



Bison Methods and Contact Algorithms

November 2020

Changing the World's Energy Future

Jason D Hales



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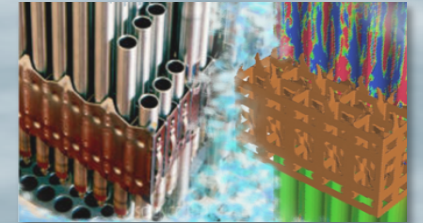
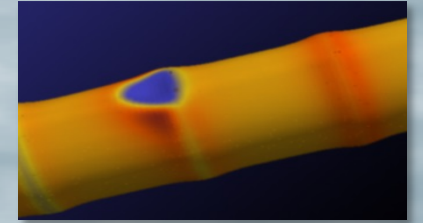
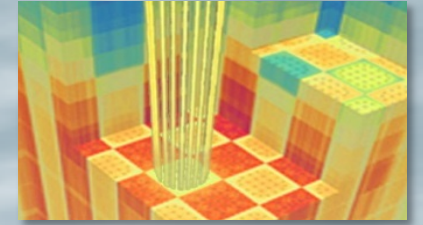
**Idaho National Laboratory
Idaho Falls, Idaho 83415**

<http://www.inl.gov>

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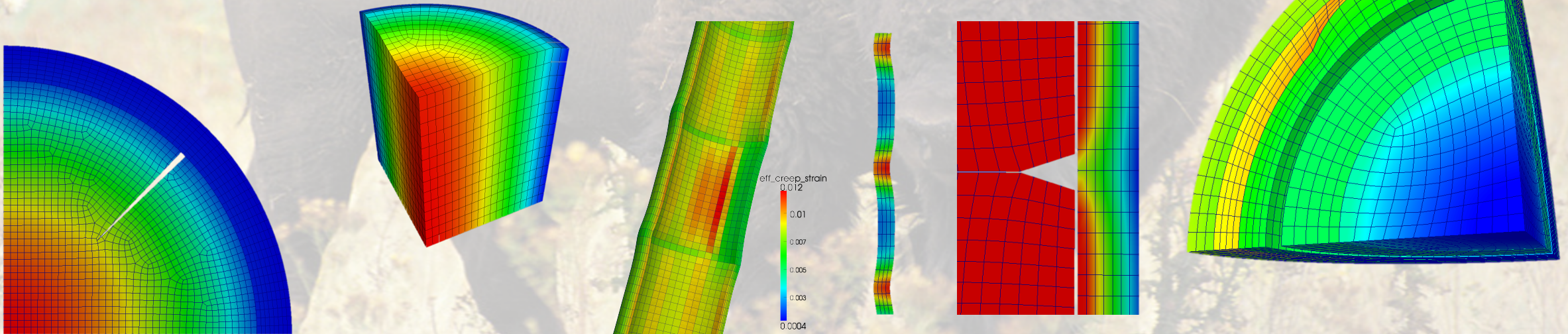
The Consortium for Advanced
Simulation of LWRs
A DOE Energy Innovation Hub



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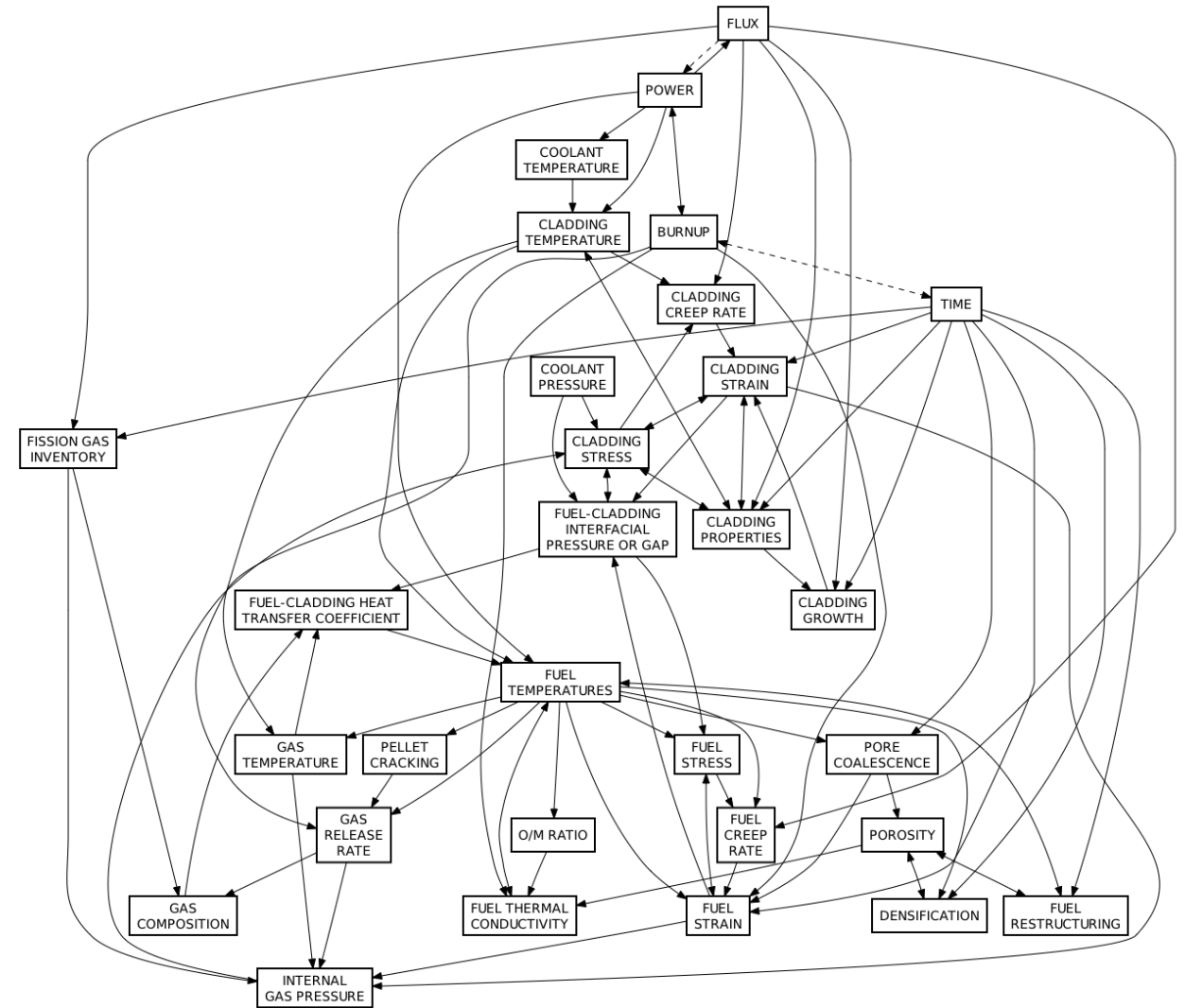
Bison: What is it?

- A finite element, thermo-mechanics code with material models and other customizations to analyze nuclear fuel
 - Accepts user-defined meshes/geometries
 - 1D, 2D, or 3D
 - Runs on one processor or many
 - Analyzes a variety of fuel types
 - Couples to other analysis codes



Fuel Behavior Modeling - Coupled Multiphysics

- Multiphysics
 - Fully-coupled nonlinear thermomechanics
 - Mass transport
 - Chemistry
 - Neutronics
 - Thermal-hydraulics
- Multi-space scale
 - Important physics operate at level of microstructure
 - Need real predictions at engineering scale
- Multi-time scale
 - Long, steady operation
 - Short power ramps
 - Rapid transients



Reproduced from Beyer et al., BNWL-1898, PNNL (1975)

Burnup

- Burnup is a measure of how much fissionable material has been used
- Bison uses FIMA (fissions per initial metal atom) as the burnup unit

$$\beta = \frac{\dot{F} t M_w}{\rho N_{av}}$$

$$\dot{F} = f_a f \dot{\bar{F}}$$

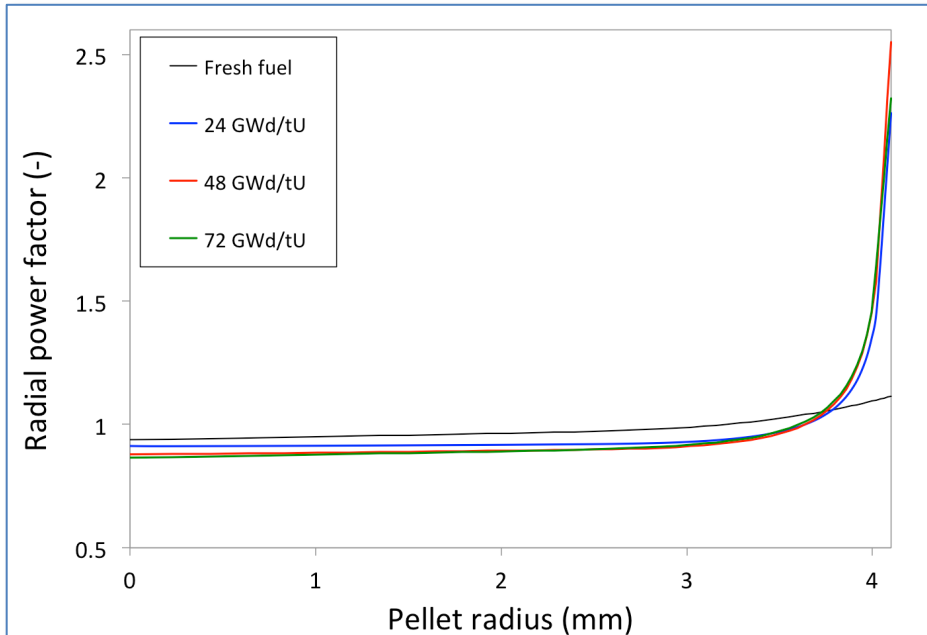
- The fission rate, \dot{F} , is a function of power, axial power factor, and radial power factor
- Axial power factor, f_a , is supplied as input
- Radial power factor, f , is estimated by Bison

Radial Power Factor

$$q'''(r) \propto \sum_k \sigma_{f,k} N_k \phi$$

$$q'''_{av} = \frac{1}{r_{max}} \int_{r_{min}}^{r_{max}} q'''(r) dr$$

$$f(r) = \frac{q'''(r)}{q'''_{av}}$$



$f(r)$

$$\frac{d N_{235}}{d t} = -\sigma_{a,235} N_{235} \phi$$

$$\frac{d N_{236}}{d t} = -\sigma_{a,236} N_{236} \phi + \sigma_{c,235} N_{235} \phi$$

$$\frac{d N_{238}}{d t} = -\sigma_{a,238} N_{238} \phi$$

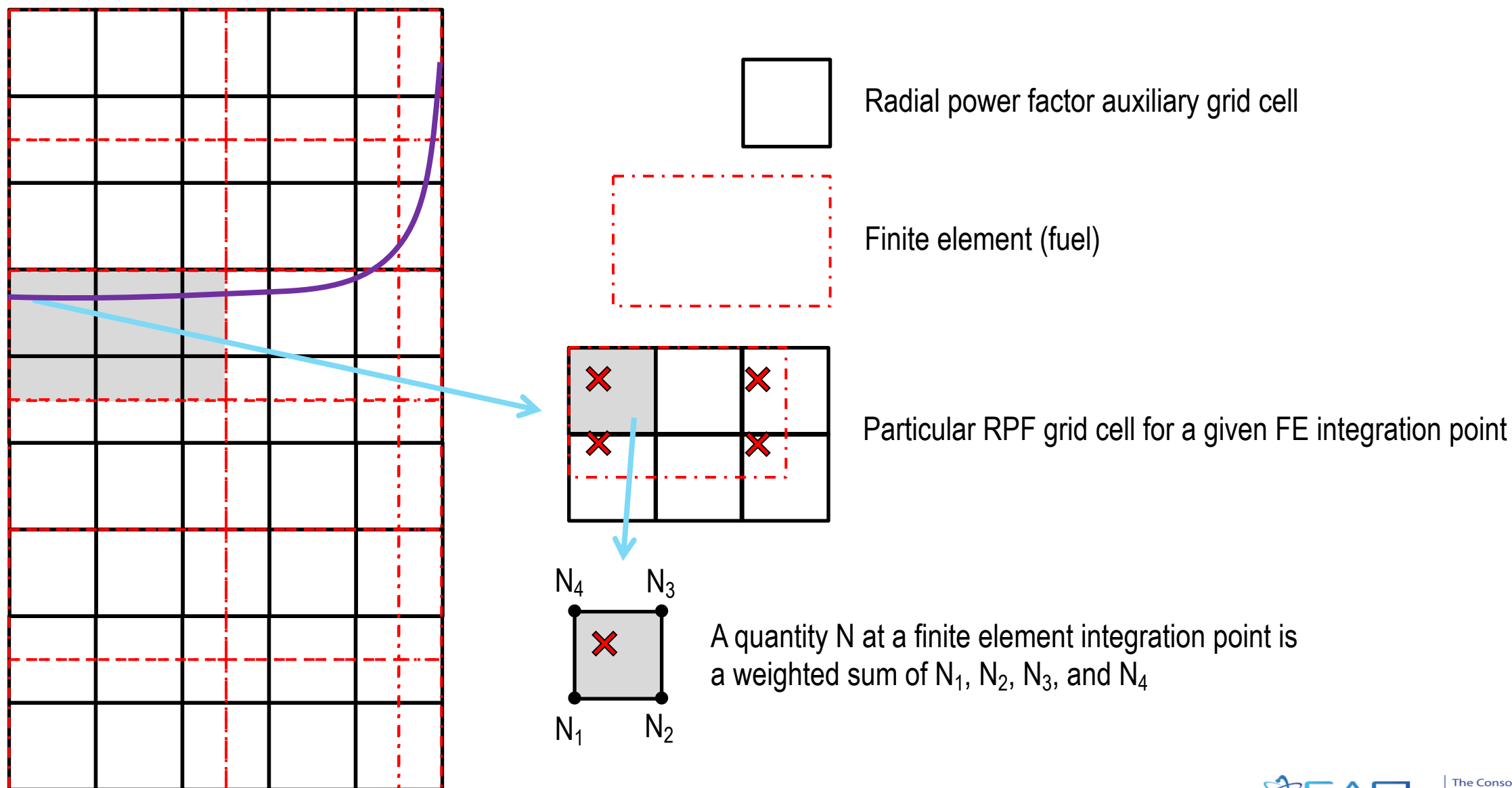
$$\frac{d N_{239}}{d t} = -\sigma_{a,239} N_{239} \phi + \sigma_{c,238} N_{238} \phi$$

$$\frac{d N_{240}}{d t} = -\sigma_{a,240} N_{240} \phi + \sigma_{c,239} N_{239} \phi$$

$$\frac{d N_{241}}{d t} = -\sigma_{a,241} N_{241} \phi + \sigma_{c,240} N_{240} \phi$$

$$\frac{d N_{242}}{d t} = -\sigma_{a,242} N_{242} \phi + \sigma_{c,241} N_{241} \phi$$

Auxiliary Radial Power Factor Grid to FE Mesh



Thermalhydraulic Boundary Condition

- The thermal boundary condition used by Bison at the outside of the cladding may be specified in a variety of ways, including setting the temperature directly.
- If desired, a simple one-dimensional enthalpy balance may be used to determine the thermal boundary condition

$$H(z) = H_{in} + \frac{\int_0^Z q''(z) \pi D_h dz + \int_0^Z f_c q' dz}{GA}$$

$$T(z) = \text{IAPWS}(H(z), P)$$

IAPWS -> International Association for the Properties of Water and Steam
P -> assumed constant in z

Heat Transfer Coefficient Correlations

- A set of correlations is available for single phase liquid forced convection, transition boiling, film boiling, saturated boiling, and other conditions.
- For single phase forced convection, the Dittus-Boelter correlation is used, giving:

$$h = \frac{0.023 Re^{0.8} Pr^{0.4} k}{D_h}$$

h -> heat transfer coefficient
Re -> Reynolds number
Pr -> Prandtl number
k -> thermal conductivity

- Then,

$$\phi = h(T_c(z) - T(z))$$

T_c -> temperature of cladding
ϕ -> heat flux

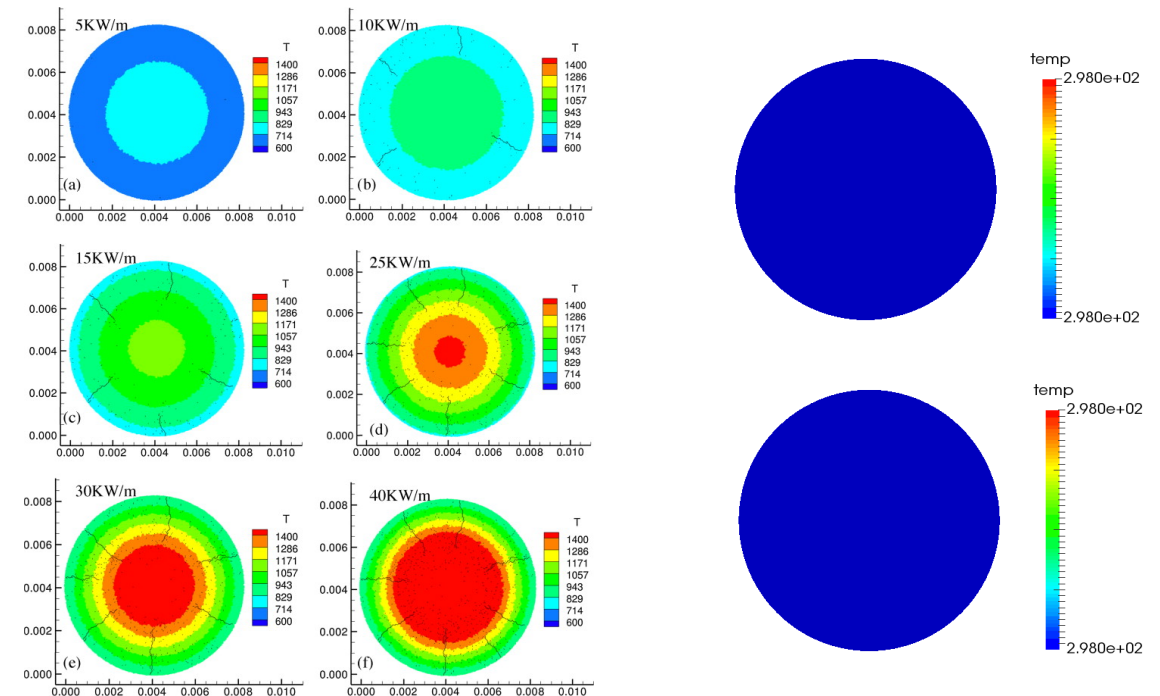
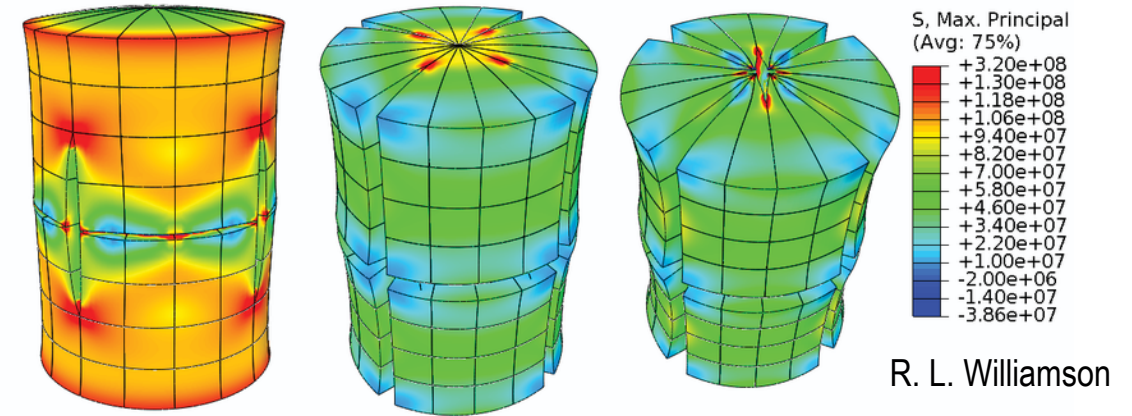
Fuel Cracking

- During the initial rise to full power, the ceramic UO_2 fuel pellets crack.
- This is due to the center of the pellet being hotter than the radial edge, which creates tensile hoop stresses at the radial edge.
- This cracking releases stress and allows the pellet to displace slightly in the outward radial direction.
- The result is a smaller gap between fuel and cladding, which affects the temperature of the fuel.
- Options for modeling include:
 - Relocation model
 - Smeared cracking
 - Isotropic softening
 - XFEM

$$E_i = \left[\frac{2}{3} \frac{2 - \nu}{2 + \nu} \frac{1}{1 - \nu} \right]^n E$$

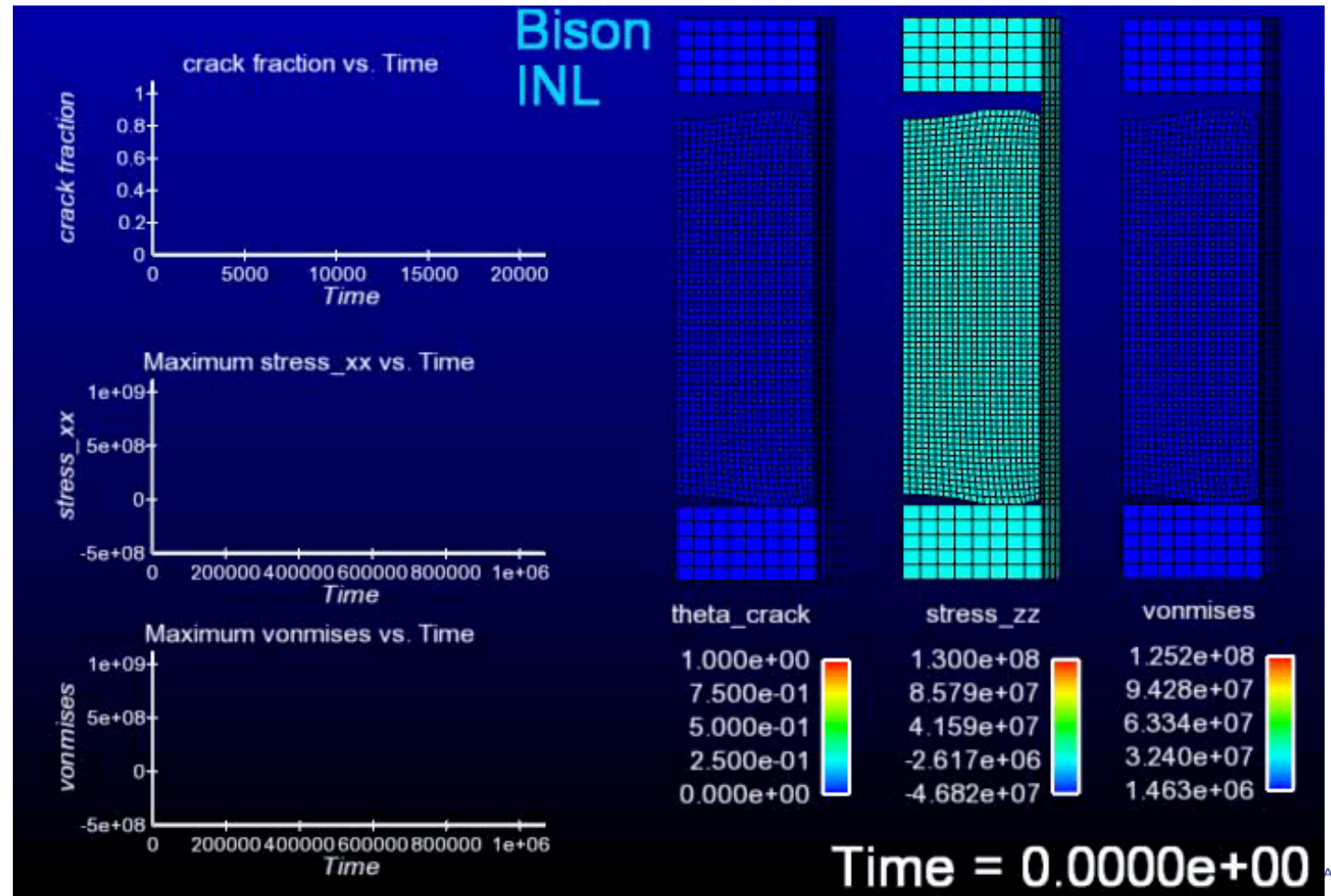
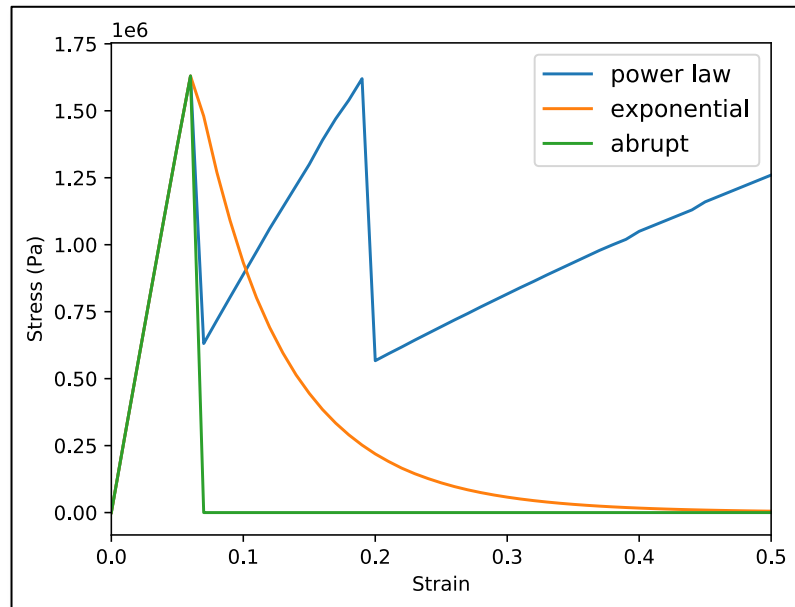
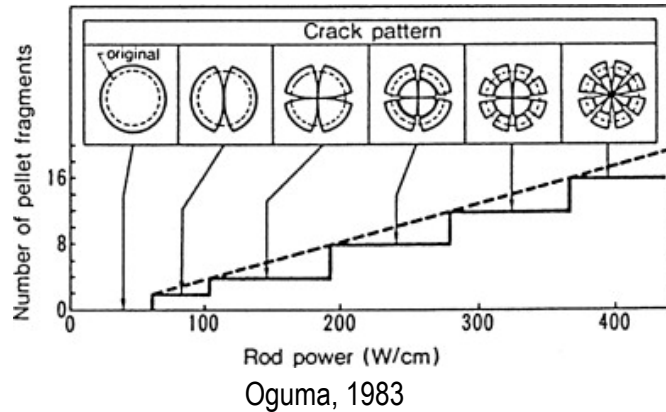
$$\nu_i = \frac{\nu}{2^n + (2^n - 1)\nu}$$

n is number of cracks



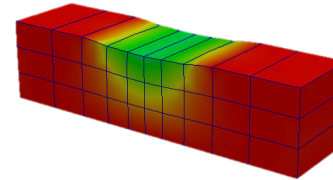
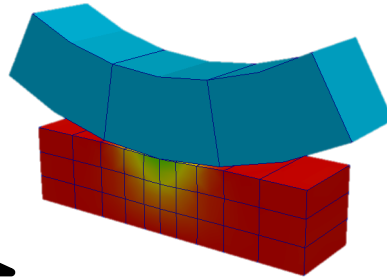
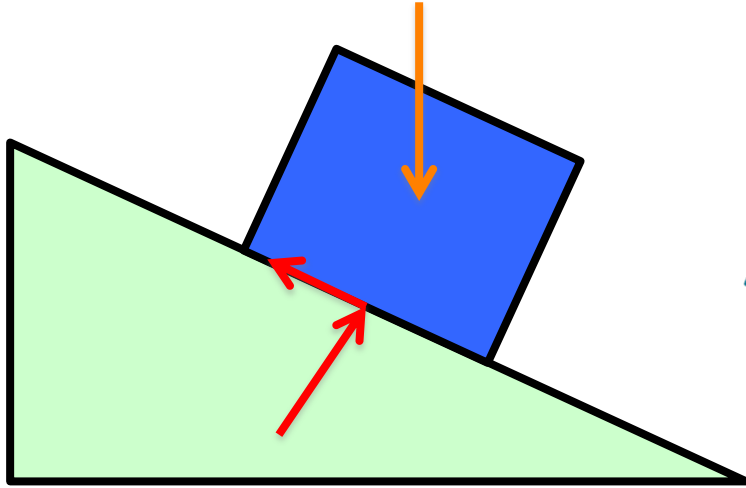
Smeared Cracking

- Smeared cracking adjusts the material stiffness at individual integration points
- The user has options for how the stiffness is reduced

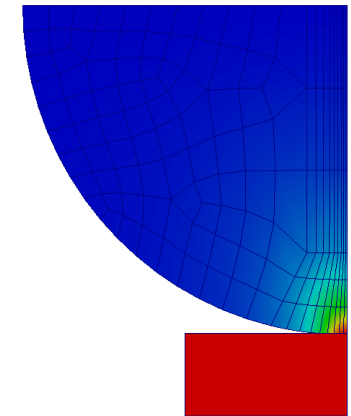
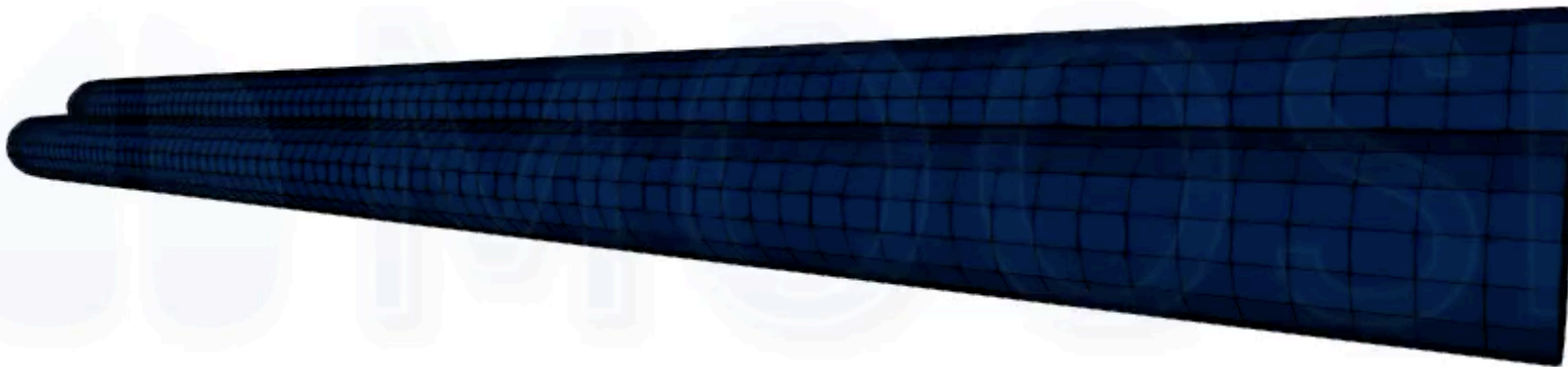


Mechanical Contact

$$F^{\text{int}}(d(t)) + F^c(d(t)) = F^{\text{ext}}(d(t))$$



- Search
 - Exterior identification
 - Nearby nodes
 - Contact existence
 - More geometric work
 - Penetration point
- Enforcement
 - Formulation of contact force (many options)
 - Formulation of Jacobian
 - Interaction with other capabilities (e.g., kinematic boundary conditions)

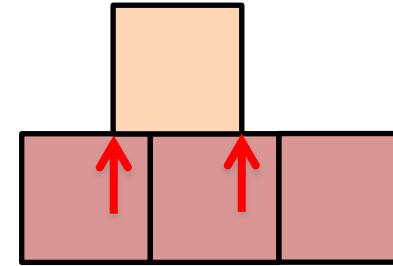


Mechanical Contact

$g \leq 0$ Distance of node through opposite surface

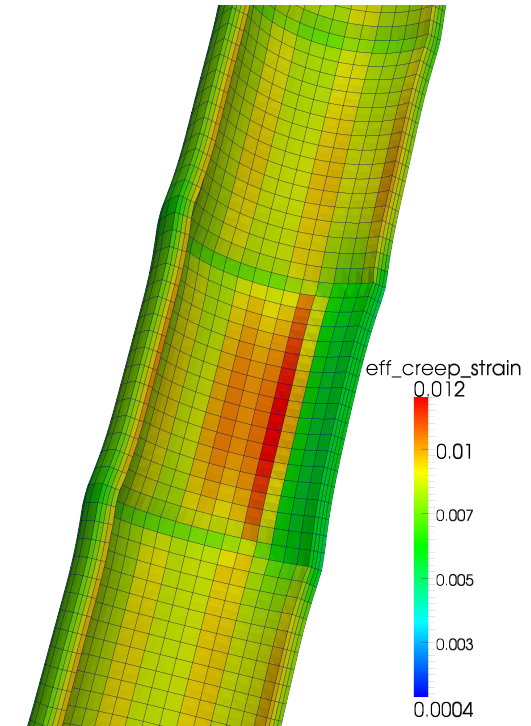
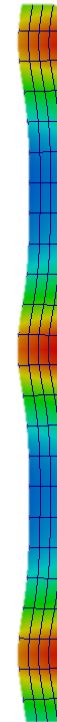
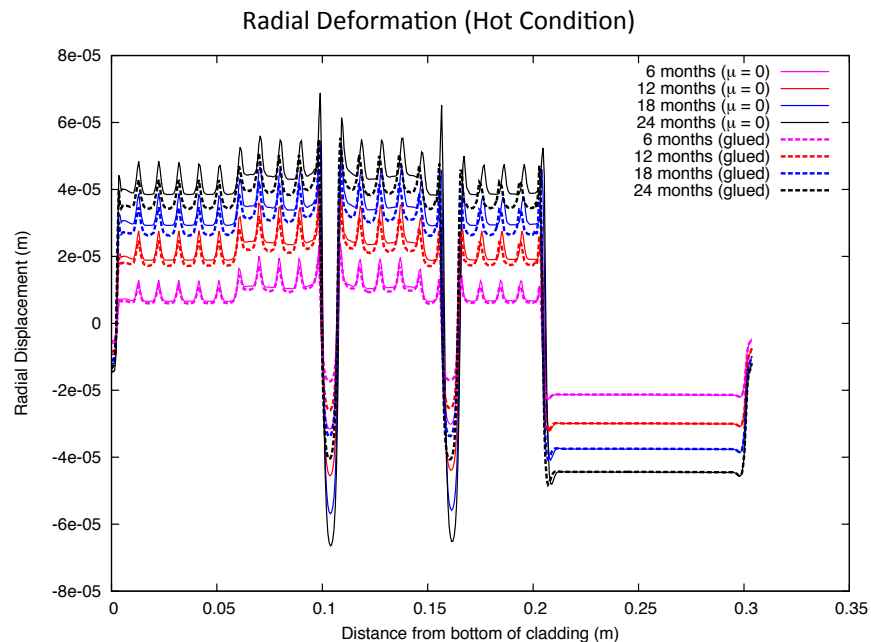
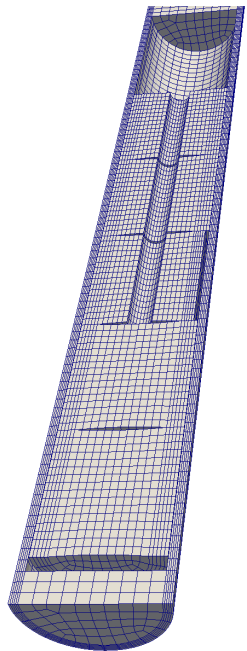
$t_N \geq 0$ Contact force in the normal direction

$$t_N g = 0$$



$$t_N = kg$$

Contact force is a penalty stiffness times the distance (e.g.)



Thermal Contact

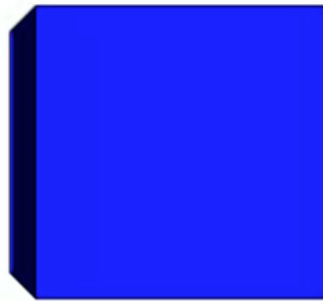
Contact constraint:
heat transfer
between separate
surfaces

$$\int_{\Gamma_1} h_{g1}(T_2 - T_1) = \int_{\Gamma_2} h_{g2}(T_2 - T_1)$$

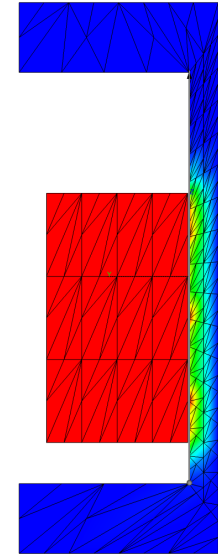
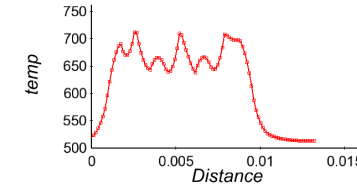
Gap conductance
for axisymmetric
system

$$\longrightarrow h_{g1} = \frac{k_g}{r_1 \left(\ln \left(\frac{r_2}{r_1} \right) + \frac{g_1}{r_1} + \frac{g_2}{r_2} \right)}$$

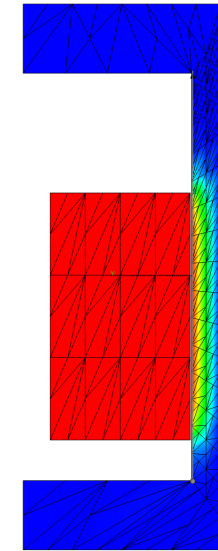
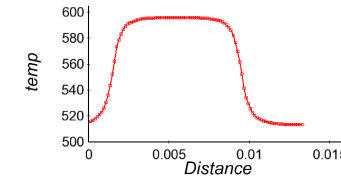
Jump distance $\longrightarrow g_1 + g_2 = 5756 \left(\frac{2 - a_{mix}}{a_{mix}} \right) \left(\frac{k_g \sqrt{T}}{P} \right) \left(\sum_{i=1}^n \frac{f_i}{M_i} \right)^{-1/2}$



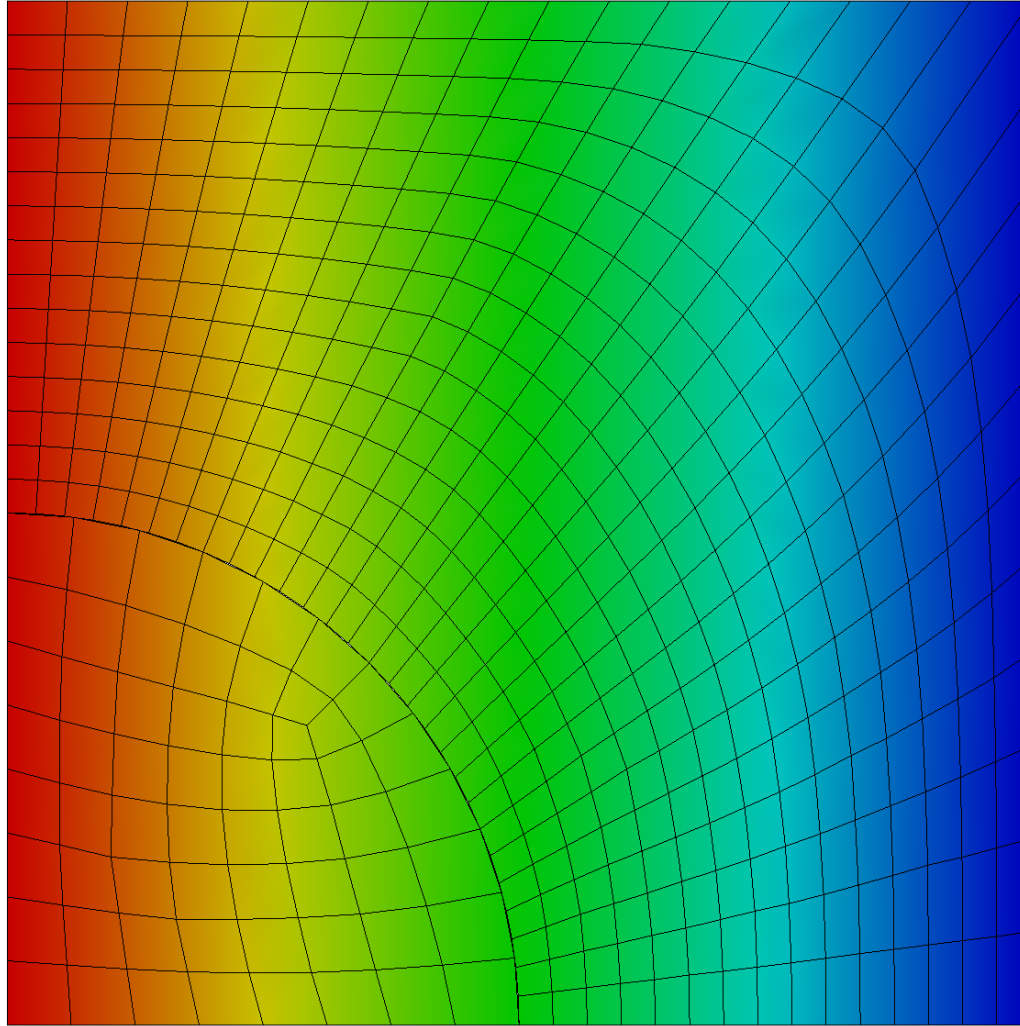
Node on Face



Quadrature/
symmetric



Advanced Contact



See
mooseframework.org/bison
for details about the
capabilities of Bison

More advanced methods (e.g., mortar) are in development



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