 - Nanoparticles, colloidal particles
 - Dust, powder, ashes
 - Sediment grains, water droplets
- The duality of 'particles' in SPH
 - They are material points
 - They have volume, mass, pressure, density, etc.



Introduction: SPH Interpolation

- Particle a has position \mathbf{r}_a , mass m_a , volume V_a , etc.
- Particle Interactions are computed using the 'kernel' w(r)
- The support of w has size 2h, h =smoothing length, w is normalized

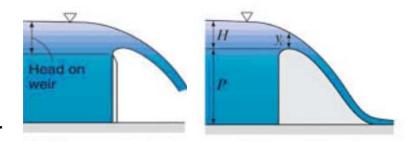


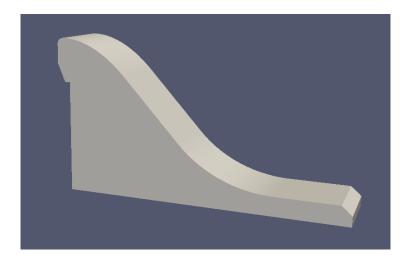
Lucy, L.B. (1977), Astron. J. **82**:1013–1024 Gingold, R.A., Monaghan, J.J. (1977), Mon. Not. R. Astron. Soc. **181**:375–389



Ogee Spillway Comparison

- Comparison Model
 - Ogee spillway with horizontal apron
 - Details of experiment provided in Flow over Ogee Spillway: Physical and Numerical Model Case Study by Bruce M. Savage and Michael C. Johnson
 - Experiment details (scaled model):
 - Measurements taken 2 m upstream
 - Flow Rate
 - Total Head
 - Ten different runs conducted
 - Prototype scale was used for the SPH comparison which required scaling the model scale up 30 times

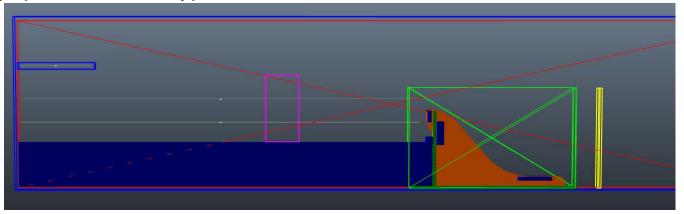






Neutrino Model

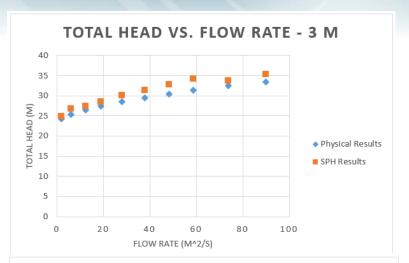
- Developmental SPH code Neutrino was used to conduct the comparison
- Model construction process:
 - Determine how to fill particles behind the spillway
 - Reduce leakage
 - Determine particle emitter location to set total head
 - Determine particle emitter location to set flow rate instead
 - Conduct parametric studies on model width and particle size
 - Reduce leakage again
 - Change particle emitter types

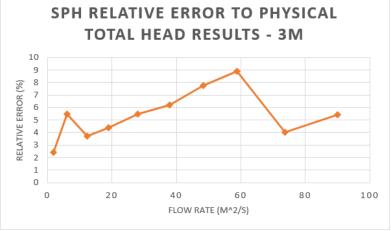




Comparison Results

Run	Flow	Physical	SPH Total	Relative
	Rate	Total Head	Head	Error
		Result	Result	
1	1.9 m ² /s ± 0.25%	24.3 m	24.9 m	2.4 %
2	6.0 m ² /s ± 0.25%	25.3 m	26.7 m	5.5 %
3	12.3 m ² /s ± 0.25%	26.5 m	27.5 m	3.7 %
4	19.0 m ² /s ± 0.25%	27.4 m	28.6 m	4.4 %
5	27.9 m ² /s ± 0.25%	28.5 m	30.0 m	5.5 %
6	$37.8 \text{ m}^2/\text{s} \pm 0.25\%$	29.5 m	31.3 m	6.2 %
7	48.2 m ² /s ± 0.25%	30.4 m	32.8 m	7.7 %
8	58.9 m ² /s ± 0.25%	31.4 m	34.1 m	8.9 %
9	$73.8 \text{ m}^2/\text{s} \pm 0.5\%$	32.4 m	33.7 m	4.0 %
10	89.9 m ² /s ± 0.5%	33.5 m	35.3 m	5.4 %



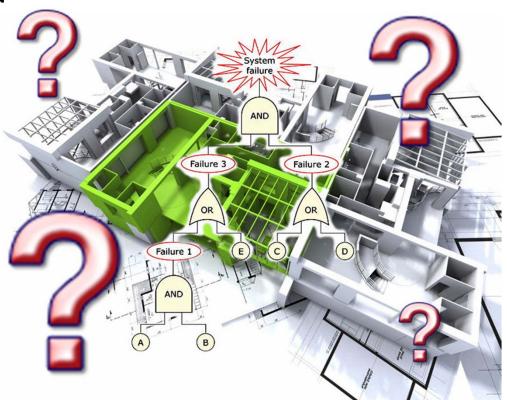




How to Join Physics Model & System Model

 Good - Run repeated simulations and add the failure information into the existing static models

- Best Dynamic PRA model that can interact with the simulation
 - No corrections needed for time dependent calculations
 - Determine average or mean time of particular outcomes
 - Analyze time order of failures to determine early protection methods





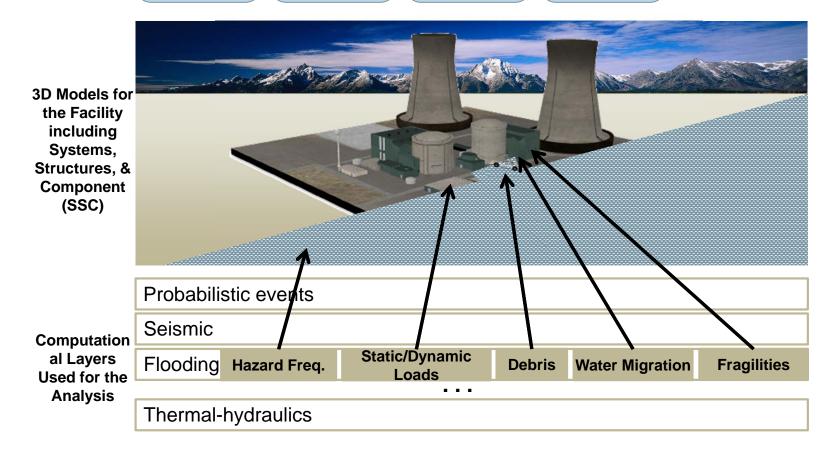
Risk Analysis Steps for Scenario Generation

Enabling Conditions

Flood

Plant SSC Response to Initiator SSC Failures & Successes

Scenario Simulation



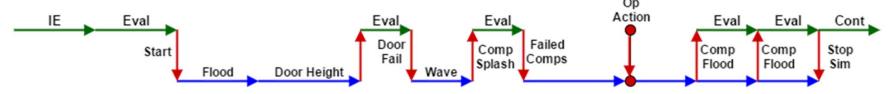


Timing is Everything



- Physics simulation are dynamic and time dependent
- Control logic is not always available in simulations
- Need to modify the behavior of the simulation at during execution.

System Model



Simulation



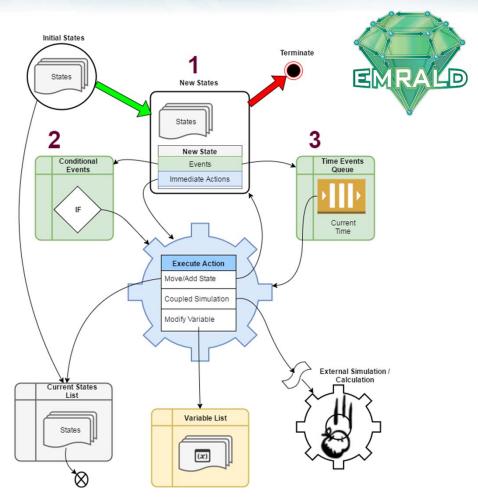
Modeling Options

- Time Steps
- Next event in time (EMRALD)

Dynamic probabilistic risk assessment (PRA) model based on a three-phased discrete event simulation

To begin, add initial start states to Current and New States List

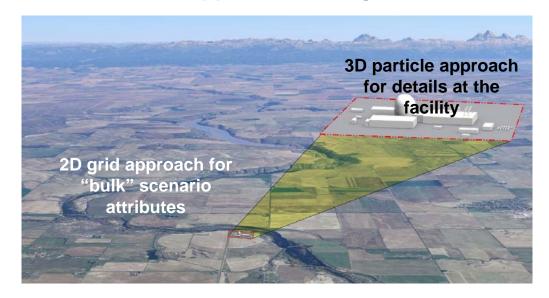
- 1. While there are States in the New Sates list, For each State :
 - Add the Events to the Time Queue or Conditional List.
 - Execute any Immediate Actions
- 2. If any Conditional Events criteria is met.
 - Execute that events action/s.
 - (Go to Step 1)
- 3. Jump to the next chronological event.
 - Process that event's actions.
 - (Go to Step 1)

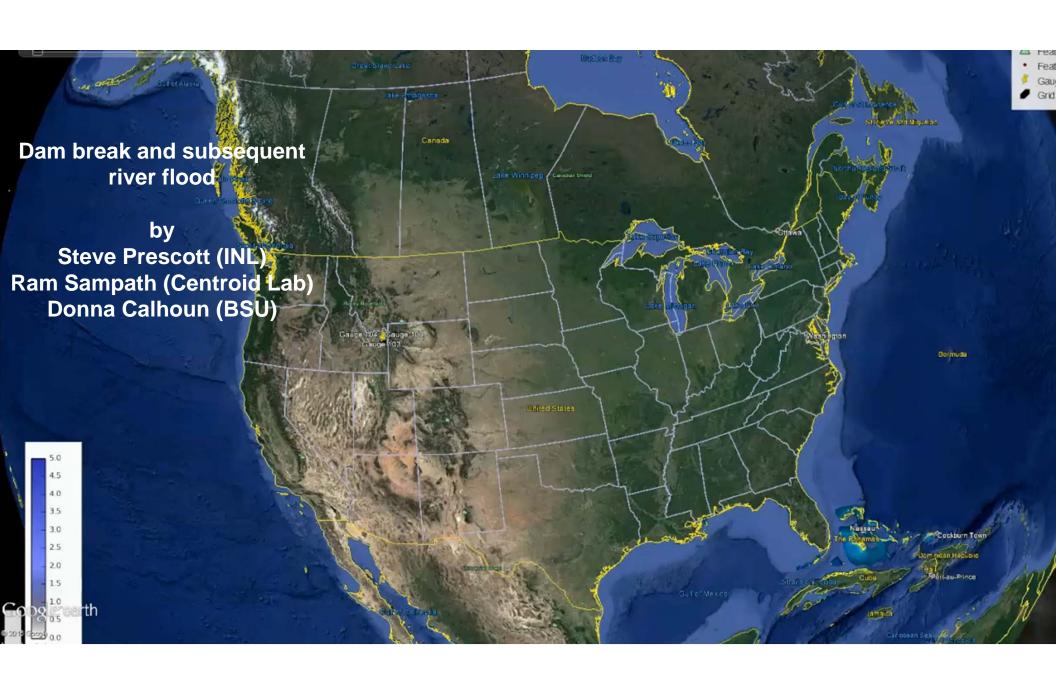




River flood modeling

- INL/EXT-15-37091, Flooding Capability for River-based Scenarios
- Evaluated two different types of potential river-based flooding tools
 - 1D/2D grid based (GeoClaw, EPA's SWMM code, and Army Corps HEC)
 - 3D particle based
 - Both the 2D and 3D methods have positives and negatives
- Combination of both seems to be best approach moving forward





NRC-INL Flood Barrier Project





Project overview

- Project will identify and assess options and develop strategies for testing nuclear power plant (NPP) flood barriers
 - Including permanent components such as flood penetration seals, water tight doors as well as temporary flood protection features
 - Flood barriers external to the plant (e.g., earthen berms, aqua berms, sandbags) are not a focus of the review
 - Will look for information that may be useful when developing strategies for testing (e.g. prospects for harvesting, in-situ non-destructive testing or enhanced inspection, in-situ destructive testing)
- Project is part of NRC's Probabilistic Flood Hazard Assessment (PFHA) Research Program
- Looking at decommissioning plants for likely source for harvesting
 - Visited Oyster Creek during December 2019
- Recently completed draft report → Goal to publish NUREG
- Will be supporting flood barrier testing workshop during the week of the NRC Regulatory Information Conference
 - Thursday and Friday (March 12-13)

