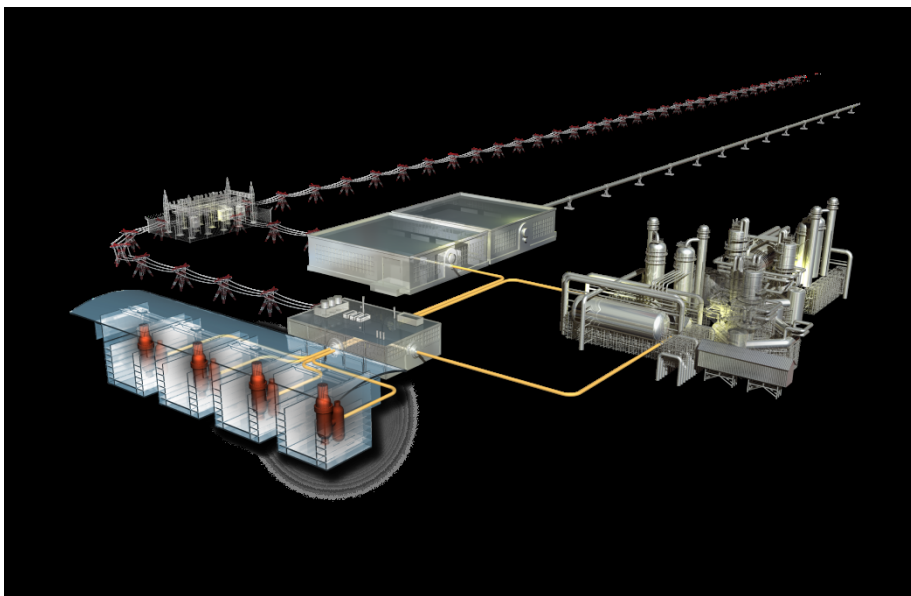


RELAP5-3D Input Model for the High Temperature Test Facility

Paul D. Bayless

June 2018

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June 2018

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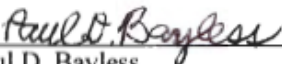
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RELAP5-3D Input Model for the High Temperature Test Facility

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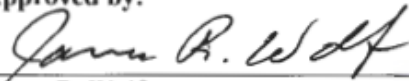

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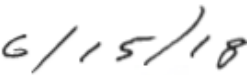
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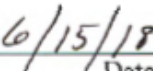

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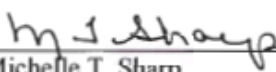
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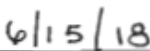

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ABSTRACT

A RELAP5-3D model of the High Temperature Test Facility at Oregon State University has been developed. The model includes the systems, components, and controls needed to perform code assessment calculations using data from the facility. Details of the model are provided. The input was developed for RELAP5-3D version 4.4.2. An independent quality assurance review of the model was performed.

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ACRONYMS

2-D	two-dimensional
ASTM	American Society for Testing and Materials
CV	control variable
DOE	Department of Energy
HTTF	High Temperature Test Facility
INL	Idaho National Laboratory
PCS	primary coolant system
RCCS	reactor cavity cooling system
RCST	reactor cavity simulation tank
SCS	secondary coolant system

RELAP5-3D Input Model for the High Temperature Test Facility

1. INTRODUCTION

A quality-assured RELAP5-3D input model has been developed for the High Temperature Test Facility (HTTF) at Oregon State University. The model was developed to perform code assessment using experiment data from the HTTF, and is consistent with the input requirements for code Version 4.4.2 (INL 2018).

The model development and quality assurance process is described in Section 2. A brief description of the HTTF is given in Section 3. Section 4 provides an overview of the input model structure. Details on each of the hydrodynamic components are provided in Section 5, followed by the heat structures in Section 6, the radiation and conduction enclosures in Section 7, material properties in Section 8, trips in Section 9, general tables in Section 10, and control variables in Section 11. An alternate nodalization of the outlet plenum and hot duct is described in Section 12. Results of a steam generator nodalization study are presented in Section 13. A list of input files significant to the model development effort is provided in Section 14. References used in developing the input model are listed in Section 15. Appendix A contains a listing of the input model.

2. MODEL DEVELOPMENT

The model was developed and documented in an Excel workbook. The principal advantage of this approach is that changes to reference information are automatically propagated throughout the workbook, altering all subsequent uses of those values, including updating the RELAP5-3D input model; this is particularly useful when the design is evolving as code calculations are being performed. One drawback is that the quality assurance effort to review the input model can become tedious.

There are two principal spreadsheets in the workbook, “geometry” and “RELAP5 input.” The geometry spreadsheet identifies the sources of reference information, and then manipulates the reference data as required to provide the RELAP5-3D input parameters. As its name suggests, the “RELAP5 input” spreadsheet is simply the RELAP5-3D input file. The input parameters are linked to the other spreadsheets in the workbook in which any necessary calculations were performed.

Other spreadsheets provide specialized input or calculations. “Materials” contains the heat structure material property data. “Convars” manipulates the geometric information from the hydrodynamic components and heat structures to generate multipliers for the control variables in the input model. “Power mapping” maps the power from the 10 heater rod banks into the three heater rod heat structures in the model. “Test 140” and “test 150” mimic the inner and outer core rings, but with actual coolant channel sizes; they are used to determine the input model channel hydraulic diameter that preserves the pressure drop through the core. “Benchmarking” contains input parameters that supersede the values originally calculated, based on results from the system characterization and shakedown testing and from the “test 140” and “test 150” calculations.

A large number of control variables are included in the input model. While some of them provide controls for establishing steady-state conditions, most generate parameters to assist in analyzing the code output, such as computing energy balances or peak temperatures. Some of the control variables also calculate parameters that are of interest in scaling analyses.

The principal sources of geometric information were the facility drawings and the facility description report (Woods 2017a). Dimensions of the stainless steel piping were taken from Crane 1988, and of the copper piping from Marks’ handbook (Baumeister, Avallone, and Baumeister 1978). Some specific component geometry was obtained from manufacturers’ product data sheets (Mueller 2011a and 2011b). Initial loss coefficients were calculated from the system geometry using formulas from Crane 1988 or Idelchik 1994. Material properties were obtained from a variety of sources, including testing done specifically for the HTTF.

A detailed, independent quality assurance review of the model was performed at several stages during the model development effort. The review consisted of several steps. First, each reference value identified in the spreadsheets was checked against the reference document. Second, a cell-by-cell check was performed of the calculations manipulating the reference data into code input format. Finally, a cell-by-cell check of the RELAP5-3D input spreadsheet was performed to ensure that each input value was linked to the proper calculated value in the supporting spreadsheets.

3. HTTF DESCRIPTION

The HTTF is a helium-cooled, electrically-heated integral experiment facility. The reference design for the facility is General Atomics' modular high-temperature gas-cooled reactor (DOE 1986), which uses prismatic graphite blocks in the core and reflectors. The HTTF primary pressure vessel and core are one-fourth scale in length and diameter. Most of the coolant channels in the core are full scale, with smaller diameter channels around the core periphery. The facility operates at low pressure, compared to the prototype reactor, and is designed primarily to investigate depressurized conduction cooldown transients.

The facility, described in detail in Woods 2017a, includes a number of systems. The primary coolant system (PCS) has a pressure vessel, a concentric hot and cold duct, a steam generator, a gas circulator, and connecting pipes. Break valves in both the hot and cold legs connect to a large reactor cavity simulation tank (RCST), whose gas composition can be initialized to a range of values to simulate the different conditions that may exist outside the reactor vessel following a loss-of-coolant accident. Figure 1 presents a rendering of the primary pressure vessel, RCST, and hot and cold ducts (Gutowska 2018).

Alumina ceramic blocks are used to simulate the core and top and bottom reflectors. Each block encompasses the radial region occupied by the central reflector, fuel, and side reflector in the reference reactor. Holes in the blocks provide channels for the heater rods, which consist of stacks of graphite rodlets. The rods are grouped into 10 heater banks, each of which contains 21 heater rods. Smaller coolant holes are arranged in a hexagonal pattern around the heater rods. Larger holes cast in the central and side reflector regions represent the core bypass flow in these regions. Permanent or outer reflector blocks, made of a different ceramic material, are located between the core blocks and the core barrel. A graphite plate in the upper plenum covers the gaps on either side of the permanent reflector blocks, so that the only flow through the core is in the holes cast in the core blocks.

The steam generator has 188 U-tubes. Feedwater is pumped from a supply tank into the downcomer on the secondary side, and any steam generated is vented to the atmosphere.

The principal feature of the reactor cavity cooling system (RCCS) is the cooling panels that surround the pressure vessel. Water flowing through the panels provides the heat sink for the PCS during most transients. Water is pumped from the same tank as the steam generator feedwater, but is recirculated back to the tank after exiting the top of the cooling panels. The inlet flow can be controlled to provide a desired panel outlet temperature, and isolation valves on the panels can be closed to simulate a degraded heat sink. There is a cover above the space between the pressure vessel and the RCCS panels, so that there is no direct natural circulation path between the building and the pressure vessel to provide unwanted cooling.

Two additional break lines are available, from the top of the primary pressure vessel to the top of the RCST, and from the bottom of the pressure vessel to the bottom of the RCST.

The facility has over 500 instruments, which are described in Woods 2018. Most of these are thermocouples in the core region to provide a temperature profile of the ceramic. There are also vertical thermocouple rakes in the upper and lower plenums, and in the hot and cold ducts, to try to capture temperature variations associated with recirculating or unmixed flow streams. The core and reflector instrumentation is generally arranged in one-sixth azimuthal sectors. The primary measurement sector is opposite the outlet plenum connection to the hot duct (on the east side of the plenum); the secondary sector is adjacent to the hot duct (west side), and the tertiary sector is next to (south of) the secondary sector.

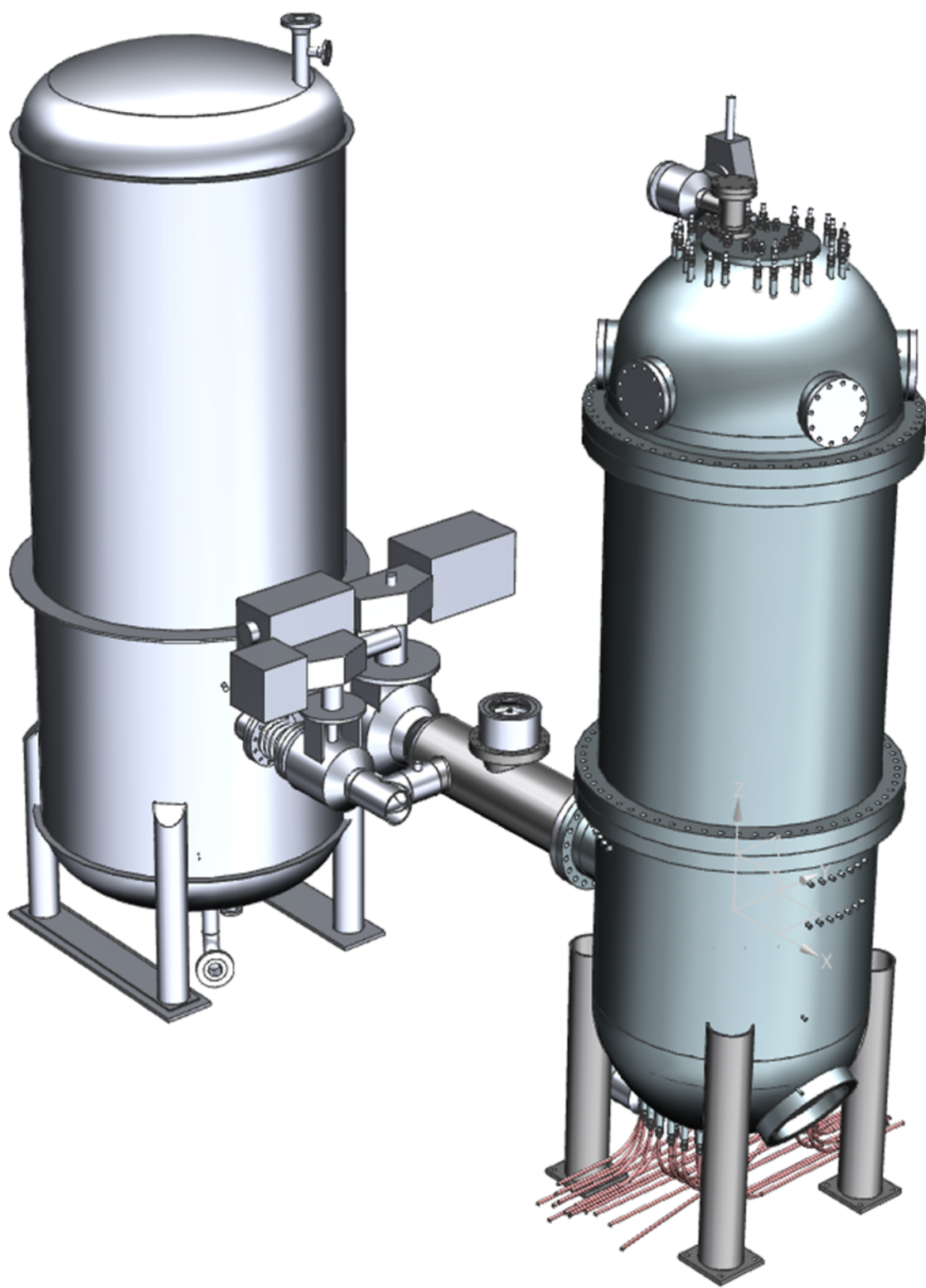


Figure 1. Diagram of the HTTF primary pressure vessel (right), RCST, and hot and cold ducts.

4. INPUT MODEL OVERVIEW

The input model includes hydrodynamic components, heat structures, trips, and control systems. Systems modeled are the PCS, secondary coolant system (SCS), RCCS, potable water system that supplies both the SCS and the RCCS, and reactor cavity. The RCST is considered part of the PCS.

The general hydrodynamic component numbering scheme is:

1-99: alternate break piping

100-199: primary pressure vessel

200-299: PCS piping and components

300-399: secondary coolant system

400-499: potable water system

900-999: reactor cavity and RCCS

More details on all of the components are provided below.

4.1 Primary Pressure Vessel

The hydrodynamic component numbers in the primary pressure vessel are from 100 to 199. Heat structures are generally numbered the same as the fluid volumes connected to them.

The primary pressure vessel nodalization is shown in Figure 2. Flow enters from the cold duct, passes through the core support structure under the outlet plenum bottom plate, then flows up between the primary pressure vessel and core barrel to the inlet plenum. Flow then passes down through various flow channels in the core and reflectors, recombines in the outlet plenum, then flows out into the hot duct.

The heated region of the core is divided into 10 equal-length axial segments, one for each block. The upper and lower reflectors each have two axial regions. This axial nodalization extends through each of the radial components in the vessel and in the RCCS.

The primary pressure vessel is divided into a number of different radial regions, as illustrated in Figure 3. The central reflector is divided into three regions: a central solid cylinder, a middle ring that contains the six 0.75-in.-diameter gap simulation channels and the ceramic that is directly influenced by the holes, and a solid outer ring that is adjacent to the core. The core is also divided into three rings, as it is designed on the hexagonal block pattern of the modular high-temperature gas-cooled reactor, which has three fueled rings. Figure 4 shows which blocks are included in each of the rings in a 60-degree sector; the boundaries of the inner and outer rings were extended beyond the full hexagonal block geometry to include all of the coolant channels. The inner ring includes 23 hexagonal blocks with 56 heater rods and 138 coolant channels, the middle ring models 24 blocks with 72 heater rods and 144 coolant channels, and the outer ring includes 39 blocks with 82 heater rods and 234 coolant channels. The side reflector is divided into three regions: an inner solid ring next to the outer core ring, a middle ring that contains the thirty-six 0.625-in.-diameter gap simulation channels and associated ceramic, and a solid outer ring. The next radial structure is the permanent or outer reflector (permanent side reflector in the reference plant), which has a coolant gap on either side (Components 164 and 166); these gaps do not have axial flow through them, as the top is covered by a plate (the upper plenum floor), leaving them open only to the outlet plenum. Continuing outward, the core barrel is next, followed by the coolant upcomer region between the core barrel and the pressure vessel wall, and finally the primary pressure vessel itself.

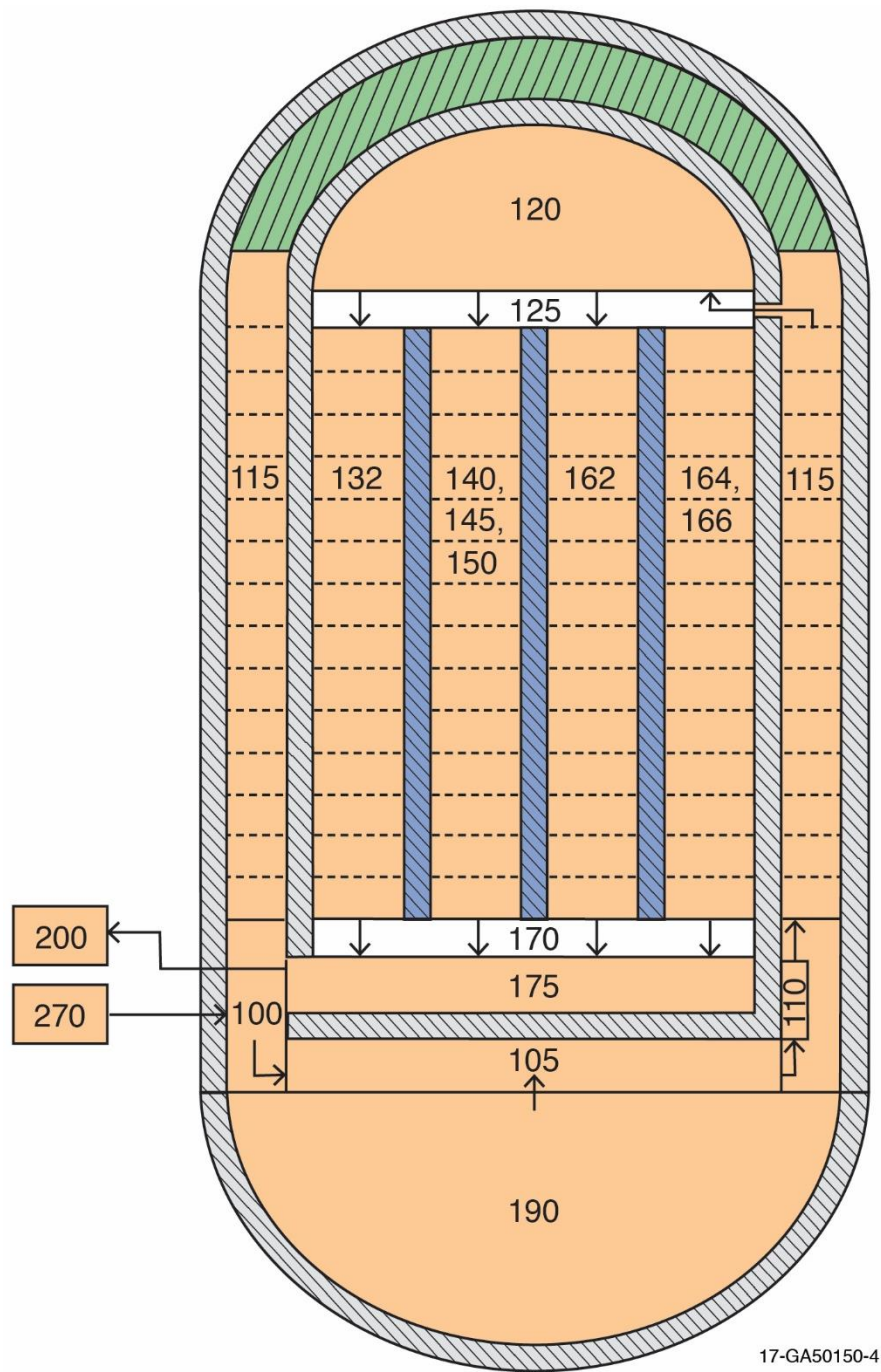
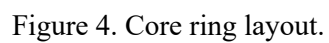
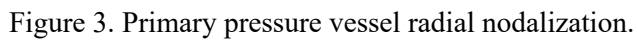


Figure 2. Primary pressure vessel nodalization.



4.2 Primary Coolant System

The hydrodynamic component numbers in the PCS are from 200 to 299. Heat structures are generally numbered the same as the fluid volumes connected to them.

The nodalization of the PCS is shown in Figure 5. Hot gas exits the primary pressure vessel into the hot duct, then flows up through a check valve and into the steam generator inlet plenum and tubes. The cooled gas flows out of the steam generator into piping that leads to the gas circulator. From the circulator, flow proceeds through an isolation valve, into a crossover pipe, into an annulus around the hot duct, and then back into the primary pressure vessel.

Break valves are located on the ends of the hot duct and the circulator discharge pipe, connecting them to the RCST. These valves are closed during steady state operation. Safety relief valves and a depressurization line are connected to the cold leg piping between the circulator and the loop isolation valve. These are modeled as a single line in the RELAP5-3D input model.

4.3 Secondary Coolant System

The hydrodynamic component numbers in the SCS are from 300 to 399. Heat structures are generally numbered the same as the fluid volumes connected to them.

The nodalization of the SCS is also provided in Figure 5. The feedwater pump draws suction from a water storage day tank and pumps it into the steam generator downcomer. The downcomer extends to near the top of the tube sheet. The water is then boiled on the outside of the tubes as it flows upward to the steam dome at the top of the steam generator. The steam then turns back downward before exiting out the side of the steam generator. The steam then flows through a pressure control valve in the steam line before flowing through more piping and being vented to the atmosphere. This downstream piping is not included in the RELAP5-3D input model. A safety relief valve is connected to a nozzle on the top of the steam generator. The piping downstream of the relief valve is not included in the input model.

4.4 Potable Water Supply System

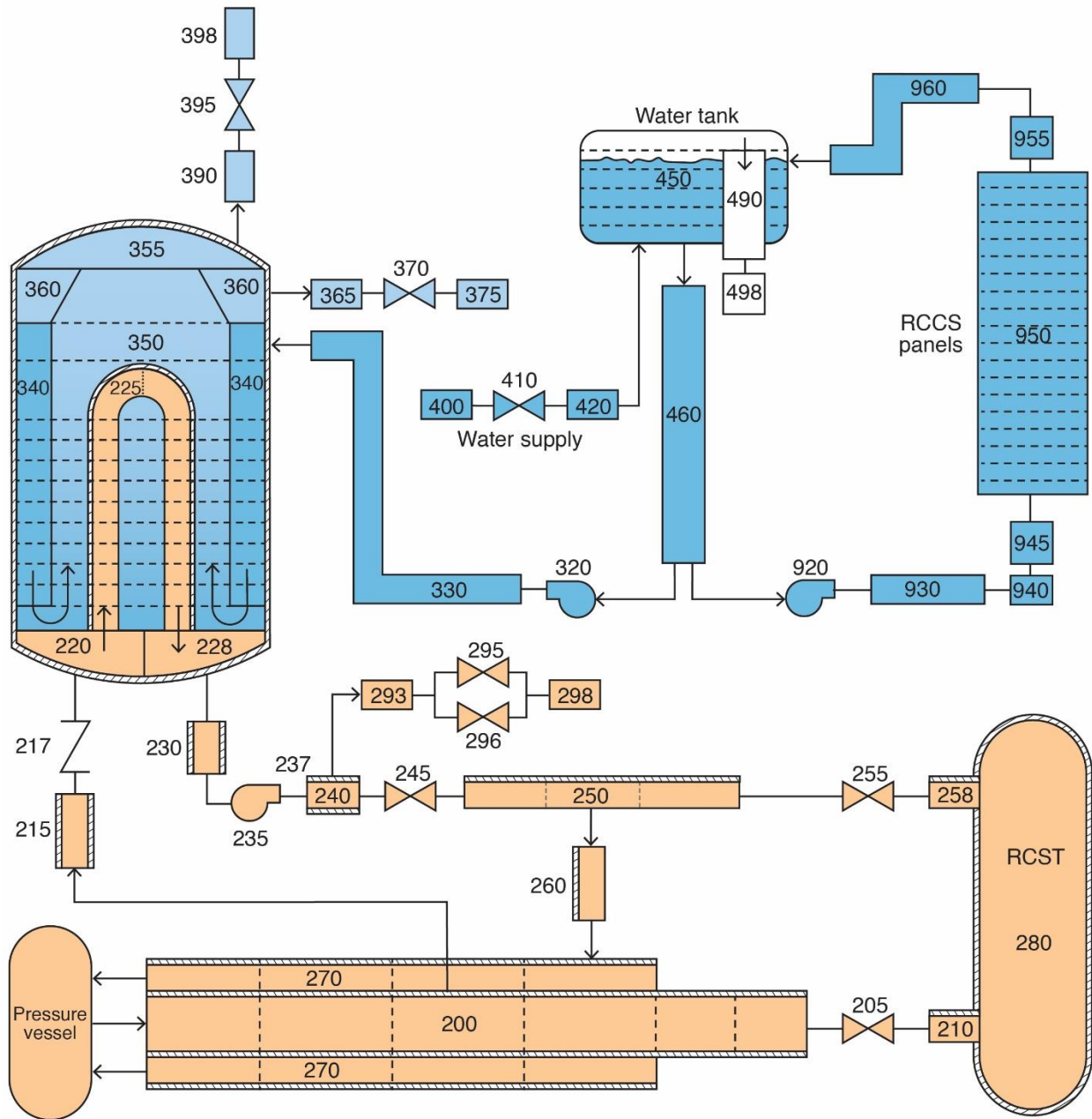
Hydrodynamic components in the potable water supply system are numbered from 400 to 499. There are no heat structures associated with this system.

The principal component in the system is the water storage day tank. This tank is the water source for both the SCS and the RCCS. The tank water level is maintained within a specified range. When the level gets too low, a valve opens in the supply line, allowing water from the public water system to flow into the tank. When the level rises to a certain level, the supply line valve is closed. The tank also has an interior drain/vent line that extends from the bottom of the tank to near the top; it is modeled as being open to the atmosphere below the tank. An outlet line is connected to the bottom of the tank; both the feedwater and RCCS pumps take suction from this outlet line.

4.5 Alternate Break Piping

Piping and valves associated with breaks located at the top and bottom of the pressure vessel are numbered from 1 to 99. Heat structures are generally numbered the same as the fluid volumes connected to them.

Figure 6 presents the nodalization for these two break lines. These components are usually inactive in the input model because they would only be active during an appropriate break simulation and would otherwise slow the system calculations down without providing any beneficial information. The component numbering was selected so that the molecular diffusion model could be used for these breaks without including volumes outside the PCS. Because molecular diffusion is expected to be important when these breaks are active, a large number of control volumes are included in the piping, with a target cell length of about 2.0 cm.



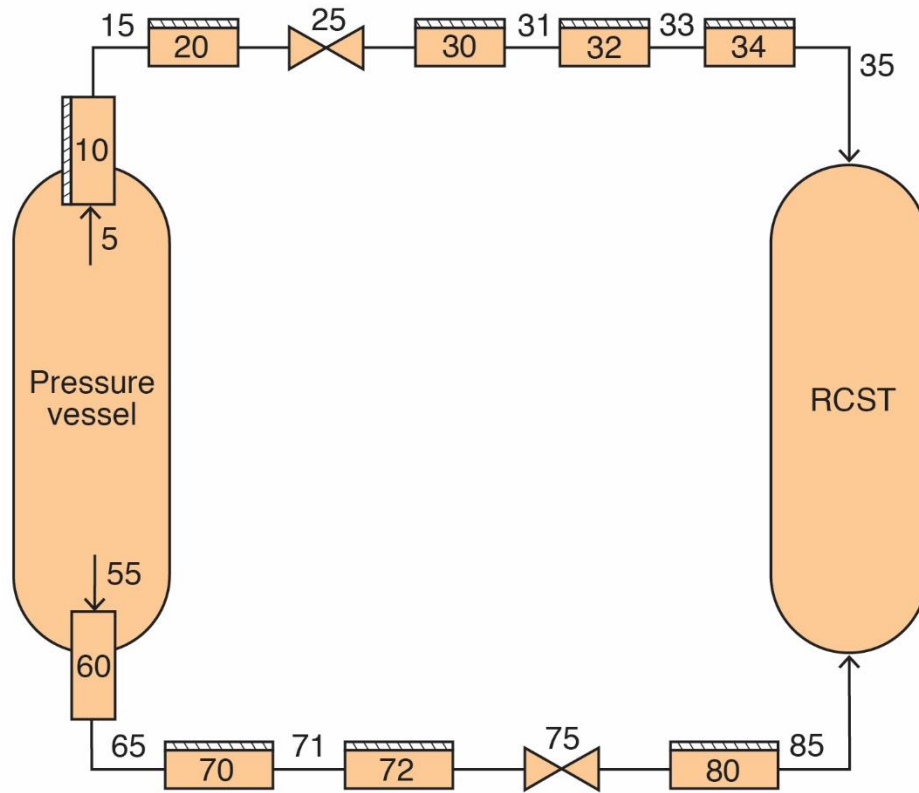
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Figure 5. PCS, SCS, and RCCS nodalizations.

4.6 Reactor Cavity and Reactor Cavity Cooling System

Hydrodynamic components in the reactor cavity and RCCS are numbered from 900 to 999. Heat structures are generally numbered the same as the fluid volumes connected to them.

The reactor cavity is modeled as a large air-filled volume at atmospheric pressure, and is located between the primary pressure vessel and the RCCS panels. The roof covering this region is not included in the model. The RCCS draws flow from the water storage tank and pumps it through a series of pipes



17-GA50150-5

Figure 6. Nodalization of vessel break lines.

into the cooling panels surrounding the primary pressure vessel. Water exiting the top of the panels is collected and returned to the water storage tank.

In some cases, it may make more sense to simplify the RCCS model so that it does not recirculate through the water storage tank; this will likely be true for post-test calculations because the temperature in the water storage tank can only be controlled manually. For this model, a time-dependent volume and junction supply the desired inlet flow rate and temperature, with the panel outlet flow being collected and discharged to a time-dependent volume.

Subsequent sections provide details on each of the components in the input model, grouped by component type. These are followed by a brief description of changes made to the model during initial steady-state testing, and then by references used in developing the input model.

5. HYDRODYNAMIC COMPONENTS

Unless otherwise noted, default values for the volume and junction flags are used.

Approximate initial conditions are entered, as it is expected that a steady-state calculation will be run to establish the desired conditions prior to a transient calculation. The initial values entered are for normal steady-state operation at full power (2200 kW).

5.1 Primary Pressure Vessel

Component 100 is a two-junction branch representing the primary pressure vessel coolant inlet region. It is a vertical volume, with the top at the midpoint of the outlet plenum and the bottom at the midpoint of the coolant region between the lower support plate and the middle distributor plate. It represents the annulus between the pressure vessel and core barrel, from the top of the bottom support plate to the bottom of the liner shell ring. Junction 1 connects the outlet of the cold duct (Component 270) to the inlet of this component, with momentum flux turned off on the vessel side of the junction (flag $s = 1$); the loss coefficients are approximated based on the area change between the cold duct and the inlet annulus. Junction 2 connects the outlet of this component to the inlet of Component 105, using an abrupt area change (flag $a = 1$) with code-calculated loss coefficients and with momentum flux from this component turned off (flag $s = 2$). Three heat structures are attached to this component: Structure 1000 (pressure vessel wall), Structure 1100, (jacket shell), and Structure 1150 (core barrel).

Component 105 is a two-volume pipe representing the coolant region below the core support plate. The first volume includes the volume between the lower support plate and the middle distributor plate; the second volume includes the volume between the middle distributor plate and the upper bulkhead plate. It is assumed that there are thirty 1.75-in.-diameter cylinders extending through both flow regions, providing the power supply to the heater rods. The coolant volume in the gaps around the power supply cylinders where they pass through the middle distributor plate is neglected. The length of each volume is assumed to be equal to the radius of the middle plate, as the flow comes from the periphery to the center, then back out to the periphery. The elevation change between the two volumes is included in the first volume. Z-direction data are also input for the component, with the length equal to the distance between the plates. Since the flow changes direction between the lower and upper volumes, a loss coefficient for a 180-degree change in flow direction is included at the internal junction. Three heat structures are attached to this component: Structure 1050 (middle distributor plate), Structure 1150 (core barrel), and Structure 1750 (outlet plenum bottom plate).

Component 110 is a two-junction branch representing the coolant in the region between the core barrel and the upcomer shell (referred to as the “jacket shell” on Drawing OSU-HTTF-PRIM-DWG-002, sheet 6). Junction 1 connects the outlet of Component 105 to the inlet of this component, and Junction 2 connects the outlet of this component to the inlet of Component 115. Junction 1 is modeled as a smooth area change with no user-input loss coefficients. Junction 2 is modeled as an abrupt area change with code-calculated loss coefficients. Two heat structures are attached to this component: Structure 1100 (jacket shell) and Structure 1150 (core barrel).

Component 115 is a 15-volume pipe representing the gap between the core barrel and the primary pressure vessel. It spans the elevation from the lower core support plate to above the flow slots in the upper plenum. The axial nodalization is the same as that inside the core barrel. The top volume is stagnant, as normal coolant flow exits the fourteenth volume. Three heat structures are attached to this component: Structure 1000 (pressure vessel wall), Structure 1150 (core barrel), and Structure 1200 (upper plenum cylinder).

Component 120 is a branch component representing the inlet (upper) plenum. It has one junction connecting to the coolant gap between the core barrel and the primary pressure vessel (Component 115). This volume extends from the top of the core barrel to the top of the upper plenum shroud. The junction is modeled as a smooth area change with loss coefficients representing the loss through the flow slots. Four heat structures are attached to this component: Structure 1001 (upper plenum shroud), Structure 1200

(upper plenum cylinder), Structure 1201 (upper plenum floor), and Structure 1202 (upper plenum internals).

Component 125 is a multiple junction component that connects the inlet plenum to the inlets of each of the core and reflector cooling channels. It has five junctions. Junction 1 connects to the central reflector, Junction 2 to the inner core ring, Junction 3 to the middle core ring, Junction 4 to the outer core ring, and Junction 5 to the side reflector. All junctions are modeled as abrupt area changes with user-input loss coefficients (flag a = 2) of 0.5 for forward flow and 1.0 for reverse flow, standard for sudden sharp-edged contractions/expansions with a large area change.

Component 132 is a 14-volume pipe component representing the six 0.75-in.-diameter holes in the central reflector. It extends from the bottom of the inlet plenum to the top of the outlet plenum. Heat Structure 1320 (central reflector middle ring) is attached to this component.

Component 140 is a 14-volume pipe component that represents the coolant channels in the inner core ring, extending from the bottom of the inlet plenum to the top of the outlet plenum. This includes the area of eighty-four 0.625-in.-diameter holes, thirty 0.5-in.-diameter holes, and twenty-four 0.375-in.-diameter holes. The hydraulic diameter of the channel was adjusted to provide the same pressure drop as if the holes were modeled individually; this diameter was determined by running a stand-alone model of this core ring with the three different holes sizes modeled individually and iterating on the combined channel hydraulic diameter. Three heat structures are attached to this component: Structure 1400 (inner core ring upper reflector), Structure 1401 (inner core ring ceramic), and Structure 1402 (inner core ring bottom reflector).

Component 141 is a 10-volume pipe component representing the helium gap around the inner core ring heater rods. It extends over the heated length. One heat structure is attached to this component: Structure 1401 (inner core ring ceramic).

Component 142 is a single junction component connecting Component 141 to Component 143.

Component 143 is a time-dependent volume that maintains a constant pressure in the helium gap around the inner core ring heater rods. Its temperature is set to the same value as in the adjacent volume in Component 141.

Component 145 is a 14-volume pipe component that represents the one hundred forty-four 0.625-in.-diameter cooling holes in the middle core ring. It extends from the bottom of the inlet plenum to the top of the outlet plenum. Three heat structures are attached to this component: Structure 1450 (middle core ring upper reflector), Structure 1451 (middle core ring ceramic), and Structure 1452 (middle core ring bottom reflector).

Component 146 is a 10-volume pipe component representing the helium gap around the middle core ring heater rods. It extends over the heated length. One heat structure is attached to this component: Structure 1451 (middle core ring ceramic).

Component 147 is a single junction component connecting Component 146 to Component 148.

Component 148 is a time-dependent volume that maintains a constant pressure in the helium gap around the middle core ring heater rods. Its temperature is set to the same value as in the adjacent volume in Component 146.

Component 150 is a 14-volume pipe component representing the coolant channels in the outer core ring, extending from the bottom of the inlet plenum to the top of the outlet plenum. This includes the area of ninety-six 0.625-in.-diameter holes, sixty-six 0.5-in.-diameter holes, and seventy-two 0.375-in.-diameter holes. As with Component 140, the channel hydraulic diameter was adjusted to provide the appropriate pressure drop. Three heat structures are attached to this component: Structure 1500 (outer core ring upper reflector), Structure 1501 (outer core ring ceramic), and Structure 1502 (outer core ring bottom reflector).

Component 151 is a 10-volume pipe component representing the helium gap around the outer core ring heater rods. It extends over the heated length. One heat structure is attached to this component: Structure 1501 (outer core ring ceramic).

Component 152 is a single junction component connecting Component 151 to Component 153.

Component 153 is a time-dependent volume that maintains a constant pressure in the helium gap around the outer core ring heater rods. Its temperature is set to the same value as in the adjacent volume in Component 151.

Component 162 is a 14-volume pipe component that represents the thirty-six 0.625-in.-diameter holes in the side reflector. It extends from the bottom of the inlet plenum to the top of the outlet plenum. Heat Structure 1620 (side reflector middle ring) is attached to this component.

Component 164 is a 14-volume pipe component that represents the gap between the side reflector and the outer reflector. It extends from the top of the upper reflector to the top of the outlet plenum. It is connected to the outlet plenum, but not to the inlet plenum, as this gap is covered by the upper reflector top plate. Two heat structures are attached to this component: Structure 1640 (side reflector outer ring) and Structure 1660 (outer reflector).

Component 166 is a 15-volume pipe component that represents the gap between the outer reflector and the core barrel. It extends from the top of the upper reflector to the bottom of the outlet plenum. It is connected to the outlet plenum, but not to the inlet plenum, as this gap is also covered by the upper reflector top plate. Two heat structures are attached to this component: Structure 1660 (outer reflector) and Structure 1150 (core barrel).

Component 168 is a single junction component connecting the middle of the last cell in Component 166 to the middle of Component 175, the outlet plenum. The connection is modeled as a crossflow junction with momentum flux turned off on both sides of the junction (flag $s = 3$). The junction area is modeled as the perimeter of the hot duct flow opening through the side reflector multiplied by the gap width between the outer reflector and the core barrel. Loss coefficients are calculated based on the ratio of the junction flow area to the hot duct flow area.

Component 170 is a multiple junction component connecting the core and reflector coolant channels and gaps to the outlet plenum. It has six junctions. Junction 1 connects to the central reflector, Junction 2 to the inner core ring, Junction 3 to the middle core ring, Junction 4 to the outer core ring, Junction 5 to the side reflector, and Junction 6 to the gap between the side and outer reflectors. These junctions are all modeled as abrupt area changes with user-input loss coefficients (flag $a = 2$). The three core channels have forward and reverse loss coefficients of 2.5 to account for the channeling of the individual flow paths in the bottom reflector region. The reflector channels have forward loss coefficients of 1.0 and reverse loss coefficients of 0.5, as they are straight flow paths with a sudden expansion into the outlet plenum.

Component 175 is a branch component representing the outlet plenum. It has one junction connecting the middle of this component to the inlet of the hot duct (Component 200); momentum flux is turned off on the plenum side of the junction (flag $s = 2$). Four heat structures are attached to this component: Structure 1150 (core barrel), Structure 1660 (outer reflector), Structure 1750 (outlet plenum bottom plate), and Structure 1751 (support posts).

Component 190 is a branch component representing the pressure vessel lower head. It has one junction connecting the outlet of this component to the middle of the first volume of Component 105. The junction area is based on flow gaps in the lower support plate. An abrupt area change (flag $a = 1$) with code-calculated loss coefficients is used, and momentum flux is turned off in the core support region volume (flag $s = 1$). Structure 1002 (pressure vessel lower head) is connected to this component.

5.2 Primary Coolant System

Component 200 is the hot duct. It is modeled as a six-volume pipe. Cell lengths are selected such that the first instrument rake, the pipe to the steam generator, and the return pipe from the circulator to the cold duct are at cell centers. The segment from the end of the fourth cell to the modeled break valve (Component 205) includes the physical valve in the facility; this segment is divided into two cells to have comparable cell lengths through the hot leg. The loss coefficient for flow through the valve is located at internal Junction 5 in the pipe, rather than in the valve junction. It is assumed that the valve flow area is equal to that of the hot duct. The loss coefficient is based on the nominal hot leg Reynolds number and flow through an open ball valve. Losses associated with the very small area change between the concentric duct and the pipe leading to the RCST are neglected. Two heat structures are attached to this component: Structure 2000 (wall between hot and cold ducts) and Structure 2001 (pipe wall outside the concentric duct region).

Component 205 is a valve representing valve V-313, the hot duct break valve leading to the RCST. It connects the outlet of Component 200 to the inlet of Component 210, and is modeled as a motor valve with a stroke time of 5 seconds (assumed value pending receipt of actual data). The abrupt area change model is used with user-input loss coefficients of 0.0 (flag $a = 2$), as the losses associated with the valve are included in Component 200. The valve area is modeled as changing linearly with the stem position. Trip 205 opens the valve, and Trip 206 closes it.

Component 210 is the pipe between valve V-313 and the RCST. It is modeled as a branch with one junction, connecting the outlet of this component to the bottom of the second volume in Component 280, the RCST. The junction is modeled as an abrupt area change with user-input loss coefficients; the forward and reverse loss coefficients are for a sudden expansion/contraction with a large area ratio. If a hot duct break is being simulated, with the spool piece installed, the junction connects the outlet of Component 282 to the outlet of this component; in this case, the area change is modeled as abrupt with code-calculated loss coefficients. Heat Structure 2100 (pipe wall) is attached to this component.

Component 215 is the pipe between the hot duct and the steam generator inlet. It consists of the steam generator nozzle and the check valve body shown on Drawing OSU-HTTF-PRIM-DWG-005A. The pipe is modeled as a branch with one junction, connecting the top of the third volume in the hot duct to the inlet of this branch. Heat Structure 2150 (pipe wall) is attached to this component.

Component 217 is the check valve (V-101) in the pipe between the hot duct and the steam generator inlet. It is modeled at the steam generator inlet plenum, connecting the outlet of Component 215 to the inlet of Component 220. The differential pressure required to open the valve is 500 Pa (assumed value pending receipt of actual data). The loss coefficients include the loss from the 45-degree elbow in the steam generator inlet line and the area change between the pipe and inlet plenum; the latter loss is assumed to be an abrupt contraction from the pipe flow area to the average flow area in the plenum. An alternate model for this component is also available, representing a 4-in. (10-cm) diameter orifice that is installed in place of the check valve during system characterization testing.

Component 220 is the steam generator inlet plenum. It includes both the plenum and the 45-degree elbow between the plenum and the flange. It is modeled as a branch with one junction, connecting the outlet of this component to the inlet of the steam generator tubes. This junction is modeled as an abrupt area change with user-input loss coefficients. The loss coefficients are based on a sudden contraction/expansion from the plenum flow area at the tube sheet to the tube flow area. The loss from the elbow and the entrance to the plenum are included in the Component 217 loss coefficient. Two heat structures are attached to this component: Structure 2200 (plenum and inlet pipe walls) and Structure 2201 (plenum pass partition).

Component 225 is the steam generator tubes. The 188 tubes are modeled as a 22-volume pipe. Cells 1–10 carry the gas flow up, Cells 11 and 12 are the U-bend, and Cells 13–22 are the downflow side. The tube bends are assumed to start at the top baffle plate. They are also assumed to be smooth 180-degree

bends, so that the radius of the bend is equal to the distance from the center of the bundle (90–270 degree line on Drawing OSU-HTTF-SEC-DWG-003C) to the center of each tube. The loss from the bend is located at the junction at the top of the tubes, Junction 11. The first and last cells include the flow length through the tube sheet. Two heat structures are attached to this component: Structure 2250 (steam generator tubes) and Structure 2251 (tube sheet).

Component 228 is the steam generator outlet plenum. It includes both the plenum and the 45-degree elbow between the plenum and the flange. It is modeled as a branch with two junctions. The inlet junction is modeled as an abrupt area change at the tube sheet with user-input loss coefficients; the loss coefficients are based on a sudden expansion/contraction from the tube flow area to the plenum flow area at the tube sheet. The outlet junction is modeled as a smooth area change with a loss coefficient equal to that of a sudden expansion from the average plenum area to the pipe area plus a 45-degree elbow. Two heat structures are attached to this component: Structure 2280 (plenum and outlet pipe walls) and Structure 2201 (plenum pass partition).

Component 230 is the pipe between the steam generator outlet and the gas circulator inlet. It is modeled using a single volume component. There are two bends in this section of piping. The losses associated with these bends are included in the circulator inlet junction; the estimated friction loss in the bends is subtracted from the published loss coefficient values, as the code will calculate the friction loss. Heat Structure 2300 (pipe wall) is attached to this component.

Component 233 is a single junction connecting the outlet of Component 230 to the inlet of Component 234; it is used only during steady-state calculations and is deleted for transient calculations.

Component 234 is a time-dependent volume that provides pressure control during steady-state calculations; it is deleted for transient calculations. The volume is maintained at a constant temperature equal to the desired primary pressure vessel inlet temperature. The pressure is controlled by control variable (CV) 234 to provide the desired pressure vessel inlet pressure.

Component 235 is the gas circulator volume. It is modeled as a branch with one junction, connecting the outlet of Component 230 to the inlet of this component. Loss coefficients represent the losses associated with the two bends in the inlet piping. Heat Structure 2350 (circulator body) is attached to this component.

Component 237 provides the circulator forced flow, connecting the outlet of Component 235 to the inlet of Component 240. It is modeled as a time-dependent junction, with the flow rate determined by CV 237 during steady state. The time-dependent junction component is expected to provide sufficient modeling of the circulator function, as transients should result in isolation of the portion of the loop piping containing the circulator.

Component 240 is the pipe between the gas circulator outlet and valve V-203 (Component 245). It is modeled as a single volume, and includes the volume of the pipe and half of the valve. The flow area of the valve is assumed to be the same as that of the pipe. Heat Structure 2400 (pipe wall) is attached to this component.

Component 245 is a valve representing valve V-203. It connects the outlet of Component 240 to the inlet of Component 250, and is modeled as a motor valve with a stroke time of 5 seconds (assumed value pending receipt of actual data). The valve area is modeled as changing linearly with the stem position. Trip 245 opens the valve, and Trip 246 closes it. The junction is modeled as an abrupt area change with user-input loss coefficients; the loss coefficients are based on flow through a ball valve and through one 90-degree bend (between the circulator and the valve).

Component 250 is the pipe between valve V-203 and valve V-311 (Component 255). It is modeled as a pipe with three volumes. The first volume extends from the middle of valve V-203 to the tee upstream of the break valve. The second volume is the straight passage of the tee. The third volume is the volume in valve V-313, which is assumed to have the same flow area as the upstream piping. The first junction includes the loss coefficient from the 90-degree elbow in the piping. Heat Structure 2500 (pipe wall) is

attached to this component.

Component 255 is valve V-311, which is the cold leg break valve leading to the RCST. It connects the outlet of Component 250 to the inlet of Component 258, and is modeled as a motor valve with a stroke time of 5 seconds (assumed value pending receipt of actual data). The valve area is modeled as changing linearly with the stem position. Trip 255 opens the valve, and Trip 256 closes it. The loss coefficient is based on the nominal cold leg Reynolds number and flow through an open ball valve.

Component 258 is the pipe between valve V-311 and the RCST. It is modeled as a branch with one junction, connecting the outlet of this component to the inlet of the second volume in Component 280, the RCST. The junction is modeled as an abrupt area change with user-input loss coefficients; the forward and reverse loss coefficients are for a sudden expansion/contraction with a large area ratio. If a hot duct break is being simulated, with the spool piece installed, the junction connects the outlet of this component to the inlet of Component 282; in this case, the area change is modeled as smooth with loss coefficients of 0.0. Heat Structure 2580 (pipe wall) is attached to this component.

Component 260 is the crossover pipe from the cold leg tee to the cold duct. It is modeled as a branch with two junctions. The first junction is the tee off of the cold leg pipe upstream of the break valve, connecting the side of the second volume of Component 250 to the inlet of this component. The forward loss coefficient is that of flow for a diverging wye, and the reverse loss coefficient is that for a converging wye; in both cases, all of the flow is through the branch. The second junction connects the outlet of this component to the side of the first volume in the cold duct. The forward loss coefficient at this junction is approximated as that of flow from the side branch of a converging wye. The reverse loss coefficient is for a diverging wye. The geometry of the connection does not match either of the formulas associated with Diagram 7-18 in Idelchik 1994; the second formula is used, and uncertainties in this loss coefficient should not be significant as reverse flow is only expected during some transient tests with natural circulation flow. Heat Structure 2600 (pipe wall) is attached to this component.

Component 270 is the cold duct. It is modeled as a four-volume pipe. The junctions are at the same locations as those in the common portion of the hot duct. Two heat structures are attached to this component: Structure 2000 (wall between hot and cold ducts) and Structure 2700 (outer pipe wall).

Component 280 is the RCST. It is normally modeled as a two-volume vertical pipe. The lower volume represents the region below the break nozzles, which is assumed to not participate in any gas mixing in the tank. The upper volume represents the portion of the tank that will participate in mixing with gas entering from the PCS. With this being modeled as a single cell, all of the fluid will be perfectly mixed. This will overestimate the temperature of gas re-entering the PCS from the tank, as no thermal stratification will occur in the tank; this is a limitation of the one-dimensional modeling of the tank. However, there is no basis for a two- or three-dimensional model, and unphysically large recirculating flows have been observed in the past when such a modeling approach was attempted. The lengths of the two volumes are distorted to maintain the top and bottom of the tank at the appropriate elevations; the total volume is preserved, and the hydraulic diameter used is that of the tank cylinder. A single-volume model is also available; this model is intended to be used when the hot duct break spool piece is installed in the tank (see Component 282). There are normally three heat structures attached to this component: Structure 2100 (hot duct nozzle), Structure 2580 (cold duct nozzle), and Structure 2800 (tank wall). Structure 2820 (spool piece wall) is also attached if the break spool piece (Component 282) is installed.

Component 282 is the spool piece that is installed for hot duct breaks, connecting the hot and cold leg break nozzles inside the RCST. It is modeled as a single volume. Without a full set of dimensional information, the pipe is assumed to be a 180-degree bend with a bend diameter equal to the distance between the hot and cold break nozzle centerlines. From Drawing OSU-HTTF-RCSS-DWG-008C, it appears that the pipe is the same size as the cold leg nozzle piping, and that is therefore assumed to be the case. Heat Structure 2820 (pipe wall) is attached to this component.

Component 293 is the piping leading to the inlet of valves PSV-100 (Component 295) and V-400 (Component 296). It is modeled as a branch with one junction connecting the side of Component 240 to

the inlet of this component. The forward loss coefficient at the junction is that of flow into the side branch of a diverging wye. The reverse loss coefficient is for flow from the side branch of a converging wye; this loss coefficient should not matter, as reverse flow through the pressure relief line should not occur.

Component 295 is the pressure relief valve (PSV-100). It connects the outlet of Component 293 to the inlet of Component 298, and is modeled as a trip valve that is open when trip 1295 is true. The flow area of the valve is set to that of the pipe, and will be adjusted when performance data for the valve are available.

Component 296 is the depressurization valve (V-400). It connects the outlet of Component 293 to the inlet of Component 298, and is modeled as a trip valve that is open when trip 1296 is true. The flow area of the valve is assumed to be the same as that of the pipe. The junction is modeled as a smooth area changed with a user-input loss coefficient based on flow through an open ball valve.

Component 298 is the pressure boundary volume downstream of the pressure relief and depressurization valves. It is modeled as a helium-filled volume at atmospheric pressure. Helium is used (rather than air) to avoid some code failures when air flowed back into the PCS through an open valve; since both valves connected to this volume are used to depressurize the PCS, backflow should not occur in the facility.

5.3 Secondary Coolant System

Component 320 is the feedwater pump (P-010). It is modeled as a time-dependent junction. The flow through the pump is determined by CV 320. The pump suction is taken from the water storage tank outlet line, Component 460. The pump discharge is connected to the inlet of Component 330.

Component 330 is the piping between the feedwater pump and the steam generator. The valves in this piping, V-011, V-012, and LCV-013, are not modeled explicitly. The logic controlling LCV-013 will be included in the controls for Component 320. The piping is modeled using a branch component with one junction; the junction connects the outlet of this component to the inlet of Component 340, with momentum flux turned off in the “to” volume (flag $s = 1$). Details of the pipe configuration are not shown on drawing OSU-HTTF-GEN-DWG-009H, so the length is estimated to be 20% greater than the elevation change between the feedwater pump and the feedwater nozzle on the steam generator to accommodate the horizontal runs. This assumption should have no effect on the calculated plant response, as the feedwater flow rate and steam generator pressure are controlled, so the pressure loss in this piping will be immaterial. The loss coefficients at the junction were calculated assuming the connection is a tee with all of the flow going between the branch and one leg of the tee. The pipe walls are not modeled with heat structures, as heat transfer in the feedwater system is not expected to be important to the steam generator conditions.

Component 340 is the steam generator downcomer. It is modeled as an 11-volume pipe extending from the bottom of the inner shell lap ring to the bottom of the inner shell. The internal junctions are located at the same elevations as those in the boiler region. Two heat structures are attached to this component: Structure 3400 (steam generator outer shell) and Structure 3500 (steam generator inner shell).

Component 345 (not shown in Figure 5) is the junction between the steam generator downcomer and the boiler region. It is modeled using a single junction component connecting the outlet of Component 340 to the outlet of the first cell in Component 350. The junction area and hydraulic diameter are those of the downcomer. The abrupt area change flag is set to 2, and the loss coefficient is based on a sudden expansion (contraction in reverse flow) into the bottom boiler volume.

Component 350 is the steam generator boiler region. It is modeled as a 13-volume pipe extending from the top of the tube sheet to the top of the inner cone. Node boundaries in the boiler region are placed at the centerlines of the baffle plates and halfway in between them, resulting in 10 cells spanning the straight portion of the tubes. The flow area at the baffle plates is modeled as just the flow around the end of the plate; it is assumed that thermal expansion of the tubes and tie rods will result in a negligible flow area between the tubes and the baffle plate. The volume occupied by the baffle plates is also neglected.

Loss coefficients at the baffle plates are estimated as though the area change was through a sharp-edged orifice, and are based on the volume flow area. Cells 11 and 12 are equal-length cells extending from the top baffle plate to the bottom of the inner cone, while cell 13 is the volume inside the inner cone. The U-bends in the steam generator tubes are contained in cell 11. The bundle interphase drag model (flag $b = 1$) is used in volumes 1–11. Three heat structures are attached to this component: Structure 3400 (steam generator outer shell), Structure 3500 (steam generator inner shell), and Structure 2250 (steam generator tubes).

Component 355 is the steam dome, the region above the top of the inner cone. It is modeled as a branch with two junctions. The dome includes only part of the rounded portion of the end cap; the rest, together with the cylindrical (straight) portion, is included in Component 360. The first junction is the inlet from Component 350 and is modeled as a smooth area change with no loss coefficients: it is assumed that the entering flow occupies the same area as the top of the inner cone, and that the flow going down into the upper annulus occupies the same area as the annulus. The second junction is the connection from the outlet of this component to the inlet of the relief valve inlet piping, Component 390. It is modeled as an abrupt area change with user-input loss coefficients based on the flow area ratios of the pipe and steam dome. Heat Structure 3550 (upper head) is attached to this component.

Component 360 is the steam annulus, the region between the upper cone and the outer shell. It is modeled as a downward-oriented branch with two junctions. The volume includes the region between the inner cone and the upper shell, and a small cylindrical section below between the inner shell and the flange. The first junction is the inlet from Component 355, which is modeled as a smooth area change with no loss coefficients. The second junction is the connection to the steam line, which is modeled as being from the side of this volume to the inlet of Component 365; the steam line area and hydraulic diameter are used for the junction. Momentum flux is turned on, as there should be a radial component to the flow in the facility as it moves around the inner cone to the steam line. The abrupt area change flag is set to 2, with loss coefficients based on an abrupt area change from the crossflow area into the pipe. Heat Structure 3400 (steam generator shell) is attached to this component.

Component 365 is the 4-in. piping in the steam line. It includes valve PCV-602 (Component 370), which is located at the end of the pipe section in the model. It is modeled using a single volume component. The check valve in this line (V-601) is not modeled explicitly. The component length is estimated, and will not have any effect on the calculated behavior in the steam generator as the steam dome pressure is controlled during steady-state operation, and the steam generator is expected to be isolated during most transients.

Component 370 is the pressure control valve (PCV-602). It connects the outlet of Component 365 to the inlet of Component 375, and is modeled as a servo valve controlled by CV 370. The flow area is the same as that of the upstream volume (Component 365). The abrupt area change model is used with code-calculated loss coefficients (flag $a = 1$). The valve area is modeled as changing linearly with the stem position. The valve is expected to be closed during transient calculations; even if it is not, the steam generator tubes will be isolated on the primary system side, so that any residual heat transfer in the steam generator will not affect the plant response of interest.

Component 375 is the pressure boundary volume downstream of the pressure control valve. It is modeled as a steam-filled volume at atmospheric pressure.

Component 390 is the pipe from the steam generator dome to valve PSV-600 (Component 395). It is modeled as a single volume component.

Component 395 is the pressure relief valve (PSV-600). It is modeled as a trip valve connecting the outlet of Component 390 to the inlet of Component 398. The valve is open when trip 1395 is true. The abrupt area change model is used with code-calculated loss coefficients. The flow area of the valve is set to that of the pipe, and will be adjusted when performance data for the valve are available.

Component 398 is the pressure boundary volume downstream of the pressure relief valve. It is modeled as a steam-filled volume at atmospheric pressure.

5.4 Potable Water Supply System

Choking is turned off (flag $c = 1$) at all junctions in this system.

Component 400 is the supply pressure boundary volume for the potable water system. It contains 290 K water at a pressure of 400 kPa (assumed values pending receipt of actual data).

Component 410 is level control valve LCV-010. It connects the outlet of Component 400 to the inlet of Component 420, and is modeled as a servo valve controlled by CV 410. The valve area is modeled as changing linearly with the stem position. The abrupt area change model is used with code-calculated loss coefficients, and choking is turned off. A very small flow is maintained through the valve to avoid occasional code thermodynamic property failures in Component 420.

Component 420 is the piping between the level control valve and tank T-010 (Component 450). It is modeled as a branch with one junction, with an assumed length long enough to prevent this volume from controlling the Courant limit. The junction connects the outlet of this component to the inlet of Component 450. User-input loss coefficients are for an abrupt area change (flag $a = 2$) between the small pipe and the large tank.

Component 450 is the RCCS/coolant day tank, tank T-010. It is modeled as a 6-volume pipe. The mixture level tracking model is turned on where permitted to try to prevent air from entering the feedwater or RCCS lines. The thermal stratification model is turned on where permitted to keep hot water returning from the RCCS panels segregated from the cooler water in the tank, and to segregate the colder supply water being added at the bottom of the tank. There are no heat structures modeling the tank wall, as heat transfer to the wall is not expected to be important to either the steam generator or RCCS behavior.

Component 460 is the tank T-010 outlet line, which provides feedwater to both the steam generator and the RCCS. It is modeled as a branch with one junction. The junction connects the bottom of the tank, the inlet of Component 450, to the inlet of this component. There are no details about the pipe configuration. Since the important part of this section of pipe is the elevation change, which provides the head at the pump suction, the pipe is modeled as a straight vertical run. There is no heat structure modeling the pipe wall, as heat transfer in this piping is not expected to be important to either the steam generator or RCCS behavior.

Component 490 is the vent/overflow line on tank T-010. It is modeled as a branch with two junctions. Its length is sufficient to allow the pipe to exit the bottom of the tank; piping beyond this is neglected. Junction 1 connects the outlet of cell 5 of Component 450 to the inlet of this component. Junction 2 connects the outlet of this component to the inlet of Component 498. Both junctions are modeled as abrupt area changes (flag $a = 2$) with user-input loss coefficients for a contraction or expansion with a large area change.

Component 498 is the pressure boundary volume at the end of the vent/overflow line on tank T-010, Component 490. It is filled with 295 K air at atmospheric pressure.

5.5 Alternate Break Piping

These components are not active in the base input model, but are activated as needed for the specific transient being modeled.

Component 5 is the junction between the upper plenum and the control rod drive break nozzle. It is modeled as a single junction connecting the outlet of Component 120 to the inlet of Component 10. The abrupt area change model is used with user-defined loss coefficients (flag $a = 2$). The loss coefficients are based on the area change between the top of the plenum and the nozzle interior.

Component 10 is the control rod drive break nozzle from the inlet to the center of the piping offtake. It is modeled as a pipe with 25 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model.

Heat Structure 0100 (pipe wall) is attached to this component.

Component 15 is the junction between the control rod drive break nozzle and the piping. It is modeled as a single junction connecting the outlet of Component 10 to the inlet of Component 20. It uses the abrupt area change model with user-input loss coefficients (flag a = 2); the loss is approximated as that through the branch of a tee.

Component 20 is the piping between the control rod drive break nozzle and valve V-332 (Component 25). It is modeled as a pipe with 35 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model. Heat Structure 0200 (pipe wall) is attached to this component.

Component 25 is the control rod drive break valve, V-332. It is modeled as a trip valve, using trip 625. It connects the outlet of Component 20 to the inlet of Component 30. The abrupt area change model is used (flag a = 2) with user-input loss coefficients. The loss coefficients are based on a large flow through the valve, but minimal flow is expected during transients when this valve is open.

Component 30 is the first third of the piping between valve V-332 and the RCST. It is modeled as a pipe with 92 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model. Heat Structure 0300 (pipe wall) is attached to this component.

Component 31 is a single junction connecting the outlet of Component 30 to the inlet of Component 32. It uses the smooth area change model with no loss coefficients.

Component 32 is the middle third of the piping between valve V-332 and the RCST. It is modeled as a pipe with 92 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model. Heat Structure 0320 (pipe wall) is attached to this component.

Component 33 is a single junction connecting the outlet of Component 32 to the inlet of Component 34. It uses the smooth area change model with no loss coefficients.

Component 34 is the final third of the piping between valve V-332 and the RCST. It is modeled as a pipe with 92 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model. Heat Structure 0340 (pipe wall) is attached to this component.

Component 35 is a single junction connecting the outlet of Component 34 to the top of the RCST, Component 280. It uses the abrupt area change model (flag a = 2) with user-input loss coefficients representing the large area change between the pipe and the tank.

Component 55 is the junction between the coolant region below the core support plate and the vessel bottom break line nozzle stub. It is modeled as a single junction connecting the bottom of the middle of the first volume in Component 105 to the inlet of Component 60. This connection places the nozzle somewhat higher in the model than in the facility, but the distortion is not expected to be significant for the transients in which the vessel bottom break line is active. The abrupt area change model is used with user-defined loss coefficients (flag a = 2). The loss coefficients are based on the area ratio between the lower support plate and the nozzle stub. Momentum flux is turned off on the vessel side of the junction (flag s = 2).

Component 60 is the vessel bottom break line nozzle stub. It is modeled as a pipe with 43 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model.

Component 65 is the junction between the bottom break line nozzle stub and the bottom break line piping. It is modeled as a single junction connecting the outlet of Component 60 to the inlet of Component 70. It used the abrupt area change model with user-input loss coefficients (flag a = 2).

Component 70 is the first half of the vessel bottom break line piping between the pressure vessel nozzle stub and valve V-331 (Component 75). It is modeled as a pipe with 73 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model. Heat Structure 0700 (pipe wall) is attached to this component.

Component 71 is a single junction connecting the outlet of Component 70 to the inlet of Component 72. It uses the smooth area change model with no loss coefficients.

Component 72 is the second half of the vessel bottom break line piping between the pressure vessel nozzle stub and valve V-331. It is modeled as a pipe with 73 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model. Heat Structure 0720 (pipe wall) is attached to this component.

Component 75 is the pressure vessel bottom break valve, V-331. It is modeled as a trip valve, using trip 675. It connects the outlet of Component 72 to the inlet of Component 80. The abrupt area change model is used (flag a = 2) with user-input loss coefficients. The loss coefficients are based on a large flow through the valve, but minimal flow is expected during transients when this valve is open.

Component 80 is the piping between valve V-331 and the RCST. It is modeled as a pipe with 96 volumes; the large number of volumes reflects the expectation that molecular diffusion will be the principal phenomenon occurring when this break is included in the model. Heat Structure 0800 (pipe wall) is attached to this component.

Component 85 is a single junction connecting the outlet of Component 80 to the bottom of the RCST, Component 280. It uses the abrupt area change model (flag a = 2) with user-input loss coefficients representing the large area change between the pipe and the tank.

5.6 Reactor Cavity and Reactor Cavity Cooling System

Choking is turned off (flag c = 1) at all junctions in the RCCS.

Component 900 is the reactor cavity between the primary pressure vessel and the RCCS panels, extending from the floor to the top of the RCCS panels. It is modeled as a single volume filled with air. An alternate model using a 20-volume pipe filled is included in the input deck for use with code versions in which the heat structure lengths cannot be input on the heat structure 500/600 series cards. The axial nodalization is consistent with the axial nodalization inside the primary pressure vessel. The only connection to the pipe is at the top, so an unphysical temperature profile will occur in the pipe if that nodalization is used. The single volume approach will overestimate the mixing in the cavity by making the air all the same temperature; this is expected to be closer to the actual conditions in the cavity than those that will be calculated using the pipe component. Three heat structures are attached to this component: Structure 1000 (pressure vessel wall), Structure 1001 (pressure vessel upper head), and Structure 9500 (RCCS panels).

Component 903 is a single junction connecting the top of the reactor cavity (outlet of Component 900) to the pressure boundary volume (inlet of Component 905).

Component 905 is the pressure boundary volume for the reactor cavity. It is a time-dependent volume containing 295 K air at a constant pressure of 100 kPa.

Component 915 is the alternate source volume for the RCCS pump. It is a time-dependent volume whose conditions need to be input by the user. The default conditions are 290 K water at a pressure of 100 kPa. This component is not active in the base input model.

Component 920 is the RCCS pump. It is modeled as a time-dependent junction, with the flow determined by CV 920. The suction is taken from the outlet of the water storage tank outlet line, Component 460, and the discharge is to the inlet of Component 930. Suction can also be taken from Component 915.

Component 930 is the piping between the RCCS pump outlet and the RCCS panel inlet headers. It also includes the short section of piping upstream of the pump, as well as the volumes in the pump and valves. The valves in this line (V-805 and PCV-807) are not modeled explicitly. This piping is modeled with a single volume component and no heat structures for the pipe walls, as heat transfer in this piping is not expected to be important to the RCCS behavior.

Component 940 represents the RCCS panel inlet headers. It is modeled as a branch with one junction, connecting the outlet of Component 930 to the inlet of this component. The junction is modeled as an abrupt area change (flag $a = 2$) with momentum flux turned off on the header side (flag $s = 1$). The loss coefficients are based on branching at a tee. There is no heat structure modeling the pipe wall, as heat transfer in this piping is not expected to be important to the RCCS behavior.

Component 945 represents the RCCS panel inlet lines. The valves in the lines are not modeled explicitly. The inlet lines are modeled as a branch with two junctions. The first junction connects the outlet of Component 940 to the inlet of this component. The second junction connects the outlet of this component to the inlet of the RCCS panels, Component 950. Since the RCCS flow is being provided by a time-dependent junction, the pressure loss in the piping is not important (the flow rate does not depend on a balance between the pump head and the piping pressure loss), and loss coefficients of 0.0 are entered for the junctions for simplicity. There is no heat structure modeling the pipe wall, as heat transfer in this piping is not expected to be important to the RCCS behavior.

Component 950 represents the RCCS panels. They are modeled with a 19-volume pipe. The axial nodalization is consistent with the axial nodalization inside the primary pressure vessel. Two heat structures are connected to this component: Structure 9500, which represents the surface facing the primary pressure vessel, and Structure 9501, which represents the back side of the panels, are connected to this component. Two heat structures are attached to this component: Structure 9500 (front panels) and Structure 9501 (back panels).

Component 955 represents the RCCS outlet lines leading to the outlet headers. They are modeled with a two-junction branch component. The first junction connects the outlet of the RCCS panels (Component 950) to the inlet of this component, and the second junction connects the outlet of this component to the inlet of Component 960. Since the RCCS flow is being provided by a time-dependent junction, the pressure loss in the piping is not important (the flow rate does not depend on a balance between the pump head and the piping pressure loss), and loss coefficients of 0.0 are entered for the junctions for simplicity. There is no heat structure modeling the pipe wall, as heat transfer in this piping is not expected to be important to the RCCS behavior.

Component 960 represents the RCCS outlet headers. The two 1-in. headers are lumped together with the two 1.5-in. pipes into a single branch component with one junction connecting the outlet of this component to the middle of the fifth cell in Component 450, the RCCS water storage tank. If water is not being recirculated to the storage tank, flow is discharged to Component 965. The hydraulic diameter of the 1-in. pipe is used, as the pressure drop through this piping is not important to the facility response. The junction loss coefficients represent the large area change between the piping and the tank. There is no heat structure modeling the pipe wall, as heat transfer in this piping is not expected to be important to the RCCS behavior.

Component 965 is the alternate sink volume for the RCCS flow, used when flow is not modeled as being recirculated to the water storage tank (Component 450). It is modeled using a time-dependent volume with constant conditions of 290 K water at a pressure of 100 kPa. This component is not active in the base input model.

6. HEAT STRUCTURES

The core region is modeled with two heat structures in each channel. The first structure is centered on a coolant channel, and models the ceramic material. The second structure represents the heater rods, and is modeled as a solid cylinder that radiates heat to the outer surface of the ceramic structure. The “dog bone” shape of the individual heater rodlets is approximated by a cylinder of the same length that preserves the total mass of graphite. This results in about a 10% larger diameter than the actual diameter of the cylindrical portion of the rodlet. This will slightly distort the surface temperature of the rodlet (lower than expected) because of the larger surface area, but this is offset somewhat by modeling only radiation heat transfer, and not convection or conduction, from the heater rods to the ceramic.

The Gnielinski correlation is being used for the core coolant channels. This is implemented by using heat transfer package 160 on the 500/600 series input cards (Word 3). Two-dimensional (2-D) conduction is used in most vertical structures. Dummy values are usually entered for the input on the 800 and 900 series cards related to critical heat flux parameters. With a single-phase vapor coolant, critical heat flux will not be a concern; the exception is the secondary side of the steam generator tubes.

The thickness of the middle rings of the central and side reflectors will likely need to be adjusted based on system characterization data. The amount of material that is influenced by the coolant channels is just estimated in this original model development effort, as appropriate measured data are not yet available.

6.1 Primary Pressure Vessel

Structure 1000 is the cylindrical portion of the primary pressure vessel. It has 17 axial structures (cell 1 is at the bottom), is made of 304 stainless steel [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 1, Rev. 0, items 2 and 3], and is connected to Components 100 and 115 on the left side and Component 900 on the right side. Axial conduction is turned on, and the node lengths are input on the 600 series cards. The left side is in a radiation enclosure (Enclosure 19) with the core barrel and the jacket shell, and the right side is in a radiation enclosure (Enclosure 21) with the RCCS.

Structure 1001 includes both the primary pressure vessel upper head and the upper plenum shield, since the volume between these two structures is filled with insulation. The upper head is made of 304 stainless steel [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 1, Rev. 1, item 1]. The upper plenum shield is made of Haynes 230 [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 6, Rev. 1, items 90-93]. The insulation is Cerablanket (alumina-silica). The structure is connected to Component 120 on the left side and Component 900 on the right side. The left side is in a radiation enclosure (Enclosure 16) with other structures in the upper plenum, and the right side is in a radiation enclosure (Enclosure 21) with the RCCS.

Structure 1002 is the primary pressure vessel lower head. It is modeled as a hemisphere, is made of 304 stainless steel [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 1, Rev. 1, item 1], and is connected to Component 190 on the left side and Component 900 of the right side. The right side is in a radiation enclosure (Enclosure 21) with the RCCS.

Structure 1050 is the middle distributor plate in the coolant inlet region below the outlet plenum. It is a single, horizontal rectangular structure made of 304 stainless steel [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 6, Rev. 1, item 103], connected to volume 105-01 on the bottom and volume 105-02 on the top.

Structure 1100 is the jacket shell, the outer plate forming the coolant upcomer between the core barrel and the primary pressure vessel in the lower vessel region. It has one axial structure, is made of 304 stainless steel [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 6, Rev. 1, item 85], and is connected to Component 110 on the left side and Component 100 on the right. Both sides of the structure are in a radiation enclosure (Enclosure 19) with the core barrel and primary pressure vessel shell.

Structure 1150 is the core barrel. It has 16 axial structures (cell 1 is at the bottom), is made of 304 stainless steel [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 6, Rev. 1, item 86], and is connected to Components 105, 166, and 175 on the left side and Components 100, 110, and 115 on the right side. Axial conduction is turned on. The left side of the structure is in a radiation enclosure (Enclosure 15) with the outer reflector, and the right side is in a radiation enclosure (Enclosure 19) with the primary pressure vessel barrel and the jacket shell.

Structure 1200 is the upper plenum cylinder. It has one axial structure, connected to Component 120 on the left side and Component 115, cell 15 on the right side. It is made of Haynes alloy 230 [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 6, Rev. 1, item 90]. The height of the structure extends only to the top of the pressure vessel cylinder, as the remainder of the upper plenum cylinder is included in the upper head/upper plenum shield structure (Structure 1001). The left side of the structure is in a radiation enclosure (Enclosure 16) with other structures in the upper plenum. The right side of the structure is in a radiation enclosure (Enclosure 19) with the primary pressure vessel cylinder.

Structure 1201 is the upper plenum floor. It is made of graphite [Drawing OSU-HTTF-PRIM-DWG-002, Sheet 6, Rev. 1, item 110], and is connected to Component 120 on the right side. The left side is not connected to a fluid volume, but is in a conduction enclosure (Enclosure 2) with the upper reflector portion of each of the core region heat structures; the right side is in a radiation enclosure (Enclosure 16) with other structures in the upper plenum.

Structure 1202 represents the upper plenum internals. It is made of 304 stainless steel, and is connected to Component 120 on the right side; the left side is adiabatic. The right side is in a radiation enclosure (Enclosure 16) with other structures in the upper plenum.

Structure 1300 is the center cylindrical region of the central reflector, which is made of Greencast ceramic. Its 14 axial cells (cell 1 is at the top) extend from the top of the upper reflector to the bottom of the lower reflector. Neither side of the structure is connected to a fluid volume. Steady-state initialization is turned off to avoid convergence problems during input processing. The right side of the structure is in a conduction enclosure (Enclosure 1) with the other two sections of the central reflector, Structures 1320 and 1340. 2-D conduction is turned on, with heat structure lengths input on the 600 series cards.

Structure 1320 is the middle ring of the central reflector, which is made of Greencast ceramic. Its 14 axial cells (cell 1 is at the top) extend from the top of the upper reflector to the bottom of the lower reflector. The left side of the structure is connected to Component 132. Steady-state initialization is turned off to avoid convergence problems during input processing. The left side of cell 14 is in a radiation enclosure (Enclosure 18) with other structures in the outlet plenum. The right side is in a conduction enclosure (Enclosure 1) with Structures 1300 and 1340. 2-D conduction is turned on.

Structure 1340 is the outer ring of the central reflector, which is made of Greencast ceramic. Its 14 axial cells (cell 1 is at the top) extend from the top of the upper reflector to the bottom of the lower reflector. Neither side of the structure is connected to a fluid volume. Steady-state initialization is turned off to avoid convergence problems during input processing. The left side of the structure is in a conduction enclosure (Enclosure 1) with Structures 1300 and 1320. The right side is in a conduction enclosure (Enclosure 2) with the three core channels and the inner ring of the outer reflector. 2-D conduction is turned on, with heat structure lengths input on the 500 series cards.

Structure 1400 is the upper reflector above the inner core ring. It is made of Greencast ceramic, and has two axial cells. 2-D conduction is turned on. The left side of the structure is connected to Component 140 and the right side is adiabatic. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate.

Structure 1401 is the ceramic in the heated region of the inner core ring. It is made of Greencast ceramic, and has 10 axial cells (cell 1 is at the top) extending over the heated length of the core. 2-D conduction is turned on. The left side of the structure is connected to Component 140, and the right side is

connected to Component 141. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate; the only axial conduction modeled in the enclosure for this structure is from the ends to the top and bottom reflectors. The right side of the structure is in a radiation enclosure (Enclosure 11) with the heater rod, Structure 1403.

Structure 1402 is the bottom reflector below the inner core ring. It is made of Greencast ceramic, and has two axial cells. 2-D conduction is turned on. The left side of the structure is connected to Component 140. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate. The right side of the second cell is in a radiation enclosure (Enclosure 18) with other structures in the outlet plenum.

Structure 1403 represents the heater rods in the inner core ring. It is made of graphite and has 10 axial cells. 2-D conduction is turned on. Both sides of the structure are adiabatic, but the right side is in a radiation enclosure (Enclosure 11) with Structure 1401. The internal heat source is provided by CV 940.

Structure 1450 is the upper reflector above the middle core ring. It is made of Greencast ceramic, and has two axial cells. 2-D conduction is turned on. The left side of the structure is connected to Component 145 and the right side is adiabatic. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate.

Structure 1451 is the ceramic in the heated region of the middle core ring. It is made of Greencast ceramic, and has 10 axial cells (cell 1 is at the top) extending over the heated length of the core. 2-D conduction is turned on. The left side of the structure is connected to Component 145, and the right side is connected to Component 146. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate; the only axial conduction modeled in the enclosure for this structure is from the ends to the top and bottom reflectors. The right side of the structure is in a radiation enclosure (Enclosure 12) with the heater rod, Structure 1453.

Structure 1452 is the bottom reflector below the middle core ring. It is made of Greencast ceramic, and has two axial cells. 2-D conduction is turned on. The left side of the structure is connected to Component 145. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate. The right side of the second cell is in a radiation enclosure (Enclosure 18) with other structures in the outlet plenum.

Structure 1453 represents the heater rods in the middle core ring. It is made of graphite and has 10 axial cells. 2-D conduction is turned on. Both sides of the structure are adiabatic, but the right side is in a radiation enclosure (Enclosure 12) with Structure 1451. The internal heat source is provided by CV 945.

Structure 1500 is the upper reflector above the outer core ring. It is made of Greencast ceramic, and has two axial cells. 2-D conduction is turned on. The left side of the structure is connected to Component 150 and the right side is adiabatic. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate.

Structure 1501 is the ceramic in the heated region of the inner core ring. It is made of Greencast ceramic, and has 10 axial cells (cell 1 is at the top) extending over the heated length of the core. 2-D conduction is turned on. The left side of the structure is connected to Component 150, and the right side is connected to Component 151. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate; the only axial conduction modeled in the enclosure for this structure is from the ends to the top and bottom reflectors. The right side of the structure is in a radiation enclosure (Enclosure 13) with the heater rod, Structure 1503.

Structure 1502 is the bottom reflector below the outer core ring. It is made of Greencast ceramic, and has two axial cells. 2-D conduction is turned on. The left side of the structure is connected to Component 150. The left side is in a conduction enclosure (Enclosure 2) with the other core channels, the outer ring of the inner reflector, the inner ring of the outer reflector, and the upper plenum plate. The right side of the second cell is in a radiation enclosure (Enclosure 18) with other structures in the outlet plenum.

Structure 1503 represents the heater rods in the outer core ring. It is made of graphite and has 10 axial cells. 2-D conduction is turned on. Both sides of the structure are adiabatic, but the right side is in a radiation enclosure (Enclosure 13) with Structure 1501. The internal heat source is provided by CV 950.

Structure 1600 is the inner ring of the side reflector, which is made of Greencast ceramic. Its 14 axial cells (cell 1 is at the top) extend from the top of the upper reflector to the bottom of the lower reflector. Neither side of the structure is connected to a fluid volume. Steady-state initialization is turned off to avoid convergence problems during input processing. The left side of the structure is in a conduction enclosure (Enclosure 2) with the three core channels and the outer ring of the central reflector. The right side of the structure is in a conduction enclosure (Enclosure 3) with the other two sections of the side reflector, Structures 1620 and 1640. 2-D conduction is turned on, with heat structure lengths input on the 500 series cards.

Structure 1620 is the middle ring of the side reflector, which is made of Greencast ceramic. Its 14 axial cells (cell 1 is at the top) extend from the top of the upper reflector to the bottom of the lower reflector. The left side of the structure is connected to Component 132. Steady-state initialization is turned off to avoid convergence problems during input processing. The left side of cell 14 is in a radiation enclosure (Enclosure 18) with other structures in the outlet plenum. The right side is in a conduction enclosure (Enclosure 3) with structures 1300 and 1340. 2-D conduction is turned on.

Structure 1640 is the outer ring of the side reflector, which is made of Greencast ceramic. Its 14 axial cells (cell 1 is at the top) extend from the top of the upper reflector to the bottom of the lower reflector. The right side of the structure is connected to Component 164. Steady-state initialization is turned off to avoid convergence problems during input processing. 2-D conduction is turned on. The left side of the structure is in a conduction enclosure (Enclosure 3) with Structures 1600 and 1620. The right side is in a radiation enclosure (Enclosure 14) with the outer reflector, Structure 1660.

Structure 1660 is the outer reflector, which is made of Shot-Tech SiC 80 ceramic. Its 15 axial cells (cell 1 is at the top) extend from the top of the upper reflector to the bottom of the outlet plenum. 2-D conduction is turned on. The left side of the structure is connected to Components 164 and 175, and the right side is connected to Component 166. Most of the left side is in a radiation enclosure (Enclosure 14) with the outer surface of the side reflector, Structure 1640, and the right side is in a radiation enclosure (Enclosure 15) with the core barrel, Structure 110; the left side of cell 15 is in a radiation enclosure (Enclosure 18) with other structures in the outlet plenum.

Structure 1750 represents the outlet plenum bottom plate, which is a composite horizontal structure that includes the outlet plenum bottom plate on the top, the upper bulkhead plate on the bottom, and insulation in between. The top of the structure is connected to Component 175, and the bottom is connected to Component 105. The top surface is in a radiation enclosure (Enclosure 18) with other structures in the outlet plenum.

Structure 1751 represents the support posts in the outlet plenum, which are made of Greencast ceramic. The right side of this solid cylinder is connected to Component 175 and is in a radiation enclosure (Enclosure 18) with other structures in the outlet plenum.

6.2 Primary Coolant System

Structure 2000 is the structure separating the hot and cold ducts. It is connected to Component 200 on the left side and to Component 270 on the right side. It consists of two cylinders of 304 stainless steel with a 3/8 in. layer of alumina silica insulation between them [Drawing OSU-HTTF-PRIM-DWG-005A,

Rev. 0, items 8-13].

Structure 2001 is the section of the hot duct from the end of the cold duct to the outlet of the isolation/break valve. It is a cylindrical structure with 304 stainless steel on the inside and insulation on the outside. It is connected to cells 5 and 6 of Component 200 on the left side, with a natural convection heat transfer coefficient from Table 951 on the right side and a heat sink temperature provided by Table 950.

Structure 2100 is the section of hot duct between the isolation/break valve and the RCST. It is a cylindrical structure made of 304 stainless steel. Since most of this pipe is on the inside of the RCST, it is modeled without insulation on the outside. It is connected to Component 210 on the left side and Component 280 on the right side.

Structure 2150 is the pipe between the hot duct and the steam generator inlet plenum. The geometry of the structure in this region is complicated, including the check valve body and a gap between the liner and the nozzle. This will be approximated by a single 304 stainless steel [Drawing OSU-HTTF-PRIM-DWG-005A, Rev. 0, items 5 and 6] cylindrical structure with an inner radius of that of the inner sleeve and an outer steel radius of the steam generator nozzle; a layer of insulation completes the structure. It is connected to Component 215 on the left side, with a natural convection heat transfer coefficient from Table 951 on the right side and a heat sink temperature provided by Table 950.

Structure 2200 is the inlet plenum portion of the steam generator shell. It is modeled as a 304 stainless steel [Drawing OSU-HTTF-SEC-DWG-003A, Rev. 0, items 8, 36, and 37] cylinder whose inner surface area and total volume are equal to those that of the inlet plenum, inlet nozzle stub, and inlet elbow. The left side is connected to Component 220, and the right side has a heat transfer coefficient boundary condition applied to the outside of the insulation (from Table 951) with a heat sink temperature provided by Table 950. The thin (0.024 in.) aluminum jacket on the outside of the insulation is not modeled, as it will provide a negligible resistance to heat transfer compared to the low thermal conductivity of the insulating material.

Structure 2201 is the dividing plate (“pass partition”) between the inlet and outlet plena of the steam generator. It is made of 304 stainless steel [Drawing OSU-HTTF-SEC-DWG-003A, Rev. 0, item 10]. It is modeled as a rectangular structure, connected to Component 220 on the left side and to Component 228 on the right side.

Structure 2250 represents the 188 steam generator tubes. The tubes are made of 304 stainless steel [Drawing OSU-HTTF-SEC-DWG-003A, Rev. 0, item 2]. The left side is connected to Component 225, and the right side is connected to Component 350. The right side uses the rod bundle with crossflow heat transfer package, as the baffle plates should force some flow across the tubes. Axial conduction is turned on in the tubes because large temperature gradients are expected along the tubes.

Structure 2251 represents the tube sheet. It is modeled as a 304 stainless steel [Drawing OSU-HTTF-SEC-DWG-003A, Rev. 0, item 1] cylindrical structure with two axial nodes: the first models the half of the tube sheet connected to the inlet end of the steam generator tubes, and the second models the half connected to the outlet end of the tubes. The structure is built around a unit cell, the inner radius being the inner radius of the tubes and the outer radius determined by conservation of mass (area). There are 188 of these unit cells in each half of the tube sheet. Heat transfer from the faces of the tube sheet to the boiler region and to the plena is not modeled as it is expected to be much smaller than the heat transfer in the flow passages.

Structure 2280 is the outlet plenum portion of the steam generator shell. It is modeled as a 304 stainless steel [Drawing OSU-HTTF-SEC-DWG-003A, Rev. 0, items 8, 38, and 39] cylinder whose inner surface area and total volume are equal to those that of the outlet plenum, outlet nozzle stub, and outlet elbow. The left side is connected to Component 228, and the right side has a natural convection heat transfer coefficient boundary condition applied to the outside of the insulation (from Table 951) with a heat sink temperature provided by Table 950. The thin (0.024 in.) aluminum jacket on the outside of the insulation is not modeled, as it will provide a negligible resistance to heat transfer compared to the low

thermal conductivity of the insulating material.

Structure 2300 is the pipe between the steam generator outlet plenum and the circulator. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and one axial structure. The left side is connected to Component 230, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 2350 is the circulator body. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and one axial structure. The left side is connected to Component 235, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 2400 is the pipe between the circulator outlet and valve V-203. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and one axial structure. The left side is connected to Component 240, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 2500 is the pipe between valve V-203 and the cold leg break valve. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and three axial structures. The left side is connected to Component 250, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 2580 is the section of cold leg between the break valve and the RCST. It is a cylindrical structure made of 304 stainless steel. Since most of this pipe is on the inside of the RCST, it is modeled without insulation on the outside. It is connected to Component 258 on the left side and Component 280 on the right side.

Structure 2600 is the crossover line between the cold leg and the cold duct. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and one axial structure. The left side is connected to Component 260, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 2700 is the outer wall of the cold duct. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and four axial structures. The left side is connected to Component 270, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 2800 is the RCST wall. It is a cylindrical structure with 304 stainless steel on the inside [Drawing OSU-HTTF-RCSS-DWG-008A, Sheet 1, Rev. 0, items 1 and 2], insulation on the outside, and either one or two axial structures. The mass of the heads is not completely accounted for with this modeling approach. The left side of the structure is connected to Component 280. The right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950. The thin (0.024 in.) aluminum jacket on the outside of the insulation is not modeled, as it will provide a negligible resistance to heat transfer compared to the low thermal conductivity of the insulating material.

Structure 2820 is the hot duct break spool piece. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and one axial structure. The left side of the structure is connected to Component 282, and the right side is connected to Component 280.

6.3 Secondary Coolant System

Structure 3400 is the steam generator outer cylindrical shell, modeled with 13 axial structures. It is made of 304 stainless steel [Drawing OSU-HTTF-SEC-DWG-003A, Rev. 0, items 4 and 5]. The thicker wall just above the tube sheet is ignored. Most of the left side is connected to Component 340, with the bottom node being connected to the first volume in Component 350 and the top node being connected to Component 360. The right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950. The thin (0.024 in.) aluminum jacket on the outside of the

insulation is not modeled, as it will provide a negligible resistance to heat transfer compared to the low thermal conductivity of the insulating material.

Structure 3500 is the steam generator inner cylindrical shell separating the downcomer from the boiler. The shell is made of 304 stainless steel [Drawing OSU-HTTF-SEC-DWG-003A, Rev. 0, item 11]. It has 11 axial nodes, and is connected to the boiler (Component 350) on the left side and the downcomer (Component 340) on the right side. The portion of the cylinder above the top of the downcomer is neglected, as there is expected to be little temperature difference between the top of the boiler and the steam annulus region, and stored energy in the steam generator structures is not expected to be important in the transients to be simulated.

Structure 3550 is the steam generator upper head. The head is made of 304 stainless steel [Drawing OSU-HTTF-SEC-DWG-003A, Rev. 0, item 7]. The left side is connected to Component 355, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950. The thin (0.024 in.) aluminum jacket on the outside of the insulation is not modeled, as it will provide a negligible resistance to heat transfer compared to the low thermal conductivity of the insulating material.

6.4 Alternate Break Piping

Structure 0100 is the pressure vessel control rod drive break nozzle. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and the same number of axial structures as the attached pipe has volumes (25). The left side is connected to Component 10, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 0200 is the section of piping between the pressure vessel control rod drive break nozzle and valve V-332. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and the same number of axial structures as the attached pipe has volumes (35). The left side is connected to Component 20, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 0300 is the first third of the piping between valve V-332 and the RCST. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and the same number of axial structures as the attached pipe has volumes (92). The left side is connected to Component 30, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 0320 is the middle third of the piping between valve V-332 and the RCST. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and the same number of axial structures as the attached pipe has volumes (92). The left side is connected to Component 32, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 0340 is the final third of the piping between valve V-332 and the RCST. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and the same number of axial structures as the attached pipe has volumes (92). The left side is connected to Component 34, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 0700 is the first half of the piping between the pressure vessel bottom break nozzle stub and valve V-331. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and the same number of axial structures as the attached pipe has volumes (73). The left side is connected to Component 70, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 0720 is the second half of the piping between the pressure vessel bottom break nozzle stub and valve V-331. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and the same number of axial structures as the attached pipe has volumes (73). The left side is connected to Component 72, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

Structure 0800 is the section of piping between valve V-331 and the RCST. It is a cylindrical structure with 304 stainless steel on the inside, insulation on the outside, and the same number of axial structures as the attached pipe has volumes (96). The left side is connected to Component 80, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950.

6.5 Reactor Cavity Cooling System

Structure 9500 is the front wall of the RCCS panels. The left side is connected to Component 900, and is in a radiation enclosure (Enclosure 21) with the primary pressure vessel. The right side is connected to Component 950.

Structure 9501 is the back wall of the RCCS panels. The left side is connected to Component 950, and the right side has a natural convection heat transfer coefficient from Table 951 and a heat sink temperature provided by Table 950. The thin (0.024 in.) aluminum jacket on the outside of the insulation is not modeled, as it will provide a negligible resistance to heat transfer compared to the low thermal conductivity of the insulating material.

7. ENCLOSURES

Both radiation and conduction enclosures are used in the model. The view factors in the radiation enclosures with concentric vertical structures are strictly radial, assuming that the cross-product terms between different axial levels will balance out enough to make them a second-order effect.

Enclosure 1 (601xxxxx cards) models the radial conduction between the three structures in the central reflector (Structures 1300, 1320, and 1340). It uses a temperature-dependent conductance from Table 601.

Enclosure 2 (602xxxxx cards) models the conduction in the core (heater rod) region. It includes radial conduction between the ceramic structures in the three core channels (Structures 1401, 1451, and 1501), as well from the core to the adjacent central and side reflector structures (Structures 1340 and 1600, respectively). It models axial conduction from the core ceramic structures to the top and bottom reflector structures (Structures 1400, 1402, 1450, 1452, 1500, and 1502). It also models conduction from the upper reflector structures to the upper plenum plate (Structure 1201). It uses a temperature-dependent conductance from Table 601.

Enclosure 3 (603xxxxx cards) models the radial conduction between the three structures in the side reflector (Structures 1600, 1620, and 1640). It uses a temperature-dependent conductance from Table 601.

Enclosure 11 (611xxxxx cards) models the radiation from the heater rods (Structure 1403) to the ceramic (Structure 1401) in the inner core ring.

Enclosure 12 (612xxxxx cards) models the radiation from the heater rods (Structure 1453) to the ceramic (Structure 1451) in the middle core ring.

Enclosure 13 (613xxxxx cards) models the radiation from the heater rods (Structure 1503) to the ceramic (Structure 1501) in the outer core ring.

Enclosure 14 (614xxxxx cards) models the radiation from the side reflector (Structure 1640) to the outer reflector (Structure 1660).

Enclosure 15 (615xxxxx cards) models the radiation from the outer reflector (Structure 1660) to the core barrel (Structure 1150).

Enclosure 16 (616xxxxx cards) models the radiation between the upper plenum plate (Structure 1201), upper plenum internals (Structure 1202), upper plenum shield (Structure 1001), and upper plenum cylinder (Structure 1200).

Enclosure 18 (618xxxxx cards) models the radiation between the core bottom reflector (Structures 1320, 1402, 1452, 1502, 1620), outlet plenum side reflector (Structure 1660), lower plenum bottom plate (Structure 1750), and lower plenum posts (Structure 1751).

Enclosure 19 (619xxxxx cards) models the radiation from the core barrel (Structure 1150) and upper plenum cylinder (Structure 1200) to the primary pressure vessel wall (Structure 1000). In the outlet plenum region, the core barrel radiates to the inner surface of the jacket shell (Structure 1100), and the outer surface of the jacket shell then radiates to the primary pressure vessel wall. Although the jacket shell extends below the outlet plenum, its total length is included in the radiation at the outlet plenum level.

Enclosure 21 (621xxxxx cards) models the radiation from the primary pressure vessel (Structures 1000, 1001, and 1002) to the RCCS panels (Structure 9500).

8. MATERIALS

Material 1 is Greencast-94F Plus ceramic. It is used in the core, central and side reflectors, top and bottom reflectors, and the posts in the outlet plenum. The product data sheet^a had thermal conductivity values for five temperatures, but temperatures both above and below the range of these data are expected. A third-order curve fit was used (R^2 value of 0.9994) to extrapolate the measured data. Data for specific heat capacity and emissivity were contracted by Oregon State University (Larsen 2012) and are used in the input model. Only four emissivity data points are available, with a maximum temperature of 150°C, which is well below the normal operating temperature of the facility. Extrapolating these data using a quadratic or cubic fit resulted in negative emissivities near the nominal steady state operating temperatures. A linear fit was therefore used to extrapolate the data to higher temperatures; although the curve fit statistics were not particularly good (R^2 value of 0.977), the values were positive over the entire expected temperature range.

Material 2 is G320 graphite. It is used in the heater rods and the upper plenum floor. Density and thermal conductivity values were taken from the data provided in Figures 10-3 and 10-4 of Cadell 2011. Specific heat capacity values were obtained from Table A6.1 of ASTM International 2014. The emissivity used is the value for unoxidized carbon from Engineering Toolbox 2017.

Material 3 is Type 304 stainless steel. It is used in the pressure vessel, piping, and steam generator. Thermodynamic properties were obtained from Siefken et al. 2001. The emissivity used is the value for polished stainless steel from Engineering ToolBox 2017.

Material 4 is Haynes 230 alloy. It is used in the upper plenum cylinder. The emissivity used is the value for polished nickel from Engineering ToolBox 2017.

Material 5 is Shot-Tech SiC 80 ceramic. It is used in the outer reflector. The only needed property information on the ceramic product data sheet^a was the density. The value of 2.37 g/cm³ is used for the constant density. Thermal conductivity and specific heat capacity values are not available. With no other information, these data are taken from measurements of Thor 80 ceramic, which has a similar chemical composition, with somewhat more alumina and less silica than the Shot-Tech. No measurements of the emissivity of Shot-Tech were made; therefore data for Thor 80 will be used. Only four emissivity data points are available, with a maximum temperature of 150°C, which is well below the normal operating temperature of the facility. As for the Greencast ceramic, a linear fit of the four data points (R^2 value of 0.979) was used to extrapolate to higher temperatures.

Material 6 is Enerwrap MA 960 insulation (Roxul 2014). It is used for the permanent insulation on the outside of the large tanks and on the back side of the RCCS panels. Heat capacity information was not provided by the manufacturer, so it is assumed to be the same as that of mineral wool (Engineering Toolbox 2014).

Material 7 is structural insulation. It is used in the metallic core support structure.

Material 8 is alumina silica insulation. It is used in the upper plenum between the upper plenum shroud and the pressure vessel upper head and between the hot and cold ducts. The upper plenum insulation is McMaster-Carr Ultra-High Temperature Ceramic Insulation Roll; the associated safety data sheet identifies the product as Cerablanket from Morgan Advanced Materials. McMaster-Carr states the density is 4 lb/ft³, which corresponds to 64 kg/m³.

Material 9 is Lewco Needled E Glass Blanket fiberglass insulation (Lewco undated). It is the removable insulation used on the outside of the piping. Heat capacity information was not provided by the manufacturer, so it is assumed to be the same as that of glass wool.

Additional information on insulation was provided in Hertel 2014, Hertel 2015, and Woods 2017b.

^a Data sheets for the ceramics were provided to Idaho National Laboratory by HTTF personnel.

9. TRIPS

Trip 25 manually opens the control rod drive break valve, V-332, Component 25. It is set to be always false, and must be changed to open the valve.

Trip 75 manually opens the vessel bottom break valve, V-331, Component 75. It is set to be always false, and must be changed to open the valve.

Trip 100 is the scram trip. It is set to be always false, and must be changed to initiate a power decrease.

Trip 205 opens the hot duct break valve, V-313, Component 205. It is set to be always false, and must be changed to initiate a break.

Trip 206 closes the hot duct break valve, V-313, Component 205. It is set to be always false, and must be changed to reclose a break.

Trip 245 opens the loop isolation valve, V-203, Component 245. It is set to be always false, and the valve is initialized to be fully open.

Trip 246 closes the loop isolation valve, V-203, Component 245. It is set to be always false, and must be changed to close the valve.

Trip 255 opens the cold leg break valve, V-311, Component 255. It is set to be always false, and must be changed to initiate a break.

Trip 256 closes the cold leg break valve, V-311, Component 255. It is set to be always false, and must be changed to reclose a break.

Trip 294 is the opening (setpoint) pressure for the PCS relief valve, PSV-100, Component 295.

Trip 295 is the closing (reseat) pressure for the PCS relief valve, PSV-100, Component 295.

Trip 296 manually opens the depressurization valve, PCV-400, Component 296. It is set to be always false, and must be changed to open the valve.

Trip 297 manually closes the depressurization valve, PCV-400, Component 296. It is set to be always false, and must be changed to close the valve.

Trip 394 is the opening (setpoint) pressure for the steam generator relief valve, PSV-600, Component 395.

Trip 395 is the closing (reseat) pressure for the steam generator relief valve, PSV-600, Component 395.

Trip 410 is the low liquid level setpoint on tank T-010 for the water supply control logic.

Trip 411 is the high liquid level setpoint on tank T-010 for the water supply control logic.

Trip 412 is true if the liquid level in tank T-010 is above mid-range (halfway between open and close setpoints)

Trip 1294 is true if valve Component 295 either should open or is already open.

Trip 1295 opens the PCS relief valve, PSV-100, Component 295.

Trip 1296 opens the depressurization valve, Component 296.

Trip 1394 is true if valve Component 395 either should open or is already open.

Trip 1395 opens the steam generator relief valve, PSV-600, Component 395.

Trip 1409 is true if the tank T-010 water supply valve, Component 410, either should open or is already open.

Trip 1410 opens the tank T-010 water supply valve, Component 410, or maintains a higher flow until the liquid level is above mid-range.

Trip 1411 is true if the tank T-010 water supply valve, Component 410, either should close or is already closed.

Trip 1412 closes the tank T-010 water supply valve, Component 410, or maintains a lower flow until the liquid level is below mid-range.

10. GENERAL TABLES

Table 1 reproduces the volumetric heat capacity for Material 1. It is used in the calculation of the stored energy in the system.

Table 2 reproduces the volumetric heat capacity for Material 2. It is used in the calculation of the stored energy in the system.

Table 3 reproduces the volumetric heat capacity for Material 3. It is used in the calculation of the stored energy in the system.

Table 4 reproduces the volumetric heat capacity for Material 4. It is used in the calculation of the stored energy in the system.

Table 5 reproduces the volumetric heat capacity for Material 5. It is used in the calculation of the stored energy in the system.

Table 601 is the temperature-dependent conductance used in the core conduction enclosures.

Table 901 is the power in heater bank 101. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 902 is the power in heater bank 102. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 903 is the power in heater bank 103. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 904 is the power in heater bank 104. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 905 is the power in heater bank 105. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 906 is the power in heater bank 106. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 907 is the power in heater bank 107. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 908 is the power in heater bank 108. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 909 is the power in heater bank 109. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 910 is the power in heater bank 110. It includes a normalized power decay curve that can be adjusted depending on the scaling factors on time and power that are appropriate for the transient being simulated. Alternatively, the measured power from an experiment could be input directly into this table.

Table 950 is the building temperature, used as a boundary temperature for the back side of the RCCS panels and for the outside of insulated structures. It is set to 300 K.

Table 951 is the convective heat transfer coefficient boundary condition for the back side of the RCCS panels and for the outside of insulated structures. It is set to a value of 15 W/m²-K, which is a representative natural convection value.

11. CONTROL VARIABLES

CV 1 calculates the heat input (W) to the coolant in Component 140, the flow path through the core region inner ring.

CV 2 calculates the heat input (W) to the coolant in Component 145, the flow path through the core region middle ring.

CV 3 calculates the heat input (W) to the coolant in Component 150, the flow path through the core region outer ring.

CV 4 calculates the heat input (W) to the coolant in Component 132, the flow path through the central reflector cooling channels.

CV 5 calculates the heat input (W) to the coolant in Component 162, the flow path through the side reflector cooling channels.

CV 6 calculates the heat input (W) to the coolant in Component 164, the gas gap between the side and outer reflectors.

CV 7 calculates the heat input (W) to the coolant in Component 166, the gas gap between the outer reflector and the core barrel.

CV 8 calculates the heat input (W) to the coolant in Component 141, the gas gap around the heater rod in the core region inner ring.

CV 9 calculates the heat input (W) to the coolant in Component 146, the gas gap around the heater rod in the core region middle ring.

CV 10 calculates the heat input (W) to the coolant in Component 151, the gas gap around the heater rod in the core region outer ring.

CV 11 calculates the total heat input (W) to the gas in the core region by adding CVs 1–10.

CV 12 integrates the total heat input (J) to the gas in the core region, CV 11.

CV 13 calculates the total heat input (W) to the gas in the primary pressure vessel by taking the difference between the flow enthalpy leaving the vessel (Junction 175-01) and that entering (Junction 100-01). This will generally only be a valid calculation under steady forced convection flow conditions.

CV 14 calculates the total heat input (J) to the gas in the primary pressure vessel by integrating CV 13.

CV 16 calculates the heat input (W) to the coolant in Component 115, the gap between the core barrel and the primary pressure vessel.

CV 20 mimics the total flow (kg/s) through the core by taking the mass flow through Junction 175-01. A minimum value of 0.001 is applied to prevent division by zero during subsequent use of this flow rate.

CV 21 calculates the flow fraction through the central reflector cooling channel by dividing the flow through the channel outlet, Junction 1700101, by the total flow, CV 20.

CV 22 calculates the flow fraction through the core inner ring by dividing the flow through the channel outlet, Junction 1700102, by the total flow, CV 20.

CV 23 calculates the flow fraction through the core middle ring by dividing the flow through the channel outlet, Junction 1700103, by the total flow, CV 20.

CV 24 calculates the flow fraction through the core outer ring by dividing the flow through the channel outlet, Junction 1700104, by the total flow, CV 20.

CV 25 calculates the flow fraction through the side reflector cooling channel by dividing the flow through the channel outlet, Junction 1700105, by the total flow, CV 20.

CV 26 calculates the flow fraction through the gap between the side reflector and the outer reflector by dividing the flow through the channel outlet, Junction 1700106, by the total flow, CV 20.

CV 27 calculates the flow fraction through the gap between the outer reflector and the core barrel by dividing the flow through the channel outlet, Junction 1680000, by the total flow, CV 20.

CV 28 calculates the total core bypass flow fraction through the channels connected to the central and side reflectors.

CV 29 calculates the total core bypass flow fraction.

CV 31 calculates the total primary-to-secondary heat transfer rate (W) by summing the heat removal from the coolant in the steam generator tubes.

CV 32 calculates the total primary-to-secondary heat transfer rate (W) by summing the heat transfer out of the steam generator tube heat structures.

CV 33 calculates the total primary-to-secondary heat transfer rate (W) by summing the heat addition to the coolant in the steam generator boiler region.

CV 35 calculates the total energy transferred to the steam generator (W) by taking the difference between the flow enthalpy leaving the steam generator (Junction 360-02) and that entering (Junction 330-01). This will generally only be a valid calculation under steady forced convection flow conditions.

CV 36 integrates CV 35 to calculate the total net energy transferred to the steam generator secondary coolant (J).

CV 45 calculates the heat added by the circulator (W) by taking the difference between the flow enthalpy downstream (Junction 245) and upstream (Junction 235-01) of the circulator. This will generally only be a valid calculation under steady forced convection flow conditions.

CV 46 integrates CV 45 to calculate the total energy (J) added to the coolant by the circulator.

CV 95 calculates the heat input (W) to the coolant in Component 950, the RCCS panels.

CV 96 integrates CV 95 to calculate the total net heat input (J) to the coolant in the RCCS panels.

CV 98 calculates the net heat transfer to the RCCS coolant in the RCCS panels (W) by taking the difference between the flow enthalpy downstream (Junction 955-01) and upstream (Junction 945-02) of the panels. This will generally only be a valid calculation under steady forced convection flow conditions.

CV 99 integrates CV 98 to calculate the total net energy deposition in the RCCS coolant (J).

CV 100 calculates the maximum volume-average structure temperature (K) for the primary pressure vessel cylinder.

CV 101 calculates the peak volume-average structure temperature (K) for the primary pressure vessel cylinder.

CV 103 calculates the maximum volume-average structure temperature (K) for the core barrel.

CV 104 calculates the peak volume-average structure temperature (K) for the core barrel.

CV 120 calculates the maximum volume-average structure temperature (K) for the central reflector inner cylinder over the heated length of the core.

CV 121 calculates the maximum volume-average structure temperature (K) for the central reflector middle ring over the heated length of the core.

CV 122 calculates the maximum volume-average structure temperature (K) for the central reflector outer ring over the heated length of the core.

CV 123 calculates the maximum volume-average structure temperature (K) for the core inner ring ceramic over the heated length of the core.

CV 124 calculates the maximum volume-average structure temperature (K) for the core middle ring ceramic over the heated length of the core.

CV 125 calculates the maximum volume-average structure temperature (K) for the core outer ring ceramic over the heated length of the core.

CV 126 calculates the maximum volume-average structure temperature (K) for the side reflector inner ring over the heated length of the core.

CV 127 calculates the maximum volume-average structure temperature (K) for the side reflector middle ring over the heated length of the core.

CV 128 calculates the maximum volume-average structure temperature (K) for the side reflector outer ring over the heated length of the core.

CV 129 calculates the maximum volume-average structure temperature (K) for the outer reflector over the heated length of the core.

CV 130 calculates the peak volume-average structure temperature (K) achieved during the simulation for the central reflector center cylinder over the heated length of the core.

CV 131 calculates the peak volume-average structure temperature (K) achieved during the simulation for the central reflector middle ring over the heated length of the core.

CV 132 calculates the peak volume-average structure temperature (K) achieved during the simulation for the central reflector outer ring over the heated length of the core.

CV 133 calculates the peak volume-average structure temperature (K) achieved during the simulation for the core inner ring ceramic over the heated length of the core.

CV 134 calculates the peak volume-average structure temperature (K) achieved during the simulation for the core middle ring ceramic over the heated length of the core.

CV 135 calculates the peak volume-average structure temperature (K) achieved during the simulation for the core outer ring ceramic over the heated length of the core.

CV 136 calculates the peak volume-average structure temperature (K) achieved during the simulation for the side reflector inner ring over the heated length of the core.

CV 137 calculates the peak volume-average structure temperature (K) achieved during the simulation for the side reflector middle ring over the heated length of the core.

CV 138 calculates the peak volume-average structure temperature (K) achieved during the simulation for the side reflector outer ring over the heated length of the core.

CV 139 calculates the peak volume-average structure temperature (K) achieved during the simulation for the outer reflector over the heated length of the core.

CV 140 calculates the maximum volume-average structure temperature (K) for the heater rod in the core inner ring.

CV 145 calculates the maximum volume-average structure temperature (K) for the heater rod in the core middle ring.

CV 150 calculates the maximum volume-average structure temperature (K) for the heater rod in the core outer ring.

CV 156 calculates the maximum volume-average structure temperature (K) for the heater rods.

CV 157 calculates the peak volume-average structure temperature (K) for the heater rods during the simulation.

CV 161 calculates the axial average structure temperature (K) for the primary pressure vessel cylinder over the core heated length.

CV 162 calculates the axial average structure temperature (K) for the core barrel over the core heated length.

CV 166 calculates the axial average structure temperature (K) for the central reflector center cylinder over the core heated length.

CV 167 calculates the axial average structure temperature (K) for the central reflector middle ring over the core heated length.

CV 168 calculates the axial average structure temperature (K) for the central reflector outer ring over the core heated length.

CV 169 calculates the axial average structure temperature (K) for the core inner ring ceramic over the core heated length.

CV 170 calculates the axial average structure temperature (K) for the core inner ring heater rod over the core heated length.

CV 171 calculates the axial average structure temperature (K) for the core middle ring ceramic over the core heated length.

CV 172 calculates the axial average structure temperature (K) for the core middle ring heater rod over the core heated length.

CV 173 calculates the axial average structure temperature (K) for the core outer ring ceramic over the core heated length.

CV 174 calculates the axial average structure temperature (K) for the core outer ring heater rod over the core heated length.

CV 175 calculates the axial average structure temperature (K) for the side reflector inner ring over the core heated length.

CV 176 calculates the axial average structure temperature (K) for the side reflector outer ring over the core heated length.

CV 177 calculates the axial average structure temperature (K) for the side reflector outer ring over the core heated length.

CV 178 calculates the axial average structure temperature (K) for the outer reflector over the core heated length.

CV 183 calculates the axial average structure temperature (K) for the front (primary pressure vessel) side of the RCCS cooling panels.

CV 184 calculates the axial average structure temperature (K) for the back side of the RCCS cooling panels.

CV 233 calculates the primary pressure vessel inlet pressure error (Pa), which is the difference between the calculated and desired steady-state pressure at the vessel inlet, Component 100.

CV 234 integrates CV 233, processing the pressure error signal. This processed signal is used to change the PCS pressure (Component 234) to achieve the desired steady-state conditions.

CV 236 calculates the primary pressure vessel outlet temperature error (K), which is the difference between the calculated and desired steady-state gas temperature in the outlet plenum, Component 175.

CV 237 integrates CV 236, processing the temperature error signal. This processed signal is used to change the PCS flow rate (Component 237) to achieve the desired steady-state conditions.

CV 275 calculates the pressure difference (Pa) between the core inlet and outlet plenums.

CV 276 calculates the pressure drop (Pa) across the primary pressure vessel.

CV 319 calculates the steam generator outlet temperature error (K), which is the difference between the calculated and desired steady-state gas temperature in the cold duct near the primary pressure vessel, volume 4 of Component 270.

CV 320 integrates CV 319, processing the temperature error signal. This processed signal is used to change the steam generator feedwater flow rate (Component 320) to achieve the desired steady-state conditions.

CV 321 integrates the feedwater flow rate, the mass flow in Component 320, to calculate the total amount of water flowing into the steam generator secondary side (kg).

CV 350 calculates the collapsed liquid level (m) in the steam generator boiler region.

CV 355 converts the collapsed liquid level from CV 350 to a level span (%) corresponding to HTTF measurement LDP-601.

CV 369 calculates the steam generator secondary pressure error (Pa), which is the difference between the calculated and desired steady-state pressure in the steam dome, Component 355.

CV 370 integrates CV 369, processing the pressure error signal. This processed signal is used to change the SCS pressure by modulating valve Component 370 to achieve the desired steady-state conditions.

CV 403 calculates the flow demand for the feedwater and RCCS systems.

CV 404 is a tripunit that has a value of 1.0 if the liquid level in the water storage tank is below the low setpoint.

CV 405 is a tripunit that has a value of -1.0 if the liquid level in the water storage tank is above the high setpoint.

CV 406 adds CV 404 and CV 405, which will provide a non-zero value if the tank liquid level is out-of-range.

CV 407 calculates a liquid level out-of-range contribution to the water storage tank flow demand signal. The amount is assumed to be 25% of the value of CV 403.

CV 408 calculates the flow demand signal for the water storage tank makeup by adding CV 403 and CV 407.

CV 409 calculates the flow error for the water storage tank makeup by subtracting the flow in Component 410 from the demand value in CV 408.

CV 410 integrates the error signal in CV 409. CV 410 is then used to modulate the valve area in Component 410, a servo valve. Minimum and maximum values of 1.0E-5 and 1.0 are specified, respectively.

CV 450 calculates the collapsed liquid level (m) in the water storage day tank (T-010).

CV 451 is a constant that provides the water storage tank low level setpoint (m).

CV 452 is a constant that provides the water storage tank high level setpoint (m).

CV 453 calculates the mid-range of the tank level setpoints by averaging CV 451 and CV 452.

CV 501 is the core differential pressure (kPa). It corresponds to HTTF measurement DP-1001.

CV 502 is the pressure difference (kPa) between the pressure vessel inlet and the hot duct. It corresponds to HTTF measurement DP-4001.

CV 503 is the pressure difference (kPa) between the pressure vessel inlet and the upper plenum. It corresponds to HTTF measurement DP-7001.

CV 504 is the pressure difference (kPa) between the pressure vessel inlet and the lower plenum. It corresponds to HTTF measurement DP-8001.

CV 505 is the pressure difference (kPa) between the pressure vessel inlet and the metallic core support structure. It corresponds to HTTF measurement DP-8002.

CV 506 is the pressure difference (kPa) between the pressure vessel inlet and the top of the upcomer. It corresponds to HTTF measurement DP-9001.

CV 507 is the pressure difference (kPa) between the RCCS panel inlet lines and the outlet lines. It corresponds to HTTF measurement DP-801.

CV 901 obtains the power (W) for heater bank 101 from Table 901.

CV 902 obtains the power (W) for heater bank 102 from Table 902.

CV 903 obtains the power (W) for heater bank 103 from Table 903.

CV 904 obtains the power (W) for heater bank 104 from Table 904.

CV 905 obtains the power (W) for heater bank 105 from Table 905.

CV 906 obtains the power (W) for heater bank 106 from Table 906.

CV 907 obtains the power (W) for heater bank 107 from Table 907.

CV 908 obtains the power (W) for heater bank 108 from Table 908.

CV 909 obtains the power (W) for heater bank 109 from Table 909.

CV 910 obtains the power (W) for heater bank 110 from Table 910.

CV 911 calculates the total core power (W) by adding CVs 901–910.

CV 912 converts the core power from CV 911 into MW.

CV 913 calculates the total energy input (MJ) during the simulation by integrating CV 912.

CV 918 is a constant that provides the desired outlet temperature (K) for the RCCS panels.

CV 919 calculates the RCCS panel coolant outlet temperature error (K).

CV 920 is a proportional-integral controller that processes the error in CV 919 to control the flow rate in the RCCS pump (Component 920).

CV 940 calculates the power input (W) to heat Structure 1403 by taking appropriate fractions of the power from the 10 heaters.

CV 945 calculates the power input (W) to heat Structure 1453 by taking appropriate fractions of the power from the 10 heaters.

CV 950 calculates the power input (W) to heat Structure 1503 by taking appropriate fractions of the power from the 10 heaters.

CV 1000 calculates the convective heat transfer (W) to the left side of the primary pressure vessel cylinder heat structure.

CV 1001 calculates the radiation heat transfer (W) to the left side of the primary pressure vessel cylinder heat structure.

CV 1002 calculates the total heat transfer (W) to the left side of the primary pressure vessel cylinder heat structure.

CV 1003 calculates the integral energy transfer (J) to the left side of the primary pressure vessel cylinder heat structure.

CV 1004 calculates the convective heat transfer (W) to the right side of the primary pressure vessel cylinder heat structure.

CV 1005 calculates the radiation heat transfer (W) to the right side of the primary pressure vessel cylinder heat structure.

CV 1006 calculates the total heat transfer (W) to the right side of the primary pressure vessel cylinder heat structure.

CV 1007 calculates the integral energy transfer (J) to the right side of the primary pressure vessel cylinder heat structure.

CV 1008 calculates the net heat transfer (W) to the primary pressure vessel cylinder heat structure.

CV 1009 calculates the integral net heat transfer (J) to the primary pressure vessel cylinder heat structure.

CV 1010 calculates the convective heat transfer (W) to the left side of the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1011 calculates the radiation heat transfer (W) to the left side of the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1012 calculates the total heat transfer (W) to the left side of the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1013 calculates the integral energy transfer (J) to the left side of the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1014 calculates the convective heat transfer (W) to the right side of the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1015 calculates the radiation heat transfer (W) to the right side of the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1016 calculates the total heat transfer (W) to the right side of the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1017 calculates the integral energy transfer (J) to the right side of the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1018 calculates the net heat transfer (W) to the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1019 calculates the integral net heat transfer (J) to the primary pressure vessel upper head/upper plenum shield heat structure.

CV 1020 calculates the convective heat transfer (W) to the left side of the core barrel heat structure.

CV 1021 calculates the radiation heat transfer (W) to the left side of the core barrel heat structure.

CV 1022 calculates the total heat transfer (W) to the left side of the core barrel heat structure.

CV 1023 calculates the integral energy transfer (J) to the left side of the core barrel heat structure.

CV 1024 calculates the convective heat transfer (W) to the right side of the core barrel heat structure.

CV 1025 calculates the radiation heat transfer (W) to the right side of the core barrel heat structure.

CV 1026 calculates the total heat transfer (W) to the right side of the core barrel heat structure.

CV 1027 calculates the integral energy transfer (J) to the right side of the core barrel heat structure.

CV 1028 calculates the net heat transfer (W) to the core barrel heat structure.

CV 1029 calculates the integral net heat transfer (J) to the core barrel heat structure.

CV 1030 calculates the convective heat transfer (W) to the left side of the upper plenum cylinder heat structure.

CV 1031 calculates the radiation heat transfer (W) to the left side of the upper plenum cylinder heat structure.

CV 1032 calculates the total heat transfer (W) to the left side of the upper plenum cylinder heat structure.

CV 1033 calculates the integral energy transfer (J) to the left side of the upper plenum cylinder heat structure.

CV 1034 calculates the convective heat transfer (W) to the right side of the upper plenum cylinder heat structure.

CV 1035 calculates the radiation heat transfer (W) to the right side of the upper plenum cylinder heat structure.

CV 1036 calculates the total heat transfer (W) to the right side of the upper plenum cylinder heat structure.

CV 1037 calculates the integral energy transfer (J) to the right side of the upper plenum cylinder heat structure.

CV 1038 calculates the net heat transfer (W) to the upper plenum cylinder heat structure.

CV 1039 calculates the integral net heat transfer (J) to the upper plenum cylinder heat structure.

CV 1041 calculates the conduction heat transfer (W) to the left side of the upper plenum floor heat structure.

CV 1042 calculates the total heat transfer (W) to the left side of the upper plenum floor heat structure.

CV 1043 calculates the integral energy transfer (J) to the left side of the upper plenum floor heat structure.

CV 1044 calculates the convective heat transfer (W) to the right side of the upper plenum floor heat structure.

CV 1045 calculates the radiation heat transfer (W) to the right side of the upper plenum floor heat structure.

CV 1046 calculates the total heat transfer (W) to the right side of the upper plenum floor heat structure.

CV 1047 calculates the integral energy transfer (J) to the right side of the upper plenum floor heat structure.

CV 1048 calculates the net heat transfer (W) to the upper plenum floor heat structure.

CV 1049 calculates the integral net heat transfer (J) to the upper plenum floor heat structure.

CV 1054 calculates the convective heat transfer (W) to the right side of the upper plenum internals heat structure.

CV 1055 calculates the radiation heat transfer (W) to the right side of the upper plenum internals heat structure.

CV 1056 calculates the total heat transfer (W) to the right side of the upper plenum internals heat structure.

CV 1057 calculates the integral energy transfer (J) to the right side of the upper plenum internals heat structure.

CV 1058 calculates the net heat transfer (W) to the upper plenum internals heat structure.

CV 1059 calculates the integral net heat transfer (J) to the upper plenum internals heat structure.

CV 1065 calculates the conduction heat transfer (W) to the right side of the central reflector center cylinder heat structure.

CV 1066 calculates the total heat transfer (W) to the right side of the central reflector center cylinder heat structure.

CV 1067 calculates the integral energy transfer (J) to the right side of the central reflector center cylinder heat structure.

CV 1068 calculates the net heat transfer (W) to the central reflector center cylinder heat structure.

CV 1069 calculates the integral net heat transfer (J) to the central reflector center cylinder heat structure.

CV 1070 calculates the convective heat transfer (W) to the left side of the central reflector middle ring heat structure.

CV 1071 calculates the radiation heat transfer (W) to the left side of the central reflector middle ring heat structure.

CV 1072 calculates the total heat transfer (W) to the left side of the central reflector middle ring heat structure.

CV 1073 calculates the integral energy transfer (J) to the left side of the central reflector middle ring heat structure.

CV 1075 calculates the conduction heat transfer (W) to the right side of the central reflector middle ring heat structure.

CV 1076 calculates the total heat transfer (W) to the right side of the central reflector middle ring heat structure.

CV 1077 calculates the integral energy transfer (J) to the right side of the central reflector middle ring heat structure.

CV 1078 calculates the net heat transfer (W) to the central reflector middle ring heat structure.

CV 1079 calculates the integral net heat transfer (J) to the central reflector middle ring heat structure.

CV 1081 calculates the conduction heat transfer (W) to the left side of the central reflector outer ring heat structure.

CV 1082 calculates the total heat transfer (W) to the left side of the central reflector outer ring heat structure.

CV 1083 calculates the integral energy transfer (J) to the left side of the central reflector outer ring heat structure.

CV 1085 calculates the conduction heat transfer (W) to the right side of the central reflector outer ring heat structure.

CV 1086 calculates the total heat transfer (W) to the right side of the central reflector outer ring heat structure.

CV 1087 calculates the integral energy transfer (J) to the right side of the central reflector outer ring heat structure.

CV 1088 calculates the net heat transfer (W) to the central reflector outer ring heat structure.

CV 1089 calculates the integral net heat transfer (J) to the central reflector outer ring heat structure.

CV 1090 calculates the convective heat transfer (W) to the left side of the inner core ring ceramic heat structure.

CV 1091 calculates the conduction heat transfer (W) to the left side of the inner core ring ceramic heat structure.

CV 1092 calculates the total heat transfer (W) to the left side of the inner core ring ceramic heat structure.

CV 1093 calculates the integral energy transfer (J) to the left side of the inner core ring ceramic heat structure.

CV 1094 calculates the convective heat transfer (W) to the right side of the inner core ring ceramic heat structure.

CV 1095 calculates the radiation heat transfer (W) to the right side of the inner core ring ceramic heat structure.

CV 1096 calculates the total heat transfer (W) to the right side of the inner core ring ceramic heat structure.

CV 1097 calculates the integral energy transfer (J) to the right side of the inner core ring ceramic heat structure.

CV 1098 calculates the net heat transfer (W) to the inner core ring ceramic heat structure.

CV 1099 calculates the integral net heat transfer (J) to the inner core ring ceramic heat structure.

CV 1100 calculates the convective heat transfer (W) to the left side of the middle core ring ceramic heat structure.

CV 1101 calculates the conduction heat transfer (W) to the left side of the middle core ring ceramic heat structure.

CV 1102 calculates the total heat transfer (W) to the left side of the middle core ring ceramic heat structure.

CV 1103 calculates the integral energy transfer (J) to the left side of the middle core ring ceramic heat structure.

CV 1104 calculates the convective heat transfer (W) to the right side of the middle core ring ceramic heat structure.

CV 1105 calculates the radiation heat transfer (W) to the right side of the middle core ring ceramic heat structure.

CV 1106 calculates the total heat transfer (W) to the right side of the middle core ring ceramic heat structure.

CV 1107 calculates the integral energy transfer (J) to the right side of the middle core ring ceramic heat structure.

CV 1108 calculates the net heat transfer (W) to the middle core ring ceramic heat structure.

CV 1109 calculates the integral net heat transfer (J) to the middle core ring ceramic heat structure.

CV 1110 calculates the convective heat transfer (W) to the left side of the outer core ring ceramic heat structure.

CV 1111 calculates the conduction heat transfer (W) to the left side of the outer core ring ceramic heat structure.

CV 1112 calculates the total heat transfer (W) to the left side of the outer core ring ceramic heat structure.

CV 1113 calculates the integral energy transfer (J) to the left side of the outer core ring ceramic heat structure.

CV 1114 calculates the convective heat transfer (W) to the right side of the outer core ring ceramic heat structure.

CV 1115 calculates the radiation heat transfer (W) to the right side of the outer core ring ceramic heat structure.

CV 1116 calculates the total heat transfer (W) to the right side of the outer core ring ceramic heat structure.

CV 1117 calculates the integral energy transfer (J) to the right side of the outer core ring ceramic heat structure.

CV 1118 calculates the net heat transfer (W) to the outer core ring ceramic heat structure.

CV 1119 calculates the integral net heat transfer (J) to the outer core ring ceramic heat structure.

CV 1121 calculates the conduction heat transfer (W) to the left side of the side reflector inner ring heat structure.

CV 1122 calculates the total heat transfer (W) to the left side of the side reflector inner ring heat structure.

CV 1123 calculates the integral energy transfer (J) to the left side of the side reflector inner ring heat structure.

CV 1125 calculates the conduction heat transfer (W) to the right side of the side reflector inner ring heat structure.

CV 1126 calculates the total heat transfer (W) to the right side of the side reflector inner ring heat structure.

CV 1127 calculates the integral energy transfer (J) to the right side of the side reflector inner ring heat structure.

CV 1128 calculates the net heat transfer (W) to the side reflector inner ring heat structure.

CV 1129 calculates the integral net heat transfer (J) to the side reflector inner ring heat structure.

CV 1130 calculates the convective heat transfer (W) to the left side of the side reflector middle ring heat structure.

CV 1131 calculates the conduction heat transfer (W) to the left side of the side reflector middle ring heat structure.

CV 1132 calculates the total heat transfer (W) to the left side of the side reflector middle ring heat structure.

CV 1133 calculates the integral energy transfer (J) to the left side of the side reflector middle ring heat structure.

CV 1135 calculates the conduction heat transfer (W) to the right side of the side reflector middle ring heat structure.

CV 1136 calculates the total heat transfer (W) to the right side of the side reflector middle ring heat structure.

CV 1137 calculates the integral energy transfer (J) to the right side of the side reflector middle ring heat structure.

CV 1138 calculates the net heat transfer (W) to the side reflector middle ring heat structure.

CV 1139 calculates the integral net heat transfer (J) to the side reflector middle ring heat structure.

CV 1141 calculates the conduction heat transfer (W) to the left side of the side reflector outer ring heat structure.

CV 1142 calculates the total heat transfer (W) to the left side of the side reflector outer ring heat structure.

CV 1143 calculates the integral energy transfer (J) to the left side of the side reflector outer ring heat structure.

CV 1144 calculates the convective heat transfer (W) to the right side of the side reflector outer ring heat structure.

CV 1145 calculates the radiation heat transfer (W) to the right side of the side reflector outer ring heat structure.

CV 1146 calculates the total heat transfer (W) to the right side of the side reflector outer ring heat structure.

CV 1147 calculates the integral energy transfer (J) to the right side of the side reflector outer ring heat structure.

CV 1148 calculates the net heat transfer (W) to the side reflector outer ring heat structure.

CV 1149 calculates the integral net heat transfer (J) to the side reflector outer ring heat structure.

CV 1150 calculates the convective heat transfer (W) to the left side of the outer reflector heat structure.

CV 1151 calculates the radiation heat transfer (W) to the left side of the outer reflector heat structure.

CV 1152 calculates the total heat transfer (W) to the left side of the outer reflector heat structure.

CV 1153 calculates the integral energy transfer (J) to the left side of the outer reflector heat structure.

CV 1154 calculates the convective heat transfer (W) to the right side of the outer reflector heat structure.

CV 1155 calculates the radiation heat transfer (W) to the right side of the outer reflector heat structure.

CV 1156 calculates the total heat transfer (W) to the right side of the outer reflector heat structure.

CV 1157 calculates the integral energy transfer (J) to the right side of the outer reflector heat structure.

CV 1158 calculates the net heat transfer (W) to the outer reflector heat structure.

CV 1159 calculates the integral net heat transfer (J) to the outer reflector heat structure.

CV 1160 calculates the convective heat transfer (W) to the left side of the outlet plenum bottom plate heat structure.

CV 1161 calculates the radiation heat transfer (W) to the left side of the outlet plenum bottom plate heat structure.

CV 1162 calculates the total heat transfer (W) to the left side of the outlet plenum bottom plate heat structure.

CV 1163 calculates the integral energy transfer (J) to the left side of the outlet plenum bottom plate heat structure.

CV 1164 calculates the convective heat transfer (W) to the right side of the outlet plenum bottom plate heat structure.

CV 1166 calculates the total heat transfer (W) to the right side of the outlet plenum bottom plate heat structure.

CV 1167 calculates the integral energy transfer (J) to the right side of the outlet plenum bottom plate heat structure.

CV 1168 calculates the net heat transfer (W) to the outlet plenum bottom plate heat structure.

CV 1169 calculates the integral net heat transfer (J) to the outlet plenum bottom plate heat structure.

CV 1174 calculates the convective heat transfer (W) to the right side of the outlet plenum support columns heat structure.

CV 1175 calculates the radiation heat transfer (W) to the right side of the outlet plenum support columns heat structure.

CV 1176 calculates the total heat transfer (W) to the right side of the outlet plenum support columns heat structure.

CV 1177 calculates the integral energy transfer (J) to the right side of the outlet plenum support columns heat structure.

CV 1178 calculates the net heat transfer (W) to the outlet plenum support columns heat structure.

CV 1179 calculates the integral net heat transfer (J) to the outlet plenum support columns heat structure.

CV 1180 calculates the convective heat transfer (W) to the left side of the RCCS panels front (vessel) side heat structure.

CV 1181 calculates the radiation heat transfer (W) to the left side of the RCCS panels front (vessel) side heat structure.

CV 1182 calculates the total heat transfer (W) to the left side of the RCCS panels front (vessel) side heat structure.

CV 1183 calculates the integral energy transfer (J) to the left side of the RCCS panels front (vessel) side heat structure.

CV 1184 calculates the convective heat transfer (W) to the right side of the RCCS panels front (vessel) side heat structure.

CV 1186 calculates the total heat transfer (W) to the right side of the RCCS panels front (vessel) side heat structure.

CV 1187 calculates the integral energy transfer (J) to the right side of the RCCS panels front (vessel) side heat structure.

CV 1188 calculates the net heat transfer (W) to the RCCS panels front (vessel) side heat structure.

CV 1189 calculates the integral net heat transfer (J) to the RCCS panels front (vessel) side heat structure.

CV 1190 calculates the convective heat transfer (W) to the left side of the RCCS panels back side heat structure.

CV 1192 calculates the total heat transfer (W) to the left side of the RCCS panels back side heat structure.

CV 1193 calculates the integral energy transfer (J) to the left side of the RCCS panels back side heat structure.

CV 1194 calculates the convective heat transfer (W) to the right side of the RCCS panels back side heat structure.

CV 1196 calculates the total heat transfer (W) to the right side of the RCCS panels back side heat structure.

CV 1197 calculates the integral energy transfer (J) to the right side of the RCCS panels back side heat structure.

CV 1198 calculates the net heat transfer (W) to the RCCS panels back side heat structure.

CV 1199 calculates the integral net heat transfer (J) to the RCCS panels back side heat structure.

CV 1200 calculates the convective heat transfer (W) to the left side of the primary pressure vessel lower head heat structure.

CV 1202 calculates the total heat transfer (W) to the left side of the primary pressure vessel lower head heat structure.

CV 1203 calculates the integral energy transfer (J) to the left side of the primary pressure vessel lower head heat structure.

CV 1204 calculates the convective heat transfer (W) to the right side of the primary pressure vessel lower head heat structure.

CV 1205 calculates the radiation heat transfer (W) to the right side of the primary pressure vessel lower head heat structure.

CV 1206 calculates the total heat transfer (W) to the right side of the primary pressure vessel lower head heat structure.

CV 1207 calculates the integral energy transfer (J) to the right side of the primary pressure vessel lower head heat structure.

CV 1208 calculates the net heat transfer (W) to the primary pressure vessel lower head heat structure.

CV 1209 calculates the integral net heat transfer (J) to the primary pressure vessel lower head heat structure.

CV 1215 calculates the radiation heat transfer (W) to the right side of the inner core ring heater rod heat structure.

CV 1216 calculates the total heat transfer (W) to the right side of the inner core ring heater rod heat structure.

CV 1217 calculates the integral energy transfer (J) to the right side of the inner core ring heater rod heat structure.

CV 1225 calculates the radiation heat transfer (W) to the right side of the middle core ring heater rod heat structure.

CV 1226 calculates the total heat transfer (W) to the right side of the middle core ring heater rod heat structure.

CV 1227 calculates the integral energy transfer (J) to the right side of the middle core ring heater rod heat structure.

CV 1235 calculates the radiation heat transfer (W) to the right side of the outer core ring heater rod heat structure.

CV 1236 calculates the total heat transfer (W) to the right side of the outer core ring heater rod heat structure.

CV 1237 calculates the integral energy transfer (J) to the right side of the outer core ring heater rod heat structure.

CV 1301 calculates the net heat removal (W) from the heater rods.

CV 1302 calculates the net heat removal (W) from the ceramic around the heater rods.

CV 1303 calculates the net heat removal (W) from the core ceramic blocks.

CV 1304 calculates the net heat removal (W) from the core and reflectors.

CV 1305 calculates the net heat removal (W) from the core, reflectors, and core barrel.

CV 1306 calculates the net heat removal (W) from the primary pressure vessel and its internals.

CV 1401 calculates the environmental heat loss (W) from Structure 2001.

CV 1403 calculates the environmental heat loss (W) from Structure 2150.

CV 1404 calculates the environmental heat loss (W) from Structure 2200.

CV 1405 calculates the environmental heat loss (W) from Structure 2280.

CV 1406 calculates the environmental heat loss (W) from Structure 2300.

CV 1407 calculates the environmental heat loss (W) from Structure 2350.

CV 1408 calculates the environmental heat loss (W) from Structure 2400.

CV 1409 calculates the environmental heat loss (W) from Structure 2500.

CV 1411 calculates the environmental heat loss (W) from Structure 2600.

CV 1412 calculates the environmental heat loss (W) from Structure 2700.

CV 1413 calculates the environmental heat loss (W) from Structure 2800.

CV 1414 calculates the environmental heat loss (W) from Structure 3400.

CV 1415 calculates the environmental heat loss (W) from Structure 3550.

CV 1416 calculates the environmental heat loss (W) from Structure 0100. (Only used if the control rod drive break line is active in the input model.)

CV 1417 calculates the environmental heat loss (W) from Structure 0200. (Only used if the control rod drive break line is active in the input model.)

CV 1418 calculates the environmental heat loss (W) from cells 1-40 in Structure 0300. (Only used if the control rod drive break line is active in the input model.)

CV 1419 calculates the environmental heat loss (W) from cells 41-80 in Structure 0300. (Only used if the control rod drive break line is active in the input model.)

CV 1420 calculates the environmental heat loss (W) from cells 81-92 in Structure 0300. (Only used if the control rod drive break line is active in the input model.)

CV 1421 calculates the total environmental heat loss (W) from Structure 0300. (Only used if the control rod drive break line is active in the input model.)

CV 1422 calculates the environmental heat loss (W) from cells 1-40 in Structure 0320. (Only used if the control rod drive break line is active in the input model.)

CV 1423 calculates the environmental heat loss (W) from cells 41-80 in Structure 0320. (Only used if the control rod drive break line is active in the input model.)

CV 1424 calculates the environmental heat loss (W) from cells 81-92 in Structure 0320. (Only used if the control rod drive break line is active in the input model.)

CV 1425 calculates the total environmental heat loss (W) from Structure 0320. (Only used if the control rod drive break line is active in the input model.)

CV 1426 calculates the environmental heat loss (W) from cells 1-40 in Structure 0340. (Only used if the control rod drive break line is active in the input model.)

CV 1427 calculates the environmental heat loss (W) from cells 41-80 in Structure 0340. (Only used if the control rod drive break line is active in the input model.)

CV 1428 calculates the environmental heat loss (W) from cells 81-92 in Structure 0340. (Only used if the control rod drive break line is active in the input model.)

CV 1429 calculates the total environmental heat loss (W) from Structure 0340. (Only used if the control rod drive break line is active in the input model.)

CV 1430 calculates the total environmental heat loss (W) from the control rod drive break piping. (Only used if the control rod drive break line is active in the input model.)

CV 1431 calculates the environmental heat loss (W) from cells 1-40 in Structure 0700. (Only used if the vessel bottom break line is active in the input model.)

CV 1432 calculates the environmental heat loss (W) from cells 41-73 in Structure 0700. (Only used if the vessel bottom break line is active in the input model.)

CV 1433 calculates the total environmental heat loss (W) from Structure 0700. (Only used if the vessel bottom break line is active in the input model.)

CV 1434 calculates the environmental heat loss (W) from cells 1-40 in Structure 0720. (Only used if the vessel bottom break line is active in the input model.)

CV 1435 calculates the environmental heat loss (W) from cells 41-73 in Structure 0720. (Only used if the vessel bottom break line is active in the input model.)

CV 1436 calculates the total environmental heat loss (W) from Structure 0720. (Only used if the vessel bottom break line is active in the input model.)

CV 1437 calculates the environmental heat loss (W) from cells 1-40 in Structure 0800. (Only used if the vessel bottom break line is active in the input model.)

CV 1438 calculates the environmental heat loss (W) from cells 41-80 in Structure 0800. (Only used if the vessel bottom break line is active in the input model.)

CV 1439 calculates the environmental heat loss (W) from cells 81-96 in Structure 0800. (Only used if the vessel bottom break line is active in the input model.)

CV 1440 calculates the total environmental heat loss (W) from Structure 0800. (Only used if the vessel bottom break line is active in the input model.)

CV 1441 calculates the total environmental heat loss (W) from the vessel bottom break piping. (Only used if the vessel bottom break line is active in the input model.)

CV 1444 calculates the total environmental heat loss (W) from the loop piping.

CV 1445 calculates the total environmental heat loss (W) from the steam generator body.

CV 1446 calculates the total environmental heat loss (W) from the PCS.

CV 1447 calculates the total environmental heat loss (W) from the SCS.

CV 1449 calculates the total environmental heat loss (W).

CV 1450 integrates the total environmental heat loss (J).

CV 1601 calculates the total fluid mass (kg) in Component 140.

CV 1602 calculates the total fluid mass (kg) in Component 145.

CV 1603 calculates the total fluid mass (kg) in Component 150.

CV 1604 calculates the total fluid mass (kg) in Component 132.

CV 1605 calculates the total fluid mass (kg) in Component 162.

CV 1606 calculates the total fluid mass (kg) in Component 164.

CV 1607 calculates the total fluid mass (kg) in Component 166.

CV 1608 calculates the total fluid mass (kg) in the core region.

CV 1609 calculates the total fluid mass (kg) in Component 115.

CV 1610 calculates the total fluid mass (kg) in the remaining components in the primary pressure vessel (100, 105, 110, 120, 175).

CV 1611 calculates the total fluid mass (kg) in the primary pressure vessel.

CV 1615 calculates the total fluid mass (kg) in the hot leg, Components 200 and 215.

CV 1616 calculates the total fluid mass (kg) on the primary side of the steam generator, Components 220, 225, and 228.

CV 1617 calculates the total fluid mass (kg) in the cold leg, Components 230, 235, 240, 250, 260, 270, and 293.

CV 1618 calculates the total fluid mass (kg) in the PCS piping.

CV 1619 calculates the total fluid mass (kg) in the PCS inside of the break valves (does not include the piping between the valves and the RCST or the RCST itself).

CV 1621 calculates the total fluid mass (kg) in the RCST, Components 210, 258, and 280.

CV 1626 calculates the total fluid mass (kg) in the secondary side of the steam generator, Components 340, 350, 355, and 360.

CV 1627 calculates the total fluid mass (kg) in the SCS.

CV 1631 calculates the total fluid mass (kg) in the RCCS cooling panels, Component 950.

CV 1632 calculates the total fluid mass (kg) in the RCCS.

CV 1636 calculates the total fluid mass (kg) in the water storage tank, Component 450.

CV 1637 calculates the total fluid mass (kg) in the potable water system.

CV 1640 calculates the total fluid mass (kg) in the water systems.

The CVs in the 2000s calculate various scaling parameters that can be used for comparison with the reference plant or other experiment facilities. The parameters below are taken from McEligot and McCreery 2004.

Non-dimensional heat flux: $q^+ = \beta q''_{\text{wall}} / (G c_p)$

Acceleration parameter: $K_v = 4 q^+ / \text{Re}_D$

Buoyancy parameter: $\text{Bo}^* = \text{Gr}^* / (\text{Re}_{\text{Dh}}^{3.425} \text{Pr}^{0.8})$

Some of these require average values over the heated length. These averages are calculated as the simple average of the values of those parameters in the first and last cells over the heated length.

CV 2001 calculates the pressure difference (Pa) across the heated length of Component 115.

CV 2002 calculates the average pressure (Pa) along the heated length of Component 115.

CV 2003 calculates the gas temperature difference (K) across the heated length of Component 115.

CV 2004 calculates the average gas temperature (K) along the heated length of Component 115.

CV 2005 calculates the average gas density (kg/m^3) along the heated length of Component 115.

CV 2006 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 115.

CV 2007 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 115.

CV 2008 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 115.

CV 2009 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 115.

CV 2010 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 115.

CV 2011 calculates the gas thermal expansion coefficient ($1/\text{K}$) near the middle of the heated length of Component 115.

CV 2012 calculates the gas specific heat capacity (J/kg-K) near the middle of the heated length of Component 115.

CV 2013 calculates the gas thermal conductivity (W/m-K) near the middle of the heated length of Component 115.

CV 2014 calculates the reciprocal gas thermal conductivity (m-K/W) near the middle of the heated length of Component 115.

CV 2015 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 115.

CV 2016 calculates the gas mass flux ($\text{kg/m}^2\text{-s}$) near the middle of the heated length of Component 115.

CV 2017 calculates the gas Reynolds number near the middle of the heated length of Component 115.

CV 2018 calculates the gas Nusselt number near the middle of the heated length of Component 115.

CV 2019 calculates the gas Prandtl number near the middle of the heated length of Component 115.

CV 2020 calculates the gas Grashof number near the middle of the heated length of Component 115.

CV 2021 calculates the gas Froude number near the middle of the heated length of Component 115.

CV 2022 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2023 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2024 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 115.

CV 2025 calculates the acceleration parameter K_v near the middle of the heated length of Component 115.

CV 2026 calculates the square of the gas Reynolds number near the middle of the heated length of Component 115.

CV 2027 calculates the gas Richardson number near the middle of the heated length of Component 115.

CV 2028 calculates the gas $Re^{3.425}$ near the middle of the heated length of Component 115. It does this by raising the square of the gas Re (CV 2026) to the 1.7125 ($=3.425/2$) power to protect against trying to raise a negative number to a real power.

CV 2029 calculates the gas $Pr^{0.8}$ near the middle of the heated length of Component 115.

CV 2030 calculates the denominator for the buoyancy parameter Bo^* .

CV 2031 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 115.

CV 2051 calculates the pressure difference (Pa) across the heated length of Component 132.

CV 2052 calculates the average pressure (Pa) along the heated length of Component 132.

CV 2053 calculates the gas temperature difference (K) across the heated length of Component 132.

CV 2054 calculates the average gas temperature (K) along the heated length of Component 132.

CV 2055 calculates the average gas density (kg/m^3) along the heated length of Component 132.

CV 2056 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 132.

CV 2057 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 132.

CV 2058 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 132.

CV 2059 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 132.

CV 2060 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 132.

CV 2061 calculates the gas thermal expansion coefficient ($1/K$) near the middle of the heated length of Component 132.

CV 2062 calculates the gas specific heat capacity (J/kg-K) near the middle of the heated length of Component 132.

CV 2063 calculates the gas thermal conductivity (W/m-K) near the middle of the heated length of Component 132.

CV 2064 calculates the reciprocal gas thermal conductivity (m-K/W) near the middle of the heated length of Component 132.

CV 2065 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 132.

CV 2066 calculates the gas mass flux (kg/m^2-s) near the middle of the heated length of Component 132.

CV 2067 calculates the gas Reynolds number near the middle of the heated length of Component 132.

CV 2068 calculates the gas Nusselt number near the middle of the heated length of Component 132.

CV 2069 calculates the gas Prandtl number near the middle of the heated length of Component 132.

CV 2070 calculates the gas Grashof number near the middle of the heated length of Component 132.

CV 2071 calculates the gas Froude number near the middle of the heated length of Component 132.

CV 2072 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2073 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2074 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 132.

CV 2075 calculates the acceleration parameter K_v near the middle of the heated length of Component 132.

CV 2076 calculates the square of the gas Reynolds number near the middle of the heated length of Component 132.

CV 2077 calculates the gas Richardson number near the middle of the heated length of Component 132.

CV 2078 calculates the gas $Re^{3.425}$ near the middle of the heated length of Component 132. It does this by raising the square of the gas Re (CV 2076) to the 1.7125 ($=3.425/2$) power to protect against trying to raise a negative number to a real power.

CV 2079 calculates the gas $Pr^{0.8}$ near the middle of the heated length of Component 132.

CV 2080 calculates the denominator for the buoyancy parameter Bo^* .

CV 2081 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 132.

CV 2101 calculates the pressure difference (Pa) across the heated length of Component 140.

CV 2102 calculates the average pressure (Pa) along the heated length of Component 140.

CV 2103 calculates the gas temperature difference (K) across the heated length of Component 140.

CV 2104 calculates the average gas temperature (K) along the heated length of Component 140.

CV 2105 calculates the average gas density (kg/m^3) along the heated length of Component 140.

CV 2106 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 140.

CV 2107 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 140.

CV 2108 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 140.

CV 2109 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 140.

CV 2110 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 140.

CV 2111 calculates the gas thermal expansion coefficient ($1/K$) near the middle of the heated length of Component 140.

CV 2112 calculates the gas specific heat capacity (J/kg-K) near the middle of the heated length of Component 140.

CV 2113 calculates the gas thermal conductivity (W/m-K) near the middle of the heated length of Component 140.

CV 2114 calculates the reciprocal gas thermal conductivity (m-K/W) near the middle of the heated length of Component 140.

CV 2115 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 140.

CV 2116 calculates the gas mass flux ($\text{kg/m}^2\text{-s}$) near the middle of the heated length of Component 140.

CV 2117 calculates the gas Reynolds number near the middle of the heated length of Component 140.

CV 2118 calculates the gas Nusselt number near the middle of the heated length of Component 140.

CV 2119 calculates the gas Prandtl number near the middle of the heated length of Component 140.

CV 2120 calculates the gas Grashof number near the middle of the heated length of Component 140.

CV 2121 calculates the gas Froude number near the middle of the heated length of Component 140.

CV 2122 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2123 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2124 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 140.

CV 2125 calculates the acceleration parameter K_v near the middle of the heated length of Component 140.

CV 2126 calculates the square of the gas Reynolds number near the middle of the heated length of Component 140.

CV 2127 calculates the gas Richardson number near the middle of the heated length of Component 140.

CV 2128 calculates the gas $\text{Re}^{3.425}$ near the middle of the heated length of Component 140. It does this by raising the square of the gas Re (CV 2126) to the 1.7125 ($=3.425/2$) power to protect against trying to raise a negative number to a real power.

CV 2129 calculates the gas $\text{Pr}^{0.8}$ near the middle of the heated length of Component 140.

CV 2130 calculates the denominator for the buoyancy parameter Bo^* .

CV 2131 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 140.

CV 2151 calculates the pressure difference (Pa) across the heated length of Component 145.

CV 2152 calculates the average pressure (Pa) along the heated length of Component 145.

CV 2153 calculates the gas temperature difference (K) across the heated length of Component 145.

CV 2154 calculates the average gas temperature (K) along the heated length of Component 145.

CV 2155 calculates the average gas density (kg/m^3) along the heated length of Component 145.

CV 2156 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 145.

CV 2157 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 145.

CV 2158 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 145.

CV 2159 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 145.

CV 2160 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 145.

CV 2161 calculates the gas thermal expansion coefficient (1/ K) near the middle of the heated length of Component 145.

CV 2162 calculates the gas specific heat capacity (J/kg-K) near the middle of the heated length of Component 145.

CV 2163 calculates the gas thermal conductivity (W/m-K) near the middle of the heated length of Component 145.

CV 2164 calculates the reciprocal gas thermal conductivity (m-K/W) near the middle of the heated length of Component 145.

CV 2165 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 145.

CV 2166 calculates the gas mass flux (kg/m²-s) near the middle of the heated length of Component 145.

CV 2167 calculates the gas Reynolds number near the middle of the heated length of Component 145.

CV 2168 calculates the gas Nusselt number near the middle of the heated length of Component 145.

CV 2169 calculates the gas Prandtl number near the middle of the heated length of Component 145.

CV 2170 calculates the gas Grashof number near the middle of the heated length of Component 145.

CV 2171 calculates the gas Froude number near the middle of the heated length of Component 145.

CV 2172 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2173 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2174 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 145.

CV 2175 calculates the acceleration parameter K_v near the middle of the heated length of Component 145.

CV 2176 calculates the square of the gas Reynolds number near the middle of the heated length of Component 145.

CV 2177 calculates the gas Richardson number near the middle of the heated length of Component 145.

CV 2178 calculates the gas $Re^{3.425}$ near the middle of the heated length of Component 145. It does this by raising the square of the gas Re (CV 2176) to the 1.7125 (=3.425/2) power to protect against trying to raise a negative number to a real power.

CV 2179 calculates the gas $Pr^{0.8}$ near the middle of the heated length of Component 145.

CV 2180 calculates the denominator for the buoyancy parameter Bo^* .

CV 2181 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 145.

CV 2201 calculates the pressure difference (Pa) across the heated length of Component 150.

CV 2202 calculates the average pressure (Pa) along the heated length of Component 150.

CV 2203 calculates the gas temperature difference (K) across the heated length of Component 150.

CV 2204 calculates the average gas temperature (K) along the heated length of Component 150.

CV 2205 calculates the average gas density (kg/m^3) along the heated length of Component 150.

CV 2206 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 150.

CV 2207 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 150.

CV 2208 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 150.

CV 2209 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 150.

CV 2210 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 150.

CV 2211 calculates the gas thermal expansion coefficient ($1/\text{K}$) near the middle of the heated length of Component 150.

CV 2212 calculates the gas specific heat capacity (J/kg-K) near the middle of the heated length of Component 150.

CV 2213 calculates the gas thermal conductivity (W/m-K) near the middle of the heated length of Component 150.

CV 2214 calculates the reciprocal gas thermal conductivity (m-K/W) near the middle of the heated length of Component 150.

CV 2215 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 150.

CV 2216 calculates the gas mass flux ($\text{kg/m}^2\text{-s}$) near the middle of the heated length of Component 150.

CV 2217 calculates the gas Reynolds number near the middle of the heated length of Component 150.

CV 2218 calculates the gas Nusselt number near the middle of the heated length of Component 150.

CV 2219 calculates the gas Prandtl number near the middle of the heated length of Component 150.

CV 2220 calculates the gas Grashof number near the middle of the heated length of Component 150.

CV 2221 calculates the gas Froude number near the middle of the heated length of Component 150.

CV 2222 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2223 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2224 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 150.

CV 2225 calculates the acceleration parameter K_v near the middle of the heated length of Component 150.

CV 2226 calculates the square of the gas Reynolds number near the middle of the heated length of Component 150.

CV 2227 calculates the gas Richardson number near the middle of the heated length of Component 150.

CV 2228 calculates the gas $Re^{3.425}$ near the middle of the heated length of Component 150. It does this by raising the square of the gas Re (CV 2226) to the 1.7125 ($=3.425/2$) power to protect against trying to raise a negative number to a real power.

CV 2229 calculates the gas $Pr^{0.8}$ near the middle of the heated length of Component 150.

CV 2230 calculates the denominator for the buoyancy parameter Bo^* .

CV 2231 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 150.

CV 2251 calculates the pressure difference (Pa) across the heated length of Component 162.

CV 2252 calculates the average pressure (Pa) along the heated length of Component 162.

CV 2253 calculates the gas temperature difference (K) across the heated length of Component 162.

CV 2254 calculates the average gas temperature (K) along the heated length of Component 162.

CV 2255 calculates the average gas density (kg/m^3) along the heated length of Component 162.

CV 2256 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 162.

CV 2257 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 162.

CV 2258 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 162.

CV 2259 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 162.

CV 2260 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 162.

CV 2261 calculates the gas thermal expansion coefficient ($1/K$) near the middle of the heated length of Component 162.

CV 2262 calculates the gas specific heat capacity (J/kg-K) near the middle of the heated length of Component 162.

CV 2263 calculates the gas thermal conductivity (W/m-K) near the middle of the heated length of Component 162.

CV 2264 calculates the reciprocal gas thermal conductivity (m-K/W) near the middle of the heated length of Component 162.

CV 2265 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 162.

CV 2266 calculates the gas mass flux (kg/m^2-s) near the middle of the heated length of Component 162.

CV 2267 calculates the gas Reynolds number near the middle of the heated length of Component 162.

CV 2268 calculates the gas Nusselt number near the middle of the heated length of Component 162.

CV 2269 calculates the gas Prandtl number near the middle of the heated length of Component 162.

CV 2270 calculates the gas Grashof number near the middle of the heated length of Component 162.

CV 2271 calculates the gas Froude number near the middle of the heated length of Component 162.

CV 2272 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2273 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2274 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 162.

CV 2275 calculates the acceleration parameter K_v near the middle of the heated length of Component 162.

CV 2276 calculates the square of the gas Reynolds number near the middle of the heated length of Component 162.

CV 2277 calculates the gas Richardson number near the middle of the heated length of Component 162.

CV 2278 calculates the gas $Re^{3.425}$ near the middle of the heated length of Component 162. It does this by raising the square of the gas Re (CV 2276) to the 1.7125 ($=3.425/2$) power to protect against trying to raise a negative number to a real power.

CV 2279 calculates the gas $Pr^{0.8}$ near the middle of the heated length of Component 162.

CV 2280 calculates the denominator for the buoyancy parameter Bo^* .

CV 2281 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 162.

CV 2301 calculates the pressure difference (Pa) across the heated length of Component 164.

CV 2302 calculates the average pressure (Pa) along the heated length of Component 164.

CV 2303 calculates the gas temperature difference (K) across the heated length of Component 164.

CV 2304 calculates the average gas temperature (K) along the heated length of Component 164.

CV 2305 calculates the average gas density (kg/m^3) along the heated length of Component 164.

CV 2306 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 164.

CV 2307 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 164.

CV 2308 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 164.

CV 2309 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 164.

CV 2310 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 164.

CV 2311 calculates the gas thermal expansion coefficient ($1/K$) near the middle of the heated length of Component 164.

CV 2312 calculates the gas specific heat capacity (J/kg-K) near the middle of the heated length of Component 164.

CV 2313 calculates the gas thermal conductivity (W/m-K) near the middle of the heated length of Component 164.

CV 2314 calculates the reciprocal gas thermal conductivity (m-K/W) near the middle of the heated length of Component 164.

CV 2315 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 164.

CV 2316 calculates the gas mass flux ($\text{kg/m}^2\text{-s}$) near the middle of the heated length of Component 164.

CV 2317 calculates the gas Reynolds number near the middle of the heated length of Component 164.

CV 2318 calculates the gas Nusselt number near the middle of the heated length of Component 164.

CV 2319 calculates the gas Prandtl number near the middle of the heated length of Component 164.

CV 2320 calculates the gas Grashof number near the middle of the heated length of Component 164.

CV 2321 calculates the gas Froude number near the middle of the heated length of Component 164.

CV 2322 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2323 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2324 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 164.

CV 2325 calculates the acceleration parameter K_v near the middle of the heated length of Component 164.

CV 2326 calculates the square of the gas Reynolds number near the middle of the heated length of Component 164.

CV 2327 calculates the gas Richardson number near the middle of the heated length of Component 164.

CV 2328 calculates the gas $\text{Re}^{3.425}$ near the middle of the heated length of Component 164. It does this by raising the square of the gas Re (CV 2326) to the 1.7125 ($=3.425/2$) power to protect against trying to raise a negative number to a real power.

CV 2329 calculates the gas $\text{Pr}^{0.8}$ near the middle of the heated length of Component 164.

CV 2330 calculates the denominator for the buoyancy parameter Bo^* .

CV 2331 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 164.

CV 2351 calculates the pressure difference (Pa) across the heated length of Component 166.

CV 2352 calculates the average pressure (Pa) along the heated length of Component 166.

CV 2353 calculates the gas temperature difference (K) across the heated length of Component 166.

CV 2354 calculates the average gas temperature (K) along the heated length of Component 166.

CV 2355 calculates the average gas density (kg/m^3) along the heated length of Component 166.

CV 2356 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 166.

CV 2357 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 166.

CV 2358 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 166.

CV 2359 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 166.

CV 2360 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 166.

CV 2361 calculates the gas thermal expansion coefficient ($1/K$) near the middle of the heated length of Component 166.

CV 2362 calculates the gas specific heat capacity ($J/kg\cdot K$) near the middle of the heated length of Component 166.

CV 2363 calculates the gas thermal conductivity ($W/m\cdot K$) near the middle of the heated length of Component 166.

CV 2364 calculates the reciprocal gas thermal conductivity ($m\cdot K/W$) near the middle of the heated length of Component 166.

CV 2365 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 166.

CV 2366 calculates the gas mass flux ($kg/m^2\cdot s$) near the middle of the heated length of Component 166.

CV 2367 calculates the gas Reynolds number near the middle of the heated length of Component 166.

CV 2368 calculates the gas Nusselt number near the middle of the heated length of Component 166.

CV 2369 calculates the gas Prandtl number near the middle of the heated length of Component 166.

CV 2370 calculates the gas Grashof number near the middle of the heated length of Component 166.

CV 2371 calculates the gas Froude number near the middle of the heated length of Component 1132.

CV 2372 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2373 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2374 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 166.

CV 2375 calculates the acceleration parameter K_v near the middle of the heated length of Component 166.

CV 2376 calculates the square of the gas Reynolds number near the middle of the heated length of Component 166.

CV 2377 calculates the gas Richardson number near the middle of the heated length of Component 166.

CV 2378 calculates the gas $Re^{3.425}$ near the middle of the heated length of Component 166. It does this by raising the square of the gas Re (CV 2376) to the 1.7125 ($=3.425/2$) power to protect against trying to raise a negative number to a real power.

CV 2379 calculates the gas $Pr^{0.8}$ near the middle of the heated length of Component 166.

CV 2380 calculates the denominator for the buoyancy parameter Bo^* .

CV 2381 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 166.

CV 2401 calculates the pressure difference (Pa) across the heated length of Component 950.

CV 2402 calculates the average pressure (Pa) along the heated length of Component 950.

CV 2403 calculates the gas temperature difference (K) across the heated length of Component 950.

CV 2404 calculates the average gas temperature (K) along the heated length of Component 950.

CV 2405 calculates the average gas density (kg/m^3) along the heated length of Component 950.

CV 2406 calculates the gas specific heat capacity (J/kg-K) at the inlet of the heated length of Component 950.

CV 2407 calculates the gas specific heat capacity (J/kg-K) at the outlet of the heated length of Component 950.

CV 2408 calculates the average gas specific heat capacity (J/kg-K) along the heated length of Component 950.

CV 2409 calculates the gas viscosity (kg/m-s) near the middle of the heated length of Component 950.

CV 2410 calculates the reciprocal gas viscosity (m-s/kg) near the middle of the heated length of Component 950.

CV 2411 calculates the gas thermal expansion coefficient (1/ K) near the middle of the heated length of Component 950.

CV 2412 calculates the gas specific heat capacity (J/kg-K) near the middle of the heated length of Component 950.

CV 2413 calculates the gas thermal conductivity (W/m-K) near the middle of the heated length of Component 950.

CV 2414 calculates the reciprocal gas thermal conductivity (m-K/W) near the middle of the heated length of Component 950.

CV 2415 calculates the wall-to-gas temperature difference (K) near the middle of the heated length of Component 950.

CV 2416 calculates the gas mass flux (kg/m²-s) near the middle of the heated length of Component 950.

CV 2417 calculates the gas Reynolds number near the middle of the heated length of Component 950.

CV 2418 calculates the gas Nusselt number near the middle of the heated length of Component 950.

CV 2419 calculates the gas Prandtl number near the middle of the heated length of Component 950.

CV 2420 calculates the gas Grashof number near the middle of the heated length of Component 950.

CV 2421 calculates the gas Froude number near the middle of the heated length of Component 950.

CV 2422 calculates the numerator for the non-dimensional heat flux parameter q^+ .

CV 2423 calculates the denominator for the non-dimensional heat flux parameter q^+ .

CV 2424 calculates the non-dimensional heat flux parameter q^+ near the middle of the heated length of Component 950.

CV 2425 calculates the acceleration parameter K_v near the middle of the heated length of Component 950.

CV 2426 calculates the square of the gas Reynolds number near the middle of the heated length of Component 950.

CV 2427 calculates the gas Richardson number near the middle of the heated length of Component 950.

CV 2428 calculates the gas $Re^{3.425}$ near the middle of the heated length of Component 950. It does this by raising the square of the gas Re (CV 2426) to the 1.7125 (=3.425/2) power to protect against trying to raise a negative number to a real power.

CV 2429 calculates the gas $Pr^{0.8}$ near the middle of the heated length of Component 950.

CV 2430 calculates the denominator for the buoyancy parameter Bo^* .

CV 2431 calculates the buoyancy parameter Bo^* near the middle of the heated length of Component 950.

The 3000 series CVs are intended to provide an approximation of the stored energy of the system. The volumetric heat capacity is in MJ/m^3-K and the stored energy is in MJ.

CV 3001 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 1.

CV 3002 calculates the stored energy (MJ) in Structure 1000, axial node 1.

CV 3003 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 2.

CV 3004 calculates the stored energy (MJ) in Structure 1000, axial node 2.

CV 3005 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 3.

CV 3006 calculates the stored energy (MJ) in Structure 1000, axial node 3.

CV 3007 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 4.

CV 3008 calculates the stored energy (MJ) in Structure 1000, axial node 4.

CV 3009 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 5.

CV 3010 calculates the stored energy (MJ) in Structure 1000, axial node 5.

CV 3011 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 6.

CV 3012 calculates the stored energy (MJ) in Structure 1000, axial node 6.

CV 3013 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 7.

CV 3014 calculates the stored energy (MJ) in Structure 1000, axial node 7.

CV 3015 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 8.

CV 3016 calculates the stored energy (MJ) in Structure 1000, axial node 8.

CV 3017 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 9.

CV 3018 calculates the stored energy (MJ) in Structure 1000, axial node 9.

CV 3019 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 10.

CV 3020 calculates the stored energy (MJ) in Structure 1000, axial node 10.

CV 3021 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 11.

CV 3022 calculates the stored energy (MJ) in Structure 1000, axial node 11.

CV 3023 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 12.

CV 3024 calculates the stored energy (MJ) in Structure 1000, axial node 12.

CV 3025 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 13.

CV 3026 calculates the stored energy (MJ) in Structure 1000, axial node 13.

CV 3027 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 14.

CV 3028 calculates the stored energy (MJ) in Structure 1000, axial node 14.

CV 3029 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 15.

CV 3030 calculates the stored energy (MJ) in Structure 1000, axial node 15.

CV 3031 calculates the volumetric heat capacity (MJ/m^3-K) in Structure 1000, axial node 16.

CV 3032 calculates the stored energy (MJ) in Structure 1000, axial node 16.

CV 3033 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1000, axial node 17.

CV 3034 calculates the stored energy (MJ) in Structure 1000, axial node 17.

CV 3035 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1001, axial node 1.

CV 3036 calculates the stored energy (MJ) in Structure 1001, axial node 1.

CV 3038 calculates the stored energy (MJ) in the pressure vessel cylinder and head, Structures 1000 and 1001.

CV 3041 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1050, axial node 1.

CV 3042 calculates the stored energy (MJ) in Structure 1050, axial node 1.

CV 3043 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1100, axial node 1.

CV 3044 calculates the stored energy (MJ) in Structure 1100, axial node 1.

CV 3049 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 1.

CV 3050 calculates the stored energy (MJ) in Structure 1150, axial node 1.

CV 3051 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 2.

CV 3052 calculates the stored energy (MJ) in Structure 1150, axial node 2.

CV 3053 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 3.

CV 3054 calculates the stored energy (MJ) in Structure 1150, axial node 3.

CV 3055 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 4.

CV 3056 calculates the stored energy (MJ) in Structure 1150, axial node 4.

CV 3057 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 5.

CV 3058 calculates the stored energy (MJ) in Structure 1150, axial node 5.

CV 3059 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 6.

CV 3060 calculates the stored energy (MJ) in Structure 1150, axial node 6.

CV 3061 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 7.

CV 3062 calculates the stored energy (MJ) in Structure 1150, axial node 7.

CV 3063 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 8.

CV 3064 calculates the stored energy (MJ) in Structure 1150, axial node 8.

CV 3065 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 9.

CV 3066 calculates the stored energy (MJ) in Structure 1150, axial node 9.

CV 3067 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 10.

CV 3068 calculates the stored energy (MJ) in Structure 1150, axial node 10.

CV 3069 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 11.

CV 3070 calculates the stored energy (MJ) in Structure 1150, axial node 11.

CV 3071 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 12.

CV 3072 calculates the stored energy (MJ) in Structure 1150, axial node 12.

CV 3073 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 13.

CV 3074 calculates the stored energy (MJ) in Structure 1150, axial node 13.

CV 3075 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 14.

CV 3076 calculates the stored energy (MJ) in Structure 1150, axial node 14.

CV 3077 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 15.

CV 3078 calculates the stored energy (MJ) in Structure 1150, axial node 15.

CV 3079 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1150, axial node 16.

CV 3080 calculates the stored energy (MJ) in Structure 1150, axial node 16.

CV 3081 calculates the stored energy (MJ) in the core barrel, Structure 1150.

CV 3083 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1200, axial node 1.

CV 3084 calculates the stored energy (MJ) in Structure 1200, axial node 1.

CV 3085 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1201, axial node 1.

CV 3086 calculates the stored energy (MJ) in Structure 1201, axial node 1.

CV 3087 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1202, axial node 1.

CV 3088 calculates the stored energy (MJ) in Structure 1202, axial node 1.

CV 3091 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 1.

CV 3092 calculates the stored energy (MJ) in Structure 1300, axial node 1.

CV 3093 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 2.

CV 3094 calculates the stored energy (MJ) in Structure 1300, axial node 2.

CV 3095 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 3.

CV 3096 calculates the stored energy (MJ) in Structure 1300, axial node 3.

CV 3097 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 4.

CV 3098 calculates the stored energy (MJ) in Structure 1300, axial node 4.

CV 3099 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 5.

CV 3100 calculates the stored energy (MJ) in Structure 1300, axial node 5.

CV 3101 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 6.

CV 3102 calculates the stored energy (MJ) in Structure 1300, axial node 6.

CV 3103 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 7.

CV 3104 calculates the stored energy (MJ) in Structure 1300, axial node 7.

CV 3105 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 8.

CV 3106 calculates the stored energy (MJ) in Structure 1300, axial node 8.

CV 3107 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 9.

CV 3108 calculates the stored energy (MJ) in Structure 1300, axial node 9.

CV 3109 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 10.

CV 3110 calculates the stored energy (MJ) in Structure 1300, axial node 10.

CV 3111 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 11.

CV 3112 calculates the stored energy (MJ) in Structure 1300, axial node 11.

CV 3113 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 12.

CV 3114 calculates the stored energy (MJ) in Structure 1300, axial node 12.

CV 3115 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 13.

CV 3116 calculates the stored energy (MJ) in Structure 1300, axial node 13.

CV 3117 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1300, axial node 14.

CV 3118 calculates the stored energy (MJ) in Structure 1300, axial node 14.

CV 3121 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 1.

CV 3122 calculates the stored energy (MJ) in Structure 1320, axial node 1.

CV 3123 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 2.

CV 3124 calculates the stored energy (MJ) in Structure 1320, axial node 2.

CV 3125 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 3.

CV 3126 calculates the stored energy (MJ) in Structure 1320, axial node 3.

CV 3127 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 4.

CV 3128 calculates the stored energy (MJ) in Structure 1320, axial node 4.

CV 3129 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 5.

CV 3130 calculates the stored energy (MJ) in Structure 1320, axial node 5.

CV 3131 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 6.

CV 3132 calculates the stored energy (MJ) in Structure 1320, axial node 6.

CV 3133 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 7.

CV 3134 calculates the stored energy (MJ) in Structure 1320, axial node 7.

CV 3135 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 8.

CV 3136 calculates the stored energy (MJ) in Structure 1320, axial node 8.

CV 3137 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 9.

CV 3138 calculates the stored energy (MJ) in Structure 1320, axial node 9.

CV 3139 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 10.

CV 3140 calculates the stored energy (MJ) in Structure 1320, axial node 10.

CV 3141 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 11.

CV 3142 calculates the stored energy (MJ) in Structure 1320, axial node 11.

CV 3143 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 12.

CV 3144 calculates the stored energy (MJ) in Structure 1320, axial node 12.

CV 3145 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 13.

CV 3146 calculates the stored energy (MJ) in Structure 1320, axial node 13.

CV 3147 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1320, axial node 14.

CV 3148 calculates the stored energy (MJ) in Structure 1320, axial node 14.

CV 3151 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 1.
CV 3152 calculates the stored energy (MJ) in Structure 1340, axial node 1.
CV 3153 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 2.
CV 3154 calculates the stored energy (MJ) in Structure 1340, axial node 2.
CV 3155 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 3.
CV 3156 calculates the stored energy (MJ) in Structure 1340, axial node 3.
CV 3157 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 4.
CV 3158 calculates the stored energy (MJ) in Structure 1340, axial node 4.
CV 3159 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 5.
CV 3160 calculates the stored energy (MJ) in Structure 1340, axial node 5.
CV 3161 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 6.
CV 3162 calculates the stored energy (MJ) in Structure 1340, axial node 6.
CV 3163 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 7.
CV 3164 calculates the stored energy (MJ) in Structure 1340, axial node 7.
CV 3165 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 8.
CV 3166 calculates the stored energy (MJ) in Structure 1340, axial node 8.
CV 3167 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 9.
CV 3168 calculates the stored energy (MJ) in Structure 1340, axial node 9.
CV 3169 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 10.
CV 3170 calculates the stored energy (MJ) in Structure 1340, axial node 10.
CV 3171 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 11.
CV 3172 calculates the stored energy (MJ) in Structure 1340, axial node 11.
CV 3173 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 12.
CV 3174 calculates the stored energy (MJ) in Structure 1340, axial node 12.
CV 3175 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 13.
CV 3176 calculates the stored energy (MJ) in Structure 1340, axial node 13.
CV 3177 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1340, axial node 14.
CV 3178 calculates the stored energy (MJ) in Structure 1340, axial node 14.
CV 3179 calculates the stored energy (MJ) in the central reflector, Structures 1300, 1320, and 1340.
CV 3181 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1400, axial node 1.
CV 3182 calculates the stored energy (MJ) in Structure 1400, axial node 1.
CV 3183 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1400, axial node 2.
CV 3184 calculates the stored energy (MJ) in Structure 1400, axial node 2.
CV 3185 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 1.
CV 3186 calculates the stored energy (MJ) in Structure 1401, axial node 1.

CV 3187 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 2.
CV 3188 calculates the stored energy (MJ) in Structure 1401, axial node 2.
CV 3189 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 3.
CV 3190 calculates the stored energy (MJ) in Structure 1401, axial node 3.
CV 3191 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 4.
CV 3192 calculates the stored energy (MJ) in Structure 1401, axial node 4.
CV 3193 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 5.
CV 3194 calculates the stored energy (MJ) in Structure 1401, axial node 5.
CV 3195 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 6.
CV 3196 calculates the stored energy (MJ) in Structure 1401, axial node 6.
CV 3197 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 7.
CV 3198 calculates the stored energy (MJ) in Structure 1401, axial node 7.
CV 3199 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 8.
CV 3200 calculates the stored energy (MJ) in Structure 1401, axial node 8.
CV 3201 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 9.
CV 3202 calculates the stored energy (MJ) in Structure 1401, axial node 9.
CV 3203 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1401, axial node 10.
CV 3204 calculates the stored energy (MJ) in Structure 1401, axial node 10.
CV 3205 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1402, axial node 1.
CV 3206 calculates the stored energy (MJ) in Structure 1402, axial node 1.
CV 3207 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1402, axial node 2.
CV 3208 calculates the stored energy (MJ) in Structure 1402, axial node 2.
CV 3211 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1450, axial node 1.
CV 3212 calculates the stored energy (MJ) in Structure 1450, axial node 1.
CV 3213 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1450, axial node 2.
CV 3214 calculates the stored energy (MJ) in Structure 1450, axial node 2.
CV 3215 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 1.
CV 3216 calculates the stored energy (MJ) in Structure 1451, axial node 1.
CV 3217 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 2.
CV 3218 calculates the stored energy (MJ) in Structure 1451, axial node 2.
CV 3219 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 3.
CV 3220 calculates the stored energy (MJ) in Structure 1451, axial node 3.
CV 3221 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 4.
CV 3222 calculates the stored energy (MJ) in Structure 1451, axial node 4.
CV 3223 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 5.

CV 3224 calculates the stored energy (MJ) in Structure 1451, axial node 5.

CV 3225 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 6.

CV 3226 calculates the stored energy (MJ) in Structure 1451, axial node 6.

CV 3227 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 7.

CV 3228 calculates the stored energy (MJ) in Structure 1451, axial node 7.

CV 3229 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 8.

CV 3230 calculates the stored energy (MJ) in Structure 1451, axial node 8.

CV 3231 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 9.

CV 3232 calculates the stored energy (MJ) in Structure 1451, axial node 9.

CV 3233 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1451, axial node 10.

CV 3234 calculates the stored energy (MJ) in Structure 1451, axial node 10.

CV 3235 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1452, axial node 1.

CV 3236 calculates the stored energy (MJ) in Structure 1452, axial node 1.

CV 3237 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1452, axial node 2.

CV 3238 calculates the stored energy (MJ) in Structure 1452, axial node 2.

CV 3241 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1500, axial node 1.

CV 3242 calculates the stored energy (MJ) in Structure 1500, axial node 1.

CV 3243 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1500, axial node 2.

CV 3244 calculates the stored energy (MJ) in Structure 1500, axial node 2.

CV 3245 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 1.

CV 3246 calculates the stored energy (MJ) in Structure 1501, axial node 1.

CV 3247 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 2.

CV 3248 calculates the stored energy (MJ) in Structure 1501, axial node 2.

CV 3249 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 3.

CV 3250 calculates the stored energy (MJ) in Structure 1501, axial node 3.

CV 3251 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 4.

CV 3252 calculates the stored energy (MJ) in Structure 1501, axial node 4.

CV 3253 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 5.

CV 3254 calculates the stored energy (MJ) in Structure 1501, axial node 5.

CV 3255 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 6.

CV 3256 calculates the stored energy (MJ) in Structure 1501, axial node 6.

CV 3257 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 7.

CV 3258 calculates the stored energy (MJ) in Structure 1501, axial node 7.

CV 3259 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 8.

CV 3260 calculates the stored energy (MJ) in Structure 1501, axial node 8.

CV 3261 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 9.

CV 3262 calculates the stored energy (MJ) in Structure 1501, axial node 9.

CV 3263 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1501, axial node 10.

CV 3264 calculates the stored energy (MJ) in Structure 1501, axial node 10.

CV 3265 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1502, axial node 1.

CV 3266 calculates the stored energy (MJ) in Structure 1502, axial node 1.

CV 3267 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1502, axial node 2.

CV 3268 calculates the stored energy (MJ) in Structure 1502, axial node 2.

CV 3269 calculates the stored energy (MJ) in the core ceramic, Structures 1400, 1401, 1402, 1450, 1451, 1452, 1500, 1501, and 1502.

CV 3271 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 1.

CV 3272 calculates the stored energy (MJ) in Structure 1403, axial node 1.

CV 3273 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 2.

CV 3274 calculates the stored energy (MJ) in Structure 1403, axial node 2.

CV 3275 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 3.

CV 3276 calculates the stored energy (MJ) in Structure 1403, axial node 3.

CV 3277 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 4.

CV 3278 calculates the stored energy (MJ) in Structure 1403, axial node 4.

CV 3279 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 5.

CV 3280 calculates the stored energy (MJ) in Structure 1403, axial node 5.

CV 3281 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 6.

CV 3282 calculates the stored energy (MJ) in Structure 1403, axial node 6.

CV 3283 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 7.

CV 3284 calculates the stored energy (MJ) in Structure 1403, axial node 7.

CV 3285 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 8.

CV 3286 calculates the stored energy (MJ) in Structure 1403, axial node 8.

CV 3287 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 9.

CV 3288 calculates the stored energy (MJ) in Structure 1403, axial node 9.

CV 3289 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1403, axial node 10.

CV 3290 calculates the stored energy (MJ) in Structure 1403, axial node 10.

CV 3291 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 1.

CV 3292 calculates the stored energy (MJ) in Structure 1453, axial node 1.

CV 3293 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 2.

CV 3294 calculates the stored energy (MJ) in Structure 1453, axial node 2.

CV 3295 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 3.

CV 3296 calculates the stored energy (MJ) in Structure 1453, axial node 3.

CV 3297 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 4.

CV 3298 calculates the stored energy (MJ) in Structure 1453, axial node 4.

CV 3299 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 5.

CV 3300 calculates the stored energy (MJ) in Structure 1453, axial node 5.

CV 3301 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 6.

CV 3302 calculates the stored energy (MJ) in Structure 1453, axial node 6.

CV 3303 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 7.

CV 3304 calculates the stored energy (MJ) in Structure 1453, axial node 7.

CV 3305 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 8.

CV 3306 calculates the stored energy (MJ) in Structure 1453, axial node 8.

CV 3307 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 9.

CV 3308 calculates the stored energy (MJ) in Structure 1453, axial node 9.

CV 3309 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1453, axial node 10.

CV 3310 calculates the stored energy (MJ) in Structure 1453, axial node 10.

CV 3311 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 1.

CV 3312 calculates the stored energy (MJ) in Structure 1503, axial node 1.

CV 3313 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 2.

CV 3314 calculates the stored energy (MJ) in Structure 1503, axial node 2.

CV 3315 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 3.

CV 3316 calculates the stored energy (MJ) in Structure 1503, axial node 3.

CV 3317 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 4.

CV 3318 calculates the stored energy (MJ) in Structure 1503, axial node 4.

CV 3319 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 5.

CV 3320 calculates the stored energy (MJ) in Structure 1503, axial node 5.

CV 3321 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 6.

CV 3322 calculates the stored energy (MJ) in Structure 1503, axial node 6.

CV 3323 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 7.

CV 3324 calculates the stored energy (MJ) in Structure 1503, axial node 7.

CV 3325 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 8.

CV 3326 calculates the stored energy (MJ) in Structure 1503, axial node 8.

CV 3327 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 9.

CV 3328 calculates the stored energy (MJ) in Structure 1503, axial node 9.

CV 3329 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1503, axial node 10.

CV 3330 calculates the stored energy (MJ) in Structure 1503, axial node 10.

CV 3331 calculates the stored energy (MJ) in the heater rods, Structures 1403, 1453, and 1503.

CV 3341 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 1.
CV 3342 calculates the stored energy (MJ) in Structure 1600, axial node 1.
CV 3343 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 2.
CV 3344 calculates the stored energy (MJ) in Structure 1600, axial node 2.
CV 3345 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 3.
CV 3346 calculates the stored energy (MJ) in Structure 1600, axial node 3.
CV 3347 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 4.
CV 3348 calculates the stored energy (MJ) in Structure 1600, axial node 4.
CV 3349 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 5.
CV 3350 calculates the stored energy (MJ) in Structure 1600, axial node 5.
CV 3351 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 6.
CV 3352 calculates the stored energy (MJ) in Structure 1600, axial node 6.
CV 3353 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 7.
CV 3354 calculates the stored energy (MJ) in Structure 1600, axial node 7.
CV 3355 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 8.
CV 3356 calculates the stored energy (MJ) in Structure 1600, axial node 8.
CV 3357 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 9.
CV 3358 calculates the stored energy (MJ) in Structure 1600, axial node 9.
CV 3359 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 10.
CV 3360 calculates the stored energy (MJ) in Structure 1600, axial node 10.
CV 3361 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 11.
CV 3362 calculates the stored energy (MJ) in Structure 1600, axial node 11.
CV 3363 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 12.
CV 3364 calculates the stored energy (MJ) in Structure 1600, axial node 12.
CV 3365 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 13.
CV 3366 calculates the stored energy (MJ) in Structure 1600, axial node 13.
CV 3367 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1600, axial node 14.
CV 3368 calculates the stored energy (MJ) in Structure 1600, axial node 14.
CV 3371 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 1.
CV 3372 calculates the stored energy (MJ) in Structure 1620, axial node 1.
CV 3373 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 2.
CV 3374 calculates the stored energy (MJ) in Structure 1620, axial node 2.
CV 3375 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 3.
CV 3376 calculates the stored energy (MJ) in Structure 1620, axial node 3.
CV 3377 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 4.

CV 3378 calculates the stored energy (MJ) in Structure 1620, axial node 4.

CV 3379 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 5.

CV 3380 calculates the stored energy (MJ) in Structure 1620, axial node 5.

CV 3381 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 6.

CV 3382 calculates the stored energy (MJ) in Structure 1620, axial node 6.

CV 3383 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 7.

CV 3384 calculates the stored energy (MJ) in Structure 1620, axial node 7.

CV 3385 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 8.

CV 3386 calculates the stored energy (MJ) in Structure 1620, axial node 8.

CV 3387 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 9.

CV 3388 calculates the stored energy (MJ) in Structure 1620, axial node 9.

CV 3389 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 10.

CV 3390 calculates the stored energy (MJ) in Structure 1620, axial node 10.

CV 3391 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 11.

CV 3392 calculates the stored energy (MJ) in Structure 1620, axial node 11.

CV 3393 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 12.

CV 3394 calculates the stored energy (MJ) in Structure 1620, axial node 12.

CV 3395 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 13.

CV 3396 calculates the stored energy (MJ) in Structure 1620, axial node 13.

CV 3397 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1620, axial node 14.

CV 3398 calculates the stored energy (MJ) in Structure 1620, axial node 14.

CV 3401 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 1.

CV 3402 calculates the stored energy (MJ) in Structure 1640, axial node 1.

CV 3403 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 2.

CV 3404 calculates the stored energy (MJ) in Structure 1640, axial node 2.

CV 3405 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 3.

CV 3406 calculates the stored energy (MJ) in Structure 1640, axial node 3.

CV 3407 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 4.

CV 3408 calculates the stored energy (MJ) in Structure 1640, axial node 4.

CV 3409 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 5.

CV 3410 calculates the stored energy (MJ) in Structure 1640, axial node 5.

CV 3411 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 6.

CV 3412 calculates the stored energy (MJ) in Structure 1640, axial node 6.

CV 3413 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 7.

CV 3414 calculates the stored energy (MJ) in Structure 1640, axial node 7.

CV 3415 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 8.
CV 3416 calculates the stored energy (MJ) in Structure 1640, axial node 8.
CV 3417 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 9.
CV 3418 calculates the stored energy (MJ) in Structure 1640, axial node 9.
CV 3419 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 10.
CV 3420 calculates the stored energy (MJ) in Structure 1640, axial node 10.
CV 3421 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 11.
CV 3422 calculates the stored energy (MJ) in Structure 1640, axial node 11.
CV 3423 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 12.
CV 3424 calculates the stored energy (MJ) in Structure 1640, axial node 12.
CV 3425 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 13.
CV 3426 calculates the stored energy (MJ) in Structure 1640, axial node 13.
CV 3427 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1640, axial node 14.
CV 3428 calculates the stored energy (MJ) in Structure 1640, axial node 14.
CV 3429 calculates the stored energy (MJ) in the side reflector, Structures 1600, 1620, and 1640.
CV 3431 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 1.
CV 3432 calculates the stored energy (MJ) in Structure 1660, axial node 1.
CV 3433 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 2.
CV 3434 calculates the stored energy (MJ) in Structure 1660, axial node 2.
CV 3435 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 3.
CV 3436 calculates the stored energy (MJ) in Structure 1660, axial node 3.
CV 3437 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 4.
CV 3438 calculates the stored energy (MJ) in Structure 1660, axial node 4.
CV 3439 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 5.
CV 3440 calculates the stored energy (MJ) in Structure 1660, axial node 5.
CV 3441 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 6.
CV 3442 calculates the stored energy (MJ) in Structure 1660, axial node 6.
CV 3443 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 7.
CV 3444 calculates the stored energy (MJ) in Structure 1660, axial node 7.
CV 3445 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 8.
CV 3446 calculates the stored energy (MJ) in Structure 1660, axial node 8.
CV 3447 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 9.
CV 3448 calculates the stored energy (MJ) in Structure 1660, axial node 9.
CV 3449 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 10.
CV 3450 calculates the stored energy (MJ) in Structure 1660, axial node 10.

CV 3451 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 11.

CV 3452 calculates the stored energy (MJ) in Structure 1660, axial node 11.

CV 3453 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 12.

CV 3454 calculates the stored energy (MJ) in Structure 1660, axial node 12.

CV 3455 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 13.

CV 3456 calculates the stored energy (MJ) in Structure 1660, axial node 13.

CV 3457 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1660, axial node 14.

CV 3458 calculates the stored energy (MJ) in Structure 1660, axial node 14.

CV 3459 calculates the stored energy (MJ) in the outer reflector, Structure 1660.

CV 3461 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1750, axial node 1.

CV 3462 calculates the stored energy (MJ) in Structure 1750, axial node 1.

CV 3463 calculates the volumetric heat capacity (MJ/m³-K) in Structure 1751, axial node 1.

CV 3464 calculates the stored energy (MJ) in Structure 1751, axial node 1.

CV 3466 calculates the stored energy (MJ) in the core region inside the core barrel.

CV 3468 calculates the stored energy (MJ) in the primary pressure vessel.

CV 3471 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2000, axial node 1.

CV 3472 calculates the stored energy (MJ) in Structure 2000, axial node 1.

CV 3473 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2000, axial node 2.

CV 3474 calculates the stored energy (MJ) in Structure 2000, axial node 2.

CV 3475 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2000, axial node 3.

CV 3476 calculates the stored energy (MJ) in Structure 2000, axial node 3.

CV 3477 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2000, axial node 4.

CV 3478 calculates the stored energy (MJ) in Structure 2000, axial node 4.

CV 3479 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2001, axial node 1.

CV 3480 calculates the stored energy (MJ) in Structure 2001, axial node 1.

CV 3481 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2001, axial node 2.

CV 3482 calculates the stored energy (MJ) in Structure 2001, axial node 2.

CV 3483 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2100, axial node 1.

CV 3484 calculates the stored energy (MJ) in Structure 2100, axial node 1.

CV 3485 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2150, axial node 1.

CV 3486 calculates the stored energy (MJ) in Structure 2150, axial node 1.

CV 3487 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2200, axial node 1.

CV 3488 calculates the stored energy (MJ) in Structure 2200, axial node 1.

CV 3489 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2201, axial node 1.

CV 3490 calculates the stored energy (MJ) in Structure 2201, axial node 1.

CV 3501 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 1.
CV 3502 calculates the stored energy (MJ) in Structure 2250, axial node 1.
CV 3503 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 2.
CV 3504 calculates the stored energy (MJ) in Structure 2250, axial node 2.
CV 3505 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 3.
CV 3506 calculates the stored energy (MJ) in Structure 2250, axial node 3.
CV 3507 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 4.
CV 3508 calculates the stored energy (MJ) in Structure 2250, axial node 4.
CV 3509 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 5.
CV 3510 calculates the stored energy (MJ) in Structure 2250, axial node 5.
CV 3511 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 6.
CV 3512 calculates the stored energy (MJ) in Structure 2250, axial node 6.
CV 3513 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 7.
CV 3514 calculates the stored energy (MJ) in Structure 2250, axial node 7.
CV 3515 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 8.
CV 3516 calculates the stored energy (MJ) in Structure 2250, axial node 8.
CV 3517 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 9.
CV 3518 calculates the stored energy (MJ) in Structure 2250, axial node 9.
CV 3519 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 10.
CV 3520 calculates the stored energy (MJ) in Structure 2250, axial node 10.
CV 3521 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 11.
CV 3522 calculates the stored energy (MJ) in Structure 2250, axial node 11.
CV 3523 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 12.
CV 3524 calculates the stored energy (MJ) in Structure 2250, axial node 12.
CV 3525 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 13.
CV 3526 calculates the stored energy (MJ) in Structure 2250, axial node 13.
CV 3527 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 14.
CV 3528 calculates the stored energy (MJ) in Structure 2250, axial node 14.
CV 3529 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 15.
CV 3530 calculates the stored energy (MJ) in Structure 2250, axial node 15.
CV 3531 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 16.
CV 3532 calculates the stored energy (MJ) in Structure 2250, axial node 16.
CV 3533 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 17.
CV 3534 calculates the stored energy (MJ) in Structure 2250, axial node 17.
CV 3535 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 18.

CV 3536 calculates the stored energy (MJ) in Structure 2250, axial node 18.

CV 3537 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 19.

CV 3538 calculates the stored energy (MJ) in Structure 2250, axial node 19.

CV 3539 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 20.

CV 3540 calculates the stored energy (MJ) in Structure 2250, axial node 20.

CV 3541 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 21.

CV 3542 calculates the stored energy (MJ) in Structure 2250, axial node 21.

CV 3543 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2250, axial node 22.

CV 3544 calculates the stored energy (MJ) in Structure 2250, axial node 22.

CV 3546 calculates the stored energy (MJ) in the steam generator tubes, Structure 2250.

CV 3547 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2251, axial node 1.

CV 3548 calculates the stored energy (MJ) in Structure 2251, axial node 1.

CV 3549 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2251, axial node 2.

CV 3550 calculates the stored energy (MJ) in Structure 2251, axial node 2.

CV 3551 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2280, axial node 1.

CV 3552 calculates the stored energy (MJ) in Structure 2280, axial node 1.

CV 3553 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2300, axial node 1.

CV 3554 calculates the stored energy (MJ) in Structure 2300, axial node 1.

CV 3555 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2350, axial node 1.

CV 3556 calculates the stored energy (MJ) in Structure 2350, axial node 1.

CV 3557 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2400, axial node 1.

CV 3558 calculates the stored energy (MJ) in Structure 2400, axial node 1.

CV 3559 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2500, axial node 1.

CV 3560 calculates the stored energy (MJ) in Structure 2500, axial node 1.

CV 3561 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2500, axial node 2.

CV 3562 calculates the stored energy (MJ) in Structure 2500, axial node 2.

CV 3563 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2500, axial node 3.

CV 3564 calculates the stored energy (MJ) in Structure 2500, axial node 3.

CV 3565 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2580, axial node 1.

CV 3566 calculates the stored energy (MJ) in Structure 2580, axial node 1.

CV 3567 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2600, axial node 1.

CV 3568 calculates the stored energy (MJ) in Structure 2600, axial node 1.

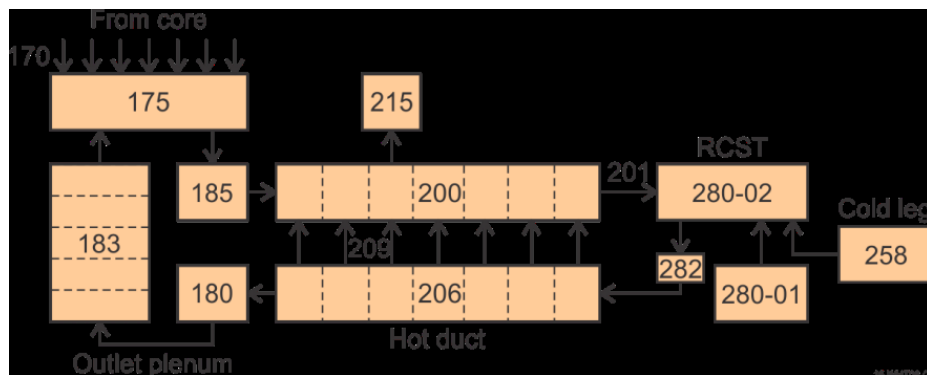
CV 3569 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2700, axial node 1.

CV 3570 calculates the stored energy (MJ) in Structure 2700, axial node 1.

CV 3571 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2700, axial node 2.

CV 3578 calculates the stored energy (MJ) in the PCS.

An alternate model of the hot duct, outlet plenum, and RCST was developed for use in the double-ended hot duct break simulations. The phenomenon of interest in this scenario is single-phase countercurrent flow in the hot duct, with hot (or lighter) gas flowing from the pressure vessel outlet plenum to the RCST along the top of the pipe, with colder (or denser) gas returning from the RCST to the outlet plenum along the bottom of the pipe. Since the code cannot simulate this directly in a single control volume, the nodalization must be changed. Figure 7 shows the revised nodalization.



The second volume in the RCST is modified so that it connects to the top half of the hot duct while maintaining the connection to the cold leg side of the break (which is not renodalized). A small volume (Component 282) is added to make the connection from this second volume to the bottom half of the hot

duct. The intent of the original model was for the second volume in the RCST to include all of the tank volume involved in the fluid mixing. This nodalization maintains that. By making the added component very small, its conditions should be very close to those in the mixing volume. No changes are needed for the heat structures.

A number of control variables were changed or added as a result of the renodalization.

Brief descriptions of the altered components are provided below.

Component 175 represents the top 2 cm of the pressure vessel outlet plenum. It is modeled as a branch with two junctions, both connected to the outlet. The first connects the outlet of this component to the inlet of Component 185, and the second connects the outlet of Component 183 to the outlet of this component. This component is also connected to all of the core channels by Component 170.

Component 180 represents a portion of the outlet plenum near the bottom half of the hot duct. It is modeled as a branch component with two junctions. The first junction connects the outlet of the bottom half of the hot duct, Component 206, to the middle of this component, and the second junction connects the outlet of this component to the inlet of Component 183.

Component 183 is a five-volume pipe representing the bulk of the outlet plenum. The number of pipe cells can be altered to try to reduce the effect of numerical diffusion in the calculations.

Component 185 represents a portion of the outlet plenum near the top half of the hot duct. It is modeled as a branch with one junction, connecting the middle of this component to the inlet of the top half of the hot duct, Component 200.

Component 200 is a pipe representing the top half of the hot duct connecting the pressure vessel outlet plenum to the RCST. It has seven internal volumes, the third of which is connected to the hot leg piping leading to the steam generator. The flow area is half that of the full pipe, the hydraulic diameter is the same as that of the full pipe, and the z-direction length is half the pipe diameter. The break valve loss coefficient is maintained at the fifth internal junction.

Component 201 connects the outlet of Component 200 to the middle of Component 280-02. It is modeled as a single junction. The smooth area change model is used, with forward and reverse loss coefficients of 1.0 and 0.5, respectively.

Component 206 is a pipe representing the bottom half of the hot duct. It has seven internal volumes, and is oriented so that positive flow is from the RCST to the outlet plenum. The flow area is half that of the full pipe, and the hydraulic diameter is the same as that of the full pipe. The z-direction length is less than half the pipe diameter, so that elevation closure is maintained with the connection to the outlet plenum. The break valve loss coefficient is maintained at the second internal junction.

Component 209 is a multiple junction component connecting the two halves of the hot duct. The seven junctions are oriented from the top of the volumes in Component 206 to the bottom of the volumes in Component 200. The junction area is set to the product of the pipe cell length and the diameter. Small loss coefficients of 0.1 are included to provide some resistance to unphysical recirculating flows that the code has had a tendency to predict in some previous calculations with similar geometry.

Component 280 is the RCST. The second volume has been compressed with this renodalization; it has the same volume as before, but now has a height of 0.14898 m instead of 4.0831 m. This allows the top of the hot duct to connect to the middle of the volume while the cold leg break connects to the bottom of the volume. All other input for the component is unchanged.

Component 282 is a small portion of the RCST between the inlet to Volume 280-02 and the inlet to the bottom half of the hot duct. It is modeled as a branch with two junctions: the first junction connects the inlet of Component 280-02 to the inlet of this component, and the second junction connects the outlet of this component to the inlet of Component 206. The area of this component is arbitrarily set to a small value, so that its fluid conditions should be nearly the same as those in Component 280-02, the mixed volume of the RCST, but not so small that its Courant limit affects the time step during the transient.

Forward and reverse loss coefficients of 0.5 and 1.0, respectively, are used at the connection to the hot duct. No heat structures are associated with this component.

Structure 1750 represents the outlet plenum lower plate. The only change from the original structure is that the left boundary volume is changed to 183010000 (from 175010000).

Structure 2000 represents a portion of the top half of the hot duct. It is identical to the original structure, except that the area factor is cut in half.

Structure 2001 represents a portion of the top half of the hot duct. It is identical to the original structure, except that the area factor is cut in half.

Structure 2002 represents the portion of the top half of the hot duct between the break valve and the RCST. It is identical to Structure 2100, except that the area factor is cut in half.

Structure 2060 represents the portion of the bottom half of the hot duct between the break valve and the RCST. It is identical to Structure 2100, except that the area factor is cut in half.

Structure 2061 represents a portion of the bottom half of the hot duct. It is identical to Structure 2001, except for the left boundary volumes.

Structure 2062 represents a portion of the bottom half of the hot duct. It is identical to Structure 2000, except for the left boundary volumes.

CV 1401 calculates the environmental heat loss (W) from Structures 2001 and 2061.

CV 1615 calculates the total fluid mass (kg) in the hot leg, Components 200 and 206.

CV 1621 calculates the total fluid mass (kg) in the RCST, Components 258, 280, and 282.

CV 3472 calculates the stored energy (MJ) in Structure 2000, axial node 1.

CV 3474 calculates the stored energy (MJ) in Structure 2000, axial node 2.

CV 3476 calculates the stored energy (MJ) in Structure 2000, axial node 3.

CV 3478 calculates the stored energy (MJ) in Structure 2000, axial node 4.

CV 3480 calculates the stored energy (MJ) in Structure 2001, axial node 1.

CV 3482 calculates the stored energy (MJ) in Structure 2001, axial node 2.

CV 3483 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2002, axial node 1.

CV 3484 calculates the stored energy (MJ) in Structure 2002, axial node 1.

CV 3577 calculates the stored energy (MJ) in the primary coolant system piping.

CV 3581 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2060, axial node 1.

CV 3582 calculates the stored energy (MJ) in Structure 2060, axial node 1.

CV 3583 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2061, axial node 1.

CV 3584 calculates the stored energy (MJ) in Structure 2061, axial node 1.

CV 3585 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2061, axial node 2.

CV 3586 calculates the stored energy (MJ) in Structure 2061, axial node 2.

CV 3587 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2062, axial node 1.

CV 3588 calculates the stored energy (MJ) in Structure 2062, axial node 1.

CV 3589 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2062, axial node 2.

CV 3590 calculates the stored energy (MJ) in Structure 2062, axial node 2.

CV 3591 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2062, axial node 3.

CV 3592 calculates the stored energy (MJ) in Structure 2062, axial node 3.

CV 3593 calculates the volumetric heat capacity (MJ/m³-K) in Structure 2062, axial node 4.

CV 3594 calculates the stored energy (MJ) in Structure 2062, axial node 4.

13. NODALIZATION STUDY

All of the calculations have been performed at full power (2.2 MW) with helium as the primary coolant.

The steam generator was originally nodalized with 12 volumes in the tubes, six up and six down, with the bend in the tubes in Cells 6 and 7. The boiler and downcomer regions of the secondary side of the steam generator were modeled with node boundaries at the same elevations. A sensitivity calculation was performed in which the number of cells in the tubes was increased to 22, by doubling the number of nodes in the straight sections and leaving the bend alone; this region of the tubes was in single-phase vapor convection heat transfer on the secondary side anyway, so doubling the nodes here would provide no benefit, but would further reduce the Courant limit. The boiler and downcomer nodalizations were also increased to match the node boundaries on the primary side. For the first and last cells in the tubes, rather than dividing the tube cell length in two, the cell boundary was located at an elevation that divided the first cell in the boiler into equal length cells. This makes the first cell in the tubes longer than the second, because the first cell includes the length of tube in the tube sheet, and results in the system Courant limit being located in the second tube cell. The more detailed model produced more stable results than the coarser nodalization.

With the steam generator modeled, the Courant limit is a little above 0.002 s, determined by the second volume in the tubes. Without the steam generator, the Courant limit is about 0.0047 s.

14. COMPUTER FILES

Computer files associated with the input file are listed in Table 1. In addition to the file name, a description of the file is included, along with the checksum value (gnu command “cksum”).

Table 1. Listing of computer files.

File name	Description	Checksum value
httf-base.i	RELAP5-3D input file	2319698913
HTTF base 2018-05-30QA.xlsx	Workbook containing the final version of the model and supporting calculations	2084154050
HTTF base 2015-02-10QA.xlsx	Excel workbook containing the version of the model and supporting calculations for the initial quality assurance review	3765750314
HTTF base 2015-06-22QA.xlsx	Excel workbook containing the version of the model and supporting calculations after the initial quality assurance review	392234047
HTTF base 2017-03-23QA.xlsx	Excel workbook containing the version of the model and supporting calculations for the second quality assurance review	2735886914
HTTF base 2017-03-30QA.xlsx	Excel workbook containing the version of the model and supporting calculations after the second quality assurance review	1132593988
HTTF base 2018-05-16QA.xlsx	Excel workbook containing the version of the model and supporting calculations for the final quality assurance review	921649429

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Table 2. HTTF drawings used in developing the input model.

Drawing Number	Sheet	Revision	Date
OSU-HTTF-CORE-DWG-001-R1	1	1	3/13/2018
OSU-HTTF-CORE-DWG-004-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-004-R0	2	A	4/1/2013
OSU-HTTF-CORE-DWG-005-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-005-R0	4	A	4/1/2013
OSU-HTTF-CORE-DWG-006-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-006-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-011-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-012-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-013-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-014-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-015-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-016-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-016-R0	2	A	4/1/2013
OSU-HTTF-CORE-DWG-016-R0	3	A	4/1/2013
OSU-HTTF-CORE-DWG-017-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-019-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-021-R0	1	A	4/1/2013
OSU-HTTF-CORE-DWG-021-R0	2	A	4/1/2013
OSU-HTTF-CORE-DWG-021-R0	3	A	4/1/2013
OSU-HTTF-CORE-DWG-026-R0	1	0	4/19/2018
OSU-HTTF-GEN-DWG-001B	2	1	6/1/2017
OSU-HTTF-GEN-DWG-009A	1	0	11/21/2016
OSU-HTTF-GEN-DWG-009C	3	0	11/21/2016
OSU-HTTF-GEN-DWG-009D	4	0	11/21/2016
OSU-HTTF-GEN-DWG-009E	5	0	11/21/2016
OSU-HTTF-GEN-DWG-009F	6	0	11/21/2016
OSU-HTTF-GEN-DWG-009G	7	0	11/21/2016
OSU-HTTF-GEN-DWG-009H	8	0	11/21/2016
OSU-HTTF-PRIM-DWG-002	1	1	2/15/2018
OSU-HTTF-PRIM-DWG-002	3	1	2/15/2018
OSU-HTTF-PRIM-DWG-002	5	1	2/15/2018
OSU-HTTF-PRIM-DWG-002	6	1	2/15/2018
OSU-HTTF-PRIM-DWG-002	7	1	2/15/2018
OSU-HTTF-PRIM-DWG-002	8	1	2/15/2018
OSU-HTTF-PRIM-DWG-002	9	1	2/15/2018
OSU-HTTF-PRIM-DWG-004A	1	0	11/21/2016
OSU-HTTF-PRIM-DWG-005A	1	0	11/21/2016

Table 2. continued

Drawing Number	Sheet	Revision	Date
OSU-HTTF-PRIM-DWG-011	1	2	3/14/2018
OSU-HTTF-PRIM-DWG-012	1	1	3/1/2018
OSU-HTTF-PRIM-DWG-019	1	0	11/20/2017
OSU-HTTF-RCCS-DWG-006A	1	0	11/21/2016
OSU-HTTF-RCCS-DWG-007A	1	0	11/21/2016
OSU-HTTF-RCSS-DWG-008A	1	0	11/21/2016
OSU-HTTF-RCSS-DWG-008C	3	0	11/21/2016
OSU-HTTF-SEC-DWG-003A	1	0	11/21/2016
OSU-HTTF-SEC-DWG-003B	2	0	11/21/2016
OSU-HTTF-SEC-DWG-003C	3	0	11/21/2016

Appendix A

Input Model Listing

Appendix A. Input Model Listing

= HTTF system model
* base model
*
* This model represents the High Temperature Test Facility (HTTF) (prismatic core design), which is being built at Oregon State University to support the Advanced Reactor Technologies program.
*
* This is a full system model developed to perform assessment calculations using experiment data from the facility. The model includes the primary pressure vessel and internals, the primary coolant system, the secondary coolant system, and the reactor cavity cooling system (RCCS).
*
* The core is modeled with three parallel channels, each representing one of the three rings in the annular heated region. The heater rods radiate to the surrounding ceramic material. The helium gap between the rods and the ceramic is included.
*
* The central reflector is modeled in three pieces: a solid inner ring, a middle ring with coolant holes, and an outer solid ring next to the heated region.
*
* The side reflector is also modeled with a solid ring next to the heated portion of the core, a middle ring with coolant holes, and a solid ring outside it. The permanent side reflector is also modeled as a solid ring.
*
* The primary coolant system includes the hot and cold ducts, the steam generator plenums and tubes, the gas circulator, pressure relief and depressurization valves, the check valve at the steam generator inlet, the loop isolation valve, and connecting piping. Break valves at the end of the hot duct and in the cold leg piping connect to the reactor cavity simulation tank (RCST).
*
* The secondary coolant system includes the feedwater pump, steam generator, the steam line pressure control valve, the pressure relief valve, and associated piping. The feedwater piping is not modeled explicitly: the approximate length and correct elevation change are input, as the flow resistance of the feedwater piping is not important to the plant response.
*
* The RCCS is modeled as a set of panels completely surrounding the primary pressure vessel. Flowing water cools the front side of the panels, and natural convection heat transfer cools the back side.
*
* The tank that provides water to the feedwater and RCCS pumps is modeled, along with its water supply, drain valve, and vent line.
*
* The air cavity between the primary pressure vessel and the RCCS panels is also included in the model.
*
* Trips and control systems are provided for the circulator, the feedwater and RCCS pumps, the break and loop isolation valves, the pressure relief and depressurization valves, and the tank water supply and drain valves.
*
* All of the vertically-oriented heat structures have 2-D conduction turned on where possible. Axial conduction between the core and the top and bottom reflectors, and in three of the four solid reflector regions, is modeled using conduction enclosures.
*
* Core power of 2.2 MW.
* Inlet coolant temperature of 258.6 C.
* Outlet coolant temperature of 687 C.
*

```

*****
1 12 54
100 new stdy-st
101 run
102 si si
107 1 1 1
110 air nitrogen
115 1.0 0.0
120 258010000 1.7907 hen Primary
121 900010000 1.7907 n2 Contain
122 950030000 1.7907 h2o SCS-RCCS
123 141010000 4.088765 hen hegap1
124 146010000 4.088765 hen hegap2
125 151010000 4.088765 hen hegap3
201 30000.0 1.0-6 0.002 19 30000 6000000 60000000
*
*****
* additional plot variables
*****
*
20800001 htmode 225000101
20800002 htmode 225000201
20800003 htmode 225000301
20800004 htmode 225000401
20800005 htmode 225000501
20800006 htmode 225000601
20800007 htmode 225000701
20800008 htmode 225000801
20800009 htmode 225000901
20800010 htmode 225001001
20800011 htmode 225001101
20800012 htmode 225001201
20800013 htmode 225001301
20800014 htmode 225001401
20800015 htmode 225001501
20800016 htmode 225001601
20800017 htmode 225001701
20800018 htmode 225001801
20800019 htmode 225001901
20800020 htmode 225002001
20800021 htmode 225002101
20800022 htmode 225002201
20800031 systms 1
20800032 systms 5
*
*****
* trips
*****
*
20600000 expanded
*
* scram trip
20601000 time 0 ge null 0 1.00E+06 1
*
* break trips
20602050 time 0 ge null 0 1.00E+06 1 * open hot duct break valve
20602060 time 0 le null 0 -1.0 1 * close hot duct break valve
20602550 time 0 ge null 0 1.00E+06 1 * open cold leg break valve
20602560 time 0 le null 0 -1.0 1 * close cold leg break valve
*20600250 time 0 le null 0 -1.0 1 * open CRD break valve
*20600750 time 0 le null 0 -1.0 1 * open vessel bottom break valve
*
* valve V-203 trips

```

```

20602450 time 0 ge null 0 -1.0 1 * open valve
20602460 time 0 le null 0 -1.0 1 * close valve
*
* primary coolant system relief valve trips
20602940 p 293010000 gt null 0 1.16E+06 n * opening pressure
20602950 p 293010000 lt null 0 1.10E+06 n * closing pressure
20612940 294 or 1295 n * initial opening or already open
20612950 1294 and -295 n * open valve
*
* primary coolant system depressurization valve trips
20602960 time 0 ge null 0 1.00E+06 n * open valve manually
20602970 time 0 ge null 0 1.00E+06 n * close valve manually
20612960 296 and -297 n * open valve
*
* steam generator relief valve trips
20603940 p 390010000 gt null 0 7.91E+05 n * opening pressure
20603950 p 390010000 lt null 0 7.70E+05 n * closing pressure
20613940 394 or 1395 n * initial opening or already open
20613950 1394 and -395 n * open valve
*
* water supply valve controls for tank T-010
20604100 cntrlvar 450 lt cntrlvar 451 0.0 n * low liquid level setpoint
20604110 cntrlvar 450 gt cntrlvar 452 0.0 n * high liquid level setpoint
20604120 cntrlvar 450 gt cntrlvar 453 0.0 n * level above mid-range
20614090 410 or 1410 n
20614100 1409 and -412 n * open supply valve
20614110 411 or 1412 n
20614120 1411 and 412 n * close supply valve
*
*****
* hydrodynamics
*****
*
* steady state pressure control
*
2330000 PCSPctrl snljun
2330101 230010000 234000000 0.0 0.0 0.0 0
2330201 0 0.0 0.0 0.0
*
2340000 cmprssr tmdpv01
2340101 0.03228 1.203 0.0 0.0 0.0 0.0 0.0 0.0 10
2340200 3
2340201 0.0 7.00E+05 531.75
2340200 3 0 cntrlvar 234
2340201 100000.0 1.00E+05 531.75
2340202 800000.0 8.00E+05 531.75
*
* pressure vessel inlet region
*
1000000 vesinlet branch
1000001 2 1
1000101 0.0 0.39395 0.1532
1000102 0.0 -90.0 -0.39395
1000103 0.000046 0.1143 0
1000200 3 7.00E+05 531.75
1001101 270010000 100000000 0.0649 0.60 0.39 0000001
1002101 100010000 105000000 0.1208 0.0 0.0 0000102
1001110 0.0 0.0 1.0 1.0
1002110 0.0 0.0 1.0 1.0
1001201 0.0 1.0 0.0
1002201 0.0 1.0 0.0
*
* coolant volume in core support structure

```



```

*
1050000  consuprt  pipe
1050001  2
1050101  0.19393  1
1050102  0.19393  2
1050301  0.7572  1
1050302  0.7572  2
1050401  0.0  2
1050601  7.7107  1
1050602  0.0  2
1050701  0.10160  1
1050702  0.0  2
1052201  0.0  0.0  0.0889  1
1052202  0.0  0.0  0.0889  2
1050801  0.000046  0.128  1
1050802  0.000046  0.136  2
1052401  0.000046  0.0  2
1050901  0.95  0.95  1
1051001  0  2
1051101  0  1
1051201  3  7.00E+05  531.75  0.0  0.0  0.0  2
1051300  1
1051301  0.0  1.0  0.0  1
1051401  0.406  0.0  1.0  1.0  1
*
* jacket shell
*
1100000  jacketsh  branch
1100001  2  1
1100101  0.0923  0.403475  0.0
1100102  0.0  90.0  0.403475
1100103  0.000046  0.0381  0
1100200  3  7.00E+05  531.75
1101101  105010000  110000000  0.1208  0.0  0.0  0
1102101  110010000  115000000  0.0  0.0  0.0  100
1101110  0.0  0.0  1.0  1.0
1102110  0.0  0.0  1.0  1.0
1101201  0.0  1.0  0.0
1102201  0.0  1.0  0.0
*
* pressure vessel/core barrel gap
*
1150000  rv-bargp  pipe
1150001  15
1150101  0.28388  15
1150301  0.25146  1
1150302  0.25146  2
1150303  0.19812  12
1150304  0.19050  13
1150305  0.20320  14
1150306  0.27320  15
1150401  0.0  15
1150601  90.0  15
1150801  0.000046  0.114  15
1150901  0.0  0.0  14
1151001  0  15
1151101  0  14
1151201  3  7.00E+05  531.75  0.0  0.0  0.0  15
1151300  1
1151301  0.0  1.0  0.0  14
1151401  0.114  0.0  1.0  1.0  14
*
* core inlet plenum

```

```

*
1200000  inltplnm  branch
1200001  1  1
1200101  0.0  0.9557  1.4051
1200102  0.0  90.0  0.9557
1200103  0.000046  0.0  0
1200200  3  7.00E+05  531.75
1201101  115140002  120000000  0.0569  2.22  2.22  0
1201110  0.045  0.0  1.0  1.0
1201201  0.0  1.0  0.0
*
* core inlet junctions
*
1250000  corejuni  mtpljun
1250001  5  1
* 0nnm  from  to  area  kfor  krev  efvcchs  sub  2ph  sup
1250011  120000000  132000000  0.0  0.5  1.0  200  1.0  1.0  1.0
* inc-frm  inc-to  0  limit
1250012  0  0  0.0  1
* 0nnm  from  to  area  kfor  krev  efvcchs  sub  2ph  sup
1250021  120000000  140000000  0.0  0.5  1.0  200  1.0  1.0  1.0
* inc-frm  inc-to  0  limit
1250022  0  0  0.0  2
* 0nnm  from  to  area  kfor  krev  efvcchs  sub  2ph  sup
1250031  120000000  145000000  0.0  0.5  1.0  200  1.0  1.0  1.0
* inc-frm  inc-to  0  limit
1250032  0  0  0.0  3
* 0nnm  from  to  area  kfor  krev  efvcchs  sub  2ph  sup
1250041  120000000  150000000  0.0  0.5  1.0  200  1.0  1.0  1.0
* inc-frm  inc-to  0  limit
1250042  0  0  0.0  4
* 0nnm  from  to  area  kfor  krev  efvcchs  sub  2ph  sup
1250051  120000000  162000000  0.0  0.5  1.0  200  1.0  1.0  1.0
* inc-frm  inc-to  0  limit
1250052  0  0  0.0  5
* 1nnm  mflowf  mflowg  #
1251011  0.0  0.01  1
1251021  0.0  0.05  2
1251031  0.0  0.05  3
1251041  0.0  0.05  4
1251051  0.0  0.01  5
* 2nnm  Dhyd  b  c  m  #
1252011  0.01905  0.0  1.0  1.0  1
1252021  0.0150  0.0  1.0  1.0  2
1252031  0.0159  0.0  1.0  1.0  3
1252041  0.0144  0.0  1.0  1.0  4
1252051  0.015875  0.0  1.0  1.0  5
*
* core bypass path through holes in central reflector ring 2
*
1320000  crcholes  pipe
1320001  14
1320101  0.0017101  14
1320301  0.20320  1
1320302  0.19050  2
1320303  0.19812  12
1320304  0.25146  13
1320305  0.25146  14
1320401  0.0  14
1320601  -90.0  14
1320801  0.00010  0.01905  14
1320901  0.08  0.08  13
1321001  0  14

```

```

1321101 0 13
1321201 3 7.00E+05 531.75 0.0 0.0 0.0 2
1321202 3 7.00E+05 531.75 0.0 0.0 0.0 3
1321203 3 7.00E+05 574.59 0.0 0.0 0.0 4
1321204 3 7.00E+05 617.43 0.0 0.0 0.0 5
1321205 3 7.00E+05 660.27 0.0 0.0 0.0 6
1321206 3 7.00E+05 703.11 0.0 0.0 0.0 7
1321207 3 7.00E+05 745.95 0.0 0.0 0.0 8
1321208 3 7.00E+05 788.79 0.0 0.0 0.0 9
1321209 3 7.00E+05 831.63 0.0 0.0 0.0 10
1321210 3 7.00E+05 874.47 0.0 0.0 0.0 11
1321211 3 7.00E+05 917.31 0.0 0.0 0.0 12
1321212 3 7.00E+05 960.15 0.0 0.0 0.0 14
1321300 1
1321301 0.0 0.01 0.0 13
1321401 0.01905 0.0 1.0 1.0 13
*
* inner core ring coolant channels
*
1400000 coreinnr pipe
1400001 14
1400101 0.02214 14
1400301 0.20320 1
1400302 0.19050 2
1400303 0.19812 12
1400304 0.25146 13
1400305 0.25146 14
1400401 0.0 14
1400601 -90.0 14
1400801 0.00010 0.0150 14
1400901 0.08 0.08 13
1401001 0 14
1401101 0 13
1401201 3 7.00E+05 531.75 0.0 0.0 0.0 2
1401202 3 7.00E+05 531.75 0.0 0.0 0.0 3
1401203 3 7.00E+05 574.59 0.0 0.0 0.0 4
1401204 3 7.00E+05 617.43 0.0 0.0 0.0 5
1401205 3 7.00E+05 660.27 0.0 0.0 0.0 6
1401206 3 7.00E+05 703.11 0.0 0.0 0.0 7
1401207 3 7.00E+05 745.95 0.0 0.0 0.0 8
1401208 3 7.00E+05 788.79 0.0 0.0 0.0 9
1401209 3 7.00E+05 831.63 0.0 0.0 0.0 10
1401210 3 7.00E+05 874.47 0.0 0.0 0.0 11
1401211 3 7.00E+05 917.31 0.0 0.0 0.0 12
1401212 3 7.00E+05 960.15 0.0 0.0 0.0 14
1401300 1
1401301 0.0 0.05 0.0 13
1401401 0.0150 0.0 1.0 1.0 13
*
* inner core ring heater rod helium gap
*
1410000 hegapin pipe
1410001 10
1410101 0.01911 10
1410301 0.19812 10
1410401 0.0 10
1410601 -90.0 10
1410801 0.00010 0.010887103 10
1410901 0.0 0.0 9
1411001 0 10
1411101 0 9
1411201 3 7.00E+05 900.0 0.0 0.0 0.0 10
1411300 1

```

```

1411301  0.0000  0.0  0.0  9
*
1420000  hegapin  sngljun
1420101  143010000  141000000  0.0  0.0  0.0  0
1420201  0  0.0  0.0  0.0
*
* helium gap boundary volume
*
1430000  hegapin  tmdpvol
1430101  0.01911  1.0  0.0  0.0  0.0  0.0  0.0  0.0  10
1430200  3  0  tempg  141010000
1430201  300.0  7.00E+05  300.0
1430202  2000.0  7.00E+05  2000.0
*
* middle core ring coolant channels
*
1450000  coremid  pipe
1450001  14
1450101  0.02850  14
1450301  0.20320  1
1450302  0.19050  2
1450303  0.19812  12
1450304  0.25146  13
1450305  0.25146  14
1450401  0.0  14
1450601  -90.0  14
1450801  0.00010  0.0159  14
1450901  0.08  0.08  13
1451001  0  14
1451101  0  13
1451201  3  7.00E+05  531.75  0.0  0.0  0.0  2
1451202  3  7.00E+05  531.75  0.0  0.0  0.0  3
1451203  3  7.00E+05  574.59  0.0  0.0  0.0  4
1451204  3  7.00E+05  617.43  0.0  0.0  0.0  5
1451205  3  7.00E+05  660.27  0.0  0.0  0.0  6
1451206  3  7.00E+05  703.11  0.0  0.0  0.0  7
1451207  3  7.00E+05  745.95  0.0  0.0  0.0  8
1451208  3  7.00E+05  788.79  0.0  0.0  0.0  9
1451209  3  7.00E+05  831.63  0.0  0.0  0.0  10
1451210  3  7.00E+05  874.47  0.0  0.0  0.0  11
1451211  3  7.00E+05  917.31  0.0  0.0  0.0  12
1451212  3  7.00E+05  960.15  0.0  0.0  0.0  14
1451300  1
1451301  0.0  0.05  0.0  13
1451401  0.0159  0.0  1.0  1.0  13
*
* middle core ring heater rod helium gap
*
1460000  hegapmid  pipe
1460001  10
1460101  0.02457  10
1460301  0.19812  10
1460401  0.0  10
1460601  -90.0  10
1460801  0.00010  0.010887103  10
1460901  0.0  0.0  9
1461001  0  10
1461101  0  9
1461201  3  7.00E+05  900.0  0.0  0.0  0.0  10
1461300  1
1461301  0.0  0.0  0.0  9
*
1470000  hegapmid  sngljun

```

```

1470101 148010000 146000000 0.0 0.0 0.0 0
1470201 0 0.0 0.0 0.0
*
* helium gap boundary volume
*
1480000 hegapmid tmdpv01
1480101 0.02457 1.0 0.0 0.0 0.0 0.0 0.0 0.0 10
1480200 3 0 tempg 146010000
1480201 300.0 7.00E+05 300.0
1480202 2000.0 7.00E+05 2000.0
*
* outer core ring coolant channels
*
1500000 coreoutr pipe
1500001 14
1500101 0.03249 14
1500301 0.20320 1
1500302 0.19050 2
1500303 0.19812 12
1500304 0.25146 13
1500305 0.25146 14
1500401 0.0 14
1500601 -90.0 14
1500801 0.00010 0.0144 14
1500901 0.08 0.08 13
1501001 0 14
1501101 0 13
1501201 3 7.00E+05 531.75 0.0 0.0 0.0 2
1501202 3 7.00E+05 531.75 0.0 0.0 0.0 3
1501203 3 7.00E+05 574.59 0.0 0.0 0.0 4
1501204 3 7.00E+05 617.43 0.0 0.0 0.0 5
1501205 3 7.00E+05 660.27 0.0 0.0 0.0 6
1501206 3 7.00E+05 703.11 0.0 0.0 0.0 7
1501207 3 7.00E+05 745.95 0.0 0.0 0.0 8
1501208 3 7.00E+05 788.79 0.0 0.0 0.0 9
1501209 3 7.00E+05 831.63 0.0 0.0 0.0 10
1501210 3 7.00E+05 874.47 0.0 0.0 0.0 11
1501211 3 7.00E+05 917.31 0.0 0.0 0.0 12
1501212 3 7.00E+05 960.15 0.0 0.0 0.0 14
1501300 1
1501301 0.0 0.05 0.0 13
1501401 0.0144 0.0 1.0 1.0 13
*
* outer core ring heater rod helium gap
*
1510000 hegapout pipe
1510001 10
1510101 0.02799 10
1510301 0.19812 10
1510401 0.0 10
1510601 -90.0 10
1510801 0.00010 0.010887103 10
1510901 0.0 0.0 9
1511001 0 10
1511101 0 9
1511201 3 7.00E+05 900.0 0.0 0.0 0.0 10
1511300 1
1511301 0.0000 0.0 0.0 9
*
1520000 hegapout sngljun
1520101 153010000 151000000 0.0 0.0 0.0 0
1520201 0 0.0 0.0 0.0
*

```

```

* helium gap boundary volume
*
1530000  hegapout  tmdpvol
1530101  0.02799  1.0  0.0  0.0  0.0  0.0  0.0  10
1530200  3  0  tempg  151010000
1530201  300.0  7.00E+05  300.0
1530202  2000.0  7.00E+05  2000.0
*
* coolant holes in side reflector
*
1620000  srcholes  pipe
1620001  14
1620101  0.00713  14
1620301  0.20320  1
1620302  0.19050  2
1620303  0.19812  12
1620304  0.25146  13
1620305  0.25146  14
1620401  0.0  14
1620601  -90.0  14
1620801  0.00010  0.015875  14
1620901  0.08  0.08  13
1621001  0  14
1621101  0  13
1621201  3  7.00E+05  531.75  0.0  0.0  0.0  2
1621202  3  7.00E+05  531.75  0.0  0.0  0.0  3
1621203  3  7.00E+05  574.59  0.0  0.0  0.0  4
1621204  3  7.00E+05  617.43  0.0  0.0  0.0  5
1621205  3  7.00E+05  660.27  0.0  0.0  0.0  6
1621206  3  7.00E+05  703.11  0.0  0.0  0.0  7
1621207  3  7.00E+05  745.95  0.0  0.0  0.0  8
1621208  3  7.00E+05  788.79  0.0  0.0  0.0  9
1621209  3  7.00E+05  831.63  0.0  0.0  0.0  10
1621210  3  7.00E+05  874.47  0.0  0.0  0.0  11
1621211  3  7.00E+05  917.31  0.0  0.0  0.0  12
1621212  3  7.00E+05  960.15  0.0  0.0  0.0  14
1621300  1
1621301  0.0  0.01  0.0  13
1621401  0.015875  0.0  1.0  1.0  13
*
* core bypass path - gap between side reflector and permanent side reflector
*
1640000  gapsr-ps  pipe
1640001  14
1640101  0.0342744  14
1640301  0.20320  1
1640302  0.19050  2
1640303  0.19812  12
1640304  0.25146  13
1640305  0.25146  14
1640401  0.0  14
1640601  -90.0  14
1640801  0.00010  0.01463  14
1640901  0.08  0.08  13
1641001  0  14
1641101  0  13
1641201  3  7.00E+05  531.75  0.0  0.0  0.0  2
1641202  3  7.00E+05  531.75  0.0  0.0  0.0  3
1641203  3  7.00E+05  574.59  0.0  0.0  0.0  4
1641204  3  7.00E+05  617.43  0.0  0.0  0.0  5
1641205  3  7.00E+05  660.27  0.0  0.0  0.0  6
1641206  3  7.00E+05  703.11  0.0  0.0  0.0  7
1641207  3  7.00E+05  745.95  0.0  0.0  0.0  8

```

```

1641208 3 7.00E+05 788.79 0.0 0.0 0.0 9
1641209 3 7.00E+05 831.63 0.0 0.0 0.0 10
1641210 3 7.00E+05 874.47 0.0 0.0 0.0 11
1641211 3 7.00E+05 917.31 0.0 0.0 0.0 12
1641212 3 7.00E+05 960.15 0.0 0.0 0.0 14
1641300 1
1641301 0.0 0.01 0.0 13
1641401 0.01463 0.0 1.0 1.0 13
*
* core bypass path - gap between permanent side reflector and core barrel
*
1660000 gapsr-cb pipe
1660001 15
1660101 0.0301457 15
1660301 0.20320 1
1660302 0.19050 2
1660303 0.19812 12
1660304 0.25146 13
1660305 0.25146 14
1660306 0.22225 15
1660401 0.0 15
1660601 -90.0 15
1660801 0.00010 0.0127 15
1660901 0.08 0.08 14
1661001 0 15
1661101 0 14
1661201 3 7.00E+05 531.75 0.0 0.0 0.0 2
1661202 3 7.00E+05 531.75 0.0 0.0 0.0 3
1661203 3 7.00E+05 574.59 0.0 0.0 0.0 4
1661204 3 7.00E+05 617.43 0.0 0.0 0.0 5
1661205 3 7.00E+05 660.27 0.0 0.0 0.0 6
1661206 3 7.00E+05 703.11 0.0 0.0 0.0 7
1661207 3 7.00E+05 745.95 0.0 0.0 0.0 8
1661208 3 7.00E+05 788.79 0.0 0.0 0.0 9
1661209 3 7.00E+05 831.63 0.0 0.0 0.0 10
1661210 3 7.00E+05 874.47 0.0 0.0 0.0 11
1661211 3 7.00E+05 917.31 0.0 0.0 0.0 12
1661212 3 7.00E+05 960.15 0.0 0.0 0.0 15
1661300 1
1661301 0.0 0.01 0.0 14
1661401 0.0127 0.0 1.0 1.0 14
*
1680000 PSRoutlt snljun
1680101 166150004 175010003 0.00596 0.84 0.46 3
1680201 0 0.0 0.01 0.0
*
* core outlet junctions
*
1700000 corejuno mtpljun
1700001 6 1
* 0nnm from to area kfor krev efvcchs sub 2ph sup
1700011 132010000 175000000 0.0 1.0 0.5 200 1.0 1.0 1.0
* inc-frm inc-to 0 limit
1700012 0 0 0 1
* 0nnm from to area kfor krev efvcchs sub 2ph sup
1700021 140010000 175000000 0.0 2.5 2.5 200 1.0 1.0 1.0
* inc-frm inc-to 0 limit
1700022 0 0 0 2
* 0nnm from to area kfor krev efvcchs sub 2ph sup
1700031 145010000 175000000 0.0 2.5 2.5 200 1.0 1.0 1.0
* inc-frm inc-to 0 limit
1700032 0 0 0 3
* 0nnm from to area kfor krev efvcchs sub 2ph sup

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1700041 150010000 175000000 0.0 2.5 2.5 200 1.0 1.0 1.0
* inc-frm inc-to 0 limit
1700042 0 0 0 4
* Onnm from to area kfor krev efvcchs sub 2ph sup
1700051 162010000 175000000 0.0 1.0 0.5 200 1.0 1.0 1.0
* inc-frm inc-to 0 limit
1700052 0 0 0 5
* Onnm from to area kfor krev efvcchs sub 2ph sup
1700061 164010000 175000000 0.0 1.0 0.5 200 1.0 1.0 1.0
* inc-frm inc-to 0 limit
1700062 0 0 0 6
* lnnm mflowf mflowg #
1701011 0.0 0.01 1
1701021 0.0 0.05 2
1701031 0.0 0.05 3
1701041 0.0 0.05 4
1701051 0.0 0.01 5
1701061 0.0 0.00 6
* 2nnm Dhyd b c m #
1702011 0.01905 0.0 1.0 1.0 1
1702021 0.0150 0.0 1.0 1.0 2
1702031 0.0159 0.0 1.0 1.0 3
1702041 0.0144 0.0 1.0 1.0 4
1702051 0.015875 0.0 1.0 1.0 5
1702061 0.01463 0.0 1.0 1.0 6
*
* core outlet plenum
*
1750000 outplenm branch
1750001 1 1
1750101 0.7296 0.22225 0.0
1750102 0.0 -90.0 -0.22225
1750103 0.000046 0.097 0
1750200 3 7.00E+05 960.15
1751101 175010004 200000000 0.06973 0.0 0.0 0000002
1751110 0.0 0.0 1.0 1.0
1751201 0.0 1.0 0.0
*
* pressure vessel bottom head
*
1900000 lowrhead branch
1900001 1 1
1900101 0.0 0.8192 1.1512
1900102 0.0 90.0 0.8192
1900103 0.000046 1.092 0
1900200 3 7.00E+05 531.75
1901101 190010000 105010005 0.00399 0.0 0.0 101
1901110 0.0 0.0 1.0 1.0
1901201 0.0 0.0 0.0
*
* hot duct
*
2000000 "hot duct" pipe
2000001 6
2000101 0.0697 4
2000102 0.0700 6
2000301 0.43180 1
2000302 0.65095 2
2000303 0.41270 3
2000304 0.41270 4
2000305 0.49058 5
2000306 0.49058 6
2001901 0.29797 6

```



```

2000401 0.0 6
2000601 0.0 6
2000801 0.000046 0.29797 4
2000802 0.000046 0.29845 6
2002401 0.0 0.0 6
2000901 0.0 0.0 4
2000902 0.057 0.057 5
2001001 0 6
2001101 0 5
2001201 3 7.00E+05 960.15 0.0 0.0 0.0 6
2001300 1
2001301 0.0 1.0 0.0 5
2001401 0.0 0.0 1.0 1.0 5
*
* valve V-313
*
2050000 V-313 valve
2050101 200010000 210000000 0.0700 0.0 0.0 0000200
2050201 0 0.0 0.0 0.0
2050300 mtrvLv
2050301 205 206 0.2 0.0
*
* hot duct pipe into RCST
*
2100000 hot-RCST branch
2100001 1 1
2100101 0.0700 0.66040 0.0
2100102 0.0 0.0 0.0
2100103 0.000046 0.2985 0
2100200 3 1.00E+05 300.00
2101101 210010000 280020001 0.06996 1.0 0.5 0000000
* replace the card above with the one below for hot duct breaks with the RCST spool
piece installed
*2101101 282010000 210010000 0.0 0.0 0.0 0000100
2101201 0.0 0.0 0.0
*
* pipe from hot duct to SG - 10"-RCH-SS6-101
*
2150000 hot-SG branch
2150001 1 1
2150101 0.0507 0.540516 0.0
2150102 0.0 90.0 0.540516
2150103 0.000046 0.254 0
2150200 3 7.00E+05 960.15
2151101 200030006 215000000 0.05067 1.6 1.6 0000000
2151110 0.254 0.0 1.0 1.0
2151201 0.0 1.0 0.0
*
* valve V-101
*
2170000 V-101 valve
2170101 215010000 220000000 0.05067 0.97 0.91 0000000
2170110 0.254 0.0 1.0 1.0
2170201 0 0.0 1.0 0.0
2170300 chkvLv
2170301 0 0.0 500.0 0
*
* orifice plate
*2170000 orifice sngljun
*2170101 215010000 220000000 0.00785 61.43 61.37 0000200
*2170110 0.1 0.0 1.0 1.0
*2170201 0 0.0 1.0 0.0
*

```

```

* steam generator inlet plenum
*
2200000  SGinplen  branch
2200001  1  1
2200101  0.0  0.58420  0.0337
2200102  0.0  90.0  0.5842
2200103  0.000046  0.000  0
2200200  3  7.00E+05  960.15
2201101  220010000  225000000  0.04050  0.33  0.43  0000200
2201110  0.0165608  0.0  1.0  1.0
2201201  0.0  1.0  0.0
*
* steam generator tubes
*
2250000  "SG tubes" pipe
2250001  22
2250101  0.04050  22
2250301  0.22344  1
2250302  0.14089  2
2250303  0.14208  10
2250304  0.18170  12
2250305  0.14208  20
2250306  0.14089  21
2250307  0.22344  22
2250401  0.0  22
2250601  90.0  10
2250602  39.54022  11
2250603  -39.54022  12
2250604  -90.0  22
2250701  0.22344  1
2250702  0.14089  2
2250703  0.14208  10
2250704  0.11568  11
2250705  -0.11568  12
2250706  -0.14208  20
2250707  -0.14089  21
2250708  -0.22344  22
2250801  0.000002  0.0166  22
2250901  0.0  0.0  10
2250902  0.29  0.29  11
2250903  0.0  0.0  21
2251001  0  22
2251101  0  21
2251201  3  7.00E+05  960.15  0.0  0.0  0.0  22
2251300  1
2251301  0.0  1.0  0.0  21
2251401  0.0166  0.0  1.0  1.0  21
*
* steam generator outlet plenum
*
2280000  SGouplen  branch
2280001  2  1
2280101  0.0  0.51440  0.0236
2280102  0.0  -90.0  -0.51440
2280103  0.000046  0.0000  0
2280200  3  7.00E+05  531.75
2281101  225010000  228000000  0.0  0.43  0.33  0000200
2282101  228010000  230000000  0.03228  0.21  0.31  0000000
2281110  0.0166  0.0  1.0  1.0
2282110  0.2027  0.0  1.0  1.0
2281201  0.0  1.0  0.0
2282201  0.0  1.0  0.0
*

```

* pipe from steam generator to circulator - 8"-PCC-SS3-200

*

2300000 SG2cmprs snglvol
2300101 0.03228 2.28273 0.0
2300102 0.0 -52.1 -1.80070
2300103 0.000046 0.2027 0
2300200 3 7.00E+05 531.75

*

* circulator

*

2350000 circultr branch
2350001 1 1
2350101 0.0 1.2033 0.6791
2350102 0.0 -16.9 -0.34920
2350103 0.000046 0.0 0
2350200 3 7.00E+05 531.75
2351101 230010000 235000000 0.03228 0.46 0.46 0
2351110 0.0 0.0 1.0 1.0
2351201 0.0 1.0 0.0

*

2370000 circultr tmdpjun
2370101 235010000 240000000 0.00000
2370200 1 0 cntrlvar 237
2370201 0.10 0.0 0.10 0.0
2370202 1.5 0.0 1.5 0.0

*

* pipe from circulator to valve V-203 - 8"-PCC-SS-201

*

2400000 cmprsout snglvol
2400101 0.03228 1.29336 0.0
2400102 0.0 36.7944 0.77465
2400103 0.000046 0.2027 0
2400200 3 7.00E+05 531.75

*

* valve V-203

*

2450000 V-203 valve
2450101 240010000 250000000 0.03228 0.25 0.25 0000200
2450201 0 0.0 1.0 0.0
2450300 mtrvlv
2450301 245 246 0.2 1.0

*

* pipe from valve V-203 to break valve - 8"-PCC-SS3-201

*

2500000 clpipe pipe
2500001 3
2500101 0.03228 3
2500301 1.09168 1
2500302 0.360896 2
2500303 0.6223 3
2500401 0.0 3
2500601 34.34827 1
2500602 0.0 3
2500701 0.61595 1
2500702 0.0 3
2500801 0.000046 0.2027174 3
2500901 0.20 0.20 1
2500902 0.0 0.0 2
2501001 0 3
2501101 0 2
2501201 3 7.00E+05 531.75 0.0 0.0 0.0 3
2501300 1
2501301 0.0 0.0 0.0 2

```

*
* valve V-311
*
2550000  V-311  valve
2550101  250010000  258000000  0.02946  0.05  0.1  0000200
2550201  0  0.0  0.0  0.0
2550300  mtrvlv
2550301  255  256  0.2  0.0
*
* cold leg pipe from valve V-311 to RCST
*
2580000  cld-RCST  branch
2580001  1  1
2580101  0.02946  1.02565  0.0
2580102  0.0  0.0  0.0
2580103  0.000046  0.194  0
2580200  3  1.00E+05  300.00
2581101  258010000  280020001  0.02946  0.5  1.0  0000200
* replace the card above with the one below for hot duct breaks with the RCST spool
piece installed
*2581101  258010000  282000000  0.0  0.0  0.0  0000000
2581201  0.0  0.0  0.0
*
* crossover pipe from cold leg tee to cold duct
*
2600000  clcross  branch
2600001  2  1
2600101  0.03228  0.36537  0.0
2600102  0.0  0.0  0.0
2600103  0.000046  0.2027  0
2600200  3  7.00E+05  531.75
2601101  250020004  260000000  0.03228  1.3  1.1  0000200
2602101  260010000  270010003  0.03228  2.8  2.2  0000200
2601201  0.0  1.0  0.0
2602201  0.0  1.0  0.0
*
* cold duct
*
2700000  coldduct  pipe
2700001  4
2700101  0.0649  4
2700301  0.41270  1
2700302  0.41270  2
2700303  0.65095  3
2700304  0.43180  4
2700401  0.0  4
2700601  0.0  4
2700801  0.000046  0.1075  4
2700901  0.0  0.0  3
2701001  0  4
2701101  0  3
2701201  3  7.00E+05  531.75  0.0  0.0  0.0  4
2701300  1
2701301  0.0  1.0  0.0  3
*
* reactor cavity simulation tank (two-volume configuration)
*
2800000  RCST  pipe
2800001  2
2800101  0.0  2
2800301  1.5240  1
2800302  4.0831  2
2800401  3.8  1

```

```

2800402 14.1 2
2800601 90.0 2
2800701 1.5240 1
2800702 4.0831 2
2800801 0.000046 2.0828 2
2800901 0.0 0.0 1
2801001 0 2
2801101 0 1
2801201 3 1.00E+05 300.00 0.0 0.0 0.0 2
2801300 1
2801301 0.0 0.0 0.0 1
*
* reactor cavity simulation tank (single-volume configuration)
*
*2800000 RCST snglvol
*2800101 0.0 5.6071 17.9212
*2800102 0.0 90.0 5.6071
*2800103 0.000046 2.0828 0
*2800200 3 1.00E+05 300.00
*
* spool piece connecting the hot and cold leg break nozzles inside the RCST
*
*2820000 RCSTspol snglvol
*2820101 0.0295 1.1172 0.0
*2820102 0.0 0.0 0.0
*2820103 0.000046 0.1937 0
*2820200 3 1.00E+05 300.00
*
* inlet piping for relief valve PSV-100
*
2930000 PSVinpip branch
2930001 1 1
2930101 0.00191 0.35560 0.0
2930102 0.0 0.0000 0.0000
2930103 0.000046 0.0493 0
2930200 3 7.00E+05 531.75
2931101 240010004 293000000 0.00191 0.05 0.04 0000000
2931201 0.0 0.0 0.0
*
* valve PSV-100
*
2950000 PSV-100 valve
2950101 293010000 298000000 0.00056 0.0 0.0 0000200
2950201 0 0.0 0.0 0.0
2950300 trpvlv
2950301 1295
*
* valve V-400
*
2960000 V-400 valve
2960101 293010000 298000000 0.00191 0.06 0.06 0000000
2960201 0 0.0 0.0 0.0
2960300 trpvlv
2960301 1296
*
* outlet boundary volume for valve PSV-100
*
2980000 PSVout tmdpvol
2980101 0.00056 1.0 0.0 0.0 0.0 0.0 0.0 0.0 10
2980200 3
2980201 0.0 1.00E+05 300.00
*
* feedwater pump P-010

```

```

*
3200000  inflow  tmdpjun
3200101  460010000  330000000  0.00050
3200200  1  0  cntrlvar  320
3200201  0.1  0.1  0.0  0.0
3200202  1.5  1.5  0.0  0.0
*
* feedwater pipe from feedwater pump to steam generator
*
3300000  fwline2  branch
3300001  1  1
3300101  0.00050  5.52607  0.0
3300102  0.0  56.4427  4.60506
3300103  0.000046  0.0253  0
3300200  3  1.00E+05  290.00
3301101  330010000  340010003  0.00050  1.0  1.0  0000201
3301201  1.0  0.0  0.0
*
* steam generator downcomer
*
3400000  SGdwncmr  pipe
3400001  11
3400101  0.0401  11
3400301  0.57012  1
3400302  0.63362  2
3400303  0.14208  10
3400304  0.14089  11
3400401  0.0  11
3400601  -90.0  11
3400801  0.000046  0.0445  11
3400901  0.0  0.0  10
3401001  0  11
3401101  0  10
3401201  3  5.15E+05  290.00  0.0  0.0  0.0  11
3401300  1
3401301  1.0  0.0  0.0  10
3401401  0.0445  0.0  1.0  1.0  10
*
3450000  SGdc-blr  sngljun
3450101  340010000  350010002  0.0401  0.6  0.4  200
3450201  1  1.0  0.0  0.0
*
* steam generator boiler
*
3500000  SGboiler  pipe
3500001  13
3500101  0.16045  1
3500102  0.0  2
3500103  0.12391  8
3500104  0.12406  10
3500105  0.0  11
3500106  0.23151  12
3500107  0.0  13
3500301  0.14089  2
3500302  0.14208  10
3500303  0.63362  12
3500304  0.50800  13
3500401  0.0  1
3500402  0.02413  2
3500403  0.0  10
3500404  0.12722  11
3500405  0.0  12
3500406  0.07357  13

```

```

3500601 90.0 13
3500801 0.000002 0.0262 1
3500802 0.000002 0.0279 2
3500803 0.000002 0.0203 8
3500804 0.000002 0.0204 10
3500805 0.000002 0.0984 11
3500806 0.000002 0.5429 12
3500807 0.000002 0.4235 13
3500901 0.0 0.0 1
3500902 20.766 20.766 2
3500903 0.0 0.0 3
3500904 20.766 20.766 4
3500905 0.0 0.0 5
3500906 20.766 20.766 6
3500907 0.0 0.0 7
3500908 20.766 20.766 8
3500909 0.0 0.0 9
3500910 20.766 20.766 10
3500911 0.0 0.0 12
3501001 100 11
3501002 0 13
3501101 0 12
3501201 3 5.15E+05 290.00 0.0 0.0 0.0 8
3501202 2 5.15E+05 1.0 0.0 0.0 0.0 13
3501300 1
3501301 1.0 0.0 0.0 12
3501401 0.0262 0.0 1.0 1.0 1
3501402 0.0279 0.0 1.0 1.0 2
3501403 0.0203 0.0 1.0 1.0 8
3501404 0.0204 0.0 1.0 1.0 10
3501405 0.5429 0.0 1.0 1.0 11
3501406 0.0 0.0 1.0 1.0 12
*
* steam generator steam dome
*
3550000 steamdom branch
3550001 2 1
3550101 0.0 0.20665 0.03855
3550102 0.0 90.0 0.20665
3550103 0.000046 0.3573 0
3550200 2 5.15E+05 1.00
3551101 350010000 355000000 0.07297 0.0 0.0 0000000
3552101 355010000 390000000 0.00477 0.5 0.9 0000200
3551110 0.3048 0.0 1.0 1.0
3552110 0.0779 0.0 1.0 1.0
3551201 0.0 0.0 0.0
3552201 0.0 0.0 0.0
*
* steam generator steam annulus
*
3600000 steamann branch
3600001 2 1
3600101 0.0 0.55880 0.0623
3600102 0.0 -90.0 -0.55880
3600103 0.000046 0.1338 0
3600200 2 5.15E+05 1.00
3601101 355000000 360000000 0.0 0.0 0.0 0000000
3602101 360010004 365000000 0.0 0.5 0.9 0000200
3601110 0.2731 0.0 1.0 1.0
3602110 0.1023 0.0 1.0 1.0
3601201 0.0 0.0 0.0
3602201 0.0 0.0 0.0
*

```

```

* steam line from steam generator to valve PCV-602
*
3650000 steamlin snglvol
3650101 0.00920 0.50000 0.0
3650102 0.0 0.0000 0.0000
3650103 0.000046 0.1082 0
3650200 2 5.15E+05 1.00
*
* valve PCV-602
*
3700000 PCV-602 valve
3700101 365010000 375000000 0.0092 0.0 0.0 0000100
3700201 0 0.0 0.0 0.0
3700300 srvvlv
3700301 370
*
* outlet boundary volume for valve PCV-602
*
3750000 V602out tmdpvvol
3750101 0.00920 1.0 0.0 0.0 0.0 0.0 0.0 0.0 10
3750200 2
3750201 0.0 1.00E+05 1.0
*
* relief line from steam generator to valve PSV-600
*
3900000 reliefln snglvol
3900101 0.00477 0.1556 0.0
3900102 0.0 90.0000 0.1556
3900103 0.000046 0.0779 0
3900200 2 5.15E+05 1.00
*
* valve PSV-600
*
3950000 PSV-600 valve
3950101 390010000 398000000 0.00477 0.0 0.0 0000100
3950201 0 0.0 0.0 0.0
3950300 trpvlv
3950301 1395
*
* outlet boundary volume for valve PSV-600
*
3980000 V600out tmdpvvol
3980101 0.00477 1.0 0.0 0.0 0.0 0.0 0.0 0.0 10
3980200 2
3980201 0.0 1.00E+05 1.0
*
* potable water source boundary volume
*
4000000 potsorce tmdpvvol
4000101 0.00050 1.0 0.0 0.0 0.0 0.0 0.0 0.0 10
4000200 3
4000201 0.0 1.50E+05 290.00
*
* valve LCV-010
*
4100000 LCV-010 valve
4100101 400010000 420000000 0.00050 0.0 0.0 0001100
4100201 0 0.0 0.0 0.0
4100300 srvvlv
4100301 410
*
* water pipe from valve LCV-010 to tank T-010
*

```



```

4200000 potwater branch
4200001 1 1
4200101 0.00050 2.00000 0.0
4200102 0.0 0.0000 0.0
4200103 0.000046 0.0253 0
4200200 3 1.00E+05 290.00
4201101 420010000 450000000 0.00050 1.0 0.5 0001200
4201201 0.0 0.0 0.0
*
* water storage tank T-010
*
4500000 tankT010 pipe
4500001 6
4500101 0.0 6
4500301 0.03490 1
4500302 0.08260 2
4500303 0.03490 4
4500304 0.08260 5
4500305 0.03490 6
4500401 0.01255 1
4500402 0.05790 2
4500403 0.02866 4
4500404 0.05790 5
4500405 0.01262 6
4500601 90.0 6
4500801 0.000046 0.0 6
4500901 0.0 0.0 5
4501001 0000000 1
4501002 1100000 4
4501003 100000 5
4501004 0000000 6
4501101 1000 5
4501201 3 2.00E+05 290.00 0.0 0.0 0.0 4
4501202 8 1.00E+05 290.00 290.00 0.8 0.9 5
4501203 8 1.00E+05 290.00 290.00 1.0 0.9 6
4501300 1
4501301 0.0 0.0 0.0 5
4501401 0.0 0.0 1.0 1.0 5
*
* outlet line from tank to SG, RCCS, and drain
*
4600000 tankout branch
4600001 1 1
4600101 0.00111 2.33918 0.0
4600102 0.0 -90.0 -2.33918
4600103 0.000046 0.03762 0
4600200 3 2.00E+05 290.00
4601101 450000000 460000000 0.00111 0.5 1.0 0001000
4601201 0.0 0.0 0.0
*
* water storage tank vent line
*
4900000 tankvent branch
4900001 2 1
4900101 0.00131 0.35560 0.0
4900102 0.0 -90.0 -0.35560
4900103 0.000046 0.04089 0
4900200 4 1.00E+05 300.00 1.0
4901101 450060001 490000000 0.0 0.5 1.0 1200
4902101 490010000 498000000 0.0 1.0 0.5 1200
4901201 0.0 0.0 0.0
4902201 0.0 0.0 0.0
*

```

```

* outlet boundary volume for tank vent line
*
4980000 ventout tmdpvol
4980101 0.00131 1.0 0.0 0.0 0.0 0.0 0.0 10
4980200 4
4980201 0.0 1.00E+05 300.00 1.0
*
* CRD break line connection from upper plenum
*
*050000 UP-CRD sngljun
*050101 120010000 10000000 0.01174 0.48 0.91 0000200
*050201 0 0.0 0.0 0.0
*
* CRD break line pressure vessel nozzle
*
*100000 CRDnozzl pipe
*100001 25
*100101 0.01174 25
*100301 0.01955 25
*100401 0.0 25
*100601 90.0 25
*100701 0.01955 25
*100801 0.000046 0.122 25
*100901 0.0 0.0 24
*101001 0 25
*101101 0 24
*101201 3 7.00E+05 531.75 0.0 0.0 0.0 25
*101300 1
*101301 0.0 0.0 0.0 24
*
* CRD break line connection from nozzle to pipe
*
*150000 UP-CRD sngljun
*150101 10010000 20000000 0.00742 0.30 1.93 0000200
*150201 0 0.0 0.0 0.0
*
* CRD break line from nozzle to valve
*
*200000 CRDbrkp1 pipe
*200001 35
*200101 0.00742 35
*200301 0.02041 35
*200401 0.0 35
*200601 0.00000 35
*200701 0.00000 35
*200801 0.000046 0.09718 35
*200901 0.0 0.0 34
*201001 0 35
*201101 0 34
*201201 3 7.00E+05 531.75 0.0 0.0 0.0 35
*201300 1
*201301 0.0 0.0 0.0 34
*
* CRD break valve
*
*250000 CRDbrkv valve * valve V-332
*250101 20010000 30000000 0.00742 0.057 0.057 0000200
*250201 0 0.0 0.0 0.0
*250300 trpvlv
*250301 25
*
* CRD break line from valve to RCST
*

```

```

*300000 CRDbrkp2 pipe
*300001 92
*300101 0.00742 92
*300301 0.01998 92
*300401 0.0 92
*300601 -3.64256 92
*300701 -0.001269 92
*300801 0.000046 0.09718 92
*300901 0.0 0.0 91
*301001 0 92
*301101 0 91
*301201 3 7.00E+05 300.00 0.0 0.0 0.0 92
*301300 1
*301301 0.0 0.0 0.0 91
*
*310000 CRD-2-3 sngljun
*310101 30010000 32000000 0.00742 0.00 0.00 0000000
*310201 0 0.0 0.0 0.0
*
*320000 CRDbrkp3 pipe
*320001 92
*320101 0.00742 92
*320301 0.01998 92
*320401 0.0 92
*320601 -3.64256 92
*320701 -0.001269 92
*320801 0.000046 0.09718 92
*320901 0.0 0.0 91
*321001 0 92
*321101 0 91
*321201 3 7.00E+05 300.00 0.0 0.0 0.0 92
*321300 1
*321301 0.0 0.0 0.0 91
*
*330000 CRD-3-4 sngljun
*330101 32010000 34000000 0.00742 0.00 0.00 0000000
*330201 0 0.0 0.0 0.0
*
*340000 CRDbrkp4 pipe
*340001 92
*340101 0.00742 92
*340301 0.01998 92
*340401 0.0 92
*340601 -3.64256 92
*340701 -0.001269 92
*340801 0.000046 0.09718 92
*340901 0.0 0.0 91
*341001 0 92
*341101 0 91
*341201 3 7.00E+05 300.00 0.0 0.0 0.0 92
*341300 1
*341301 0.0 0.0 0.0 91
*
* CRD break line connection to RCST
*
*350000 CRD-RCST sngljun
*350101 34010000 280010000 0.00742 1.00 0.50 0000200
*350201 0 0.0 0.0 0.0
*
* vessel bottom break line connection from core support region
*
*550000 vs-btbrk sngljun
*550101 105010005 60000000 0.00742 0.50 0.99 0000202

```

```

*550201 0 0.0 0.0 0.0
*
* vessel bottom break line pressure vessel nozzle stub
*
*600000 vbtnoz1 pipe
*600001 43
*600101 0.00742 43
*600301 0.020084 43
*600401 0.0 43
*600601 -90.0 43
*600701 -0.0200837 43
*600801 0.000046 0.097 43
*600901 0.0 0.0 42
*601001 0 43
*601101 0 42
*601201 3 7.00E+05 531.75 0.0 0.0 0.0 43
*601300 1
*601301 0.0 0.0 0.0 42
*
* vessel bottom break line connection from nozzle to pipe
*
*650000 nozl-pip sngljun
*650101 60010000 70000000 0.00742 0.5 1.0 0000200
*650201 0 0.0 0.0 0.0
*
* vessel bottom break line from nozzle to valve
*
*700000 vbtbrkp1 pipe
*700001 73
*700101 0.00742 73
*700301 0.02009 73
*700401 0.0 73
*700601 -5.33641 73
*700701 -0.001868 73
*700801 0.000046 0.09718 73
*700901 0.0 0.0 72
*701001 0 73
*701101 0 72
*701201 3 7.00E+05 531.75 0.0 0.0 0.0 73
*701300 1
*701301 0.0 0.0 0.0 72
*
*710000 vbt-1-2 sngljun
*710101 70010000 72000000 0.00742 0.0 0.0 0000000
*710201 0 0.0 0.0 0.0
*
* vessel bottom break line from nozzle to valve
*
*720000 vbtbrkp1 pipe
*720001 73
*720101 0.00742 73
*720301 0.02009 73
*720401 0.0 73
*720601 -5.33641 73
*720701 -0.001868 73
*720801 0.000046 0.09718 73
*720901 0.0 0.0 72
*721001 0 73
*721101 0 72
*721201 3 7.00E+05 531.75 0.0 0.0 0.0 73
*721300 1
*721301 0.0 0.0 0.0 72
*

```

```

* vessel bottom break valve
*
*750000 vbtbrkv valve * valve V-331
*750101 72010000 80000000 0.00742 0.057 0.057 0000200
*750201 0 0.0 0.0 0.0
*750300 trpvlv
*750301 75
*
* vessel bottom break line from valve to RCST
*
*800000 vbtbrkp3 pipe
*800001 96
*800101 0.00742 96
*800301 0.01999 96
*800401 0.0 96
*800601 0.00000 96
*800701 0.00000 96
*800801 0.000046 0.09718 96
*800901 0.0 0.0 95
*801001 0 96
*801101 0 95
*801201 3 1.00E+05 300.00 0.0 0.0 0.0 96
*801300 1
*801301 0.0 0.0 0.0 95
*
* vessel bottom break line connection to RCST
*
*850000 vbt-RCST sngljun
*850101 80010000 280000000 0.00742 1.00 0.50 0000200
*850201 0 0.0 0.0 0.0
*
* cavity air volume
*
*9000000 cavity pipe
*9000001 20
*9000101 3.8 20
*9000301 1.35230 1
*9000302 0.32728 2
*9000303 0.22225 3
*9000304 0.25146 4
*9000305 0.25146 5
*9000306 0.19812 15
*9000307 0.19050 16
*9000308 0.20320 17
*9000309 0.27320 18
*9000310 0.83185 19
*9000311 1.69969 20
*9000401 0.0 20
*9000601 90.0 20
*9000801 0.000046 0.0 20
*9000901 0 0.0 19
*9001001 0 20
*9001101 0 19
*9001201 4 1.00E+05 300.00 0.0 0.0 0.0 20
*9001300 1
*9001301 0.0 0.0 0.0 19
*9001401 0.0 0.0 1.0 1.0 19
*
9030000 confineo sngljun
9030101 900010000 905000000 0.0 0.0 0.0 0
9030201 0 0.0 0.0 0.0
*

```

* The single volume below can be used instead of the pipe if axial conduction in the vessel and RCCS are not modeled
 * or if the code input provides the height for each structure instead of defaulting to that of the adjacent fluid volume.

*

```
9000000 cavity snglvol
9000101 3.77189 5.8 0.0
9000102 0.0 90.0 5.8
9000103 0.000046 0 0
9000200 4 1.00E+05 300.00 0.0
```

*

```
9050000 confinea tmdpvvol
9050101 3.8 1.0 0.0 0.0 0.0 0.0 0.0 0.0 10
9050200 4
9050201 0.0 1.00E+05 300.00 0.0
```

*

* alternate RCCS source volume

*

```
*9150000 RCCSsrc tmdpvvol
*9150101 0.0011 1.0 0.0 0.0 0.0 0.0 0.0 0.0 10
*9150200 3
*9150201 0.0 1.00E+05 290.00
```

*

* RCCS pump

*

```
9200000 RCCSpump tmdpjun
9200101 460010000 930000000 0.00050
* use the card below if the alternate source volume (Component 915) is used
*9200101 915010000 930000000 0.00050
9200200 1 0 cntrlvar 920
9200201 0.02 0.02 0.0 0.0
9200202 4.0 4.0 0.0 0.0
```

*

* RCCS piping from pump to inlet headers

*

```
9300000 RCCSinp2 snglvol
9300101 0.00050 3.00000 0.0
9300102 0.0 -3.7 -0.19320
9300103 0.000046 0.02527 0
9300200 3 2.00E+05 290.00
```

*

* RCCS inlet header

*

```
9400000 RCCSihdr branch
9400001 1 1
9400101 0.00050 8.68680 0.0
9400102 0.0 0.0 0.0
9400103 0.000046 0.0 0
9400200 3 2.00E+05 290.00
9401101 930010000 940010003 0.00050 1.1 0.7 0001201
9401201 0.0 0.0 0.0
```

*

* RCCS panel inlet lines

*

```
9450000 RCCSpnli branch
9450001 2 1
9450101 0.00225 1.00000 0.0
9450102 0.0 13.21466 0.22860
9450103 0.000046 0.01892 0
9450200 3 2.00E+05 290.00
9451101 940010004 945000000 0.0 0.0 0 1000
9452101 945010000 950000000 0.0 0.0 0.0 1000
9451201 0.0 0.0 0.0
```

```

9452201  0.0  0.0  0.0
*
* RCCS panels
*
9500000  RCCSpanl  pipe
9500001  19
9500101  0.2230  19
9500301  1.02210  1
9500302  0.32728  2
9500303  0.22225  3
9500304  0.25146  4
9500305  0.25146  5
9500306  0.19812  15
9500307  0.19050  16
9500308  0.20320  17
9500309  0.27320  18
9500310  0.74846  19
9500401  0.0  19
9500601  90.0  19
9500801  0.000046  0.051  19
9500901  0.0  0.0  18
9501001  0  19
9501101  1000  18
9501201  3  2.00E+05  290.00  0.0  0.0  0.0  19
9501300  1
9501301  0.01  0.0  0.0  18
9501401  0.051  0.0  1.0  1.0  18
*
* RCCS panel outlet lines
*
9550000  RCCSpnlo  branch
9550001  2  1
9550101  0.0022  1.0000  0.0
9550102  0.0  5.7  0.0987
9550103  0.000046  0.0189  0
9550200  3  2.00E+05  290.00
9551101  950010000  955000000  0.0  0.0  0.0  1000
9552101  955010000  960000000  0.0  0.0  0.0  1000
9551110  0.0189  0.0  1.0  1.0
9552110  0.0189  0.0  1.0  1.0
9551201  0.0  0.0  0.0
9552201  0.0  0.0  0.0
*
* RCCS outlet headers
*
9600000  RCCSohdr  branch
9600001  1  1
9600101  0.0  5.4758  0.009198
9600102  0.0  -33.6898  -3.0374
9600103  0.000046  0.0253  0
9600200  3  2.00E+05  290.00
9601101  960010000  450050003  0.0022  1.0  0.5  0001000
* use the card below for the once-through RCCS model (Component 965 enabled)
*9601101  960010000  965000000  0.0022  0.0  0.0  0001000
9601110  0.0376  0.0  1.0  1.0
9601201  0.0  0.0  0.0
*
* use this component for the once-through RCCS model
*
*9650000  RCCSout  tmdpvol
*9650101  0.0022  1.0  0.0  0.0  0.0  0.0  0.0  0.0  10
*9650200  3
*9650201  0.0  1.00E+05  290.00

```

```

*
*****
* heat structures
*****
*
* primary pressure vessel cylindrical wall - heat structure 1000
*
11000000 17 6 2 1 0.81915 3
11000100 0 1
11000101 5 0.83185
11000201 3 5 * 304 stainless steel
11000301 0.0 5
11000400 0
11000401 531.75 6
11000501 100010000 0 1 1 0.3273 1
11000502 100010000 0 1 1 0.2223 2
11000503 115010000 0 1 1 0.2515 3
11000504 115020000 0 1 1 0.2515 4
11000505 115030000 10000 1 1 0.1981 14
11000506 115130000 0 1 1 0.1905 15
11000507 115140000 0 1 1 0.2032 16
11000508 115150000 0 1 1 0.2732 17
11000600 1
11000601 900010000 0 1 1 0.3273 0.3273 1
11000602 900010000 0 1 1 0.2223 0.2223 2
11000603 900010000 0 1 1 0.2515 0.2515 3
11000604 900010000 0 1 1 0.2515 0.2515 4
11000605 900010000 0 1 1 0.1981 0.1981 14
11000606 900010000 0 1 1 0.1905 0.1905 15
11000607 900010000 0 1 1 0.2032 0.2032 16
11000608 900010000 0 1 1 0.2732 0.2732 17
11000701 0 0.0 0.0 0.0 17
11000800 1
11000801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 3.7 1.1 1.0 17
11000900 1
11000901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 3.7 1.1 1.0 17
*
* primary pressure vessel upper head/upper plenum shroud - heat structure 1001
*
11001000 1 14 3 1 0.7635875 0
11001100 0 1
11001101 2 0.76662534 * shroud
11001102 6 0.81915 * insulation
11001103 5 0.83185 * vessel head
11001201 -4 2 * Haynes 230
11001202 -8 8 * Cerablanket
11001203 3 13 * 304 stainless steel
11001301 0.0 13
11001400 0
11001401 531.75 14
11001501 120010000 0 1 1 0.5 1
11001601 900010000 0 1 1 0.5 1
11001701 0 0.0 0.0 0.0 1
11001800 1
11001801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.76 1.1 1.0 1
11001900 1
11001901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.83 1.1 1.0 1
*
* primary pressure vessel lower head - heat structure 1002
*
11002000 1 6 3 1 0.81915 0
11002100 0 1
11002101 5 0.83185

```



```

11002201 3 5
11002301 0.00 5
11002400 0
11002401 531.75 6
11002501 190010000 0 1 1 0.5 1
11002601 900010000 0 1 1 0.5 1
11002701 0 0.0 0.0 0.0 1
11002800 1
11002801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.82 1.1 1.0 1
11002900 1
11002901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.83 1.1 1.0 1
*
* middle distributor plate - heat structure 1050
*
11050000 1 3 1 1 0.0 0
11050100 0 1
11050101 2 0.01270
11050201 3 2
11050301 0.0 2
11050400 0
11050401 531.75 3
11050501 105010000 0 1 0 1.61089 1
11050601 105020000 0 1 0 1.61089 1
11050701 0 0.0 0.0 0.0 1
11050800 1
11050801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.01 1.1 1.0 1
11050900 1
11050901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.01 1.1 1.0 1
*
* jacket shell/coolant upcomer
*
11100000 1 4 2 1 0.78105 3
11100100 0 1
11100101 3 0.7858125
11100201 3 3
11100301 0 3
11100400 0
11100401 531.75 4
11100501 110010000 0 1 1 0.403475 1
11100601 100010000 0 1 1 0.403475 1
11100701 0 0 0 0 1
11100800 1
11100801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.40 1.1 1.0 1
11100900 1
11100901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.40 1.1 1.0 1
*
* core barrel - heat structure 1150
*
11150000 16 5 2 1 0.7572375 3
11150100 0 1
11150101 4 0.762
11150201 3 4
11150301 0.0 4
11150400 0
11150401 531.75 5
11150501 105010000 0 1 1 0.327275 1
11150502 166150000 0 1 1 0.22225 2
11150503 166140000 0 1 1 0.25146 3
11150504 166130000 0 1 1 0.25146 4
11150505 166120000 -10000 1 1 0.19812 14
11150506 166020000 0 1 1 0.1905 15
11150507 166010000 0 1 1 0.2032 16
11150601 100010000 0 1 1 0.327275 1

```

```

11150602 110010000 0 1 1 0.22225 2
11150603 115010000 0 1 1 0.25146 3
11150604 115020000 0 1 1 0.25146 4
11150605 115030000 10000 1 1 0.19812 14
11150606 115130000 0 1 1 0.19050 15
11150607 115140000 0 1 1 0.20320 16
11150701 0.0 0.0 0.0 0.0 16
11150800 1
11150801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 3.4 1.1 1.0 16
11150900 1
11150901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 3.4 1.1 1.0 16
*
* upper plenum cylinder - heat structure 1200
*
11200000 1 5 2 1 0.76359
11200100 0 1
11200101 4 0.76663
11200201 4 4
11200301 0.0 4
11200400 0
11200401 531.75 5
11200501 120010000 0 1 1 0.27320 1
11200601 115150000 0 1 1 0.27320 1
11200701 0 0.0 0.0 0.0 1
11200800 1
11200801 0.00 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.3 1.1 1.0 1
11200900 1
11200901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.3 1.1 1.0 1
*
* upper plenum floor - heat structure 1201
*
11201000 1 5 1 1 0.0 0
11201100 0 1
11201101 4 0.01270
11201201 2 4 * graphite
11201301 0.0 4
11201400 0
11201401 531.75 5
11201501 0 0 0 0 1.67326 1
11201601 120010000 0 1 0 1.67326 1
11201701 0 0.0 0.0 0.0 1
11201900 1
11201901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.01 1.1 1.0 1
*
* upper plenum internals - heat structure 1202
*
11202000 1 3 2 1 0.01100 0
11202100 0 1
11202101 2 0.01300
11202201 3 2
11202301 0 2
11202400 0
11202401 531.75 3
11202501 0 0 0 1 35.0622 1
11202601 120010000 0 1 1 35.0622 1
11202701 0 0.0 0.0 0.0 1
11202900 1
11202901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.96 1.1 1.0 1
*
* central reflector inner piece - heat structure 1300
*
11300000 14 7 2 0 0.0 3
11300100 0 1

```

```

11300101 6 0.0751364
11300201 1 6
11300301 0.0 6
11300400 -1
11300401 533.20 533.20 533.20 533.20 533.20 533.20 533.20
11300402 537.57 537.57 537.57 537.57 537.57 537.57 537.57
11300403 739.67 739.67 739.67 739.67 739.67 739.67 739.67
11300404 791.93 791.93 791.93 791.93 791.93 791.93 791.93
11300405 839.49 839.49 839.49 839.49 839.49 839.49 839.49
11300406 887.12 887.12 887.12 887.12 887.12 887.12 887.12
11300407 933.84 933.84 933.84 933.84 933.84 933.84 933.84
11300408 978.77 978.77 978.77 978.77 978.77 978.77 978.77
11300409 1024.2 1024.2 1024.2 1024.2 1024.2 1024.2 1024.2
11300410 1069.7 1069.7 1069.7 1069.7 1069.7 1069.7 1069.7
11300411 1115.2 1115.2 1115.2 1115.2 1115.2 1115.2 1115.2
11300412 1158.4 1158.4 1158.4 1158.4 1158.4 1158.4 1158.4
11300413 1025.5 1025.5 1025.5 1025.5 1025.5 1025.5 1025.5
11300414 1024.5 1024.5 1024.5 1024.5 1024.5 1024.5 1024.5
11300501 0 0 0 1 0.1905 1
11300502 0 0 0 1 0.1905 2
11300503 0 0 0 1 0.1981 12
11300504 0 0 0 1 0.2515 13
11300505 0 0 0 1 0.2515 14
11300600 1
11300601 0 0 0 1 0.1905 0.1905 1
11300602 0 0 0 1 0.1905 0.1905 2
11300603 0 0 0 1 0.1981 0.1981 12
11300604 0 0 0 1 0.2515 0.2515 13
11300605 0 0 0 1 0.2515 0.2515 14
11300701 0.0 0.0 0.0 0.0 14
11300900 1
11300901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 14
*
* central reflector middle piece - heat structure 1320
*
11320000 14 6 2 0 0.009525 3
11320100 0 1
11320101 5 0.0601091
11320201 1 5
11320301 0.0 5
11320400 -1
11320401 532.96 533.04 533.10 533.14 533.17 533.20
11320402 535.95 536.49 536.86 537.15 537.37 537.57
11320403 680.83 700.65 714.18 724.46 732.74 739.67
11320404 724.45 747.18 762.70 774.48 783.98 791.93
11320405 765.58 790.48 807.48 820.38 830.78 839.49
11320406 807.41 834.26 852.59 866.51 877.72 887.12
11320407 849.19 877.70 897.17 911.95 923.86 933.84
11320408 890.21 920.04 940.41 955.87 968.34 978.77
11320409 931.99 963.05 984.26 1000.4 1013.3 1024.2
11320410 974.19 1006.4 1028.3 1045.0 1058.4 1069.7
11320411 1016.8 1049.9 1072.6 1089.8 1103.6 1115.2
11320412 1058.1 1091.9 1114.9 1132.5 1146.6 1158.4
11320413 983.51 997.65 1007.3 1014.6 1020.5 1025.5
11320414 982.86 996.88 1006.5 1013.7 1019.6 1024.5
11320501 132010000 0 160 1 1.1430 1
11320502 132020000 0 160 1 1.1430 2
11320503 132030000 10000 160 1 1.1887 12
11320504 132130000 0 160 1 1.5088 13
11320505 132140000 0 160 1 1.5088 14
11320601 0 0 0 1 1.1430 1
11320602 0 0 0 1 1.1430 2
11320603 0 0 0 1 1.1887 12

```

```

11320604 0 0 0 1 1.5088 13
11320605 0 0 0 1 1.5088 14
11320701 0 0.0 0.0 0.0 14
11320800 1
11320801 0.0 0.10 2.77 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11320802 0.0 0.29 2.58 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2
11320803 0.0 0.48 2.39 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 3
11320804 0.0 0.68 2.19 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 4
11320805 0.0 0.88 1.99 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 5
11320806 0.0 1.07 1.79 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 6
11320807 0.0 1.27 1.59 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 7
11320808 0.0 1.47 1.39 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 8
11320809 0.0 1.67 1.20 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 9
11320810 0.0 1.87 1.00 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 10
11320811 0.0 2.07 0.80 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 11
11320812 0.0 2.26 0.60 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 12
11320813 0.0 2.49 0.38 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 13
11320814 0.0 2.74 0.13 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 14

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*

* central reflector outer piece - heat structure 1340

*

```

11340000 14 7 2 0 0.1653000 3
11340100 0 1
11340101 6 0.1771399
11340201 1 6
11340301 0.0 6
11340400 -1
11340401 533.20 533.20 533.20 533.20 533.20 533.20 533.20
11340402 537.57 537.57 537.57 537.57 537.57 537.57 537.57
11340403 739.67 739.67 739.67 739.67 739.67 739.67 739.67
11340404 791.93 791.93 791.93 791.93 791.93 791.93 791.93
11340405 839.49 839.49 839.49 839.49 839.49 839.49 839.49
11340406 887.12 887.12 887.12 887.12 887.12 887.12 887.12
11340407 933.84 933.84 933.84 933.84 933.84 933.84 933.84
11340408 978.77 978.77 978.77 978.77 978.77 978.77 978.77
11340409 1024.2 1024.2 1024.2 1024.2 1024.2 1024.2 1024.2
11340410 1069.7 1069.7 1069.7 1069.7 1069.7 1069.7 1069.7
11340411 1115.2 1115.2 1115.2 1115.2 1115.2 1115.2 1115.2
11340412 1158.4 1158.4 1158.4 1158.4 1158.4 1158.4 1158.4
11340413 1025.5 1025.5 1025.5 1025.5 1025.5 1025.5 1025.5
11340414 1024.5 1024.5 1024.5 1024.5 1024.5 1024.5 1024.5
11340500 1
11340501 0 0 0 1 0.1905 0.1905 1
11340502 0 0 0 1 0.1905 0.1905 2
11340503 0 0 0 1 0.1981 0.1981 12
11340504 0 0 0 1 0.2515 0.2515 13
11340505 0 0 0 1 0.2515 0.2515 14
11340601 0 0 0 1 0.1905 1
11340602 0 0 0 1 0.1905 2
11340603 0 0 0 1 0.1981 12
11340604 0 0 0 1 0.2515 13
11340605 0 0 0 1 0.2515 14
11340701 0.0 0.0 0.0 0.0 14
11340800 1
11340801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 14
11340900 1
11340901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 14

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*

* upper reflector above inner core ring - heat structure 1400

*

```

11400000 2 3 2 1 0.0079375 3
11400100 0 1
11400101 2 0.0187832

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```

11400201 1 2
11400301 0.0 2
11400400 0
11400401 533.2 3
11400501 140010000 0 160 1 23.32 1
11400502 140020000 0 160 1 23.32 2
11400601 0 0 0 1 23.32 1
11400602 0 0 0 1 23.32 2
11400701 0 0.0 0.0 0.0 2
11400800 1
11400801 0.0 0.10 2.77 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11400802 0.0 0.29 2.58 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2
*
* inner core ring - heat structure 1401
*
11401000 10 5 2 1 0.0079375 3
11401100 0 1
11401101 4 0.0187832
11401201 1 4
11401301 0.0 4
11401400 -1
11401401 767.99 774.87 780.36 784.93 788.84
11401402 827.26 834.21 839.76 844.38 848.33
11401403 880.60 887.42 892.86 897.39 901.27
11401404 933.46 940.15 945.50 949.95 953.76
11401405 984.62 991.22 996.49 1000.9 1004.6
11401406 1033.0 1039.6 1044.8 1049.1 1052.8
11401407 1081.7 1088.2 1093.3 1097.6 1101.3
11401408 1130.2 1136.6 1141.7 1145.9 1149.5
11401409 1178.4 1184.7 1189.8 1194.0 1197.5
11401410 1223.8 1229.9 1234.8 1238.9 1242.3
11401501 140030000 10000 160 1 24.25 10
11401601 141010000 10000 1 1 24.25 10
11401701 0 0.0 0.0 0.0 10
11401800 1
11401801 0.0 0.48 2.39 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11401802 0.0 0.68 2.19 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2
11401803 0.0 0.88 1.99 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 3
11401804 0.0 1.07 1.79 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 4
11401805 0.0 1.27 1.59 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 5
11401806 0.0 1.47 1.39 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 6
11401807 0.0 1.67 1.20 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 7
11401808 0.0 1.87 1.00 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 8
11401809 0.0 2.07 0.80 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 9
11401810 0.0 2.26 0.60 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 10
11401900 1
11401901 0.0 0.10 1.88 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 1
11401902 0.0 0.30 1.68 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 2
11401903 0.0 0.50 1.49 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 3
11401904 0.0 0.69 1.29 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 4
11401905 0.0 0.89 1.09 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 5
11401906 0.0 1.09 0.89 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 6
11401907 0.0 1.29 0.69 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 7
11401908 0.0 1.49 0.50 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 8
11401909 0.0 1.68 0.30 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 9
11401910 0.0 1.88 0.10 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 10
*
* lower reflector below inner core ring - heat structure 1402
*
11402000 2 3 2 1 0.0079375 3
11402100 0 1
11402101 2 0.0187832
11402201 1 2

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11402301 0.0 2
11402400 0
11402401 1070.0 3
11402501 140130000 0 160 1 30.78 1
11402502 140140000 0 160 1 30.78 2
11402601 0 0 0 1 30.78 1
11402602 0 0 0 1 30.78 2
11402701 0 0.0 0.0 0.0 2
11402800 1
11402801 0.0 2.49 0.38 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11402802 0.0 2.74 0.13 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2
*
* inner core ring heater rod - heat structure 1403
*
11403000 10 4 2 1 0.0 3
11403100 0 1
11403101 3 0.007256448
11403201 2 3
11403301 1.0 3
11403400 -1
11403401 767.99 774.87 780.36 784.93
11403402 827.26 834.21 839.76 844.38
11403403 880.60 887.42 892.86 897.39
11403404 933.46 940.15 945.50 949.95
11403405 984.62 991.22 996.49 1000.9
11403406 1033.0 1039.6 1044.8 1049.1
11403407 1081.7 1088.2 1093.3 1097.6
11403408 1130.2 1136.6 1141.7 1145.9
11403409 1178.4 1184.7 1189.8 1194.0
11403410 1223.8 1229.9 1234.8 1238.9
11403501 0 0 0 1 11.09 10
11403600 1
11403601 0 0 0 1 11.09 0.19812 10
11403701 10940 0.1000 0.0 0.0 1
11403702 10940 0.1000 0.0 0.0 2
11403703 10940 0.1000 0.0 0.0 3
11403704 10940 0.1000 0.0 0.0 4
11403705 10940 0.1000 0.0 0.0 5
11403706 10940 0.1000 0.0 0.0 6
11403707 10940 0.1000 0.0 0.0 7
11403708 10940 0.1000 0.0 0.0 8
11403709 10940 0.1000 0.0 0.0 9
11403710 10940 0.1000 0.0 0.0 10
11403900 1
11403901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 10
*
* upper reflector above middle core ring - heat structure 1450
*
11450000 2 3 2 1 0.0079375 3
11450100 0 1
11450101 2 0.0171146
11450201 1 2
11450301 0.0 2
11450400 0
11450401 533.2 3
11450501 145010000 0 160 1 27.43 1
11450502 145020000 0 160 1 27.43 2
11450601 0 0 0 1 27.43 1
11450602 0 0 0 1 27.43 2
11450701 0 0.0 0.0 0.0 2
11450800 1
11450801 0.0 0.10 2.77 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11450802 0.0 0.29 2.58 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2

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*
* middle core ring - heat structure 1451
*
11451000 10 5 2 1 0.0079375 3
11451100 0 1
11451101 4 0.0171146
11451201 1 4
11451301 0.0 4
11451400 -1
11451401 733.78 739.23 743.69 747.47 750.75
11451402 786.29 791.85 796.41 800.27 803.61
11451403 834.38 839.90 844.43 848.26 851.59
11451404 882.29 887.77 892.26 896.07 899.37
11451405 929.80 935.23 939.68 943.46 946.73
11451406 976.68 982.06 986.47 990.20 993.44
11451407 1023.4 1028.7 1033.1 1036.8 1040.0
11451408 1068.4 1073.7 1078.0 1081.7 1084.9
11451409 1112.3 1117.6 1122.0 1125.6 1128.8
11451410 1154.1 1159.3 1163.6 1167.2 1170.3
11451501 145030000 10000 160 1 28.53 10
11451601 146010000 10000 1 1 28.53 10
11451701 0 0.0 0.0 0.0 10
11451800 1
11451801 0.0 0.48 2.39 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11451802 0.0 0.68 2.19 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2
11451803 0.0 0.88 1.99 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 3
11451804 0.0 1.07 1.79 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 4
11451805 0.0 1.27 1.59 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 5
11451806 0.0 1.47 1.39 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 6
11451807 0.0 1.67 1.20 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 7
11451808 0.0 1.87 1.00 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 8
11451809 0.0 2.07 0.80 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 9
11451810 0.0 2.26 0.60 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 10
11451900 1
11451901 0.0 0.10 1.88 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 1
11451902 0.0 0.30 1.68 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 2
11451903 0.0 0.50 1.49 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 3
11451904 0.0 0.69 1.29 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 4
11451905 0.0 0.89 1.09 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 5
11451906 0.0 1.09 0.89 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 6
11451907 0.0 1.29 0.69 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 7
11451908 0.0 1.49 0.50 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 8
11451909 0.0 1.68 0.30 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 9
11451910 0.0 1.88 0.10 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 10
*
* lower reflector below middle core ring - heat structure 1452
*
11452000 2 3 2 1 0.0079375 3
11452100 0 1
11452101 2 0.0171146
11452201 1 2
11452301 0.0 2
11452400 0
11452401 1020.0 3
11452501 145130000 0 160 1 36.21 1
11452502 145140000 0 160 1 36.21 2
11452601 0 0 0 1 36.21 1
11452602 0 0 0 1 36.21 2
11452701 0 0.0 0.0 0.0 2
11452800 1
11452801 0.0 2.49 0.38 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11452802 0.0 2.74 0.13 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2
*

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* middle core ring heater rod - heat structure 1453
*
11453000 10 4 2 1 0.0 3
11453100 0 1
11453101 3 0.007256448
11453201 2 3
11453301 1.0 3
11453400 -1
11453401 767.99 774.87 780.36 784.93
11453402 827.26 834.21 839.76 844.38
11453403 880.60 887.42 892.86 897.39
11453404 933.46 940.15 945.50 949.95
11453405 984.62 991.22 996.49 1000.9
11453406 1033.0 1039.6 1044.8 1049.1
11453407 1081.7 1088.2 1093.3 1097.6
11453408 1130.2 1136.6 1141.7 1145.9
11453409 1178.4 1184.7 1189.8 1194.0
11453410 1223.8 1229.9 1234.8 1238.9
11453501 0 0 0 1 14.26 10
11453600 1
11453601 0 0 0 1 14.26 0.19812 10
11453701 10945 0.1000 0.0 0.0 1
11453702 10945 0.1000 0.0 0.0 2
11453703 10945 0.1000 0.0 0.0 3
11453704 10945 0.1000 0.0 0.0 4
11453705 10945 0.1000 0.0 0.0 5
11453706 10945 0.1000 0.0 0.0 6
11453707 10945 0.1000 0.0 0.0 7
11453708 10945 0.1000 0.0 0.0 8
11453709 10945 0.1000 0.0 0.0 9
11453710 10945 0.1000 0.0 0.0 10
11453900 1
11453901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 10
*
* upper reflector above outer core ring - heat structure 1500
*
11500000 2 3 2 1 0.0079375 3
11500100 0 1
11500101 2 0.0198877
11500201 1 2
11500301 0.0 2
11500400 0
11500401 533.2 3
11500501 150010000 0 160 1 36.58 1
11500502 150020000 0 160 1 36.58 2
11500601 0 0 0 1 36.58 1
11500602 0 0 0 1 36.58 2
11500701 0 0 0 0 2
11500800 1
11500801 0.0 0.10 2.77 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11500802 0.0 0.29 2.58 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2
*
* outer core ring - heat structure 1501
*
11501000 10 5 2 1 0.0079375 3
11501100 0 1
11501101 4 0.0198877
11501201 1 4
11501301 0.0 4
11501400 -1
11501401 695.29 701.05 705.62 709.39 712.61
11501402 737.65 743.55 748.21 752.08 755.37
11501403 776.46 782.33 786.97 790.81 794.09

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11503405 984.62 991.22 996.49 1000.9
11503406 1033.0 1039.6 1044.8 1049.1
11503407 1081.7 1088.2 1093.3 1097.6
11503408 1130.2 1136.6 1141.7 1145.9
11503409 1178.4 1184.7 1189.8 1194.0
11503410 1223.8 1229.9 1234.8 1238.9
11503501 0 0 0 1 16.25 10
11503600 1
11503601 0 0 0 1 16.25 0.19812 10
11503701 10950 0.1000 0.0 0.0 1
11503702 10950 0.1000 0.0 0.0 2
11503703 10950 0.1000 0.0 0.0 3
11503704 10950 0.1000 0.0 0.0 4
11503705 10950 0.1000 0.0 0.0 5
11503706 10950 0.1000 0.0 0.0 6
11503707 10950 0.1000 0.0 0.0 7
11503708 10950 0.1000 0.0 0.0 8
11503709 10950 0.1000 0.0 0.0 9
11503710 10950 0.1000 0.0 0.0 10
11503900 1
11503901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.0 1.1 1.0 10
*
* side reflector inner ring - heat structure 1600
*
11600000 14 7 2 0 0.4734264 3
11600100 0 1
11600101 6 0.5082523
11600201 1 6
11600301 0.0 6
11600400 -1
11600401 532.45 532.49 532.52 532.54 532.56 532.58 532.60
11600402 533.68 533.85 533.98 534.08 534.17 534.25 534.31
11600403 610.58 617.55 622.90 627.24 630.89 634.04 636.82
11600404 638.11 646.48 652.91 658.13 662.52 666.30 669.64
11600405 664.63 674.11 681.39 687.29 692.27 696.56 700.33
11600406 691.84 702.33 710.39 716.93 722.43 727.18 731.35
11600407 719.76 731.19 739.96 747.08 753.07 758.24 762.79
11600408 748.37 760.65 770.08 777.73 784.17 789.73 794.62
11600409 777.65 790.73 800.77 808.92 815.78 821.70 826.90
11600410 807.46 821.26 831.86 840.46 847.70 853.95 859.44
11600411 837.78 852.25 863.36 872.37 879.96 886.51 892.27
11600412 867.64 882.63 894.15 903.49 911.35 918.14 924.11
11600413 831.52 838.99 844.73 849.39 853.31 856.70 859.67
11600414 831.19 838.63 844.34 848.97 852.88 856.24 859.21
11600500 1
11600501 0 0 0 1 0.1905 0.1905 1
11600502 0 0 0 1 0.1905 0.1905 2
11600503 0 0 0 1 0.1981 0.1981 12
11600504 0 0 0 1 0.2515 0.2515 13
11600505 0 0 0 1 0.2515 0.2515 14
11600601 0 0 0 1 0.1905 1
11600602 0 0 0 1 0.1905 2
11600603 0 0 0 1 0.1981 12
11600604 0 0 0 1 0.2515 13
11600605 0 0 0 1 0.2515 14
11600701 0.0 0.0 0.0 0.0 14
11600800 1
11600801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 14
11600900 1
11600901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 14
*
* side reflector middle ring - heat structure 1620
*

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11620000 14 7 2 0 0.007938 3
11620100 0 1
11620101 6 0.045085
11620201 1 6
11620301 0.0 6
11620400 -1
11620401 532.45 532.49 532.52 532.54 532.56 532.58 532.60
11620402 533.68 533.85 533.98 534.08 534.17 534.25 534.31
11620403 610.58 617.55 622.90 627.24 630.89 634.04 636.82
11620404 638.11 646.48 652.91 658.13 662.52 666.30 669.64
11620405 664.63 674.11 681.39 687.29 692.27 696.56 700.33
11620406 691.84 702.33 710.39 716.93 722.43 727.18 731.35
11620407 719.76 731.19 739.96 747.08 753.07 758.24 762.79
11620408 748.37 760.65 770.08 777.73 784.17 789.73 794.62
11620409 777.65 790.73 800.77 808.92 815.78 821.70 826.90
11620410 807.46 821.26 831.86 840.46 847.70 853.95 859.44
11620411 837.78 852.25 863.36 872.37 879.96 886.51 892.27
11620412 867.64 882.63 894.15 903.49 911.35 918.14 924.11
11620413 831.52 838.99 844.73 849.39 853.31 856.70 859.67
11620414 831.19 838.63 844.34 848.97 852.88 856.24 859.21
11620501 162010000 0 160 1 6.8580 1
11620502 162020000 0 160 1 6.8580 2
11620503 162030000 10000 160 1 7.1323 12
11620504 162130000 0 160 1 9.0526 13
11620505 162140000 0 160 1 9.0526 14
11620601 0 0 0 1 6.8580 1
11620602 0 0 0 1 6.8580 2
11620603 0 0 0 1 7.1323 12
11620604 0 0 0 1 9.0526 13
11620605 0 0 0 1 9.0526 14
11620701 0 0.0 0.0 0.0 14
11620800 1
11620801 0.0 0.10 2.77 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 1
11620802 0.0 0.29 2.58 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 2
11620803 0.0 0.48 2.39 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 3
11620804 0.0 0.68 2.19 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 4
11620805 0.0 0.88 1.99 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 5
11620806 0.0 1.07 1.79 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 6
11620807 0.0 1.27 1.59 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 7
11620808 0.0 1.47 1.39 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 8
11620809 0.0 1.67 1.20 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 9
11620810 0.0 1.87 1.00 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 10
11620811 0.0 2.07 0.80 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 11
11620812 0.0 2.26 0.60 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 12
11620813 0.0 2.49 0.38 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 13
11620814 0.0 2.74 0.13 0.0 0.0 0.0 0.0 1.0 2.9 1.1 1.0 14

```

*

* side reflector outer ring - heat structure 1640

*

```

11640000 14 7 2 0 0.575757 3
11640100 0 1
11640101 6 0.604430
11640201 1 6
11640301 0.0 6
11640400 -1
11640401 532.63 532.67 532.71 532.75 532.78 532.82 532.85
11640402 534.12 533.91 533.71 533.52 533.33 533.16 532.98
11640403 629.11 620.77 612.75 605.04 597.61 590.44 583.52
11640404 662.39 654.55 647.01 639.76 632.78 626.04 619.53
11640405 693.39 685.87 678.66 671.71 665.02 658.56 652.32
11640406 724.55 717.18 710.11 703.30 696.74 690.41 684.29
11640407 756.03 748.73 741.71 734.95 728.44 722.16 716.10
11640408 787.87 780.57 773.56 766.81 760.31 754.03 747.97

```

11640409	820.13	812.80	805.76	798.98	792.45	786.15	780.07					
11640410	852.63	845.27	838.19	831.38	824.81	818.48	812.36					
11640411	885.42	878.00	870.88	864.02	857.42	851.05	844.89					
11640412	917.30	909.94	902.87	896.06	889.50	883.17	877.06					
11640413	859.88	860.11	860.32	860.53	860.73	860.92	861.10					
11640414	859.48	859.77	860.05	860.32	860.58	860.83	861.08					
11640501	0	0	0	1	0.1905	1						
11640502	0	0	0	1	0.1905	2						
11640503	0	0	0	1	0.1981	12						
11640504	0	0	0	1	0.2515	13						
11640505	0	0	0	1	0.2515	14						
11640601	164010000	0	160	1	0.1905	1						
11640602	164020000	0	160	1	0.1905	2						
11640603	164030000	10000	160	1	0.1981	12						
11640604	164130000	0	160	1	0.2515	13						
11640605	164140000	0	160	1	0.2515	14						
11640701	0	0.0	0.0	0.0	14							
11640900	1											
11640901	0.0	0.10	2.77	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	1
11640902	0.0	0.29	2.58	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	2
11640903	0.0	0.48	2.39	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	3
11640904	0.0	0.68	2.19	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	4
11640905	0.0	0.88	1.99	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	5
11640906	0.0	1.07	1.79	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	6
11640907	0.0	1.27	1.59	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	7
11640908	0.0	1.47	1.39	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	8
11640909	0.0	1.67	1.20	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	9
11640910	0.0	1.87	1.00	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	10
11640911	0.0	2.07	0.80	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	11
11640912	0.0	2.26	0.60	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	12
11640913	0.0	2.49	0.38	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	13
11640914	0.0	2.74	0.13	0.0	0.0	0.0	0.0	1.0	2.9	1.1	1.23	14

*

* permanent side reflector - heat structure 1660

*

11660000	15	7	2	1	0.613389	3						
11660100	0	1										
11660101	6	0.750875										
11660201	5	6										
11660301	0.0	6										
11660400	-1											
11660401	532.63	532.67	532.71	532.75	532.78	532.82	532.85					
11660402	534.12	533.91	533.71	533.52	533.33	533.16	532.98					
11660403	629.11	620.77	612.75	605.04	597.61	590.44	583.52					
11660404	662.39	654.55	647.01	639.76	632.78	626.04	619.53					
11660405	693.39	685.87	678.66	671.71	665.02	658.56	652.32					
11660406	724.55	717.18	710.11	703.30	696.74	690.41	684.29					
11660407	756.03	748.73	741.71	734.95	728.44	722.16	716.10					
11660408	787.87	780.57	773.56	766.81	760.31	754.03	747.97					
11660409	820.13	812.80	805.76	798.98	792.45	786.15	780.07					
11660410	852.63	845.27	838.19	831.38	824.81	818.48	812.36					
11660411	885.42	878.00	870.88	864.02	857.42	851.05	844.89					
11660412	917.30	909.94	902.87	896.06	889.50	883.17	877.06					
11660413	859.88	860.11	860.32	860.53	860.73	860.92	861.10					
11660414	859.48	859.77	860.05	860.32	860.58	860.83	861.08					
11660415	859.48	859.77	860.05	860.32	860.58	860.83	861.08					
11660501	164010000	0	1	1	0.1905	1						
11660502	164020000	0	1	1	0.1905	2						
11660503	164030000	10000	1	1	0.1981	12						
11660504	164130000	0	1	1	0.2515	13						
11660505	164140000	0	1	1	0.2515	14						
11660506	175010000	0	1	1	0.2223	15						
11660601	166010000	0	160	1	0.1905	1						

```

11660602 166020000 0 160 1 0.1905 2
11660603 166030000 10000 160 1 0.1981 12
11660604 166130000 0 160 1 0.2515 13
11660605 166140000 0 160 1 0.2515 14
11660606 166150000 0 160 1 0.2223 15
11660701 0 0.0 0.0 0.0 15
11660800 1
11660801 0.0 0.10 3.00 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 1
11660802 0.0 0.29 2.80 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 2
11660803 0.0 0.48 2.61 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 3
11660804 0.0 0.68 2.41 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 4
11660805 0.0 0.88 2.21 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 5
11660806 0.0 1.07 2.01 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 6
11660807 0.0 1.27 1.81 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 7
11660808 0.0 1.47 1.62 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 8
11660809 0.0 1.67 1.42 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 9
11660810 0.0 1.87 1.22 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 10
11660811 0.0 2.07 1.02 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 11
11660812 0.0 2.26 0.82 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 12
11660813 0.0 2.49 0.60 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 13
11660814 0.0 2.74 0.35 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 14
11660815 0.0 2.98 0.11 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.22 15
11660900 1
11660901 0.0 0.10 3.00 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 1
11660902 0.0 0.29 2.80 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 2
11660903 0.0 0.48 2.61 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 3
11660904 0.0 0.68 2.41 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 4
11660905 0.0 0.88 2.21 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 5
11660906 0.0 1.07 2.01 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 6
11660907 0.0 1.27 1.81 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 7
11660908 0.0 1.47 1.62 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 8
11660909 0.0 1.67 1.42 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 9
11660910 0.0 1.87 1.22 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 10
11660911 0.0 2.07 1.02 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 11
11660912 0.0 2.26 0.82 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 12
11660913 0.0 2.49 0.60 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 13
11660914 0.0 2.74 0.35 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 14
11660915 0.0 2.98 0.11 0.0 0.0 0.0 0.0 1.0 3.1 1.1 1.0 15

```

*

* outlet plenum lower plate - heat structure 1750

*

```

11750000 1 9 1 1 0.0 0
11750100 0 1
11750101 4 0.079375
11750102 2 0.111375
11750103 2 0.136775
11750201 -1 4
11750202 -1 6
11750203 3 8
11750301 0.0 8
11750400 0
11750401 700.0 9
11750501 175010000 0 1 1 1.7713 1
11750601 105020000 0 1 1 1.7713 1
11750701 0 0.0 0.0 0.0 1
11750800 1
11750801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.14 1.1 1.0 1
11750900 1
11750901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.14 1.1 1.0 1

```

*

* outlet plenum support columns - heat structure 1751

*

```

11751000 1 4 2 1 0.0 0

```

```

11751100 0 1
11751101 3 0.028575
11751201 1 3
11751301 0.0 3
11751400 0
11751401 960.15 4
11751501 0 0 0 1 37.1412 1
11751601 175010000 0 1 1 37.1412 1
11751701 0 0.0 0.0 0.0 1
11751900 1
11751901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.22 1.1 1.0 1
*
* hot duct - heat structure 2000
*
12000000 4 9 2 1 0.148984 0
12000100 0 1
12000101 1 0.1524
12000102 4 0.161925
12000103 3 0.1653413
12000201 3 1 * 304 stainless steel
12000202 -8 5 * alumina silica insulation
12000203 3 8 * 304 stainless steel
12000301 0.0 8
12000400 0
12000401 960.15 9
12000501 200010000 0 1 1 0.4318 1
12000502 200020000 0 1 1 0.6510 2
12000503 200030000 0 1 1 0.4127 3
12000504 200040000 0 1 1 0.4127 4
12000601 270040000 0 1 1 0.4318 1
12000602 270030000 0 1 1 0.6510 2
12000603 270020000 0 1 1 0.4127 3
12000604 270010000 0 1 1 0.4127 4
12000701 0 0.0 0.0 0.0 4
12000800 1
12000801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 4
12000900 1
12000901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.33 1.1 1.0 4
*
* hot leg - heat structure 2001
*
12001000 2 7 2 1 0.149225 0
12001100 0 1
12001101 3 0.161925
12001102 3 0.212925
12001201 3 3 * 304 stainless steel
12001202 -9 6 * pipe insulation
12001301 0 6
12001400 0
12001401 960.15 7
12001501 200050000 10000 1 1 0.4906 2
12001601 -950 0 3951 1 0.4906 2
12001701 0 0.0 0.0 0.0 2
12001800 1
12001801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 2
*
* hot leg from valve V-311 into RCST - heat structure 2100
*
12100000 1 4 2 1 0.1492 0
12100100 0 1
12100101 3 0.161925
12100201 3 3 * 304 stainless steel
12100301 0.0 3

```

```

12100400 0
12100401 960.15 4
12100501 210010000 0 1 1 0.6604 1
12100601 280020000 0 1 1 0.6604 1
*12100601 280010000 0 1 1 0.6604 1 * use with single-volume RCST
12100701 0 0.0 0.0 0.0 1
12100800 1
12100801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 1
12100900 1
12100901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.32 1.1 1.0 1
*
* pipe from hot duct to steam generator inlet plenum - heat structure 2150
*
12150000 1 7 2 1 0.1270 0
12150100 0 1
12150101 3 0.16195
12150102 3 0.21295
12150201 3 3 * 304 stainless steel
12150202 -9 6 * pipe insulation
12150301 0.0 6
12150400 0
12150401 960.15 7
12150501 215010000 0 1 1 0.5405 1
12150601 -950 0 3951 1 0.5405 1
12150701 0 0.0 0.0 0.0 1
12150800 1
12150801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.54 1.1 1.0 1
*
* steam generator inlet plenum - heat structure 2200
*
12200000 1 7 2 1 0.1752 0
12200100 0 1
12200101 3 0.1912
12200102 3 0.2422
12200201 3 3
12200202 -6 6 * permanent insulation
12200301 0.0 6
12200400 0
12200401 960.15 7
12200501 220010000 0 1 1 0.58 1
12200601 -950 0 3951 1 0.58 1
12200701 0 0.0 0.0 0.0 1
12200800 1
12200801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.58 1.1 1.0 1
*
* steam generator plenum divider ("pass partition") - heat structure 2201
*
12201000 1 3 1 1 0.0
12201100 0 1
12201101 2 0.0127
12201201 3 2
12201301 0.0 2
12201400 0
12201401 960.15 3
12201501 220010000 0 1 1 0.0893 1
12201601 228010000 0 1 1 0.0893 1
12201701 0 0.0 0.0 0.0 1
12201800 1
12201801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.16 1.1 1.0 1
12201900 1
12201901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.16 1.1 1.0 1
*
* steam generator tubes - heat structure 2250

```

```

*
12250000 22 4 2 1 0.008280 3
12250100 0 1
12250101 3 0.009525
12250201 3 3
12250301 0.0 3
12250400 0
12250401 960.15 4
12250501 225010000 10000 1 1 26.4874 2
12250502 225030000 10000 1 1 26.7113 10
12250503 225110000 10000 1 1 34.1603 12
12250504 225130000 10000 1 1 26.7113 20
12250505 225200000 10000 1 1 26.4874 22
12250601 350010000 10000 111 1 26.4874 2
12250602 350030000 10000 111 1 26.7113 10
12250603 350110000 0 111 1 34.1603 12
12250604 350100000 -10000 111 1 26.7113 20
12250605 350020000 -10000 111 1 26.4874 22
12250701 0 0.0 0.0 0.0 22
12250800 1
12250801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 1.62 1.1 1.0 22
12250900 1
12250901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 1.62 1.25 1.0 22
*
* steam generator tube sheet - heat structure 2251
*
12251000 2 3 2 1 0.008280
12251100 0 1
12251101 2 0.015719
12251201 3 2
12251301 0.0 2
12251400 0
12251401 960.15 3
12251501 225010000 210000 1 1 15.5194 2
12251601 0 0 0 1 15.5194 2
12251701 0 0.0 0.0 0.0 2
12251800 1
12251801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.08 1.1 1.0 2
*
* steam generator outlet plenum - heat structure 2280
*
12280000 1 7 2 1 0.1667 0
12280100 0 1
12280101 3 0.182786133
12280102 3 0.233786133
12280201 3 3
12280202 -6 6 * permanent insulation
12280301 0 6
12280400 0
12280401 531.75 7
12280501 228010000 0 1 1 0.51 1
12280601 -950 0 3951 1 0.51 1
12280701 0 0.0 0.0 0.0 1
12280800 1
12280801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.51 1.1 1.0 1
*
* pipe from steam generator outlet plenum to circulator inlet - heat structure 2300
*
12300000 1 7 2 1 0.1014 0
12300100 0 1
12300101 3 0.1095375
12300102 3 0.1605375
12300201 3 3

```



```

12300202 -9 6 * pipe insulation
12300301 0.0 6
12300400 0
12300401 531.75 7
12300501 230010000 0 1 1 2.2827 1
12300601 -950 0 3951 1 2.2827 1
12300701 0 0.0 0.0 0.0 1
12300800 1
12300801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 1.80 1.1 1.0 1
*
* circulator - heat structure 2350
*
12350000 1 7 2 1 0.5000 0
12350100 0 1
12350101 3 0.6
12350102 3 0.6508
12350201 3 3
12350202 -9 6 * pipe insulation
12350301 0.0 6
12350400 0
12350401 531.75 7
12350501 235010000 0 1 1 0.5000 1
12350601 -950 0 3951 1 0.5000 1
12350701 0 0.0 0.0 0.0 1
12350800 1
12350801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.35 1.1 1.0 1
*
* pipe from circulator outlet to valve V-203 - heat structure 2400
*
12400000 1 7 2 1 0.1014 0
12400100 0 1
12400101 3 0.1095375
12400102 3 0.1605375
12400201 3 3
12400202 -9 6 * pipe insulation
12400301 0.0 6
12400400 0
12400401 531.75 7
12400501 240010000 0 1 1 1.2934 1
12400601 -950 0 3951 1 1.2934 1
12400701 0 0.0 0.0 0.0 1
12400800 1
12400801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.77 1.1 1.0 1
*
* pipe from valve V-203 to cold leg break valve - heat structure 2500
*
12500000 3 7 2 1 0.1014 0
12500100 0 1
12500101 3 0.1095375
12500102 3 0.1605375
12500201 3 3
12500202 -9 6 * pipe insulation
12500301 0.0 6
12500400 0
12500401 531.75 7
12500501 250010000 0 1 1 1.0917 1
12500502 250020000 0 1 1 0.3609 2
12500503 250030000 0 1 1 0.6223 3
12500601 -950 0 3951 1 1.0917 1
12500602 -950 0 3951 1 0.3609 2
12500603 -950 0 3951 1 0.6223 3
12500701 0 0.0 0.0 0.0 3
12500800 1

```

```

12500801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.62 1.1 1.0 1
12500802 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.20 1.1 1.0 3
*
* cold duct from valve V-311 into RCST - heat structure 2580
*
12580000 1 4 2 1 0.0968 0
12580100 0 1
12580101 3 0.1095375
12580201 3 3
12580301 0.0 3
12580400 0
12580401 531.75 4
12580501 258010000 0 1 1 0.6604 1
12580601 280020000 0 1 1 0.6604 1
*12580601 280010000 0 1 1 0.6604 1 * for single-volume RCST
12580701 0 0.0 0.0 0.0 1
12580800 1
12580801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.19 1.1 1.0 1
12580900 1
12580901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.22 1.1 1.0 1
*
* crossover line from cold leg to cold duct - heat structure 2600
*
12600000 1 7 2 1 0.1014 0
12600100 0 1
12600101 3 0.1095375
12600102 3 0.1605375
12600201 3 3
12600202 -9 6 * pipe insulation
12600301 0.0 6
12600400 0
12600401 531.75 7
12600501 260010000 0 1 1 0.3654 1
12600601 -950 0 3951 1 0.3654 1
12600701 0 0.0 0.0 0.0 1
12600800 1
12600801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.20 1.1 1.0 1
*
* cold duct - heat structure 2700
*
12700000 4 7 2 1 0.2191 0
12700100 0 1
12700101 3 0.2286
12700102 3 0.2796
12700201 3 3
12700202 -9 6 * pipe insulation
12700301 0.0 6
12700400 0
12700401 531.75 7
12700501 270010000 0 1 1 0.4127 1
12700502 270020000 0 1 1 0.4127 2
12700503 270030000 0 1 1 0.6510 3
12700504 270040000 0 1 1 0.4318 4
12700601 -950 0 3951 1 0.4127 1
12700602 -950 0 3951 1 0.4127 2
12700603 -950 0 3951 1 0.6510 3
12700604 -950 0 3951 1 0.4318 4
12700701 0 0.0 0.0 0.0 4
12700800 1
12700801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.44 1.1 1.0 4
*
* RCST - heat structure 2800 (two-volume configuration)
*

```

```

12800000 2 7 2 1 1.0414 0
12800100 0 1
12800101 3 1.0509
12800102 3 1.1019
12800201 3 3 * 304 stainless steel
12800202 -6 6 * permanent insulation
12800301 0.0 6
12800400 0
12800401 300.00 7
12800501 280010000 0 1 1 1.2954 1
12800502 280020000 0 1 1 4.3117 2
12800601 -950 0 3951 1 1.2954 1
12800602 -950 0 3951 1 4.3117 2
12800701 0 0.0 0.0 0.0 2
12800800 1
12800801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 5.61 1.1 1.0 2
*
* RCST - heat structure 2800 (single-volume configuration)
*
*12800000 1 7 2 1 1.0414 0
*12800100 0 1
*12800101 3 1.0509
*12800102 3 1.1019
*12800201 3 3 * 304 stainless steel
*12800202 -6 6 * permanent insulation
*12800301 0.0 6
*12800400 0
*12800401 300.00 7
*12800501 280010000 0 1 1 5.6071 1
*12800601 -950 0 3951 1 5.6071 1
*12800701 0 0.0 0.0 0.0 1
*12800800 1
*12800801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 5.61 1.1 1.0 1
*
* hot duct break spool piece - heat structure 2820
*
*12820000 1 7 2 1 0.0968 0
*12820100 0 1
*12820101 3 0.1095
*12820102 3 0.1603
*12820201 3 3 * 304 stainless steel
*12820202 9 6 * pipe insulation
*12820301 0.0 6
*12820400 0
*12820401 300.00 7
*12820501 282010000 0 1 1 1.1172 1
*12820601 280010000 0 1 1 1.1172 1
*12820701 0 0.0 0.0 0.0 1
*12820800 1
*12820801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.19 1.1 1.0 1
*12820900 1
*12820901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.32 1.1 1.0 1
*
* steam generator outer cylindrical shell - heat structure 3400
*
13400000 13 7 2 1 0.2985 0
13400100 0 1
13400101 3 0.3048
13400102 3 0.3558
13400201 3 3
13400202 -6 6 * permanent insulation
13400301 0.0 6
13400400 0

```

```

13400401 290.00 7
13400501 350010000 0 1 1 0.1409 1
13400502 340110000 0 1 1 0.1409 2
13400503 340100000 -10000 1 1 0.1421 10
13400504 340020000 0 1 1 0.6336 11
13400505 340010000 0 1 1 0.5701 12
13400506 360010000 0 1 1 0.5588 13
13400601 -950 0 3951 1 0.1409 2
13400602 -950 0 3951 1 0.1421 10
13400603 -950 0 3951 1 0.6336 11
13400604 -950 0 3951 1 0.5701 12
13400605 -950 0 3951 1 0.5588 13
13400701 0 0.0 0.0 0.0 13
13400800 1
13400801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 3.18 1.1 1.0 13
13400900 1
13400901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 3.18 1.1 1.0 13
*
* steam generator inner cylindrical shell - heat structure 3500
*
13500000 11 4 2 1 0.2715 0
13500100 0 1
13500101 3 0.276225
13500201 3 3
13500301 0.0 3
13500400 0
13500401 290.00 4
13500501 350020000 0 1 1 0.1409 1
13500502 350030000 10000 1 1 0.1421 9
13500503 350110000 0 1 1 0.6336 10
13500504 350120000 0 1 1 0.5701 11
13500601 340110000 0 1 1 0.1409 1
13500602 340100000 -10000 1 1 0.1421 9
13500603 340020000 0 1 1 0.6336 10
13500604 340010000 0 1 1 0.5701 11
13500701 0 0.0 0.0 0.0 11
13500800 1
13500801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.48 1.1 1.0 11
13500900 1
13500901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 2.48 1.1 1.0 11
*
* steam generator upper head - heat structure 3550
*
13550000 1 7 3 1 0.2739 0
13550100 0 1
13550101 3 0.280208376
13550102 3 0.331208376
13550201 3 3
13550202 -6 6 * permanent insulation
13550301 0.0 6
13550400 0
13550401 960.15 7
13550501 355010000 0 1 1 0.5 1
13550601 -950 0 3951 1 0.5 1
13550701 0 0.0 0.0 0.0 1
13550800 1
13550801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.27 1.1 1.0 1
13550900 1
13550901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.33 1.1 1.0 1
*
* CRD break nozzle - heat structure 0100
*
*10100000 25 7 2 1 0.0611 0

```

```

*10100100 0 1
*10100101 3 0.0707
*10100102 3 0.1217
*10100201 3 3
*10100202 -9 6 * pipe insulation
*10100301 0.0 6
*10100400 0
*10100401 531.75 7
*10100501 10010000 10000 1 1 0.0196 25
*10100601 -950 0 3951 1 0.0196 25
*10100701 0 0.0 0.0 0.0 25
*10100800 1
*10100801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.00 1.1 1.0 25
*
* CRD break line piping from pressure vessel nozzle to valve V-332 - heat structure
0200
*
*10200000 35 7 2 1 0.0486 0
*10200100 0 1
*10200101 3 0.05715
*10200102 3 0.10815
*10200201 3 3
*10200202 -9 6 * pipe insulation
*10200301 0.0 6
*10200400 0
*10200401 531.75 7
*10200501 20010000 10000 1 1 0.0204 35
*10200601 -950 0 3951 1 0.0204 35
*10200701 0 0.0 0.0 0.0 35
*10200800 1
*10200801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.00 1.1 1.0 35
*
* CRD break line piping from valve V-332 to RCST, section 1 - heat structure 0300
*
*10300000 92 7 2 1 0.0486 0
*10300100 0 1
*10300101 3 0.05715
*10300102 3 0.10815
*10300201 3 3
*10300202 -9 6 * pipe insulation
*10300301 0.0 6
*10300400 0
*10300401 300.00 7
*10300501 30010000 10000 1 1 0.0200 92
*10300601 -950 0 3951 1 0.0200 92
*10300701 0 0.0 0.0 0.0 92
*10300800 1
*10300801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.10 1.1 1.0 92
*
* CRD break line piping from valve V-332 to RCST, section 2 - heat structure 0320
*
*10320000 92 7 2 1 0.0486 0
*10320100 0 1
*10320101 3 0.05715
*10320102 3 0.10815
*10320201 3 3
*10320202 -9 6 * pipe insulation
*10320301 0.0 6
*10320400 0
*10320401 300.00 7
*10320501 32010000 10000 1 1 0.0200 92
*10320601 -950 0 3951 1 0.0200 92
*10320701 0 0.0 0.0 0.0 92

```

```

*10320800 1
*10320801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.10 1.1 1.0 92
*
* CRD break line piping from valve V-332 to RCST, section 3 - heat structure 0340
*
*10340000 92 7 2 1 0.0486 0
*10340100 0 1
*10340101 3 0.05715
*10340102 3 0.10815
*10340201 3 3
*10340202 -9 6 * pipe insulation
*10340301 0.0 6
*10340400 0
*10340401 300.00 7
*10340501 34010000 10000 1 1 0.0200 92
*10340601 -950 0 3951 1 0.0200 92
*10340701 0 0.0 0.0 0.0 92
*10340800 1
*10340801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.10 1.1 1.0 92
*
* pressure vessel bottom break line piping from pressure vessel nozzle stub to valve
V-331, section 1 - heat structure 0700
*
*10700000 73 7 2 1 0.0486 0
*10700100 0 1
*10700101 3 0.05715
*10700102 3 0.10815
*10700201 3 3
*10700202 -9 6 * pipe insulation
*10700301 0.0 6
*10700400 0
*10700401 531.75 7
*10700501 70010000 10000 1 1 0.0201 73
*10700601 -950 0 3951 1 0.0201 73
*10700701 0 0.0 0.0 0.0 73
*10700800 1
*10700801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.27 1.1 1.0 73
*
* pressure vessel bottom break line piping from pressure vessel nozzle stub to valve
V-331, section 1 - heat structure 0720
*
*10720000 73 7 2 1 0.0486 0
*10720100 0 1
*10720101 3 0.05715
*10720102 3 0.10815
*10720201 3 3
*10720202 -9 6 * pipe insulation
*10720301 0.0 6
*10720400 0
*10720401 531.75 7
*10720501 72010000 10000 1 1 0.0201 73
*10720601 -950 0 3951 1 0.0201 73
*10720701 0 0.0 0.0 0.0 73
*10720800 1
*10720801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.27 1.1 1.0 73
*
* pressure vessel bottom break line piping from valve V-331 to RCST - heat structure
0800
*
*10800000 96 7 2 1 0.0486 0
*10800100 0 1
*10800101 3 0.05715
*10800102 3 0.10815

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```

*10800201 3 3
*10800202 -9 6 * pipe insulation
*10800301 0.0 6
*10800400 0
*10800401 300.00 7
*10800501 80010000 10000 1 1 0.0200 96
*10800601 -950 0 3951 1 0.0200 96
*10800701 0 0.0 0.0 0.0 96
*10800800 1
*10800801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.10 1.1 1.0 96
*
* RCCS front panel (facing vessel) - heat structure 9500
*
19500000 19 4 1 1 0.0 0
19500100 0 1
19500101 3 0.00267
19500201 3 3
19500301 0.0 3
19500400 0
19500401 300.00 4
19500501 900010000 0 1 1 9.9692 1
19500502 900010000 0 1 1 3.1921 2
19500503 900010000 0 1 1 2.1677 3
19500504 900010000 0 1 1 2.4526 4
19500505 900010000 0 1 1 2.4526 5
19500506 900010000 0 1 1 1.9324 15
19500507 900010000 0 1 1 1.8581 16
19500508 900010000 0 1 1 1.9819 17
19500509 900010000 0 1 1 2.6647 18
19500510 900010000 0 1 1 7.3001 19
19500601 950010000 0 1 1 9.9692 1
19500602 950020000 0 1 1 3.1921 2
19500603 950030000 0 1 1 2.1677 3
19500604 950040000 0 1 1 2.4526 4
19500605 950050000 0 1 1 2.4526 5
19500606 950060000 10000 1 1 1.9324 15
19500607 950160000 0 1 1 1.8581 16
19500608 950170000 0 1 1 1.9819 17
19500609 950180000 0 1 1 2.6647 18
19500610 950190000 0 1 1 7.3001 19
19500701 0 0.0 0.0 0.0 19
19500800 1
19500801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 5.3 1.1 1.0 19
19500900 1
19500901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 5.3 1.1 1.0 19
*
* RCCS rear panel - heat structure 9501
*
19501000 19 7 1 1 0.0 0
19501100 0 1
19501101 3 0.000902
19501102 3 0.038902
19501201 3 3 * stainless steel
19501202 -6 6 * permanent insulation
19501301 0.0 6
19501400 0
19501401 290.0 7
19501501 950010000 0 1 1 9.9692 1
19501502 950020000 0 1 1 3.1921 2
19501503 950030000 0 1 1 2.1677 3
19501504 950040000 0 1 1 2.4526 4
19501505 950050000 0 1 1 2.4526 5
19501506 950060000 10000 1 1 1.9324 15

```

```

19501507  950160000  0  1  1  1.8581  16
19501508  950170000  0  1  1  1.9819  17
19501509  950180000  0  1  1  2.6647  18
19501510  950190000  0  1  1  7.3001  19
19501601  -950  0  3951  1  9.9692  1
19501602  -950  0  3951  1  3.1921  2
19501603  -950  0  3951  1  2.1677  3
19501604  -950  0  3951  1  2.4526  4
19501605  -950  0  3951  1  2.4526  5
19501606  -950  0  3951  1  1.9324  15
19501607  -950  0  3951  1  1.8581  16
19501608  -950  0  3951  1  1.9819  17
19501609  -950  0  3951  1  2.6647  18
19501610  -950  0  3951  1  7.3001  19
19501701  0  0.0  0.0  0.0  19
19501800  1
19501801  0.0  1.0  1.0  0.0  0.0  0.0  0.0  1.0  5.3  1.1  1.0  19
19501900  1
19501901  0.0  1.0  1.0  0.0  0.0  0.0  0.0  1.0  5.3  1.1  1.0  19
*
*****
* conduction/radiation sets
*****
*
60000000  12
*
* central reflector radial conduction
*
60100000  -42  0.0  0.0  601
*
* upper reflector, top
60101001  1300001  1  46.9
60102001  1320001  1  46.9
60103001  1340001  0  46.9
* upper reflector, bottom
60104001  1300002  1  46.9
60105001  1320002  1  46.9
60106001  1340002  0  46.9
* core level 1
60107001  1300003  1  46.9
60108001  1320003  1  46.9
60109001  1340003  0  46.9
* core level 2
60110001  1300004  1  46.9
60111001  1320004  1  46.9
60112001  1340004  0  46.9
* core level 3
60113001  1300005  1  46.9
60114001  1320005  1  46.9
60115001  1340005  0  46.9
* core level 4
60116001  1300006  1  46.9
60117001  1320006  1  46.9
60118001  1340006  0  46.9
* core level 5
60119001  1300007  1  46.9
60120001  1320007  1  46.9
60121001  1340007  0  46.9
* core level 6
60122001  1300008  1  46.9
60123001  1320008  1  46.9
60124001  1340008  0  46.9
* core level 7

```



```

60125001 1300009 1 46.9
60126001 1320009 1 46.9
60127001 1340009 0 46.9
* core level 8
60128001 1300010 1 46.9
60129001 1320010 1 46.9
60130001 1340010 0 46.9
* core level 9
60131001 1300011 1 46.9
60132001 1320011 1 46.9
60133001 1340011 0 46.9
* core level 10
60134001 1300012 1 46.9
60135001 1320012 1 46.9
60136001 1340012 0 46.9
* bottom reflector, upper
60137001 1300013 1 46.9
60138001 1320013 1 46.9
60139001 1340013 0 46.9
* bottom reflector, lower
60140001 1300014 1 46.9
60141001 1320014 1 46.9
60142001 1340014 0 46.9
* conduction area factors
* upper reflector, top
60101101 0.0 1 1.340979 2 0.0 42
60102101 0.279371 1 0.0 2 0.614615 3 0.0 42
60103101 0.0 1 1.340979 2 0.0 42
* upper reflector, bottom
60104101 0.0 4 1.340979 5 0.0 42
60105101 0.0 3 0.279371 4 0.0 5 0.614615 6 0.0 42
60106101 0.0 4 1.340979 5 0.0 42
* core level 1
60107101 0.0 7 1.340979 8 0.0 42
60108101 0.0 6 0.279371 7 0.0 8 0.614615 9 0.0 42
60109101 0.0 7 1.340979 8 0.0 42
* core level 2
60110101 0.0 10 1.340979 11 0.0 42
60111101 0.0 9 0.279371 10 0.0 11 0.614615 12 0.0 42
60112101 0.0 10 1.340979 11 0.0 42
* core level 3
60113101 0.0 13 1.340979 14 0.0 42
60114101 0.0 12 0.279371 13 0.0 14 0.614615 15 0.0 42
60115101 0.0 13 1.340979 14 0.0 42
* core level 4
60116101 0.0 16 1.340979 17 0.0 42
60117101 0.0 15 0.279371 16 0.0 17 0.614615 18 0.0 42
60118101 0.0 16 1.340979 17 0.0 42
* core level 5
60119101 0.0 19 1.340979 20 0.0 42
60120101 0.0 18 0.279371 19 0.0 20 0.614615 21 0.0 42
60121101 0.0 19 1.340979 20 0.0 42
* core level 6
60122101 0.0 22 1.340979 23 0.0 42
60123101 0.0 21 0.279371 22 0.0 23 0.614615 24 0.0 42
60124101 0.0 22 1.340979 23 0.0 42
* core level 7
60125101 0.0 25 1.340979 26 0.0 42
60126101 0.0 24 0.279371 25 0.0 26 0.614615 27 0.0 42
60127101 0.0 25 1.340979 26 0.0 42
* core level 8
60128101 0.0 28 1.340979 29 0.0 42
60129101 0.0 27 0.279371 28 0.0 29 0.614615 30 0.0 42

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```

60130101  0.0  28  1.340979  29  0.0  42
* core level 9
60131101  0.0  31  1.340979  32  0.0  42
60132101  0.0  30  0.279371  31  0.0  32  0.614615  33  0.0  42
60133101  0.0  31  1.340979  32  0.0  42
* core level 10
60134101  0.0  34  1.340979  35  0.0  42
60135101  0.0  33  0.279371  34  0.0  35  0.614615  36  0.0  42
60136101  0.0  34  1.340979  35  0.0  42
* bottom reflector, upper
60137101  0.0  37  1.340979  38  0.0  42
60138101  0.0  36  0.279371  37  0.0  38  0.614615  39  0.0  42
60139101  0.0  37  1.340979  38  0.0  42
* bottom reflector, lower
60140101  0.0  40  1.340979  41  0.0  42
60141101  0.0  39  0.279371  40  0.0  41  0.614615  42
60142101  0.0  40  1.340979  41  0.0  42
*
* core region radial and axial conduction
*
60200000  -71  0.0  0.0  601
* upper reflector, top
60201001  1340001  1  46.9
60202001  1400001  0  46.9
60203001  1450001  0  46.9
60204001  1500001  0  46.9
60205001  1600001  0  46.9
* upper reflector, bottom
60206001  1340002  1  46.9
60207001  1400002  0  46.9
60208001  1450002  0  46.9
60209001  1500002  0  46.9
60210001  1600002  0  46.9
* core level 1
60211001  1340003  1  46.9
60212001  1401001  0  46.9
60213001  1451001  0  46.9
60214001  1501001  0  46.9
60215001  1600003  0  46.9
* core level 2
60216001  1340004  1  46.9
60217001  1401002  0  46.9
60218001  1451002  0  46.9
60219001  1501002  0  46.9
60220001  1600004  0  46.9
* core level 3
60221001  1340005  1  46.9
60222001  1401003  0  46.9
60223001  1451003  0  46.9
60224001  1501003  0  46.9
60225001  1600005  0  46.9
* core level 4
60226001  1340006  1  46.9
60227001  1401004  0  46.9
60228001  1451004  0  46.9
60229001  1501004  0  46.9
60230001  1600006  0  46.9
* core level 5
60231001  1340007  1  46.9
60232001  1401005  0  46.9
60233001  1451005  0  46.9
60234001  1501005  0  46.9
60235001  1600007  0  46.9

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```

* core level 6
60236001 1340008 1 46.9
60237001 1401006 0 46.9
60238001 1451006 0 46.9
60239001 1501006 0 46.9
60240001 1600008 0 46.9
* core level 7
60241001 1340009 1 46.9
60242001 1401007 0 46.9
60243001 1451007 0 46.9
60244001 1501007 0 46.9
60245001 1600009 0 46.9
* core level 8
60246001 1340010 1 46.9
60247001 1401008 0 46.9
60248001 1451008 0 46.9
60249001 1501008 0 46.9
60250001 1600010 0 46.9
* core level 9
60251001 1340011 1 46.9
60252001 1401009 0 46.9
60253001 1451009 0 46.9
60254001 1501009 0 46.9
60255001 1600011 0 46.9
* core level 10
60256001 1340012 1 46.9
60257001 1401010 0 46.9
60258001 1451010 0 46.9
60259001 1501010 0 46.9
60260001 1600012 0 46.9
* bottom reflector, upper
60261001 1340013 1 46.9
60262001 1402001 0 46.9
60263001 1452001 0 46.9
60264001 1502001 0 46.9
60265001 1600013 0 46.9
* bottom reflector, lower
60266001 1340014 1 46.9
60267001 1402002 0 46.9
60268001 1452002 0 46.9
60269001 1502002 0 46.9
60270001 1600014 0 46.9
* upper plenum plate
60271001 1201001 0 46.9
* conduction area factors
* upper reflector, top
60201101 0.0 1 1.115715 2 0.0 70 0.038996 71
60202101 0.203425 1 0.0 2 0.190291 3 0.0 70 0.062205 71
60203101 0.0 1 0.161747 2 0.0 3 0.215708 4 0.0 70
60203102 0.049348 71
60204101 0.0 2 0.161781 3 0.0 4 0.370550 5 0.0 70
60204102 0.071373 71
60205101 0.0 3 1.192833 4 0.0 70 0.123034 71
60271101 0.004941 1 0.043232 2 0.040349 3 0.077810 4 0.041667 5
60271102 0.0 71
* upper reflector, bottom
60206101 0.0 6 1.115715 7 0.0 71
60207101 0.0 5 0.203425 6 0.0 7 0.190291 8 0.0 11
60207102 0.015477 12 0.0 71
60208101 0.0 6 0.161747 7 0.0 8 0.215708 9 0.0 12
60208102 0.013957 13 0.0 71
60209101 0.0 7 0.161781 8 0.0 9 0.370550 10 0.0 13
60209102 0.016411 14 0.0 71

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60210101 0.0 8 1.192833 9 0.0 71
* core level 1
60211101 0.0 11 1.661174 12 0.0 71
60212101 0.0 6 0.014881 7 0.0 10 0.302877 11 0.0 12
60212102 0.293809 13 0.0 71
60213101 0.0 7 0.013421 8 0.0 11 0.249738 12 0.0 13
60213102 0.323498 14 0.0 71
60214101 0.0 8 0.015780 9 0.0 12 0.242623 13 0.0 14
60214102 0.523730 15 0.0 71
60215101 0.0 13 1.685933 14 0.0 71
* core level 2
60216101 0.0 16 1.661174 17 0.0 71
60217101 0.0 15 0.302877 16 0.0 17 0.293809 18 0.0 71
60218101 0.0 16 0.249738 17 0.0 18 0.323498 19 0.0 71
60219101 0.0 17 0.242623 18 0.0 19 0.523730 20 0.0 71
60220101 0.0 18 1.685933 19 0.0 71
* core level 3
60221101 0.0 21 1.661174 22 0.0 71
60222101 0.0 20 0.302877 21 0.0 22 0.293809 23 0.0 71
60223101 0.0 21 0.249738 22 0.0 23 0.323498 24 0.0 71
60224101 0.0 22 0.242623 23 0.0 24 0.523730 25 0.0 71
60225101 0.0 23 1.685933 24 0.0 71
* core level 4
60226101 0.0 26 1.661174 27 0.0 71
60227101 0.0 25 0.302877 26 0.0 27 0.293809 28 0.0 71
60228101 0.0 26 0.249738 27 0.0 28 0.323498 29 0.0 71
60229101 0.0 27 0.242623 28 0.0 29 0.523730 30 0.0 71
60230101 0.0 28 1.685933 29 0.0 71
* core level 5
60231101 0.0 31 1.661174 32 0.0 71
60232101 0.0 30 0.302877 31 0.0 32 0.293809 33 0.0 71
60233101 0.0 31 0.249738 32 0.0 33 0.323498 34 0.0 71
60234101 0.0 32 0.242623 33 0.0 34 0.523730 35 0.0 71
60235101 0.0 33 1.685933 34 0.0 71
* core level 6
60236101 0.0 36 1.661174 37 0.0 71
60237101 0.0 35 0.302877 36 0.0 37 0.293809 38 0.0 71
60238101 0.0 36 0.249738 37 0.0 38 0.323498 39 0.0 71
60239101 0.0 37 0.242623 38 0.0 39 0.523730 40 0.0 71
60240101 0.0 38 1.685933 39 0.0 71
* core level 7
60241101 0.0 41 1.661174 42 0.0 71
60242101 0.0 40 0.302877 41 0.0 42 0.293809 43 0.0 71
60243101 0.0 41 0.249738 42 0.0 43 0.323498 44 0.0 71
60244101 0.0 42 0.242623 43 0.0 44 0.523730 45 0.0 71
60245101 0.0 43 1.685933 44 0.0 71
* core level 8
60246101 0.0 46 1.661174 47 0.0 71
60247101 0.0 45 0.302877 46 0.0 47 0.293809 48 0.0 71
60248101 0.0 46 0.249738 47 0.0 48 0.323498 49 0.0 71
60249101 0.0 47 0.242623 48 0.0 49 0.523730 50 0.0 71
60250101 0.0 48 1.685933 49 0.0 71
* core level 9
60251101 0.0 51 1.661174 52 0.0 71
60252101 0.0 50 0.302877 51 0.0 52 0.293809 53 0.0 71
60253101 0.0 51 0.249738 52 0.0 53 0.323498 54 0.0 71
60254101 0.0 52 0.242623 53 0.0 54 0.523730 55 0.0 71
60255101 0.0 53 1.685933 54 0.0 71
* core level 10
60256101 0.0 56 1.661174 57 0.0 71
60257101 0.0 55 0.302877 56 0.0 57 0.293809 58 0.0 61
60257102 0.012522 62 0.0 71
60258101 0.0 56 0.249738 57 0.0 58 0.323498 59 0.0 62

```

```

60258102  0.011229  63  0.0  71
60259101  0.0  57  0.242623  58  0.0  59  0.523730  60  0.0  63
60259102  0.013323  64  0.0  71
60260101  0.0  58  1.685933  59  0.0  71
* bottom reflector, upper
60261101  0.0  61  1.115715  62  0.0  71
60262101  0.0  56  0.009866  57  0.0  60  0.203425  61  0.0  62
60262102  0.190291  63  0.0  71
60263101  0.0  57  0.008847  58  0.0  61  0.161747  62  0.0  63
60263102  0.215708  64  0.0  71
60264101  0.0  58  0.010497  59  0.0  62  0.161781  63  0.0  64
60264102  0.370550  65  0.0  71
60265101  0.0  63  1.192833  64  0.0  71
* bottom reflector, lower
60266101  0.0  66  1.115715  67  0.0  71
60267101  0.0  65  0.203425  66  0.0  67  0.190291  68  0.0  71
60268101  0.0  66  0.161747  67  0.0  68  0.215708  69  0.0  71
60269101  0.0  67  0.161781  68  0.0  69  0.370550  70  0.0  71
60270101  0.0  68  1.192833  69  0.0  71
*
* side reflector radial conduction
*
60300000  -42  0.0  0.0  601
*
* upper reflector, top
60301001  1600001  1  46.9
60302001  1620001  1  46.9
60303001  1640001  0  46.9
* upper reflector, bottom
60304001  1600002  1  46.9
60305001  1620002  1  46.9
60306001  1640002  0  46.9
* core level 1
60307001  1600003  1  46.9
60308001  1620003  1  46.9
60309001  1640003  0  46.9
* core level 2
60310001  1600004  1  46.9
60311001  1620004  1  46.9
60312001  1640004  0  46.9
* core level 3
60313001  1600005  1  46.9
60314001  1620005  1  46.9
60315001  1640005  0  46.9
* core level 4
60316001  1600006  1  46.9
60317001  1620006  1  46.9
60318001  1640006  0  46.9
* core level 5
60319001  1600007  1  46.9
60320001  1620007  1  46.9
60321001  1640007  0  46.9
* core level 6
60322001  1600008  1  46.9
60323001  1620008  1  46.9
60324001  1640008  0  46.9
* core level 7
60325001  1600009  1  46.9
60326001  1620009  1  46.9
60327001  1640009  0  46.9
* core level 8
60328001  1600010  1  46.9
60329001  1620010  1  46.9

```

```

60330001 1640010 0 46.9
* core level 9
60331001 1600011 1 46.9
60332001 1620011 1 46.9
60333001 1640011 0 46.9
* core level 10
60334001 1600012 1 46.9
60335001 1620012 1 46.9
60336001 1640012 0 46.9
* bottom reflector, upper
60337001 1600013 1 46.9
60338001 1620013 1 46.9
60339001 1640013 0 46.9
* bottom reflector, lower
60340001 1600014 1 46.9
60341001 1620014 1 46.9
60342001 1640014 0 46.9
* conduction area factors
* upper reflector, top
60301101 0.0 1 1.781545 2 0.0 42
60302101 0.557881 1 0.0 2 0.631977 3 0.0 42
60303101 0.0 1 1.781545 2 0.0 42
* upper reflector, bottom
60304101 0.0 4 1.781545 5 0.0 42
60305101 0.0 3 0.557881 4 0.0 5 0.631977 6 0.0 42
60306101 0.0 4 1.781545 5 0.0 42
* core level 1
60307101 0.0 7 1.781545 8 0.0 42
60308101 0.0 6 0.557881 7 0.0 8 0.631977 9 0.0 42
60309101 0.0 7 1.781545 8 0.0 42
* core level 2
60310101 0.0 10 1.781545 11 0.0 42
60311101 0.0 9 0.557881 10 0.0 11 0.631977 12 0.0 42
60312101 0.0 10 1.781545 11 0.0 42
* core level 3
60313101 0.0 13 1.781545 14 0.0 42
60314101 0.0 12 0.557881 13 0.0 14 0.631977 15 0.0 42
60315101 0.0 13 1.781545 14 0.0 42
* core level 4
60316101 0.0 16 1.781545 17 0.0 42
60317101 0.0 15 0.557881 16 0.0 17 0.631977 18 0.0 42
60318101 0.0 16 1.781545 17 0.0 42
* core level 5
60319101 0.0 19 1.781545 20 0.0 42
60320101 0.0 18 0.557881 19 0.0 20 0.631977 21 0.0 42
60321101 0.0 19 1.781545 20 0.0 42
* core level 6
60322101 0.0 22 1.781545 23 0.0 42
60323101 0.0 21 0.557881 22 0.0 23 0.631977 24 0.0 42
60324101 0.0 22 1.781545 23 0.0 42
* core level 7
60325101 0.0 25 1.781545 26 0.0 42
60326101 0.0 24 0.557881 25 0.0 26 0.631977 27 0.0 42
60327101 0.0 25 1.781545 26 0.0 42
* core level 8
60328101 0.0 28 1.781545 29 0.0 42
60329101 0.0 27 0.557881 28 0.0 29 0.631977 30 0.0 42
60330101 0.0 28 1.781545 29 0.0 42
* core level 9
60331101 0.0 31 1.781545 32 0.0 42
60332101 0.0 30 0.557881 31 0.0 32 0.631977 33 0.0 42
60333101 0.0 31 1.781545 32 0.0 42
* core level 10

```

```

60334101  0.0  34  1.781545  35  0.0  42
60335101  0.0  33  0.557881  34  0.0  35  0.631977  36  0.0  42
60336101  0.0  34  1.781545  35  0.0  42
* bottom reflector, upper
60337101  0.0  37  1.781545  38  0.0  42
60338101  0.0  36  0.557881  37  0.0  38  0.631977  39  0.0  42
60339101  0.0  37  1.781545  38  0.0  42
* bottom reflector, lower
60340101  0.0  40  1.781545  41  0.0  42
60341101  0.0  39  0.557881  40  0.0  41  0.631977  42
60342101  0.0  40  1.781545  41  0.0  42

```

```

*
* radiation from heater rod to ceramic, inner core ring
*

```

```

61100000  20  300.0  0.0

```

```

*
61101001  1403001  1  0.810
61102001  1401001  1  0.581
61103001  1403002  1  0.810
61104001  1401002  1  0.581
61105001  1403003  1  0.810
61106001  1401003  1  0.581
61107001  1403004  1  0.810
61108001  1401004  1  0.581
61109001  1403005  1  0.810
61110001  1401005  1  0.581
61111001  1403006  1  0.810
61112001  1401006  1  0.581
61113001  1403007  1  0.810
61114001  1401007  1  0.581
61115001  1403008  1  0.810
61116001  1401008  1  0.581
61117001  1403009  1  0.810
61118001  1401009  1  0.581
61119001  1403010  1  0.810
61120001  1401010  1  0.581

```

```

*
61101101  0.0  1  1.0  2  0.0  20
61102101  0.176751  1  0.823249  2  0.0  20
61103101  0.0  3  1.0  4  0.0  20
61104101  0.0  2  0.176751  3  0.823249  4  0.0  20
61105101  0.0  5  1.0  6  0.0  20
61106101  0.0  4  0.176751  5  0.823249  6  0.0  20
61107101  0.0  7  1.0  8  0.0  20
61108101  0.0  6  0.176751  7  0.823249  8  0.0  20
61109101  0.0  9  1.0  10  0.0  20
61110101  0.0  8  0.176751  9  0.823249  10  0.0  20
61111101  0.0  11  1.0  12  0.0  20
61112101  0.0  10  0.176751  11  0.823249  12  0.0  20
61113101  0.0  13  1.0  14  0.0  20
61114101  0.0  12  0.176751  13  0.823249  14  0.0  20
61115101  0.0  15  1.0  16  0.0  20
61116101  0.0  14  0.176751  15  0.823249  16  0.0  20
61117101  0.0  17  1.0  18  0.0  20
61118101  0.0  16  0.176751  17  0.823249  18  0.0  20
61119101  0.0  19  1.0  20
61120101  0.0  18  0.176751  19  0.823249  20

```

```

*
* radiation from heater rod to ceramic, middle core ring
*

```

```

61200000  20  300.0  0.0

```

```

*
61201001  1453001  1  0.810

```

61202001	1451001	1	0.581
61203001	1453002	1	0.810
61204001	1451002	1	0.581
61205001	1453003	1	0.810
61206001	1451003	1	0.581
61207001	1453004	1	0.810
61208001	1451004	1	0.581
61209001	1453005	1	0.810
61210001	1451005	1	0.581
61211001	1453006	1	0.810
61212001	1451006	1	0.581
61213001	1453007	1	0.810
61214001	1451007	1	0.581
61215001	1453008	1	0.810
61216001	1451008	1	0.581
61217001	1453009	1	0.810
61218001	1451009	1	0.581
61219001	1453010	1	0.810
61220001	1451010	1	0.581

*

61201101	0.0	1	1.0	2	0.0	20
61202101	0.211996	1	0.788004	2	0.0	20
61203101	0.0	3	1.0	4	0.0	20
61204101	0.0	2	0.211996	3	0.788004	4 0.0 20
61205101	0.0	5	1.0	6	0.0	20
61206101	0.0	4	0.211996	5	0.788004	6 0.0 20
61207101	0.0	7	1.0	8	0.0	20
61208101	0.0	6	0.211996	7	0.788004	8 0.0 20
61209101	0.0	9	1.0	10	0.0	20
61210101	0.0	8	0.211996	9	0.788004	10 0.0 20
61211101	0.0	11	1.0	12	0.0	20
61212101	0.0	10	0.211996	11	0.788004	12 0.0 20
61213101	0.0	13	1.0	14	0.0	20
61214101	0.0	12	0.211996	13	0.788004	14 0.0 20
61215101	0.0	15	1.0	16	0.0	20
61216101	0.0	14	0.211996	15	0.788004	16 0.0 20
61217101	0.0	17	1.0	18	0.0	20
61218101	0.0	16	0.211996	17	0.788004	18 0.0 20
61219101	0.0	19	1.0	20		
61220101	0.0	18	0.211996	19	0.788004	20

*

* radiation from heater rod to ceramic, outer core ring

*

61300000	20	300.0	0.0
----------	----	-------	-----

*

61301001	1503001	1	0.810
61302001	1501001	1	0.581
61303001	1503002	1	0.810
61304001	1501002	1	0.581
61305001	1503003	1	0.810
61306001	1501003	1	0.581
61307001	1503004	1	0.810
61308001	1501004	1	0.581
61309001	1503005	1	0.810
61310001	1501005	1	0.581
61311001	1503006	1	0.810
61312001	1501006	1	0.581
61313001	1503007	1	0.810
61314001	1501007	1	0.581
61315001	1503008	1	0.810
61316001	1501008	1	0.581
61317001	1503009	1	0.810
61318001	1501009	1	0.581


```

61319001 1503010 1 0.810
61320001 1501010 1 0.581
*
61301101 0.0 1 1.0 2 0.0 20
61302101 0.155830 1 0.844170 2 0.0 20
61303101 0.0 3 1.0 4 0.0 20
61304101 0.0 2 0.155830 3 0.844170 4 0.0 20
61305101 0.0 5 1.0 6 0.0 20
61306101 0.0 4 0.155830 5 0.844170 6 0.0 20
61307101 0.0 7 1.0 8 0.0 20
61308101 0.0 6 0.155830 7 0.844170 8 0.0 20
61309101 0.0 9 1.0 10 0.0 20
61310101 0.0 8 0.155830 9 0.844170 10 0.0 20
61311101 0.0 11 1.0 12 0.0 20
61312101 0.0 10 0.155830 11 0.844170 12 0.0 20
61313101 0.0 13 1.0 14 0.0 20
61314101 0.0 12 0.155830 13 0.844170 14 0.0 20
61315101 0.0 15 1.0 16 0.0 20
61316101 0.0 14 0.155830 15 0.844170 16 0.0 20
61317101 0.0 17 1.0 18 0.0 20
61318101 0.0 16 0.155830 17 0.844170 18 0.0 20
61319101 0.0 19 1.0 20
61320101 0.0 18 0.155830 19 0.844170 20
*
* radiation from side reflector to permanent reflector
*
61400000 28 300.0 0.0
*
61401001 1640001 1 0.788
61402001 1660001 0 0.707
61403001 1640002 1 0.788
61404001 1660002 0 0.707
61405001 1640003 1 0.788
61406001 1660003 0 0.707
61407001 1640004 1 0.788
61408001 1660004 0 0.707
61409001 1640005 1 0.788
61410001 1660005 0 0.707
61411001 1640006 1 0.788
61412001 1660006 0 0.707
61413001 1640007 1 0.788
61414001 1660007 0 0.707
61415001 1640008 1 0.788
61416001 1660008 0 0.707
61417001 1640009 1 0.788
61418001 1660009 0 0.707
61419001 1640010 1 0.788
61420001 1660010 0 0.707
61421001 1640011 1 0.788
61422001 1660011 0 0.707
61423001 1640012 1 0.788
61424001 1660012 0 0.707
61425001 1640013 1 0.788
61426001 1660013 0 0.707
61427001 1640014 1 0.788
61428001 1660014 0 0.707
*
61401101 0.0 1 1.0 2 0.0 28
61402101 0.985395 1 0.014605 2 0.0 28
61403101 0.0 2 0.0 3 1.0 4 0.0 28
61404101 0.0 2 0.985395 3 0.014605 4 0.0 28
61405101 0.0 4 0.0 5 1.0 6 0.0 28
61406101 0.0 4 0.985395 5 0.014605 6 0.0 28

```

61407101	0.0	6	0.0	7	1.0	8	0.0	28
61408101	0.0	6	0.985395	7	0.014605	8	0.0	28
61409101	0.0	8	0.0	9	1.0	10	0.0	28
61410101	0.0	8	0.985395	9	0.014605	10	0.0	28
61411101	0.0	10	0.0	11	1.0	12	0.0	28
61412101	0.0	10	0.985395	11	0.014605	12	0.0	28
61413101	0.0	12	0.0	13	1.0	14	0.0	28
61414101	0.0	12	0.985395	13	0.014605	14	0.0	28
61415101	0.0	14	0.0	15	1.0	16	0.0	28
61416101	0.0	14	0.985395	15	0.014605	16	0.0	28
61417101	0.0	16	0.0	17	1.0	18	0.0	28
61418101	0.0	16	0.985395	17	0.014605	18	0.0	28
61419101	0.0	18	0.0	19	1.0	20	0.0	28
61420101	0.0	18	0.985395	19	0.014605	20	0.0	28
61421101	0.0	20	0.0	21	1.0	22	0.0	28
61422101	0.0	20	0.985395	21	0.014605	22	0.0	28
61423101	0.0	22	0.0	23	1.0	24	0.0	28
61424101	0.0	22	0.985395	23	0.014605	24	0.0	28
61425101	0.0	24	0.0	25	1.0	26	0.0	28
61426101	0.0	24	0.985395	25	0.014605	26	0.0	28
61427101	0.0	26	0.0	27	1.0	28		
61428101	0.0	26	0.985395	27	0.014605	28		

*

* radiation from permanent side reflector to core barrel

*

61500000	30	300.0	0.0
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*

61501001	1660001	1	0.721
61502001	1150016	0	0.075
61503001	1660002	1	0.721
61504001	1150015	0	0.075
61505001	1660003	1	0.721
61506001	1150014	0	0.075
61507001	1660004	1	0.721
61508001	1150013	0	0.075
61509001	1660005	1	0.721
61510001	1150012	0	0.075
61511001	1660006	1	0.721
61512001	1150011	0	0.075
61513001	1660007	1	0.721
61514001	1150010	0	0.075
61515001	1660008	1	0.721
61516001	1150009	0	0.075
61517001	1660009	1	0.721
61518001	1150008	0	0.075
61519001	1660010	1	0.721
61520001	1150007	0	0.075
61521001	1660011	1	0.721
61522001	1150006	0	0.075
61523001	1660012	1	0.721
61524001	1150005	0	0.075
61525001	1660013	1	0.721
61526001	1150004	0	0.075
61527001	1660014	1	0.721
61528001	1150003	0	0.075
61529001	1660015	1	0.721
61530001	1150002	0	0.075

*

61501101	0.0	1	1.0	2	0.0	30
61502101	0.929623	1	0.070377	2	0.0	30
61503101	0.0	3	1.0	4	0.0	30
61504101	0.0	2	0.991597	3	0.008403	4 0.0 30
61505101	0.0	5	1.0	6	0.0	30

61506101	0.0	4	0.991597	5	0.008403	6	0.0	30
61507101	0.0	7	1.0	8	0.0	30		
61508101	0.0	6	0.991597	7	0.008403	8	0.0	30
61509101	0.0	9	1.0	10	0.0	30		
61510101	0.0	8	0.991597	9	0.008403	10	0.0	30
61511101	0.0	11	1.0	12	0.0	30		
61512101	0.0	10	0.991597	11	0.008403	12	0.0	30
61513101	0.0	13	1.0	14	0.0	30		
61514101	0.0	12	0.991597	13	0.008403	14	0.0	30
61515101	0.0	15	1.0	16	0.0	30		
61516101	0.0	14	0.991597	15	0.008403	16	0.0	30
61517101	0.0	17	1.0	18	0.0	30		
61518101	0.0	16	0.991597	17	0.008403	18	0.0	30
61519101	0.0	19	1.0	20	0.0	30		
61520101	0.0	18	0.991597	19	0.008403	20	0.0	30
61521101	0.0	21	1.0	22	0.0	30		
61522101	0.0	20	0.991597	21	0.008403	22	0.0	30
61523101	0.0	23	1.0	24	0.0	30		
61524101	0.0	22	0.991597	23	0.008403	24	0.0	30
61525101	0.0	25	1.0	26	0.0	30		
61526101	0.0	24	0.991597	25	0.008403	26	0.0	30
61527101	0.0	27	1.0	28	0.0	30		
61528101	0.0	26	0.991597	27	0.008403	28	0.0	30
61529101	0.0	29	1.0	30				
61530101	0.0	28	0.991597	29	0.008403	30		
*								
* radiation from upper plenum plate to upper plenum shield/upper head								
*								
61600000	4	300.0	0.0					
*								
61601001	1201001	1	0.810					
61602001	1202001	1	0.075					
61603001	1001001	0	0.072					
61604001	1200001	0	0.075					
*								
61601101	0.0	1	0.049499	2	0.850501	3	0.100000	4
61602101	0.028920	1	0.400000	2	0.367582	3	0.203498	4
61603101	0.388455	1	0.287355	2	0.224190	3	0.100000	4
61604101	0.127657	1	0.444634	2	0.279498	3	0.148211	4
*								
* radiation from bottom reflector to outlet plenum bottom plate								
*								
61800000	8	300.0	0.0					
*								
61801001	1320014	0	0.702					
61802001	1402002	1	0.612					
61803001	1452002	1	0.612					
61804001	1502002	1	0.612					
61805001	1620014	0	0.747					
61806001	1751001	1	0.630					
61807001	1660015	0	0.494					
61808001	1750001	0	0.747					
*								
61801101	0.264687	1	0	5	0.514719	6	0.0	7
61802101	0.0	1	0.961510	2	0.0	5	0.026943	6
61802102	0.0	7	0.011547	8				
61803101	0.0	2	0.963920	3	0.0	5	0.025256	6
61803102	0.0	7	0.010824	8				
61804101	0.0	3	0.959868	4	0.0	5	0.028093	6
61804102	0.0	7	0.012040	8				
61805101	0.0	4	0.506591	5	0.345386	6	0.0	7
61806101	0.006970	1	0.014677	2	0.014748	3	0.025416	4
61806102	0.023384	5	0.600000	6	0.102613	7	0.212193	8

```

61807101  0.0  5  0.798854  6  0.069445  7  0.131701  8
61808101  0.011245  1  0.023680  2  0.023795  3  0.041008  4
61808102  0.037729  5  0.798854  6  0.063689  7  0.0  8
*
* radiation from core barrel to primary pressure vessel
*
61900000  36  300.0  0.0
* core support region
61901001  1150001  1  0.075
61902001  1000001  0  0.075
* outlet plenum
61903001  1150002  1  0.075
61904001  1100001  0  0.075
61905001  1100001  1  0.075
61906001  1000002  0  0.075
*bottom reflector, bottom
61907001  1150003  1  0.075
61908001  1000003  0  0.075
* bottom reflector, top
61909001  1150004  1  0.075
61910001  1000004  0  0.075
* core level 10
61911001  1150005  1  0.075
61912001  1000005  0  0.075
* core level 9
61913001  1150006  1  0.075
61914001  1000006  0  0.075
* core level 8
61915001  1150007  1  0.075
61916001  1000007  0  0.075
* core level 7
61917001  1150008  1  0.075
61918001  1000008  0  0.075
* core level 6
61919001  1150009  1  0.075
61920001  1000009  0  0.075
* core level 5
61921001  1150010  1  0.075
61922001  1000010  0  0.075
* core level 4
61923001  1150011  1  0.075
61924001  1000011  0  0.075
* core level 3
61925001  1150012  1  0.075
61926001  1000012  0  0.075
* core level 2
61927001  1150013  1  0.075
61928001  1000013  0  0.075
* core level 1
61929001  1150014  1  0.075
61930001  1000014  0  0.075
* upper reflector, bottom
61931001  1150015  1  0.075
61932001  1000015  0  0.075
* upper reflector, top
61933001  1150016  1  0.075
61934001  1000016  0  0.075
* upper plenum region
61935001  1200001  1  0.075
61936001  1000017  0  0.075
* view factors
* core support region
61901101  0.0  1  1.0  2  0.0  36

```

```

61902101 0.930233 1 0.069767 2 0.0 36
* outlet plenum
61903101 0.0 3 1.0 4 0.0 36
61904101 0.0 2 0.537 3 0.462596 4 0.0 36
61905101 0.0 4 0.425791 5 0.574209 6 0.0 36
61906101 0.0 4 1.0 5 0.0 6 0.0 36
*bottom reflector, bottom
61907101 0.0 7 1.0 8 0.0 36
61908101 0.0 6 0.930233 7 0.069767 8 0.0 36
* bottom reflector, top
61909101 0.0 9 1.0 10 0.0 36
61910101 0.0 8 0.930233 9 0.069767 10 0.0 36
* core level 10
61911101 0.0 11 1.0 12 0.0 36
61912101 0.0 10 0.930233 11 0.069767 12 0.0 36
* core level 9
61913101 0.0 13 1.0 14 0.0 36
61914101 0.0 12 0.930233 13 0.069767 14 0.0 36
* core level 8
61915101 0.0 15 1.0 16 0.0 36
61916101 0.0 14 0.930233 15 0.069767 16 0.0 36
* core level 7
61917101 0.0 17 1.0 18 0.0 36
61918101 0.0 16 0.930233 17 0.069767 18 0.0 36
* core level 6
61919101 0.0 19 1.0 20 0.0 36
61920101 0.0 18 0.930233 19 0.069767 20 0.0 36
* core level 5
61921101 0.0 21 1.0 22 0.0 36
61922101 0.0 20 0.930233 21 0.069767 22 0.0 36
* core level 4
61923101 0.0 23 1.0 24 0.0 36
61924101 0.0 22 0.930233 23 0.069767 24 0.0 36
* core level 3
61925101 0.0 25 1.0 26 0.0 36
61926101 0.0 24 0.930233 25 0.069767 26 0.0 36
* core level 2
61927101 0.0 27 1.0 28 0.0 36
61928101 0.0 26 0.930233 27 0.069767 28 0.0 36
* core level 1
61929101 0.0 29 1.0 30 0.0 36
61930101 0.0 28 0.930233 29 0.069767 30 0.0 36
* upper reflector, bottom
61931101 0.0 31 1.0 32 0.0 36
61932101 0.0 30 0.930233 31 0.069767 32 0.0 36
* upper reflector, top
61933101 0.0 33 1.0 34 0.0 36
61934101 0.0 32 0.930233 33 0.069767 34 0.0 36
* upper plenum region
61935101 0.0 35 1.0 36
61936101 0.0 34 0.935879 35 0.064121 36
*
* radiation from primary pressure vessel to RCCS
*
62100000 38 300.0 0.000
* lower head region
62101001 1002001 1 0.075
62102001 9500001 0 0.075
* core support region
62103001 1000001 1 0.075
62104001 9500002 0 0.075
* outlet plenum
62105001 1000002 1 0.075

```

```

62106001  9500003  0  0.075
* bottom reflector, bottom
62107001  1000003  1  0.075
62108001  9500004  0  0.075
* bottom reflector, top
62109001  1000004  1  0.075
62110001  9500005  0  0.075
* core level 10
62111001  1000005  1  0.075
62112001  9500006  0  0.075
* core level 9
62113001  1000006  1  0.075
62114001  9500007  0  0.075
* core level 8
62115001  1000007  1  0.075
62116001  9500008  0  0.075
* core level 7
62117001  1000008  1  0.075
62118001  9500009  0  0.075
* core level 6
62119001  1000009  1  0.075
62120001  9500010  0  0.075
* core level 5
62121001  1000010  1  0.075
62122001  9500011  0  0.075
* core level 4
62123001  1000011  1  0.075
62124001  9500012  0  0.075
* core level 3
62125001  1000012  1  0.075
62126001  9500013  0  0.075
* core level 2
62127001  1000013  1  0.075
62128001  9500014  0  0.075
* core level 1
62129001  1000014  1  0.075
62130001  9500015  0  0.075
* upper reflector, bottom
62131001  1000015  1  0.075
62132001  9500016  0  0.075
* upper reflector, top
62133001  1000016  1  0.075
62134001  9500017  0  0.075
* upper plenum cylinder
62135001  1000017  1  0.075
62136001  9500018  0  0.075
* upper head
62137001  1001001  1  0.075
62138001  9500019  0  0.075
*
* view factors
* lower head region
62101101  0.0  1  1.0  2  0.0  38
62102101  0.436126  1  0.563874  2  0.0  38
* core support region
62103101  0.0  2  0.0  3  1.0  4  0.0  38
62104101  0.0  2  0.535871  3  0.464129  4  0.0  38
* outlet plenum
62105101  0.0  4  0.0  5  1.0  6  0.0  38
62106101  0.0  4  0.535871  5  0.464129  6  0.0  38
* bottom reflector, bottom
62107101  0.0  6  0.0  7  1.0  8  0.0  38
62108101  0.0  6  0.535871  7  0.464129  8  0.0  38

```

```

* bottom reflector, top
62109101 0.0 8 0.0 9 1.0 10 0.0 38
62110101 0.0 8 0.535871 9 0.464129 10 0.0 38
* core level 10
62111101 0.0 10 0.0 11 1.0 12 0.0 38
62112101 0.0 10 0.535871 11 0.464129 12 0.0 38
* core level 9
62113101 0.0 12 0.0 13 1.0 14 0.0 38
62114101 0.0 12 0.535871 13 0.464129 14 0.0 38
* core level 8
62115101 0.0 14 0.0 15 1.0 16 0.0 38
62116101 0.0 14 0.535871 15 0.464129 16 0.0 38
* core level 7
62117101 0.0 16 0.0 17 1.0 18 0.0 38
62118101 0.0 16 0.535871 17 0.464129 18 0.0 38
* core level 6
62119101 0.0 18 0.0 19 1.0 20 0.0 38
62120101 0.0 18 0.535871 19 0.464129 20 0.0 38
* core level 5
62121101 0.0 20 0.0 21 1.0 22 0.0 38
62122101 0.0 20 0.535871 21 0.464129 22 0.0 38
* core level 4
62123101 0.0 22 0.0 23 1.0 24 0.0 38
62124101 0.0 22 0.535871 23 0.464129 24 0.0 38
* core level 3
62125101 0.0 24 0.0 25 1.0 26 0.0 38
62126101 0.0 24 0.535871 25 0.464129 26 0.0 38
* core level 2
62127101 0.0 26 0.0 27 1.0 28 0.0 38
62128101 0.0 26 0.535871 27 0.464129 28 0.0 38
* core level 1
62129101 0.0 28 0.0 29 1.0 30 0.0 38
62130101 0.0 28 0.535871 29 0.464129 30 0.0 38
* upper reflector, bottom
62131101 0.0 30 0.0 31 1.0 32 0.0 38
62132101 0.0 30 0.535871 31 0.464129 32 0.0 38
* upper reflector, top
62133101 0.0 32 0.0 33 1.0 34 0.0 38
62134101 0.0 32 0.535871 33 0.464129 34 0.0 38
* upper plenum cylinder
62135101 0.0 34 0.0 35 1.0 36 0.0 38
62136101 0.0 34 0.535871 35 0.464129 36 0.0 38
* upper head
62137101 0.0 36 0.0 37 1.0 38
62138101 0.0 36 0.595579 37 0.404421 38
*
*****
* material properties
*****
*
* Greencast-94F plus ceramic
*
20100100 tbl/fctn 1 1
*20100101 250.0 5.25
*20100102 478.0 5.25
*20100103 698.0 3.58
*20100104 923.0 2.83
*20100105 1143.0 2.49
*20100106 1368.0 2.47
*20100107 2000.0 2.47
* curve-fit values
20100101 250.0 7.37
20100102 300.0 7.37

```

20100103	400.0	6.06
20100104	500.0	5.01
20100105	600.0	4.18
20100106	700.0	3.56
20100107	800.0	3.10
20100108	900.0	2.78
20100109	1000.0	2.58
20100110	1100.0	2.46
20100111	1200.0	2.40
20100112	1300.0	2.37
20100113	1400.0	2.33
20100114	1500.0	2.27
20100115	1600.0	2.15
20100116	1700.0	1.95
20100117	1800.0	1.63
20100118	1900.0	1.17
20100119	2000.0	0.54
*		
20100151	250.0	2.74E+06
20100152	335.5	2.74E+06
20100153	422.1	3.21E+06
20100154	506.4	3.65E+06
20100155	589.3	3.68E+06
20100156	671.3	3.45E+06
20100157	752.4	3.45E+06
20100158	832.8	3.47E+06
20100159	912.5	3.50E+06
20100160	991.4	3.53E+06
20100161	1069.8	3.65E+06
20100162	1147.5	3.50E+06
20100163	1224.6	3.50E+06
20100164	1301.3	3.45E+06
20100165	1377.7	3.47E+06
20100166	1453.9	3.56E+06
20100167	1530.0	3.77E+06
20100168	1606.1	3.77E+06
20100169	1682.3	3.77E+06
20100170	1758.2	8.91E+06
20100171	1834.3	3.71E+06
20100172	2000.0	3.71E+06
*		
* heater rod		
*		
20100200	tbl/fctn	1 1
20100201	250.0	93.00
20100202	293.2	93.00
20100203	443.2	81.84
20100204	593.2	69.75
20100205	773.2	61.38
20100206	1003.2	51.15
20100207	1123.2	46.50
20100208	1273.2	42.78
20100209	1673.2	29.76
20100210	3000.0	29.76
*		
20100251	250.0	1.25E+06
20100252	300.0	1.25E+06
20100253	400.0	1.68E+06
20100254	500.0	2.08E+06
20100255	600.0	2.40E+06
20100256	700.0	2.65E+06
20100257	800.0	2.86E+06
20100258	900.0	3.02E+06

20100259	1000.0	3.14E+06
20100260	1100.0	3.24E+06
20100261	1200.0	3.33E+06
20100262	1300.0	3.40E+06
20100263	1400.0	3.45E+06
20100264	1500.0	3.50E+06
20100265	1600.0	3.54E+06
20100266	1700.0	3.58E+06
20100267	1800.0	3.62E+06
20100268	1900.0	3.65E+06
20100269	2000.0	3.68E+06
20100270	2100.0	3.70E+06
20100271	2200.0	3.73E+06
20100272	2300.0	3.75E+06
20100273	2400.0	3.77E+06
20100274	2500.0	3.79E+06
20100275	2600.0	3.80E+06
20100276	2700.0	3.82E+06
20100277	2800.0	3.84E+06
20100278	2900.0	3.85E+06
20100279	3000.0	3.87E+06

*

* 304 stainless steel

*

20100300	tbl/fctn	1	1
20100301	250.0	13.25	
20100302	300.0	13.25	
20100303	1671.0	39.1619	
20100304	1727.0	20.0	
20100305	3000.0	20.0	

*

20100351	250.0	3.72E+06
20100352	300.0	3.72E+06
20100353	400.0	3.94E+06
20100354	500.0	4.12E+06
20100355	600.0	4.29E+06
20100356	700.0	4.44E+06
20100357	800.0	4.57E+06
20100358	900.0	4.69E+06
20100359	1000.0	4.81E+06
20100360	1100.0	4.92E+06
20100361	1200.0	5.01E+06
20100362	1300.0	5.11E+06
20100363	1400.0	5.19E+06
20100364	1500.0	5.27E+06
20100365	1600.0	5.35E+06
20100366	1671.0	5.40E+06
20100367	3000.0	5.40E+06

*

* Haynes 230

*

20100400	tbl/fctn	1	1
20100401	250.0	8.9	
20100402	293.0	8.9	
20100403	373.0	10.4	
20100404	473.0	12.4	
20100405	573.0	14.4	
20100406	673.0	16.4	
20100407	773.0	18.4	
20100408	873.0	20.4	
20100409	973.0	22.4	
20100410	1073.0	24.4	
20100411	1173.0	26.4	

20100412	1273.0	28.4
20100413	1573.0	28.4
*		
20100451	250.0	3.59E+06
20100452	293.0	3.59E+06
20100453	373.0	3.79E+06
20100454	473.0	3.94E+06
20100455	573.0	4.05E+06
20100456	673.0	4.21E+06
20100457	773.0	4.28E+06
20100458	873.0	4.40E+06
20100459	973.0	5.19E+06
20100460	1073.0	5.38E+06
20100461	1173.0	5.51E+06
20100462	1273.0	5.58E+06
20100463	1573.0	5.58E+06
*		
* Shot-Tech SiC 80 ceramic		
*		
20100500	tbl/fctn	1 1
20100501	250.0	7.56
20100502	473.0	7.56
20100503	673.0	6.58
20100504	873.0	6.73
20100505	1073.0	6.95
20100506	1573.0	6.95
*		
20100551	250.0	1.78E+06
20100552	327.3	1.78E+06
20100553	397.9	2.11E+06
20100554	466.9	2.30E+06
20100555	534.7	2.42E+06
20100556	601.6	2.54E+06
20100557	668.0	2.61E+06
20100558	733.8	2.68E+06
20100559	799.2	2.70E+06
20100560	864.1	2.75E+06
20100561	928.4	2.77E+06
20100562	992.2	2.80E+06
20100563	1055.7	2.80E+06
20100564	1118.9	2.87E+06
20100565	1181.7	2.87E+06
20100566	1244.1	2.89E+06
20100567	1306.2	2.87E+06
20100568	1368.1	2.63E+06
20100569	1429.9	2.89E+06
20100570	1573.0	2.89E+06
*		
* Enerwrap MA 960 insulation		
*		
20100600	tbl/fctn	1 1
20100601	250.0	0.036
20100602	311.0	0.036
20100603	366.0	0.043
20100604	423.0	0.049
20100605	477.0	0.058
20100606	533.0	0.069
20100607	589.0	0.084
20100608	644.0	0.098
20100609	3000.0	0.098
*		
20100651	7.64E+04	
*		

* Structural insulation

*

20100700	tbl/fctn	1	1
20100701	250.0	0.078	
20100702	366.0	0.078	
20100703	477.0	0.088	
20100704	588.0	0.097	
20100705	700.0	0.105	
20100706	3000.0	0.105	

*

20100751	250.0	1.31E+05	
20100752	294.0	1.31E+05	
20100753	366.0	1.35E+05	
20100754	477.0	1.44E+05	
20100755	589.0	1.53E+05	
20100756	700.0	1.61E+05	
20100757	811.0	1.70E+05	
20100758	922.0	1.79E+05	
20100759	1033.0	1.87E+05	
20100760	1144.0	1.96E+05	
20100761	1255.0	2.04E+05	
20100762	1366.0	2.13E+05	
20100763	3000.0	2.13E+05	

*

* Cerablanket alumina-silica insulation

*

20100800	tbl/fctn	1	1
20100801	250.0	0.070	
20100802	473.0	0.070	
20100803	673.0	0.120	
20100804	873.0	0.200	
20100805	1073.0	0.300	
20100806	1273.0	0.430	
20100807	3000.0	0.430	

*

20100851	7.23E+04		
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*

* Lewco Needled 10# E Glass Blanket insulation

*

20100900	tbl/fctn	1	1
20100901	250.0	0.050	
20100902	422.0	0.050	
20100903	533.2	0.069	
20100904	644.3	0.092	
20100905	755.4	0.112	
20100906	2000.0	0.112	

*

20100951	1.07E+05		
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*

* general tables

*

* volumetric heat capacities

*

* Greencast-94F plus ceramic

20200100	reac-t		
20200101	250.0	2744800.0	
20200102	335.5	2744800.0	
20200103	422.1	3212000.0	
20200104	506.4	3650000.0	
20200105	589.3	3679200.0	
20200106	671.3	3445600.0	

20200107	752.4	3445600.0
20200108	832.8	3474800.0
20200109	912.5	3504000.0
20200110	991.4	3533200.0
20200111	1069.8	3650000.0
20200112	1147.5	3504000.0
20200113	1224.6	3504000.0
20200114	1301.3	3445600.0
20200115	1377.7	3474800.0
20200116	1453.9	3562400.0
20200117	1530.0	3766800.0
20200118	1606.1	3766800.0
20200119	1682.3	3766800.0
20200120	1758.2	8906000.0
20200121	1834.3	3708400.0
20200122	2000.0	3708400.0

*

* heater rod

20200200	reac-t	
20200201	300.0	1247750.0
20200202	400.0	1681750.0
20200203	500.0	2077250.0
20200204	600.0	2397500.0
20200205	700.0	2653000.0
20200206	800.0	2856000.0
20200207	900.0	3015250.0
20200208	1000.0	3143000.0
20200209	1100.0	3244500.0
20200210	1200.0	3326750.0
20200211	1300.0	3395000.0
20200212	1400.0	3451000.0
20200213	1500.0	3500000.0
20200214	1600.0	3542000.0
20200215	1700.0	3580500.0
20200216	1800.0	3615500.0
20200217	1900.0	3645250.0
20200218	2000.0	3675000.0
20200219	2100.0	3701250.0
20200220	2200.0	3725750.0
20200221	2300.0	3748500.0
20200222	2400.0	3769500.0
20200223	2500.0	3788750.0
20200224	2600.0	3804500.0
20200225	2700.0	3822000.0
20200226	2800.0	3837750.0
20200227	2900.0	3853500.0
20200228	3000.0	3872750.0

*

* 304 stainless steel

20200300	reac-t	
20200301	250.0	3724428.5
20200302	300.0	3724428.5
20200303	400.0	3937320.4
20200304	500.0	4122643.2
20200305	600.0	4287368.5
20200306	700.0	4435836.2
20200307	800.0	4570983.8
20200308	900.0	4694918.8
20200309	1000.0	4809219.3
20200310	1100.0	4915106.5
20200311	1200.0	5013550.6
20200312	1300.0	5105338.8
20200313	1400.0	5191121.1

20200314	1500.0	5271442.7
20200315	1600.0	5346766.2
20200316	1671.0	5397444.0
20200317	3000.0	5397444.0

*

* Haynes 230

20200400	reac-t	
20200401	250.0	3592850.0
20200402	293.0	3592850.0
20200403	373.0	3791950.0
20200404	473.0	3936750.0
20200405	573.0	4054400.0
20200406	673.0	4208250.0
20200407	773.0	4280650.0
20200408	873.0	4398300.0
20200409	973.0	5194700.0
20200410	1073.0	5384750.0
20200411	1173.0	5511450.0
20200412	1273.0	5583850.0
20200413	1573.0	5583850.0

*

* Shot-Tech SiC 80 ceramic

20200500	reac-t	
20200501	250.0	1777500.0
20200502	327.3	1777500.0
20200503	397.9	2109300.0
20200504	466.9	2298900.0
20200505	534.7	2417400.0
20200506	601.6	2535900.0
20200507	668.0	2607000.0
20200508	733.8	2678100.0
20200509	799.2	2701800.0
20200510	864.1	2749200.0
20200511	928.4	2772900.0
20200512	992.2	2796600.0
20200513	1055.7	2796600.0
20200514	1118.9	2867700.0
20200515	1181.7	2867700.0
20200516	1244.1	2891400.0
20200517	1306.2	2867700.0
20200518	1368.1	2630700.0
20200519	1429.9	2891400.0
20200520	1573.0	2891400.0

*

* Temperature-dependent conductance

*

20260100	htc-temp	
20260101	300.0	130.64
20260102	400.0	114.02
20260103	500.0	99.34
20260104	600.0	86.60
20260105	700.0	77.85
20260106	800.0	70.61
20260107	900.0	66.09
20260108	1000.0	63.68
20260109	1100.0	56.00
20260110	1200.0	53.48
20260111	1300.0	51.30
20260112	1400.0	50.03
20260113	1500.0	52.82
20260114	1600.0	52.54
20260115	1700.0	39.06
20260116	1800.0	36.33

```
20260117 1900.0 32.35
20260118 2000.0 26.83
*
* power in heater 101
*
20290100 power 100 1.0 1.0
20290101 -1.0 220000.0
20290102 0.0 56700.0
20290103 30.0 56700.0
20290104 30.0 38200.0
20290105 75.0 38200.0
20290106 75.0 31900.0
20290107 200.0 31900.0
20290108 200.0 27881.8
20290109 300.0 27881.8
20290110 300.0 25956.5
20290111 400.0 25956.5
20290112 400.0 24504.4
20290113 500.0 24504.4
20290114 500.0 22703.2
20290115 750.0 22703.2
20290116 750.0 20708.8
20290117 1000.0 20708.8
20290118 1000.0 18039.7
20290119 2000.0 18039.7
20290120 2000.0 15304.5
20290121 3000.0 15304.5
20290122 3000.0 13863.9
20290123 4000.0 13863.9
20290124 4000.0 12932.5
20290125 5000.0 12932.5
20290126 5000.0 11921.7
20290127 7500.0 11921.7
20290128 7500.0 10906.8
20290129 10000.0 10906.8
20290130 10000.0 9696.9
20290131 20000.0 9696.9
20290132 20000.0 8453.4
20290133 30000.0 8453.4
20290134 30000.0 7754.1
20290135 40000.0 7754.1
20290136 40000.0 7274.1
20290137 50000.0 7274.1
20290138 50000.0 6721.0
20290139 75000.0 6721.0
20290140 75000.0 6135.8
20290141 100000.0 6135.8
20290142 100000.0 5362.9
20290143 200000.0 5362.9
20290144 200000.0 4534.1
20290145 300000.0 4534.1
20290146 300000.0 4053.0
20290147 400000.0 4053.0
20290148 400000.0 3727.4
20290149 500000.0 3727.4
20290150 500000.0 3369.0
20290151 750000.0 3369.0
20290152 750000.0 3002.8
20290153 1000000.0 3002.8
20290154 1000000.0 2552.4
20290155 2000000.0 2552.4
*
* power in heater 102
```

*
20290200 power 100 1.0 1.0
20290201 -1.0 220000.0
20290202 0.0 56700.0
20290203 30.0 56700.0
20290204 30.0 38200.0
20290205 75.0 38200.0
20290206 75.0 31900.0
20290207 200.0 31900.0
20290208 200.0 27881.8
20290209 300.0 27881.8
20290210 300.0 25956.5
20290211 400.0 25956.5
20290212 400.0 24504.4
20290213 500.0 24504.4
20290214 500.0 22703.2
20290215 750.0 22703.2
20290216 750.0 20708.8
20290217 1000.0 20708.8
20290218 1000.0 18039.7
20290219 2000.0 18039.7
20290220 2000.0 15304.5
20290221 3000.0 15304.5
20290222 3000.0 13863.9
20290223 4000.0 13863.9
20290224 4000.0 12932.5
20290225 5000.0 12932.5
20290226 5000.0 11921.7
20290227 7500.0 11921.7
20290228 7500.0 10906.8
20290229 10000.0 10906.8
20290230 10000.0 9696.9
20290231 20000.0 9696.9
20290232 20000.0 8453.4
20290233 30000.0 8453.4
20290234 30000.0 7754.1
20290235 40000.0 7754.1
20290236 40000.0 7274.1
20290237 50000.0 7274.1
20290238 50000.0 6721.0
20290239 75000.0 6721.0
20290240 75000.0 6135.8
20290241 100000.0 6135.8
20290242 100000.0 5362.9
20290243 200000.0 5362.9
20290244 200000.0 4534.1
20290245 300000.0 4534.1
20290246 300000.0 4053.0
20290247 400000.0 4053.0
20290248 400000.0 3727.4
20290249 500000.0 3727.4
20290250 500000.0 3369.0
20290251 750000.0 3369.0
20290252 750000.0 3002.8
20290253 1000000.0 3002.8
20290254 1000000.0 2552.4
20290255 2000000.0 2552.4

*
* power in heater 103
*
20290300 power 100 1.0 1.0
20290301 -1.0 220000.0
20290302 0.0 56700.0

20290303	30.0	56700.0
20290304	30.0	38200.0
20290305	75.0	38200.0
20290306	75.0	31900.0
20290307	200.0	31900.0
20290308	200.0	27881.8
20290309	300.0	27881.8
20290310	300.0	25956.5
20290311	400.0	25956.5
20290312	400.0	24504.4
20290313	500.0	24504.4
20290314	500.0	22703.2
20290315	750.0	22703.2
20290316	750.0	20708.8
20290317	1000.0	20708.8
20290318	1000.0	18039.7
20290319	2000.0	18039.7
20290320	2000.0	15304.5
20290321	3000.0	15304.5
20290322	3000.0	13863.9
20290323	4000.0	13863.9
20290324	4000.0	12932.5
20290325	5000.0	12932.5
20290326	5000.0	11921.7
20290327	7500.0	11921.7
20290328	7500.0	10906.8
20290329	10000.0	10906.8
20290330	10000.0	9696.9
20290331	20000.0	9696.9
20290332	20000.0	8453.4
20290333	30000.0	8453.4
20290334	30000.0	7754.1
20290335	40000.0	7754.1
20290336	40000.0	7274.1
20290337	50000.0	7274.1
20290338	50000.0	6721.0
20290339	75000.0	6721.0
20290340	75000.0	6135.8
20290341	100000.0	6135.8
20290342	100000.0	5362.9
20290343	200000.0	5362.9
20290344	200000.0	4534.1
20290345	300000.0	4534.1
20290346	300000.0	4053.0
20290347	400000.0	4053.0
20290348	400000.0	3727.4
20290349	500000.0	3727.4
20290350	500000.0	3369.0
20290351	750000.0	3369.0
20290352	750000.0	3002.8
20290353	1000000.0	3002.8
20290354	1000000.0	2552.4
20290355	2000000.0	2552.4
*		
* power in heater 104		
*		
20290400	power	100 1.0 1.0
20290401	-1.0	220000.0
20290402	0.0	56700.0
20290403	30.0	56700.0
20290404	30.0	38200.0
20290405	75.0	38200.0
20290406	75.0	31900.0

20290407	200.0	31900.0
20290408	200.0	27881.8
20290409	300.0	27881.8
20290410	300.0	25956.5
20290411	400.0	25956.5
20290412	400.0	24504.4
20290413	500.0	24504.4
20290414	500.0	22703.2
20290415	750.0	22703.2
20290416	750.0	20708.8
20290417	1000.0	20708.8
20290418	1000.0	18039.7
20290419	2000.0	18039.7
20290420	2000.0	15304.5
20290421	3000.0	15304.5
20290422	3000.0	13863.9
20290423	4000.0	13863.9
20290424	4000.0	12932.5
20290425	5000.0	12932.5
20290426	5000.0	11921.7
20290427	7500.0	11921.7
20290428	7500.0	10906.8
20290429	10000.0	10906.8
20290430	10000.0	9696.9
20290431	20000.0	9696.9
20290432	20000.0	8453.4
20290433	30000.0	8453.4
20290434	30000.0	7754.1
20290435	40000.0	7754.1
20290436	40000.0	7274.1
20290437	50000.0	7274.1
20290438	50000.0	6721.0
20290439	75000.0	6721.0
20290440	75000.0	6135.8
20290441	100000.0	6135.8
20290442	100000.0	5362.9
20290443	200000.0	5362.9
20290444	200000.0	4534.1
20290445	300000.0	4534.1
20290446	300000.0	4053.0
20290447	400000.0	4053.0
20290448	400000.0	3727.4
20290449	500000.0	3727.4
20290450	500000.0	3369.0
20290451	750000.0	3369.0
20290452	750000.0	3002.8
20290453	1000000.0	3002.8
20290454	1000000.0	2552.4
20290455	2000000.0	2552.4
*		
* power in heater 105		
*		
20290500	power	100 1.0 1.0
20290501	-1.0	220000.0
20290502	0.0	56700.0
20290503	30.0	56700.0
20290504	30.0	38200.0
20290505	75.0	38200.0
20290506	75.0	31900.0
20290507	200.0	31900.0
20290508	200.0	27881.8
20290509	300.0	27881.8
20290510	300.0	25956.5

20290511	400.0	25956.5
20290512	400.0	24504.4
20290513	500.0	24504.4
20290514	500.0	22703.2
20290515	750.0	22703.2
20290516	750.0	20708.8
20290517	1000.0	20708.8
20290518	1000.0	18039.7
20290519	2000.0	18039.7
20290520	2000.0	15304.5
20290521	3000.0	15304.5
20290522	3000.0	13863.9
20290523	4000.0	13863.9
20290524	4000.0	12932.5
20290525	5000.0	12932.5
20290526	5000.0	11921.7
20290527	7500.0	11921.7
20290528	7500.0	10906.8
20290529	10000.0	10906.8
20290530	10000.0	9696.9
20290531	20000.0	9696.9
20290532	20000.0	8453.4
20290533	30000.0	8453.4
20290534	30000.0	7754.1
20290535	40000.0	7754.1
20290536	40000.0	7274.1
20290537	50000.0	7274.1
20290538	50000.0	6721.0
20290539	75000.0	6721.0
20290540	75000.0	6135.8
20290541	100000.0	6135.8
20290542	100000.0	5362.9
20290543	200000.0	5362.9
20290544	200000.0	4534.1
20290545	300000.0	4534.1
20290546	300000.0	4053.0
20290547	400000.0	4053.0
20290548	400000.0	3727.4
20290549	500000.0	3727.4
20290550	500000.0	3369.0
20290551	750000.0	3369.0
20290552	750000.0	3002.8
20290553	1000000.0	3002.8
20290554	1000000.0	2552.4
20290555	2000000.0	2552.4
*		
* power in heater 106		
*		
20290600	power	100 1.0 1.0
20290601	-1.0	220000.0
20290602	0.0	56700.0
20290603	30.0	56700.0
20290604	30.0	38200.0
20290605	75.0	38200.0
20290606	75.0	31900.0
20290607	200.0	31900.0
20290608	200.0	27881.8
20290609	300.0	27881.8
20290610	300.0	25956.5
20290611	400.0	25956.5
20290612	400.0	24504.4
20290613	500.0	24504.4
20290614	500.0	22703.2

20290615	750.0	22703.2
20290616	750.0	20708.8
20290617	1000.0	20708.8
20290618	1000.0	18039.7
20290619	2000.0	18039.7
20290620	2000.0	15304.5
20290621	3000.0	15304.5
20290622	3000.0	13863.9
20290623	4000.0	13863.9
20290624	4000.0	12932.5
20290625	5000.0	12932.5
20290626	5000.0	11921.7
20290627	7500.0	11921.7
20290628	7500.0	10906.8
20290629	10000.0	10906.8
20290630	10000.0	9696.9
20290631	20000.0	9696.9
20290632	20000.0	8453.4
20290633	30000.0	8453.4
20290634	30000.0	7754.1
20290635	40000.0	7754.1
20290636	40000.0	7274.1
20290637	50000.0	7274.1
20290638	50000.0	6721.0
20290639	75000.0	6721.0
20290640	75000.0	6135.8
20290641	100000.0	6135.8
20290642	100000.0	5362.9
20290643	200000.0	5362.9
20290644	200000.0	4534.1
20290645	300000.0	4534.1
20290646	300000.0	4053.0
20290647	400000.0	4053.0
20290648	400000.0	3727.4
20290649	500000.0	3727.4
20290650	500000.0	3369.0
20290651	750000.0	3369.0
20290652	750000.0	3002.8
20290653	1000000.0	3002.8
20290654	1000000.0	2552.4
20290655	2000000.0	2552.4
*		
* power in heater 107		
*		
20290700	power 100	1.0 1.0
20290701	-1.0	220000.0
20290702	0.0	56700.0
20290703	30.0	56700.0
20290704	30.0	38200.0
20290705	75.0	38200.0
20290706	75.0	31900.0
20290707	200.0	31900.0
20290708	200.0	27881.8
20290709	300.0	27881.8
20290710	300.0	25956.5
20290711	400.0	25956.5
20290712	400.0	24504.4
20290713	500.0	24504.4
20290714	500.0	22703.2
20290715	750.0	22703.2
20290716	750.0	20708.8
20290717	1000.0	20708.8
20290718	1000.0	18039.7

20290719	2000.0	18039.7
20290720	2000.0	15304.5
20290721	3000.0	15304.5
20290722	3000.0	13863.9
20290723	4000.0	13863.9
20290724	4000.0	12932.5
20290725	5000.0	12932.5
20290726	5000.0	11921.7
20290727	7500.0	11921.7
20290728	7500.0	10906.8
20290729	10000.0	10906.8
20290730	10000.0	9696.9
20290731	20000.0	9696.9
20290732	20000.0	8453.4
20290733	30000.0	8453.4
20290734	30000.0	7754.1
20290735	40000.0	7754.1
20290736	40000.0	7274.1
20290737	50000.0	7274.1
20290738	50000.0	6721.0
20290739	75000.0	6721.0
20290740	75000.0	6135.8
20290741	100000.0	6135.8
20290742	100000.0	5362.9
20290743	200000.0	5362.9
20290744	200000.0	4534.1
20290745	300000.0	4534.1
20290746	300000.0	4053.0
20290747	400000.0	4053.0
20290748	400000.0	3727.4
20290749	500000.0	3727.4
20290750	500000.0	3369.0
20290751	750000.0	3369.0
20290752	750000.0	3002.8
20290753	1000000.0	3002.8
20290754	1000000.0	2552.4
20290755	2000000.0	2552.4
*		
* power in heater 108		
*		
20290800	power	100 1.0 1.0
20290801	-1.0	220000.0
20290802	0.0	56700.0
20290803	30.0	56700.0
20290804	30.0	38200.0
20290805	75.0	38200.0
20290806	75.0	31900.0
20290807	200.0	31900.0
20290808	200.0	27881.8
20290809	300.0	27881.8
20290810	300.0	25956.5
20290811	400.0	25956.5
20290812	400.0	24504.4
20290813	500.0	24504.4
20290814	500.0	22703.2
20290815	750.0	22703.2
20290816	750.0	20708.8
20290817	1000.0	20708.8
20290818	1000.0	18039.7
20290819	2000.0	18039.7
20290820	2000.0	15304.5
20290821	3000.0	15304.5
20290822	3000.0	13863.9

20290823	4000.0	13863.9
20290824	4000.0	12932.5
20290825	5000.0	12932.5
20290826	5000.0	11921.7
20290827	7500.0	11921.7
20290828	7500.0	10906.8
20290829	10000.0	10906.8
20290830	10000.0	9696.9
20290831	20000.0	9696.9
20290832	20000.0	8453.4
20290833	30000.0	8453.4
20290834	30000.0	7754.1
20290835	40000.0	7754.1
20290836	40000.0	7274.1
20290837	50000.0	7274.1
20290838	50000.0	6721.0
20290839	75000.0	6721.0
20290840	75000.0	6135.8
20290841	100000.0	6135.8
20290842	100000.0	5362.9
20290843	200000.0	5362.9
20290844	200000.0	4534.1
20290845	300000.0	4534.1
20290846	300000.0	4053.0
20290847	400000.0	4053.0
20290848	400000.0	3727.4
20290849	500000.0	3727.4
20290850	500000.0	3369.0
20290851	750000.0	3369.0
20290852	750000.0	3002.8
20290853	1000000.0	3002.8
20290854	1000000.0	2552.4
20290855	2000000.0	2552.4

*

* power in heater 109

*

20290900	power	100	1.0	1.0
20290901	-1.0	220000.0		
20290902	0.0	56700.0		
20290903	30.0	56700.0		
20290904	30.0	38200.0		
20290905	75.0	38200.0		
20290906	75.0	31900.0		
20290907	200.0	31900.0		
20290908	200.0	27881.8		
20290909	300.0	27881.8		
20290910	300.0	25956.5		
20290911	400.0	25956.5		
20290912	400.0	24504.4		
20290913	500.0	24504.4		
20290914	500.0	22703.2		
20290915	750.0	22703.2		
20290916	750.0	20708.8		
20290917	1000.0	20708.8		
20290918	1000.0	18039.7		
20290919	2000.0	18039.7		
20290920	2000.0	15304.5		
20290921	3000.0	15304.5		
20290922	3000.0	13863.9		
20290923	4000.0	13863.9		
20290924	4000.0	12932.5		
20290925	5000.0	12932.5		
20290926	5000.0	11921.7		

20290927	7500.0	11921.7
20290928	7500.0	10906.8
20290929	10000.0	10906.8
20290930	10000.0	9696.9
20290931	20000.0	9696.9
20290932	20000.0	8453.4
20290933	30000.0	8453.4
20290934	30000.0	7754.1
20290935	40000.0	7754.1
20290936	40000.0	7274.1
20290937	50000.0	7274.1
20290938	50000.0	6721.0
20290939	75000.0	6721.0
20290940	75000.0	6135.8
20290941	100000.0	6135.8
20290942	100000.0	5362.9
20290943	200000.0	5362.9
20290944	200000.0	4534.1
20290945	300000.0	4534.1
20290946	300000.0	4053.0
20290947	400000.0	4053.0
20290948	400000.0	3727.4
20290949	500000.0	3727.4
20290950	500000.0	3369.0
20290951	750000.0	3369.0
20290952	750000.0	3002.8
20290953	1000000.0	3002.8
20290954	1000000.0	2552.4
20290955	2000000.0	2552.4

*
 * power in heater 110
 *

20291000	power	100	1.0	1.0
20291001	-1.0	220000.0		
20291002	0.0	56700.0		
20291003	30.0	56700.0		
20291004	30.0	38200.0		
20291005	75.0	38200.0		
20291006	75.0	31900.0		
20291007	200.0	31900.0		
20291008	200.0	27881.8		
20291009	300.0	27881.8		
20291010	300.0	25956.5		
20291011	400.0	25956.5		
20291012	400.0	24504.4		
20291013	500.0	24504.4		
20291014	500.0	22703.2		
20291015	750.0	22703.2		
20291016	750.0	20708.8		
20291017	1000.0	20708.8		
20291018	1000.0	18039.7		
20291019	2000.0	18039.7		
20291020	2000.0	15304.5		
20291021	3000.0	15304.5		
20291022	3000.0	13863.9		
20291023	4000.0	13863.9		
20291024	4000.0	12932.5		
20291025	5000.0	12932.5		
20291026	5000.0	11921.7		
20291027	7500.0	11921.7		
20291028	7500.0	10906.8		
20291029	10000.0	10906.8		
20291030	10000.0	9696.9		

```

20291031 20000.0 9696.9
20291032 20000.0 8453.4
20291033 30000.0 8453.4
20291034 30000.0 7754.1
20291035 40000.0 7754.1
20291036 40000.0 7274.1
20291037 50000.0 7274.1
20291038 50000.0 6721.0
20291039 75000.0 6721.0
20291040 75000.0 6135.8
20291041 100000.0 6135.8
20291042 100000.0 5362.9
20291043 200000.0 5362.9
20291044 200000.0 4534.1
20291045 300000.0 4534.1
20291046 300000.0 4053.0
20291047 400000.0 4053.0
20291048 400000.0 3727.4
20291049 500000.0 3727.4
20291050 500000.0 3369.0
20291051 750000.0 3369.0
20291052 750000.0 3002.8
20291053 1000000.0 3002.8
20291054 1000000.0 2552.4
20291055 2000000.0 2552.4
*
* building temperature boundary for RCCS and insulated structures
*
20295000 temp
20295001 0.0 300.0
*
* natural convection heat transfer coefficient for outside of RCCS rear panels and
insulated structures
*
20295100 htc-t
20295101 0.0 15.0
*
*****
* control variables
*****
*
20500000 9999
*
*****
* steady state control variables
*
* inlet flow controller
*
20502360 temperr sum 1.0 0.0 0
20502361 -960.15 1.0 tempg 175010000
*
20502370 inflow integral 0.001 1.0 0
20502371 cntrlvar 236
*
* outlet pressure controller
*
20502330 presserr sum 1.0 0.0 0
20502331 700000.0 -1.0 p 100010000
*
20502340 inpress integral 0.5 7.00E+05 0
20502341 cntrlvar 233
*
* feedwater flow control

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*
20503190 SGtmperr sum 1.0 0.0 0
20503191 -531.75 1.0 tempg 270040000 * temperature setpoint
*
20503200 SGFWflow prop-int 1.00000 0.8 0
20503201 0.007 0.000007 cntrlvar 319
*
20503210 Fwfloint integral 1.0 0.0 0
20503211 mflowj 320000000
*
* steam pressure control
*
20503690 SG-P-err sum 1.0 0.0 0
20503691 -515000.0 1.0 p 355010000 * steam pressure
*
20503700 V370pos integral 1.00E-09 1.0 0 3 0.0 1.0
20503701 cntrlvar 369
*
*****
* energy balance control variables
*
* core
*
20500010 corelpow sum 1.0 0.0 1
20500011 0.0 1.0 q 140010000 1.0 q 140020000
20500012 1.0 q 140030000 1.0 q 140040000
20500013 1.0 q 140050000 1.0 q 140060000
20500014 1.0 q 140070000 1.0 q 140080000
20500015 1.0 q 140090000 1.0 q 140100000
20500016 1.0 q 140110000 1.0 q 140120000
20500017 1.0 q 140130000 1.0 q 140140000
*
20500020 core2pow sum 1.0 0.0 1
20500021 0.0 1.0 q 145010000 1.0 q 145020000
20500022 1.0 q 145030000 1.0 q 145040000
20500023 1.0 q 145050000 1.0 q 145060000
20500024 1.0 q 145070000 1.0 q 145080000
20500025 1.0 q 145090000 1.0 q 145100000
20500026 1.0 q 145110000 1.0 q 145120000
20500027 1.0 q 145130000 1.0 q 145140000
*
20500030 core3pow sum 1.0 0.0 1
20500031 0.0 1.0 q 150010000 1.0 q 150020000
20500032 1.0 q 150030000 1.0 q 150040000
20500033 1.0 q 150050000 1.0 q 150060000
20500034 1.0 q 150070000 1.0 q 150080000
20500035 1.0 q 150090000 1.0 q 150100000
20500036 1.0 q 150110000 1.0 q 150120000
20500037 1.0 q 150130000 1.0 q 150140000
*
20500040 bypirpow sum 1.0 0.0 1
20500041 0.0 1.0 q 132010000 1.0 q 132020000
20500042 1.0 q 132030000 1.0 q 132040000
20500043 1.0 q 132050000 1.0 q 132060000
20500044 1.0 q 132070000 1.0 q 132080000
20500045 1.0 q 132090000 1.0 q 132100000
20500046 1.0 q 132110000 1.0 q 132120000
20500047 1.0 q 132130000 1.0 q 132140000
*
20500050 byporpow sum 1.0 0.0 1
20500051 0.0 1.0 q 162010000 1.0 q 162020000
20500052 1.0 q 162030000 1.0 q 162040000
20500053 1.0 q 162050000 1.0 q 162060000

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20500054 1.0 q 162070000 1.0 q 162080000
20500055 1.0 q 162090000 1.0 q 162100000
20500056 1.0 q 162110000 1.0 q 162120000
20500057 1.0 q 162130000 1.0 q 162140000
*
20500060 bypsppow sum 1.0 0.0 1
20500061 0.0 1.0 q 164010000 1.0 q 164020000
20500062 1.0 q 164030000 1.0 q 164040000
20500063 1.0 q 164050000 1.0 q 164060000
20500064 1.0 q 164070000 1.0 q 164080000
20500065 1.0 q 164090000 1.0 q 164100000
20500066 1.0 q 164110000 1.0 q 164120000
20500067 1.0 q 164130000 1.0 q 164140000
*
20500070 byppbpow sum 1.0 0.0 1
20500071 0.0 1.0 q 166010000 1.0 q 166020000
20500072 1.0 q 166030000 1.0 q 166040000
20500073 1.0 q 166050000 1.0 q 166060000
20500074 1.0 q 166070000 1.0 q 166080000
20500075 1.0 q 166090000 1.0 q 166100000
20500076 1.0 q 166110000 1.0 q 166120000
20500077 1.0 q 166130000 1.0 q 166140000
*
20500080 hr140gap sum 1.0 0.0 1
20500081 0.0 1.0 q 141010000 1.0 q 141020000
20500082 1.0 q 141030000 1.0 q 141040000
20500083 1.0 q 141050000 1.0 q 141060000
20500084 1.0 q 141070000 1.0 q 141080000
20500085 1.0 q 141090000 1.0 q 141100000
*
20500090 hr145gap sum 1.0 0.0 1
20500091 0.0 1.0 q 146010000 1.0 q 146020000
20500092 1.0 q 146030000 1.0 q 146040000
20500093 1.0 q 146050000 1.0 q 146060000
20500094 1.0 q 146070000 1.0 q 146080000
20500095 1.0 q 146090000 1.0 q 146100000
*
20500100 hr150gap sum 1.0 0.0 1
20500101 0.0 1.0 q 151010000 1.0 q 151020000
20500102 1.0 q 151030000 1.0 q 151040000
20500103 1.0 q 151050000 1.0 q 151060000
20500104 1.0 q 151070000 1.0 q 151080000
20500105 1.0 q 151090000 1.0 q 151100000
*
20500110 corepow sum 1.0 0.0 1
20500111 0.0 1.0 cntrlvar 1 1.0 cntrlvar 2
20500112 1.0 cntrlvar 3 1.0 cntrlvar 4
20500113 1.0 cntrlvar 5 1.0 cntrlvar 6
20500114 1.0 cntrlvar 7 1.0 cntrlvar 8
20500115 1.0 cntrlvar 9 1.0 cntrlvar 10
*
20500120 corenerg integral 1.0 0.0 0
20500121 cntrlvar 11
*
* core power from flow enthalpy
*
20500130 corflowh sum 1.0 0.0 1
20500131 0.0 1.0 flenth 175010000 -1.0 flenth 100010000
*
20500140 corflowE integral 1.0 0.0 0
20500141 cntrlvar 13
*
* coolant riser heat input

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*
20500160  chl15q  sum  1.0  0.0  1
20500161  0.0  1.0  q  115010000  1.0  q  115020000
20500162  1.0  q  115030000  1.0  q  115040000
20500163  1.0  q  115050000  1.0  q  115060000
20500164  1.0  q  115070000  1.0  q  115080000
20500165  1.0  q  115090000  1.0  q  115100000
20500166  1.0  q  115110000  1.0  q  115120000
20500167  1.0  q  115130000  1.0  q  115140000
20500168  1.0  q  115150000
*
* core flow distribution
*
20500200  corflowo  sum  1.0  0.001  1  1  0.001
20500201  0.0  1.0  mflowj  175010000
*
20500210  bypasscr  div  1.0  0.0  1
20500211  cntrlvar  20  mflowj  170010100
*
20500220  corel40r  div  1.0  0.0  1
20500221  cntrlvar  20  mflowj  170010200
*
20500230  corel45r  div  1.0  0.0  1
20500231  cntrlvar  20  mflowj  170010300
*
20500240  corel50r  div  1.0  0.0  1
20500241  cntrlvar  20  mflowj  170010400
*
20500250  bypasssr  div  1.0  0.0  1
20500251  cntrlvar  20  mflowj  170010500
*
20500260  bypasssp  div  1.0  0.0  1
20500261  cntrlvar  20  mflowj  170010600
*
20500270  bypasspb  div  1.0  0.0  1
20500271  cntrlvar  20  mflowj  168000000
*
20500280  byprefl  sum  1.0  0.0  1
20500281  0.0  1.0  cntrlvar  21  1.0  cntrlvar  25
20500282  1.0  cntrlvar  26
*
20500290  bypastot  sum  1.0  0.0  1
20500291  0.0  1.0  cntrlvar  27  1.0  cntrlvar  28
*
* steam generator heat transfer
*
20500310  SGtubeq  sum  -1.0  0.0  1
20500311  0.0  1.0  q  225010000  1.0  q  225020000
20500312  1.0  q  225030000  1.0  q  225040000
20500313  1.0  q  225050000  1.0  q  225060000
20500314  1.0  q  225070000  1.0  q  225080000
20500315  1.0  q  225090000  1.0  q  225100000
20500316  1.0  q  225110000  1.0  q  225120000
20500317  1.0  q  225130000  1.0  q  225140000
20500318  1.0  q  225150000  1.0  q  225160000
+ 1.0  q  225170000  1.0  q  225180000
+ 1.0  q  225190000  1.0  q  225200000
+ 1.0  q  225210000  1.0  q  225220000
*
20500320  Sgtubeht  sum  1.0  0.0  1
20500321  0.0  1.585  htrnr  225000101  1.585  htrnr  225000201
20500322  1.599  htrnr  225000301  1.599  htrnr  225000401
20500323  1.599  htrnr  225000501  1.599  htrnr  225000601

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20500324 1.599 htrnr 225000701 1.599 htrnr 225000801
20500325 1.599 htrnr 225000901 1.599 htrnr 225001001
20500326 2.044 htrnr 225001101 2.044 htrnr 225001201
20500327 1.599 htrnr 225001301 1.599 htrnr 225001401
20500328 1.599 htrnr 225001501 1.599 htrnr 225001601
+ 1.599 htrnr 225001701 1.599 htrnr 225001801
+ 1.599 htrnr 225001901 1.599 htrnr 225002001
+ 1.585 htrnr 225002101 1.585 htrnr 225002201
*
20500330 Sgboilrq sum 1.0 0.0 1
20500331 0.0 1.0 q 350010000 1.0 q 350020000
20500332 1.0 q 350030000 1.0 q 350040000
20500333 1.0 q 350050000 1.0 q 350060000
20500334 1.0 q 350070000 1.0 q 350080000
20500335 1.0 q 350090000 1.0 q 350100000
20500336 1.0 q 350110000
*
* steam generator flow enthalpy
*
20500350 SGflowh sum 1.0 0.0 0
20500351 0.0 1.0 flenth 360020000 -1.0 flenth 330010000
*
20500360 SGflowE integral 1.0 0.0 0
20500361 cntrlvar 35
*
* circulator flow enthalpy
*
20500450 cprflowh sum 1.0 0.0 0
20500451 0.0 1.0 flenth 245000000 -1.0 flenth 235010000
*
20500460 cprflowE integral 1.0 0.0 0
20500461 cntrlvar 45
*
* RCCS coolant net heat addition
*
20500950 RCCSpnlQ sum 1.0 0.0 1
20500951 0.0 1.0 q 950010000 1.0 q 950020000
20500952 1.0 q 950030000 1.0 q 950040000
20500953 1.0 q 950050000 1.0 q 950060000
20500954 1.0 q 950070000 1.0 q 950080000
20500955 1.0 q 950090000 1.0 q 950100000
20500956 1.0 q 950110000 1.0 q 950120000
20500957 1.0 q 950130000 1.0 q 950140000
20500958 1.0 q 950150000 1.0 q 950160000
+ 1.0 q 950170000 1.0 q 950180000
+ 1.0 q 950190000
*
20500960 RCCSpnlE integral 1.0 0.0 0
20500961 cntrlvar 95
*
* RCCS flow enthalpy
*
20500980 RCCSflwh sum 1.0 0.0 0
20500981 0.0 1.0 flenth 955010000 -1.0 flenth 945020000
*
20500990 RCCSflwE integral 1.0 0.0 0
20500991 cntrlvar 98
*
20501200 crefinpt stdfnctn 1.0 0.0 1
20501201 max htvat 1300003 htvat 1300004
20501202 htvat 1300005 htvat 1300006
20501203 htvat 1300007 htvat 1300008
20501204 htvat 1300009 htvat 1300010

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20501205  htvat  1300011  htvat  1300012
*
20501210  crefmdpt  stdfnctn  1.0  0.0  1
20501211  max  htvat  1320003  htvat  1320004
20501212  htvat  1320005  htvat  1320006
20501213  htvat  1320007  htvat  1320008
20501214  htvat  1320009  htvat  1320010
20501215  htvat  1320011  htvat  1320012
*
20501220  crefoupt  stdfnctn  1.0  0.0  1
20501221  max  htvat  1340003  htvat  1340004
20501222  htvat  1340005  htvat  1340006
20501223  htvat  1340007  htvat  1340008
20501224  htvat  1340009  htvat  1340010
20501225  htvat  1340011  htvat  1340012
*
20501230  corincpt  stdfnctn  1.0  0.0  1
20501231  max  htvat  1401001  htvat  1401002
20501232  htvat  1401003  htvat  1401004
20501233  htvat  1401005  htvat  1401006
20501234  htvat  1401007  htvat  1401008
20501235  htvat  1401009  htvat  1401010
*
20501240  cormdcpt  stdfnctn  1.0  0.0  1
20501241  max  htvat  1451001  htvat  1451002
20501242  htvat  1451003  htvat  1451004
20501243  htvat  1451005  htvat  1451006
20501244  htvat  1451007  htvat  1451008
20501245  htvat  1451009  htvat  1451010
*
20501250  coroucpt  stdfnctn  1.0  0.0  1
20501251  max  htvat  1501001  htvat  1501002
20501252  htvat  1501003  htvat  1501004
20501253  htvat  1501005  htvat  1501006
20501254  htvat  1501007  htvat  1501008
20501255  htvat  1501009  htvat  1501010
*
20501260  srefinpt  stdfnctn  1.0  0.0  1
20501261  max  htvat  1600003  htvat  1600004
20501262  htvat  1600005  htvat  1600006
20501263  htvat  1600007  htvat  1600008
20501264  htvat  1600009  htvat  1600010
20501265  htvat  1600011  htvat  1600012
*
20501270  srefmdpt  stdfnctn  1.0  0.0  1
20501271  max  htvat  1620003  htvat  1620004
20501272  htvat  1620005  htvat  1620006
20501273  htvat  1620007  htvat  1620008
20501274  htvat  1620009  htvat  1620010
20501275  htvat  1620011  htvat  1620012
*
20501280  srefoupt  stdfnctn  1.0  0.0  1
20501281  max  htvat  1640003  htvat  1640004
20501282  htvat  1640005  htvat  1640006
20501283  htvat  1640007  htvat  1640008
20501284  htvat  1640009  htvat  1640010
20501285  htvat  1640011  htvat  1640012
*
20501290  oreftp  stdfnctn  1.0  0.0  1
20501291  max  htvat  1660003  htvat  1660004
20501292  htvat  1660005  htvat  1660006
20501293  htvat  1660007  htvat  1660008
20501294  htvat  1660009  htvat  1660010

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20501295  htvat  1660011  htvat  1660012
*
20501300  crinmaxt  stdfnctn  1.0  0.0  1
20501301  max  cntrlvar  120  cntrlvar  130
*
20501310  crmdmaxt  stdfnctn  1.0  0.0  1
20501311  max  cntrlvar  121  cntrlvar  131
*
20501320  croumaxt  stdfnctn  1.0  0.0  1
20501321  max  cntrlvar  122  cntrlvar  132
*
20501330  corinmxt  stdfnctn  1.0  0.0  1
20501331  max  cntrlvar  123  cntrlvar  133
*
20501340  cormdmxt  stdfnctn  1.0  0.0  1
20501341  max  cntrlvar  124  cntrlvar  134
*
20501350  coroumxt  stdfnctn  1.0  0.0  1
20501351  max  cntrlvar  125  cntrlvar  135
*
20501360  srinmaxt  stdfnctn  1.0  0.0  1
20501361  max  cntrlvar  126  cntrlvar  136
*
20501370  srmdmaxt  stdfnctn  1.0  0.0  1
20501371  max  cntrlvar  127  cntrlvar  137
*
20501380  sroumaxt  stdfnctn  1.0  0.0  1
20501381  max  cntrlvar  128  cntrlvar  138
*
20501390  orefmaxt  stdfnctn  1.0  0.0  1
20501391  max  cntrlvar  129  cntrlvar  139
*
* peak primary pressure vessel temperature
*
20501000  rvpeakt  stdfnctn  1.0  0.0  1
20501001  max  htvat  1000001  htvat  1000002
20501002  htvat  1000003  htvat  1000004
20501003  htvat  1000005  htvat  1000006
20501004  htvat  1000007  htvat  1000008
20501005  htvat  1000009  htvat  1000010
20501006  htvat  1000011  htvat  1000012
20501007  htvat  1000013  htvat  1000014
20501008  htvat  1000015  htvat  1000016
+  htvat  1000017
*
20501010  rvmaxt  stdfnctn  1.0  0.0  1
20501011  max  cntrlvar  100  cntrlvar  101
*
* peak core barrel temperature
*
20501030  cbpeakt  stdfnctn  1.0  0.0  1
20501031  max  htvat  1150001  htvat  1150002
20501032  htvat  1150003  htvat  1150004
20501033  htvat  1150005  htvat  1150006
20501034  htvat  1150007  htvat  1150008
20501035  htvat  1150009  htvat  1150010
20501036  htvat  1150011  htvat  1150012
20501037  htvat  1150013  htvat  1150014
20501038  htvat  1150015  htvat  1150016
*
20501040  cbmaxt  stdfnctn  1.0  0.0  1
20501041  max  cntrlvar  103  cntrlvar  104
*

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* peak heater rod temperatures
*
20501400 corinmxt stdfnctn 1.0 0.0 1
20501401 max htvat 1403001 htvat 1403002
20501402 htvat 1403003 htvat 1403004
20501403 htvat 1403005 htvat 1403006
20501404 htvat 1403007 htvat 1403008
20501405 htvat 1403009 htvat 1403010
*
20501450 cormimxt stdfnctn 1.0 0.0 1
20501451 max htvat 1453001 htvat 1453002
20501452 htvat 1453003 htvat 1453004
20501453 htvat 1453005 htvat 1453006
20501454 htvat 1453007 htvat 1453008
20501455 htvat 1453009 htvat 1453010
*
20501500 coroumxt stdfnctn 1.0 0.0 1
20501501 max htvat 1503001 htvat 1503002
20501502 htvat 1503003 htvat 1503004
20501503 htvat 1503005 htvat 1503006
20501504 htvat 1503007 htvat 1503008
20501505 htvat 1503009 htvat 1503010
*
20501560 coremaxt stdfnctn 1.0 0.0 1
20501561 max cntrlvar 140 cntrlvar 145 cntrlvar 150
*
20501570 corpeakt stdfnctn 1.0 0.0 1
20501571 max cntrlvar 156 cntrlvar 157
*
* structure axial average temperatures over heated length
*
20501610 rvtave sum 0.1 0.0 1
20501611 0.0 1.0 htvat 1000005 1.0 htvat 1000006
20501612 1.0 htvat 1000007 1.0 htvat 1000008
20501613 1.0 htvat 1000009 1.0 htvat 1000010
20501614 1.0 htvat 1000011 1.0 htvat 1000012
20501615 1.0 htvat 1000013 1.0 htvat 1000014
*
20501620 cbartave sum 0.1 0.0 1
20501621 0.0 1.0 htvat 1150005 1.0 htvat 1150006
20501622 1.0 htvat 1150007 1.0 htvat 1150008
20501623 1.0 htvat 1150009 1.0 htvat 1150010
20501624 1.0 htvat 1150011 1.0 htvat 1150012
20501625 1.0 htvat 1150013 1.0 htvat 1150014
*
20501660 hs1300tv sum 0.1 0.0 1
20501661 0.0 1.0 htvat 1300003 1.0 htvat 1300004
20501662 1.0 htvat 1300005 1.0 htvat 1300006
20501663 1.0 htvat 1300007 1.0 htvat 1300008
20501664 1.0 htvat 1300009 1.0 htvat 1300010
20501665 1.0 htvat 1300011 1.0 htvat 1300012
*
20501670 hs1320tv sum 0.1 0.0 1
20501671 0.0 1.0 htvat 1320003 1.0 htvat 1320004
20501672 1.0 htvat 1320005 1.0 htvat 1320006
20501673 1.0 htvat 1320007 1.0 htvat 1320008
20501674 1.0 htvat 1320009 1.0 htvat 1320010
20501675 1.0 htvat 1320011 1.0 htvat 1320012
*
20501680 hs1340tv sum 0.1 0.0 1
20501681 0.0 1.0 htvat 1340003 1.0 htvat 1340004
20501682 1.0 htvat 1340005 1.0 htvat 1340006
20501683 1.0 htvat 1340007 1.0 htvat 1340008

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20501684 1.0 htvat 1340009 1.0 htvat 1340010
20501685 1.0 htvat 1340011 1.0 htvat 1340012
*
20501690 hs1401tv sum 0.1 0.0 1
20501691 0.0 1.0 htvat 1401001 1.0 htvat 1401002
20501692 1.0 htvat 1401003 1.0 htvat 1401004
20501693 1.0 htvat 1401005 1.0 htvat 1401006
20501694 1.0 htvat 1401007 1.0 htvat 1401008
20501695 1.0 htvat 1401009 1.0 htvat 1401010
*
20501700 hs1403tv sum 0.1 0.0 1
20501701 0.0 1.0 htvat 1403001 1.0 htvat 1403002
20501702 1.0 htvat 1403003 1.0 htvat 1403004
20501703 1.0 htvat 1403005 1.0 htvat 1403006
20501704 1.0 htvat 1403007 1.0 htvat 1403008
20501705 1.0 htvat 1403009 1.0 htvat 1403010
*
20501710 hs1451tv sum 0.1 0.0 1
20501711 0.0 1.0 htvat 1451001 1.0 htvat 1451002
20501712 1.0 htvat 1451003 1.0 htvat 1451004
20501713 1.0 htvat 1451005 1.0 htvat 1451006
20501714 1.0 htvat 1451007 1.0 htvat 1451008
20501715 1.0 htvat 1451009 1.0 htvat 1451010
*
20501720 hs1453tv sum 0.1 0.0 1
20501721 0.0 1.0 htvat 1453001 1.0 htvat 1453002
20501722 1.0 htvat 1453003 1.0 htvat 1453004
20501723 1.0 htvat 1453005 1.0 htvat 1453006
20501724 1.0 htvat 1453007 1.0 htvat 1453008
20501725 1.0 htvat 1453009 1.0 htvat 1453010
*
20501730 hs1501tv sum 0.1 0.0 1
20501731 0.0 1.0 htvat 1501001 1.0 htvat 1501002
20501732 1.0 htvat 1501003 1.0 htvat 1501004
20501733 1.0 htvat 1501005 1.0 htvat 1501006
20501734 1.0 htvat 1501007 1.0 htvat 1501008
20501735 1.0 htvat 1501009 1.0 htvat 1501010
*
20501740 hs1503tv sum 0.1 0.0 1
20501741 0.0 1.0 htvat 1503001 1.0 htvat 1503002
20501742 1.0 htvat 1503003 1.0 htvat 1503004
20501743 1.0 htvat 1503005 1.0 htvat 1503006
20501744 1.0 htvat 1503007 1.0 htvat 1503008
20501745 1.0 htvat 1503009 1.0 htvat 1503010
*
20501750 hs1600tv sum 0.1 0.0 1
20501751 0.0 1.0 htvat 1600003 1.0 htvat 1600004
20501752 1.0 htvat 1600005 1.0 htvat 1600006
20501753 1.0 htvat 1600007 1.0 htvat 1600008
20501754 1.0 htvat 1600009 1.0 htvat 1600010
20501755 1.0 htvat 1600011 1.0 htvat 1600012
*
20501760 hs1620tv sum 0.1 0.0 1
20501761 0.0 1.0 htvat 1620003 1.0 htvat 1620004
20501762 1.0 htvat 1620005 1.0 htvat 1620006
20501763 1.0 htvat 1620007 1.0 htvat 1620008
20501764 1.0 htvat 1620009 1.0 htvat 1620010
20501765 1.0 htvat 1620011 1.0 htvat 1620012
*
20501770 hs1640tv sum 0.1 0.0 1
20501771 0.0 1.0 htvat 1640003 1.0 htvat 1640004
20501772 1.0 htvat 1640005 1.0 htvat 1640006
20501773 1.0 htvat 1640007 1.0 htvat 1640008

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20501774 1.0 htvat 1640009 1.0 htvat 1640010
20501775 1.0 htvat 1640011 1.0 htvat 1640012
*
20501780 hs1660tv sum 0.1 0.0 1
20501781 0.0 1.0 htvat 1660003 1.0 htvat 1660004
20501782 1.0 htvat 1660005 1.0 htvat 1660006
20501783 1.0 htvat 1660007 1.0 htvat 1660008
20501784 1.0 htvat 1660009 1.0 htvat 1660010
20501785 1.0 htvat 1660011 1.0 htvat 1660012
*
20501830 hs9500tv sum 0.189487 0.0 1
20501831 0.0 1.0221 htvat 9500001 0.3273 htvat 9500002
20501832 0.2223 htvat 9500003 0.2515 htvat 9500004
20501833 0.2515 htvat 9500005 0.1981 htvat 9500006
20501834 0.1981 htvat 9500007 0.1981 htvat 9500008
20501835 0.1981 htvat 9500009 0.1981 htvat 9500010
20501836 0.1981 htvat 9500011 0.1981 htvat 9500012
20501837 0.1981 htvat 9500013 0.1981 htvat 9500014
20501838 0.1981 htvat 9500015 0.1905 htvat 9500016
+ 0.2032 htvat 9500017 0.2732 htvat 9500018
+ 0.748455 htvat 9500019
*
20501840 hs9501tv sum 0.189487 0.0 1
20501841 0.0 1.0221 htvat 9501001 0.3273 htvat 9501002
20501842 0.2223 htvat 9501003 0.2515 htvat 9501004
20501843 0.2515 htvat 9501005 0.1981 htvat 9501006
20501844 0.1981 htvat 9501007 0.1981 htvat 9501008
20501845 0.1981 htvat 9501009 0.1981 htvat 9501010
20501846 0.1981 htvat 9501011 0.1981 htvat 9501012
20501847 0.1981 htvat 9501013 0.1981 htvat 9501014
20501848 0.1981 htvat 9501015 0.1905 htvat 9501016
+ 0.2032 htvat 9501017 0.2732 htvat 9501018
+ 0.748455 htvat 9501019
*
* differential pressures
*
20502750 coredp sum 1.0 0.0 1
20502751 0.0 1.0 p 120010000 -1.0 p 175010000
*
20502760 rvessdp sum 1.0 0.0 1
20502761 0.0 1.0 p 100010000 -1.0 p 200010000
*
* feedwater flow control (for transients with steam generator PCS isolation)
*
*20503190 SGlevert sum 1.0 0.0 0
*20503191 2.0520 -1.0 cntrlvar 350
*
*20503200 SGFWflow integral 0.01 0.0 0
*20503201 cntrlvar 319
*
* liquid level in steam generator boiler
*
20503500 SGlevel sum 1.0 0.0 1
20503501 0.0 0.1409 voidf 350010000 0.1409 voidf 350020000
20503502 0.1421 voidf 350030000 0.1421 voidf 350040000
20503503 0.1421 voidf 350050000 0.1421 voidf 350060000
20503504 0.1421 voidf 350070000 0.1421 voidf 350080000
20503505 0.1421 voidf 350090000 0.1421 voidf 350100000
20503506 0.6336 voidf 350110000 0.6336 voidf 350120000
*
* facility steam generator liquid level (% of span)
*
20503550 LDP-601 sum 44.58116 50.0 1

```



```

20503551 -0.03815 1.0 cntrlvar 350
*
* potable water supply valve controls
*
* determine flow setpoint
*
20504030 flowdmnd sum 1.0 0.0 1
20504031 0.0 1.0 mflowj 320000000
* if the alternate RCCS source volume is being used and flow is not being discharged
to the storage tank, delete the card below
20504032 1.0 mflowj 945010000 -1.0000 mflowj 955010000
* if the normal RCCS water source is being used but flow is not recirculated to the
storage tank, use the card below
*20504032 1.0 mflowj 945010000
* if the alternate RCCS source volume is being used but flow is being discharged to
the storage tank, use the card below
*20504032 -1.0 mflowj 955010000
*
20504040 lowlevel tripunit 1.0 0.0 0
20504041 1410
*
20504050 hilevel tripunit -1.0 0.0 0
20504051 1412
*
20504060 leveloor sum 1.0 0.0 0
20504061 0.0 1.0 cntrlvar 404 1.0 cntrlvar 405
*
20504070 levelctb mult 0.25 0.0 0
20504071 cntrlvar 403 cntrlvar 406
*
20504080 flosetpt sum 1.0 0.0 1
20504081 0.0 1.0 cntrlvar 403 1.0 cntrlvar 407
*
* flow demand error and valve controller
*
20504090 flowerr sum 1.0 0.0 0
20504091 0.0 1.0 cntrlvar 408 -1.0 mflowj 410000000
*
20504100 V410pos integral 0.01 0.06 0 3 1.00E-05 1.0
20504101 cntrlvar 409
*
* liquid level in tank T-010
*
20504500 level450 sum 1.0 0.0 1
20504501 0.0 0.0349 voidf 450010000 0.0826 voidf 450020000
20504502 0.0349 voidf 450030000 0.0349 voidf 450040000
20504503 0.0826 voidf 450050000 0.0349 voidf 450060000
*
* tank level setpoints
*
20504510 lev450lo constant 0.1 * low level setpoint (m)
20504520 lev450hi constant 0.24 * high level setpoint (m)
* mid-range level
20504530 lev450md sum 1.0 0.25 0
20504531 0 0.5 cntrlvar 451 0.5 cntrlvar 452
*
* facility measurements
*
20505010 "DP-1001" sum 0.001 0.0 1
20505011 0.0 1.0 p 145010000 -1.0 p 145130000
*
20505020 "DP-4001" sum 0.001 0.0 1
20505021 0.0 1.0 p 270040000 -1.0 p 200010000

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*
20505030 "DP-7001" sum 0.001 0.0 1
20505031 0.0 1.0 p 270040000 -1.0 p 120010000
*
20505040 "DP-8001" sum 0.001 0.0 1
20505041 0.0 1.0 p 270040000 -1.0 p 175010000
*
20505050 "DP-8002" sum 0.001 0.0 1
20505051 0.0 1.0 p 270040000 -1.0 p 105010000
*
20505060 "DP-9001" sum 0.001 0.0 1
20505061 0.0 1.0 p 270040000 -1.0 p 115150000
*
20505070 "DP-801" sum 0.001 0.0 1
20505071 0.0 1.0 p 945010000 -1.0 p 955010000
*
* core power input
*
* heater powers
*
20509010 power101 function 1.0 2.20E+05 1
20509011 time 0 901
*
20509020 power102 function 1.0 2.20E+05 1
20509021 time 0 902
*
20509030 power103 function 1.0 2.20E+05 1
20509031 time 0 903
*
20509040 power104 function 1.0 2.20E+05 1
20509041 time 0 904
*
20509050 power105 function 1.0 2.20E+05 1
20509051 time 0 905
*
20509060 power106 function 1.0 2.20E+05 1
20509061 time 0 906
*
20509070 power107 function 1.0 2.20E+05 1
20509071 time 0 907
*
20509080 power108 function 1.0 2.20E+05 1
20509081 time 0 908
*
20509090 power109 function 1.0 2.20E+05 1
20509091 time 0 909
*
20509100 power110 function 1.0 2.20E+05 1
20509101 time 0 910
*
* core power in W
*
20509110 corepow sum 1.0 2.20E+06 1
20509111 0.0 1.0 cntrlvar 901 1.0 cntrlvar 902
20509112 1.0 cntrlvar 903 1.0 cntrlvar 904
20509113 1.0 cntrlvar 905 1.0 cntrlvar 906
20509114 1.0 cntrlvar 907 1.0 cntrlvar 908
20509115 1.0 cntrlvar 909 1.0 cntrlvar 910
*
* core power in MW
*
20509120 coreheat sum 1.00E-06 2.2 1
20509121 0.0 1.0 cntrlvar 911

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*
* integrated core heat generation in MJ
*
20509130 corehtin integral 1.0 0.0 0
20509131 cntrlvar 912
*
* heater rod power input
*
20509400 powin140 sum 1.0 586666.7 1
20509401 0.0 0.904762 cntrlvar 901 0.428571 cntrlvar 910
20509402 0.904762 cntrlvar 906 0.428571 cntrlvar 907
*
20509450 powin145 sum 1.0 754285.7 1
20509451 0.0 0.095238 cntrlvar 901 0.523810 cntrlvar 910
20509452 0.857143 cntrlvar 903 0.142857 cntrlvar 908
20509453 0.095238 cntrlvar 905 0.095238 cntrlvar 906
20509454 0.523810 cntrlvar 907 0.857143 cntrlvar 904
20509455 0.142857 cntrlvar 909 0.095238 cntrlvar 902
*
20509500 powin150 sum 1.0 859047.6 1
20509501 0.0 0.047619 cntrlvar 910 0.142857 cntrlvar 903
20509502 0.857143 cntrlvar 908 0.904762 cntrlvar 905
20509503 0.047619 cntrlvar 907 0.142857 cntrlvar 904
20509504 0.857143 cntrlvar 909 0.904762 cntrlvar 902
*
* RCCS flow control
*
20509180 RCCStout constant 305.0 * RCCS desired outlet temperature
*
20509190 RCCSterr sum 1.0 0.0 0
20509191 0.0 1.0 tempf 955010000 -1.0 cntrlvar 918
*
20509200 RCCSflo prop-int 1.0 1.0 0 1 0.0
20509201 0.07 0.0001 cntrlvar 919
*
* heat structure convection/radiation/conduction
*
20510000 qcv10001 sum 1.0 0.0 1
20510001 0.0 1.684 htrnr 100000100 1.144 htrnr 100000200
20510002 1.294 htrnr 100000300 1.294 htrnr 100000400
20510003 1.020 htrnr 100000500 1.020 htrnr 100000600
20510004 1.020 htrnr 100000700 1.020 htrnr 100000800
20510005 1.020 htrnr 100000900 1.020 htrnr 100001000
20510006 1.020 htrnr 100001100 1.020 htrnr 100001200
20510007 1.020 htrnr 100001300 1.020 htrnr 100001400
20510008 0.980 htrnr 100001500 1.046 htrnr 100001600
+ 1.406 htrnr 100001700
*
20510010 qrc10001 sum 1.0 0.0 1
20510011 0.0 1.684 qrad 1902 1.144 qrad 1906
20510012 1.294 qrad 1908 1.294 qrad 1910
20510013 1.020 qrad 1912 1.020 qrad 1914
20510014 1.020 qrad 1916 1.020 qrad 1918
20510015 1.020 qrad 1920 1.020 qrad 1922
20510016 1.020 qrad 1924 1.020 qrad 1926
20510017 1.020 qrad 1928 1.020 qrad 1930
20510018 0.980 qrad 1932 1.046 qrad 1934
+ 1.406 qrad 1936
*
20510020 qt10001 sum 1.0 0.0 1
20510021 0.0 1.0 cntrlvar 1000 1.0 cntrlvar 1001
*
20510030 qil10001 integral 1.0 0.0 0

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```

20510031  cntrlvar  1002
*
20510040  qcv1000r  sum  1.0  0.0  1
20510041  0.0  1.711  htrnr  100000101  1.162  htrnr  100000201
20510042  1.314  htrnr  100000301  1.314  htrnr  100000401
20510043  1.036  htrnr  100000501  1.036  htrnr  100000601
20510044  1.036  htrnr  100000701  1.036  htrnr  100000801
20510045  1.036  htrnr  100000901  1.036  htrnr  100001001
20510046  1.036  htrnr  100001101  1.036  htrnr  100001201
20510047  1.036  htrnr  100001301  1.036  htrnr  100001401
20510048  0.996  htrnr  100001501  1.062  htrnr  100001601
+  1.428  htrnr  100001701
*
20510050  qrc1000r  sum  1.0  0.0  1
20510051  0.0  1.711  qrad  2103  1.162  qrad  2105
20510052  1.314  qrad  2107  1.314  qrad  2109
20510053  1.036  qrad  2111  1.036  qrad  2113
20510054  1.036  qrad  2115  1.036  qrad  2117
20510055  1.036  qrad  2119  1.036  qrad  2121
20510056  1.036  qrad  2123  1.036  qrad  2125
20510057  1.036  qrad  2127  1.036  qrad  2129
20510058  0.996  qrad  2131  1.062  qrad  2133
+  1.428  qrad  2135
*
20510060  qt1000r  sum  1.0  0.0  1
20510061  0.0  1.0  cntrlvar  1004  1.0  cntrlvar  1005
*
20510070  qil000r  integral  1.0  0.0  0
20510071  cntrlvar  1006
*
20510080  qt1000  sum  1.0  0.0  0
20510081  0.0  1.0  cntrlvar  1002  1.0  cntrlvar  1006
*
20510090  qil000  sum  1.0  0.0  0
20510091  0.0  1.0  cntrlvar  1003  1.0  cntrlvar  1007
*
20510100  qcv1001l  mult  3.664  0.0  1
20510101  htrnr  100100100
*
20510110  qrc1001l  mult  3.664  0.0  1
20510111  qrad  1603
*
20510120  qt1001l  sum  1.0  0.0  1
20510121  0.0  1.0  cntrlvar  1010  1.0  cntrlvar  1011
*
20510130  qil001l  integral  1.0  0.0  0
20510131  cntrlvar  1012
*
20510140  qcv1001r  mult  4.348  0.0  1
20510141  htrnr  100100101
*
20510150  qrc1001r  mult  4.348  0.0  1
20510151  qrad  2137
*
20510160  qt1001r  sum  1.0  0.0  1
20510161  0.0  1.0  cntrlvar  1014  1.0  cntrlvar  1015
*
20510170  qil001r  integral  1.0  0.0  0
20510171  cntrlvar  1016
*
20510180  qt1001  sum  1.0  0.0  0
20510181  0.0  1.0  cntrlvar  1012  1.0  cntrlvar  1016
*

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```

20510190 qil001 sum 1.0 0.0 0
20510191 0.0 1.0 cntrlvar 1013 1.0 cntrlvar 1017
*
20510200 qcv11501 sum 1.0 0.0 1
20510201 0.0 1.557 htrnr 115000100 1.057 htrnr 115000200
20510202 1.196 htrnr 115000300 1.196 htrnr 115000400
20510203 0.943 htrnr 115000500 0.943 htrnr 115000600
20510204 0.943 htrnr 115000700 0.943 htrnr 115000800
20510205 0.943 htrnr 115000900 0.943 htrnr 115001000
20510206 0.943 htrnr 115001100 0.943 htrnr 115001200
20510207 0.943 htrnr 115001300 0.943 htrnr 115001400
20510208 0.906 htrnr 115001500 0.967 htrnr 115001600
*
20510210 qrc11501 sum 1.0 0.0 1
20510211 0.0 1.057 qrad 1806 1.196 qrad 1528
20510212 1.196 qrad 1526 0.943 qrad 1524
20510213 0.943 qrad 1522 0.943 qrad 1520
20510214 0.943 qrad 1518 0.943 qrad 1516
20510215 0.943 qrad 1514 0.943 qrad 1512
20510216 0.943 qrad 1510 0.943 qrad 1508
20510217 0.943 qrad 1506 0.906 qrad 1504
20510218 0.967 qrad 1502
*
20510220 qt11501 sum 1.0 0.0 1
20510221 0.0 1.0 cntrlvar 1020 1.0 cntrlvar 1021
*
20510230 qil11501 integral 1.0 0.0 0
20510231 cntrlvar 1022
*
20510240 qcv1150r sum 1.0 0.0 1
20510241 0.0 1.567 htrnr 115000101 1.064 htrnr 115000201
20510242 1.204 htrnr 115000301 1.204 htrnr 115000401
20510243 0.949 htrnr 115000501 0.949 htrnr 115000601
20510244 0.949 htrnr 115000701 0.949 htrnr 115000801
20510245 0.949 htrnr 115000901 0.949 htrnr 115001001
20510246 0.949 htrnr 115001101 0.949 htrnr 115001201
20510247 0.949 htrnr 115001301 0.949 htrnr 115001401
20510248 0.912 htrnr 115001501 0.973 htrnr 115001601
*
20510250 qrc1150r sum 1.0 0.0 1
20510251 0.0 1.567 qrad 1901 1.064 qrad 1903
20510252 1.204 qrad 1907 1.204 qrad 1909
20510253 0.949 qrad 1911 0.949 qrad 1913
20510254 0.949 qrad 1915 0.949 qrad 1917
20510255 0.949 qrad 1919 0.949 qrad 1921
20510256 0.949 qrad 1923 0.949 qrad 1925
20510257 0.949 qrad 1927 0.949 qrad 1929
20510258 0.912 qrad 1931 0.973 qrad 1933
*
20510260 qt1150r sum 1.0 0.0 1
20510261 0.0 1.0 cntrlvar 1024 1.0 cntrlvar 1025
*
20510270 qil1150r integral 1.0 0.0 0
20510271 cntrlvar 1026
*
20510280 qt1150 sum 1.0 0.0 0
20510281 0.0 1.0 cntrlvar 1022 1.0 cntrlvar 1026
*
20510290 qil1150 sum 1.0 0.0 0
20510291 0.0 1.0 cntrlvar 1023 1.0 cntrlvar 1027
*
20510300 qcv12001 mult 1.311 0.0 1
20510301 htrnr 120000100

```

```

*
20510310 qrc1200l mult 1.311 0.0 1
20510311 grad 1604
*
20510320 qt1200l sum 1.0 0.0 1
20510321 0.0 1.0 cntrlvar 1030 1.0 cntrlvar 1031
*
20510330 qil200l integral 1.0 0.0 0
20510331 cntrlvar 1032
*
20510340 qcv1200r mult 1.316 0.0 1
20510341 htrnr 120000101
*
20510350 qrc1200r mult 1.316 0.0 1
20510351 grad 1935
*
20510360 qt1200r sum 1.0 0.0 1
20510361 0.0 1.0 cntrlvar 1034 1.0 cntrlvar 1035
*
20510370 qil200r integral 1.0 0.0 0
20510371 cntrlvar 1036
*
20510380 qt1200 sum 1.0 0.0 0
20510381 0.0 1.0 cntrlvar 1032 1.0 cntrlvar 1036
*
20510390 qil200 sum 1.0 0.0 0
20510391 0.0 1.0 cntrlvar 1033 1.0 cntrlvar 1037
*
20510410 qrc1201l mult 1.673 0.0 1
20510411 grad 271
*
20510420 qt1201l sum 1.0 0.0 1
20510421 0.0 1.0 cntrlvar 1041
*
20510430 qil201l integral 1.0 0.0 0
20510431 cntrlvar 1042
*
20510440 qcv1201r mult 1.673 0.0 1
20510441 htrnr 120100101
*
20510450 qrc1201r mult 1.673 0.0 1
20510451 grad 1601
*
20510460 qt1201r sum 1.0 0.0 1
20510461 0.0 1.0 cntrlvar 1044 1.0 cntrlvar 1045
*
20510470 qil201r integral 1.0 0.0 0
20510471 cntrlvar 1046
*
20510480 qt1201 sum 1.0 0.0 0
20510481 0.0 1.0 cntrlvar 1042 1.0 cntrlvar 1046
*
20510490 qil201 sum 1.0 0.0 0
20510491 0.0 1.0 cntrlvar 1043 1.0 cntrlvar 1047
*
20510540 qcv1202r mult 2.864 0.0 1
20510541 htrnr 120200101
*
20510550 qrc1202r mult 2.864 0.0 1
20510551 grad 1602
*
20510560 qt1202r sum 1.0 0.0 1
20510561 0.0 1.0 cntrlvar 1054 1.0 cntrlvar 1055

```

```

*
20510570 qil202r integral 1.0 0.0 0
20510571 cntrlvar 1056
*
20510580 qt1202r sum 1.0 0.0 0
20510581 0.0 1.0 cntrlvar 1056 *1.0 cntrlvar 1056
*
20510590 qil202r sum 1.0 0.0 0
20510591 0.0 1.0 cntrlvar 1057 *1.0 cntrlvar 1057
*
20510650 qrc1300r sum 1.0 0.0 1
20510651 0.0 0.090 qrad 101 0.090 qrad 104
20510652 0.094 qrad 107 0.094 qrad 110
20510653 0.094 qrad 113 0.094 qrad 116
20510654 0.094 qrad 119 0.094 qrad 122
20510655 0.094 qrad 125 0.094 qrad 128
20510656 0.094 qrad 131 0.094 qrad 134
20510657 0.119 qrad 137 0.119 qrad 140
*
20510660 qt1300r sum 1.0 0.0 1
20510661 0.0 1.0 cntrlvar 1065
*
20510670 qil300r integral 1.0 0.0 0
20510671 cntrlvar 1066
*
20510680 qt1300 sum 1.0 0.0 0
20510681 0.0 1.0 cntrlvar 1066
*
20510690 qil300 sum 1.0 0.0 0
20510691 0.0 1.0 cntrlvar 1067
*
20510700 qcv13201 sum 1.0 0.0 1
20510701 0.0 0.068 htrnr 132000100 0.068 htrnr 132000200
20510702 0.071 htrnr 132000300 0.071 htrnr 132000400
20510703 0.071 htrnr 132000500 0.071 htrnr 132000600
20510704 0.071 htrnr 132000700 0.071 htrnr 132000800
20510705 0.071 htrnr 132000900 0.071 htrnr 132001000
20510706 0.071 htrnr 132001100 0.071 htrnr 132001200
20510707 0.090 htrnr 132001300 0.090 htrnr 132001400
*
20510710 qrc13201 sum 1.0 0.0 1
20510711 0.0 0.090 qrad 1801
*
20510720 qt13201 sum 1.0 0.0 1
20510721 0.0 1.0 cntrlvar 1070 1.0 cntrlvar 1071
*
20510730 qil3201 integral 1.0 0.0 0
20510731 cntrlvar 1072
*
20510750 qrc1320r sum 1.0 0.0 1
20510751 0.0 0.432 qrad 102 0.432 qrad 105
20510752 0.449 qrad 108 0.449 qrad 111
20510753 0.449 qrad 114 0.449 qrad 117
20510754 0.449 qrad 120 0.449 qrad 123
20510755 0.449 qrad 126 0.449 qrad 129
20510756 0.449 qrad 132 0.449 qrad 135
20510757 0.570 qrad 138 0.570 qrad 141
*
20510760 qt1320r sum 1.0 0.0 1
20510761 0.0 1.0 cntrlvar 1075
*
20510770 qil320r integral 1.0 0.0 0
20510771 cntrlvar 1076

```

```

*
20510780 qt1320 sum 1.0 0.0 0
20510781 0.0 1.0 cntrlvar 1072 1.0 cntrlvar 1076
*
20510790 qil320 sum 1.0 0.0 0
20510791 0.0 1.0 cntrlvar 1073 1.0 cntrlvar 1077
*
20510810 qrc1340l sum 1.0 0.0 1
20510811 0.0 0.198 qrad 103 0.198 qrad 106
20510812 0.206 qrad 109 0.206 qrad 112
20510813 0.206 qrad 115 0.206 qrad 118
20510814 0.206 qrad 121 0.206 qrad 124
20510815 0.206 qrad 127 0.206 qrad 130
20510816 0.206 qrad 133 0.206 qrad 136
20510817 0.261 qrad 139 0.261 qrad 142
*
20510820 qt1340l sum 1.0 0.0 1
20510821 0.0 1.0 cntrlvar 1081
*
20510830 qil340l integral 1.0 0.0 0
20510831 cntrlvar 1082
*
20510850 qrc1340r sum 1.0 0.0 1
20510851 0.0 0.212 qrad 201 0.212 qrad 206
20510852 0.221 qrad 211 0.221 qrad 216
20510853 0.221 qrad 221 0.221 qrad 226
20510854 0.221 qrad 231 0.221 qrad 236
20510855 0.221 qrad 241 0.221 qrad 246
20510856 0.221 qrad 251 0.221 qrad 256
20510857 0.280 qrad 261 0.280 qrad 266
*
20510860 qt1340r sum 1.0 0.0 1
20510861 0.0 1.0 cntrlvar 1085
*
20510870 qil340r integral 1.0 0.0 0
20510871 cntrlvar 1086
*
20510880 qt1340 sum 1.0 0.0 0
20510881 0.0 1.0 cntrlvar 1082 1.0 cntrlvar 1086
*
20510890 qil340 sum 1.0 0.0 0
20510891 0.0 1.0 cntrlvar 1083 1.0 cntrlvar 1087
*
20510900 qcv1401l sum 1.0 0.0 1
20510901 0.0 1.163 htrnr 140000100 1.163 htrnr 140000200
20510902 1.209 htrnr 140100100 1.209 htrnr 140100200
20510903 1.209 htrnr 140100300 1.209 htrnr 140100400
20510904 1.209 htrnr 140100500 1.209 htrnr 140100600
20510905 1.209 htrnr 140100700 1.209 htrnr 140100800
20510906 1.209 htrnr 140100900 1.209 htrnr 140101000
20510907 1.535 htrnr 140200100 1.535 htrnr 140200200
*
20510910 qrc1401l sum 1.0 0.0 1
20510911 0.0 1.163 qrad 202 1.163 qrad 207
20510912 1.209 qrad 212 1.209 qrad 217
20510913 1.209 qrad 222 1.209 qrad 227
20510914 1.209 qrad 232 1.209 qrad 237
20510915 1.209 qrad 242 1.209 qrad 247
20510916 1.209 qrad 252 1.209 qrad 257
20510917 1.535 qrad 262 1.535 qrad 267
*
20510920 qt1401l sum 1.0 0.0 1
20510921 0.0 1.0 cntrlvar 1090 1.0 cntrlvar 1091

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*
20510930 qil401l integral 1.0 0.0 0
20510931 cntrlvar 1092
*
20510940 qcv1401r sum 1.0 0.0 1
20510941 0.0 2.862 htrnr 140100101 2.862 htrnr 140100201
20510942 2.862 htrnr 140100301 2.862 htrnr 140100401
20510943 2.862 htrnr 140100501 2.862 htrnr 140100601
20510944 2.862 htrnr 140100701 2.862 htrnr 140100801
20510945 2.862 htrnr 140100901 2.862 htrnr 140101001
*
20510950 qrc1401r sum 1.0 0.0 1
20510951 0.0 2.862 qrad 1102 2.862 qrad 1104
20510952 2.862 qrad 1106 2.862 qrad 1108
20510953 2.862 qrad 1110 2.862 qrad 1112
20510954 2.862 qrad 1114 2.862 qrad 1116
20510955 2.862 qrad 1118 2.862 qrad 1120
20510956 3.632 qrad 1802
*
20510960 qt1401r sum 1.0 0.0 1
20510961 0.0 1.0 cntrlvar 1095 1.0 cntrlvar 1094
*
20510970 qil401r integral 1.0 0.0 0
20510971 cntrlvar 1096
*
20510980 qt1401 sum 1.0 0.0 0
20510981 0.0 1.0 cntrlvar 1092 1.0 cntrlvar 1096
*
20510990 qil401 sum 1.0 0.0 0
20510991 0.0 1.0 cntrlvar 1093 1.0 cntrlvar 1097
*
20511000 qcv1451l sum 1.0 0.0 1
20511001 0.0 1.368 htrnr 145000100 1.368 htrnr 145000200
20511002 1.423 htrnr 145100100 1.423 htrnr 145100200
20511003 1.423 htrnr 145100300 1.423 htrnr 145100400
20511004 1.423 htrnr 145100500 1.423 htrnr 145100600
20511005 1.423 htrnr 145100700 1.423 htrnr 145100800
20511006 1.423 htrnr 145100900 1.423 htrnr 145101000
20511007 1.806 htrnr 145200100 1.806 htrnr 145200200
*
20511010 qrc1451l sum 1.0 0.0 1
20511011 0.0 1.368 qrad 203 1.368 qrad 208
20511012 1.423 qrad 213 1.423 qrad 218
20511013 1.423 qrad 223 1.423 qrad 228
20511014 1.423 qrad 233 1.423 qrad 238
20511015 1.423 qrad 243 1.423 qrad 248
20511016 1.423 qrad 253 1.423 qrad 258
20511017 1.806 qrad 263 1.806 qrad 268
*
20511020 qt1451l sum 1.0 0.0 1
20511021 0.0 1.0 cntrlvar 1100 1.0 cntrlvar 1101
*
20511030 qil451l integral 1.0 0.0 0
20511031 cntrlvar 1102
*
20511040 qcv1451r sum 1.0 0.0 1
20511041 0.0 3.068 htrnr 145100101 3.068 htrnr 145100201
20511042 3.068 htrnr 145100301 3.068 htrnr 145100401
20511043 3.068 htrnr 145100501 3.068 htrnr 145100601
20511044 3.068 htrnr 145100701 3.068 htrnr 145100801
20511045 3.068 htrnr 145100901 3.068 htrnr 145101001
*
20511050 qrc1451r sum 1.0 0.0 1

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20511051 0.0 3.068 qrad 1202 3.068 qrad 1204
20511052 3.068 qrad 1206 3.068 qrad 1208
20511053 3.068 qrad 1210 3.068 qrad 1212
20511054 3.068 qrad 1214 3.068 qrad 1216
20511055 3.068 qrad 1218 3.068 qrad 1220
20511056 3.894 qrad 1803
*
20511060 qt1451r sum 1.0 0.0 1
20511061 0.0 1.0 cntrlvar 1105 1.0 cntrlvar 1104
*
20511070 qil451r integral 1.0 0.0 0
20511071 cntrlvar 1106
*
20511080 qt1451 sum 1.0 0.0 0
20511081 0.0 1.0 cntrlvar 1102 1.0 cntrlvar 1106
*
20511090 qil451 sum 1.0 0.0 0
20511091 0.0 1.0 cntrlvar 1103 1.0 cntrlvar 1107
*
20511100 qcv1501l sum 1.0 0.0 1
20511101 0.0 1.824 htrnr 150000100 1.824 htrnr 150000200
20511102 1.897 htrnr 150100100 1.897 htrnr 150100200
20511103 1.897 htrnr 150100300 1.897 htrnr 150100400
20511104 1.897 htrnr 150100500 1.897 htrnr 150100600
20511105 1.897 htrnr 150100700 1.897 htrnr 150100800
20511106 1.897 htrnr 150100900 1.897 htrnr 150101000
20511107 2.408 htrnr 150200100 2.408 htrnr 150200200
*
20511110 qrc1501l sum 1.0 0.0 1
20511111 0.0 1.824 qrad 204 1.824 qrad 209
20511112 1.897 qrad 214 1.897 qrad 219
20511113 1.897 qrad 224 1.897 qrad 229
20511114 1.897 qrad 234 1.897 qrad 239
20511115 1.897 qrad 244 1.897 qrad 249
20511116 1.897 qrad 254 1.897 qrad 259
20511117 2.408 qrad 264 2.408 qrad 269
*
20511120 qt1501l sum 1.0 0.0 1
20511121 0.0 1.0 cntrlvar 1110 1.0 cntrlvar 1111
*
20511130 qil501l integral 1.0 0.0 0
20511131 cntrlvar 1112
*
20511140 qcv1501r sum 1.0 0.0 1
20511141 0.0 4.753 htrnr 150100101 4.753 htrnr 150100201
20511142 4.753 htrnr 150100301 4.753 htrnr 150100401
20511143 4.753 htrnr 150100501 4.753 htrnr 150100601
20511144 4.753 htrnr 150100701 4.753 htrnr 150100801
20511145 4.753 htrnr 150100901 4.753 htrnr 150101001
*
20511150 qrc1501r sum 1.0 0.0 1
20511151 0.0 4.753 qrad 1302 4.753 qrad 1304
20511152 4.753 qrad 1306 4.753 qrad 1308
20511153 4.753 qrad 1310 4.753 qrad 1312
20511154 4.753 qrad 1314 4.753 qrad 1316
20511155 4.753 qrad 1318 4.753 qrad 1320
20511156 6.033 qrad 1804
*
20511160 qt1501r sum 1.0 0.0 1
20511161 0.0 1.0 cntrlvar 1115 1.0 cntrlvar 1114
*
20511170 qil501r integral 1.0 0.0 0
20511171 cntrlvar 1116

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*
20511180 qt1501 sum 1.0 0.0 0
20511181 0.0 1.0 cntrlvar 1112 1.0 cntrlvar 1116
*
20511190 qil501 sum 1.0 0.0 0
20511191 0.0 1.0 cntrlvar 1113 1.0 cntrlvar 1117
*
20511210 qrc16001 sum 1.0 0.0 1
20511211 0.0 0.567 qrad 205 0.567 qrad 210
20511212 0.589 qrad 215 0.589 qrad 220
20511213 0.589 qrad 225 0.589 qrad 230
20511214 0.589 qrad 235 0.589 qrad 240
20511215 0.589 qrad 245 0.589 qrad 250
20511216 0.589 qrad 255 0.589 qrad 260
20511217 0.748 qrad 265 0.748 qrad 270
*
20511220 qt16001 sum 1.0 0.0 1
20511221 0.0 1.0 cntrlvar 1121
*
20511230 qil6001 integral 1.0 0.0 0
20511231 cntrlvar 1122
*
20511250 qrc1600r sum 1.0 0.0 1
20511251 0.0 0.608 qrad 301 0.608 qrad 304
20511252 0.633 qrad 307 0.633 qrad 310
20511253 0.633 qrad 313 0.633 qrad 316
20511254 0.633 qrad 319 0.633 qrad 322
20511255 0.633 qrad 325 0.633 qrad 328
20511256 0.633 qrad 331 0.633 qrad 334
20511257 0.803 qrad 337 0.803 qrad 340
*
20511260 qt1600r sum 1.0 0.0 1
20511261 0.0 1.0 cntrlvar 1125
*
20511270 qil600r integral 1.0 0.0 0
20511271 cntrlvar 1126
*
20511280 qt1600 sum 1.0 0.0 0
20511281 0.0 1.0 cntrlvar 1122 1.0 cntrlvar 1126
*
20511290 qil600 sum 1.0 0.0 0
20511291 0.0 1.0 cntrlvar 1123 1.0 cntrlvar 1127
*
20511300 qcv16201 sum 1.0 0.0 1
20511301 0.0 0.342 htrnr 162000100 0.342 htrnr 162000200
20511302 0.356 htrnr 162000300 0.356 htrnr 162000400
20511303 0.356 htrnr 162000500 0.356 htrnr 162000600
20511304 0.356 htrnr 162000700 0.356 htrnr 162000800
20511305 0.356 htrnr 162000900 0.356 htrnr 162001000
20511306 0.356 htrnr 162001100 0.356 htrnr 162001200
20511307 0.451 htrnr 162001300 0.451 htrnr 162001400
*
20511310 qrc16201 sum 1.0 0.0 1
20511311 0.0 0.451 qrad 1805
*
20511320 qt16201 sum 1.0 0.0 1
20511321 0.0 1.0 cntrlvar 1130 1.0 cntrlvar 1131
*
20511330 qil6201 integral 1.0 0.0 0
20511331 cntrlvar 1132
*
20511350 qrc1620r sum 1.0 0.0 1
20511351 0.0 1.943 qrad 302 1.943 qrad 305

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20511352 2.020 qrad 308 2.020 qrad 311
20511353 2.020 qrad 314 2.020 qrad 317
20511354 2.020 qrad 320 2.020 qrad 323
20511355 2.020 qrad 326 2.020 qrad 329
20511356 2.020 qrad 332 2.020 qrad 335
20511357 2.564 qrad 338 2.564 qrad 341
*
20511360 qt1620r sum 1.0 0.0 1
20511361 0.0 1.0 cntrlvar 1135
*
20511370 qil620r integral 1.0 0.0 0
20511371 cntrlvar 1136
*
20511380 qt1620 sum 1.0 0.0 0
20511381 0.0 1.0 cntrlvar 1132 1.0 cntrlvar 1136
*
20511390 qil620 sum 1.0 0.0 0
20511391 0.0 1.0 cntrlvar 1133 1.0 cntrlvar 1137
*
20511410 qrc1640l sum 1.0 0.0 1
20511411 0.0 0.689 qrad 303 0.689 qrad 306
20511412 0.717 qrad 309 0.717 qrad 312
20511413 0.717 qrad 315 0.717 qrad 318
20511414 0.717 qrad 321 0.717 qrad 324
20511415 0.717 qrad 327 0.717 qrad 330
20511416 0.717 qrad 333 0.717 qrad 336
20511417 0.910 qrad 339 0.910 qrad 342
*
20511420 qt1640l sum 1.0 0.0 1
20511421 0.0 1.0 cntrlvar 1141
*
20511430 qil640l integral 1.0 0.0 0
20511431 cntrlvar 1142
*
20511440 qcv1640r sum 1.0 0.0 1
20511441 0.0 0.723 htrnr 164000101 0.723 htrnr 164000201
20511442 0.752 htrnr 164000301 0.752 htrnr 164000401
20511443 0.752 htrnr 164000501 0.752 htrnr 164000601
20511444 0.752 htrnr 164000701 0.752 htrnr 164000801
20511445 0.752 htrnr 164000901 0.752 htrnr 164001001
20511446 0.752 htrnr 164001101 0.752 htrnr 164001201
20511447 0.955 htrnr 164001301 0.955 htrnr 164001401
*
20511450 qrc1640r sum 1.0 0.0 1
20511451 0.0 0.723 qrad 1401 0.723 qrad 1403
20511452 0.752 qrad 1405 0.752 qrad 1407
20511453 0.752 qrad 1409 0.752 qrad 1411
20511454 0.752 qrad 1413 0.752 qrad 1415
20511455 0.752 qrad 1417 0.752 qrad 1419
20511456 0.752 qrad 1421 0.752 qrad 1423
20511457 0.955 qrad 1425 0.955 qrad 1427
*
20511460 qt1640r sum 1.0 0.0 1
20511461 0.0 1.0 cntrlvar 1144 1.0 cntrlvar 1145
*
20511470 qil640r integral 1.0 0.0 0
20511471 cntrlvar 1146
*
20511480 qt1640 sum 1.0 0.0 0
20511481 0.0 1.0 cntrlvar 1142 1.0 cntrlvar 1146
*
20511490 qil640 sum 1.0 0.0 0
20511491 0.0 1.0 cntrlvar 1143 1.0 cntrlvar 1147

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*
20511500 qcv16601 sum 1.0 0.0 1
20511501 0.0 0.734 htrnr 166000100 0.734 htrnr 166000200
20511502 0.764 htrnr 166000300 0.764 htrnr 166000400
20511503 0.764 htrnr 166000500 0.764 htrnr 166000600
20511504 0.764 htrnr 166000700 0.764 htrnr 166000800
20511505 0.764 htrnr 166000900 0.764 htrnr 166001000
20511506 0.764 htrnr 166001100 0.764 htrnr 166001200
20511507 0.969 htrnr 166001300 0.969 htrnr 166001400
*
20511510 qrc16601 sum 1.0 0.0 1
20511511 0.0 0.734 qrad 1402 0.734 qrad 1404
20511512 0.764 qrad 1406 0.764 qrad 1408
20511513 0.764 qrad 1410 0.764 qrad 1412
20511514 0.764 qrad 1414 0.764 qrad 1416
20511515 0.764 qrad 1418 0.764 qrad 1420
20511516 0.764 qrad 1420 0.764 qrad 1424
20511517 0.969 qrad 1426 0.969 qrad 1428
*
20511520 qt16601 sum 1.0 0.0 1
20511521 0.0 1.0 cntrlvar 1150 1.0 cntrlvar 1151
*
20511530 qil6601 integral 1.0 0.0 0
20511531 cntrlvar 1152
*
20511540 qcv1660r sum 1.0 0.0 1
20511541 0.0 0.899 htrnr 166000101 0.899 htrnr 166000201
20511542 0.935 htrnr 166000301 0.935 htrnr 166000401
20511543 0.935 htrnr 166000501 0.935 htrnr 166000601
20511544 0.935 htrnr 166000701 0.935 htrnr 166000801
20511545 0.935 htrnr 166000901 0.935 htrnr 166001001
20511546 0.935 htrnr 166001101 0.935 htrnr 166001201
20511547 1.186 htrnr 166001301 1.186 htrnr 166001401
*
20511550 qrc1660r sum 1.0 0.0 1
20511551 0.0 0.899 qrad 1501 0.899 qrad 1503
20511552 0.935 qrad 1505 0.935 qrad 1507
20511553 0.935 qrad 1509 0.935 qrad 1511
20511554 0.935 qrad 1513 0.935 qrad 1515
20511555 0.935 qrad 1517 0.935 qrad 1519
20511556 0.935 qrad 1521 0.935 qrad 1523
20511557 1.186 qrad 1525 1.186 qrad 1527
*
20511560 qt1660r sum 1.0 0.0 1
20511561 0.0 1.0 cntrlvar 1154 1.0 cntrlvar 1155
*
20511570 qil660r integral 1.0 0.0 0
20511571 cntrlvar 1156
*
20511580 qt1660 sum 1.0 0.0 0
20511581 0.0 1.0 cntrlvar 1152 1.0 cntrlvar 1156
*
20511590 qil660 sum 1.0 0.0 0
20511591 0.0 1.0 cntrlvar 1153 1.0 cntrlvar 1157
*
20511600 qcv17501 sum 1.0 0.0 1
20511601 0.0 1.771 htrnr 175000100
*
20511610 qrc17501 sum 1.0 0.0 1
20511611 0.0 1.771 qrad 1808
*
20511620 qt17501 sum 1.0 0.0 1
20511621 0.0 1.0 cntrlvar 1160 1.0 cntrlvar 1161

```

```

*
20511630 qil750l integral 1.0 0.0 0
20511631 cntrlvar 1162
*
20511640 qcv1750r sum 1.0 0.0 1
20511641 0.0 1.771 htrnr 175000101
*
20511660 qt1750r sum 1.0 0.0 1
20511661 0.0 1.0 cntrlvar 1164
*
20511670 qil750r integral 1.0 0.0 0
20511671 cntrlvar 1166
*
20511680 qt1750 sum 1.0 0.0 0
20511681 0.0 1.0 cntrlvar 1162 1.0 cntrlvar 1166
*
20511690 qil750 sum 1.0 0.0 0
20511691 0.0 1.0 cntrlvar 1163 1.0 cntrlvar 1167
*
20511740 qcv1751r mult 6.668 0.0 1
20511741 htrnr 175100101
*
20511750 qrc1751r sum 1.0 0.0 1
20511751 0 6.668 qrad 1806
*
20511760 qt1751r sum 1.0 0.0 1
20511761 0.0 1.0 cntrlvar 1174 1.0 cntrlvar 1175
*
20511770 qil751r integral 1.0 0.0 0
20511771 cntrlvar 1176
*
20511780 qt1751r sum 1.0 0.0 0
20511781 0.0 1.0 cntrlvar 1176
*
20511790 qil751r sum 1.0 0.0 0
20511791 0.0 1.0 cntrlvar 1177
*
20511800 qcv9500l sum 1.0 0.0 1
20511801 0.0 9.969 htrnr 950000100 3.192 htrnr 950000200
20511802 2.168 htrnr 950000300 2.453 htrnr 950000400
20511803 2.453 htrnr 950000500 2.453 htrnr 950000600
20511804 2.453 htrnr 950000700 2.453 htrnr 950000800
20511805 2.453 htrnr 950000900 2.453 htrnr 950001000
20511806 2.453 htrnr 950001100 2.453 htrnr 950001200
20511807 2.453 htrnr 950001300 2.453 htrnr 950001400
20511808 1.932 htrnr 950001500 1.858 htrnr 950001600
+ 1.982 htrnr 950001700 2.665 htrnr 950001800
+ 7.300 htrnr 950001900
*
20511810 qrc9500l sum 1.0 0.0 1
20511811 0.0 9.969 qrad 2102 3.192 qrad 2104
20511812 2.168 qrad 2106 2.453 qrad 2108
20511813 2.453 qrad 2110 2.453 qrad 2112
20511814 2.453 qrad 2114 2.453 qrad 2116
20511815 2.453 qrad 2118 2.453 qrad 2120
20511816 2.453 qrad 2122 2.453 qrad 2124
20511817 2.453 qrad 2126 2.453 qrad 2128
20511818 1.932 qrad 2130 1.858 qrad 2132
+ 1.982 qrad 2134 2.665 qrad 2136
+ 7.300 qrad 2138
*
20511820 qt9500l sum 1.0 0.0 1
20511821 0.0 1.0 cntrlvar 1180 1.0 cntrlvar 1181

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*
20511830 qi95001 integral 1.0 0.0 0
20511831 cntrlvar 1182
*
20511840 qcv9500r sum 1.0 0.0 1
20511841 0.0 9.969 htrnr 950000101 3.192 htrnr 950000201
20511842 2.168 htrnr 950000301 2.453 htrnr 950000401
20511843 2.453 htrnr 950000501 2.453 htrnr 950000601
20511844 2.453 htrnr 950000701 2.453 htrnr 950000801
20511845 2.453 htrnr 950000901 2.453 htrnr 950001001
20511846 2.453 htrnr 950001101 2.453 htrnr 950001201
20511847 2.453 htrnr 950001301 2.453 htrnr 950001401
20511848 1.932 htrnr 950001501 1.858 htrnr 950001601
+ 1.982 htrnr 950001701 2.665 htrnr 950001801
+ 7.300 htrnr 950001901
*
20511860 qt9500r sum 1.0 0.0 1
20511861 0.0 1.0 cntrlvar 1184 * 1.0 cntrlvar 1185
*
20511870 qi9500r integral 1.0 0.0 0
20511871 cntrlvar 1186
*
20511880 qt9500 sum 1.0 0.0 0
20511881 0.0 1.0 cntrlvar 1182 1.0 cntrlvar 1186
*
20511890 qi9500 sum 1.0 0.0 0
20511891 0.0 1.0 cntrlvar 1183 1.0 cntrlvar 1187
*
20511900 qcv9501l sum 1.0 0.0 1
20511901 0.0 9.969 htrnr 950100100 3.192 htrnr 950100200
20511902 2.168 htrnr 950100300 2.453 htrnr 950100400
20511903 2.453 htrnr 950100500 2.453 htrnr 950100600
20511904 2.453 htrnr 950100700 2.453 htrnr 950100800
20511905 2.453 htrnr 950100900 2.453 htrnr 950101000
20511906 2.453 htrnr 950101100 2.453 htrnr 950101200
20511907 2.453 htrnr 950101300 2.453 htrnr 950101400
20511908 1.932 htrnr 950101500 1.858 htrnr 950101600
+ 1.982 htrnr 950101700 2.665 htrnr 950101800
+ 7.300 htrnr 950101900
*
20511920 qt9501l sum 1.0 0.0 1
20511921 0.0 1.0 cntrlvar 1190
*
20511930 qi9501l integral 1.0 0.0 0
20511931 cntrlvar 1192
*
20511940 qcv9501r sum 1.0 0.0 1
20511941 0.0 9.969 htrnr 950100101 3.192 htrnr 950100201
20511942 2.168 htrnr 950100301 2.453 htrnr 950100401
20511943 2.453 htrnr 950100501 2.453 htrnr 950100601
20511944 2.453 htrnr 950100701 2.453 htrnr 950100801
20511945 2.453 htrnr 950100901 2.453 htrnr 950101001
20511946 2.453 htrnr 950101101 2.453 htrnr 950101201
20511947 2.453 htrnr 950101301 2.453 htrnr 950101401
20511948 1.932 htrnr 950101501 1.858 htrnr 950101601
+ 1.982 htrnr 950101701 2.665 htrnr 950101801
+ 7.300 htrnr 950101901
*
20511960 qt9501r sum 1.0 0.0 1
20511961 0.0 1.0 cntrlvar 1194
*
20511970 qi9501r integral 1.0 0.0 0
20511971 cntrlvar 1196

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*
20511980 qt9501 sum 1.0 0.0 0
20511981 0.0 1.0 cntrlvar 1192 1.0 cntrlvar 1196
*
20511990 qi9501 sum 1.0 0.0 0
20511991 0.0 1.0 cntrlvar 1193 1.0 cntrlvar 1197
*
20512000 qcv1002l sum 1.0 0.0 1
20512001 0.0 4.216 htrnr 100200100
*
20512020 qt1002l sum 1.0 0.0 1
20512021 0.0 1.0 cntrlvar 1200
*
20512030 qi1002l integral 1.0 0.0 0
20512031 cntrlvar 1202
*
20512040 qcv1002r sum 1.0 0.0 1
20512041 0.0 4.348 htrnr 100200101
*
20512050 qrc1002r sum 1.0 0.0 1
20512051 0.0 4.348 qrad 2101
*
20512060 qt1002r sum 1.0 0.0 1
20512061 0.0 1.0 cntrlvar 1204 1.0 cntrlvar 1205
*
20512070 qi1002r integral 1.0 0.0 0
20512071 cntrlvar 1206
*
20512080 qt1002 sum 1.0 0.0 1
20512081 0.0 1.0 cntrlvar 1202 1.0 cntrlvar 1206
*
20512090 qi1002 sum 1.0 0.0 1
20512091 0.0 1.0 cntrlvar 1203 1.0 cntrlvar 1207
*
20512150 qrc1403r sum 1.0 0.0 1
20512151 0.0 0.506 qrad 1101 0.506 qrad 1103
20512152 0.506 qrad 1105 0.506 qrad 1107
20512153 0.506 qrad 1109 0.506 qrad 1111
20512154 0.506 qrad 1113 0.506 qrad 1115
20512155 0.506 qrad 1117 0.506 qrad 1119
*
20512160 qt1403r sum 1.0 0.0 1
20512161 0.0 1.0 cntrlvar 1215
*
20512170 qi1403r integral 1.0 0.0 0
20512171 cntrlvar 1216
*
20512250 qrc1453r sum 1.0 0.0 1
20512251 0.0 0.650 qrad 1201 0.650 qrad 1203
20512252 0.650 qrad 1205 0.650 qrad 1207
20512253 0.650 qrad 1209 0.650 qrad 1211
20512254 0.650 qrad 1213 0.650 qrad 1215
20512255 0.650 qrad 1217 0.650 qrad 1219
*
20512260 qt1453r sum 1.0 0.0 1
20512261 0.0 1.0 cntrlvar 1225
*
20512270 qi1453r integral 1.0 0.0 0
20512271 cntrlvar 1226
*
20512350 qrc1503r sum 1.0 0.0 1
20512351 0.0 0.741 qrad 1301 0.741 qrad 1303
20512352 0.741 qrad 1305 0.741 qrad 1307

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20512353 0.741 qgrad 1309 0.741 qgrad 1311
20512354 0.741 qgrad 1313 0.741 qgrad 1315
20512355 0.741 qgrad 1317 0.741 qgrad 1319
*
20512360 qt1503r sum 1.0 0.0 1
20512361 0.0 1.0 cntrlvar 1235
*
20512370 qil503r integral 1.0 0.0 0
20512371 cntrlvar 1236
*
* net heat out of heater rods
*
20513010 qhtrsout sum 1.0 0.0 0
20513011 0.0 -1.0 cntrlvar 907 1.0 cntrlvar 1216
20513012 1.0 cntrlvar 1226 1.0 cntrlvar 1236
*
* net heat out of core heater region ceramic
*
20513020 qcoreout sum 1.0 0.0 0
20513021 0.0 1.0 cntrlvar 1301 1.0 cntrlvar 1098
20513022 1.0 cntrlvar 1108 1.0 cntrlvar 1118
*
* net heat out of core block
*
20513030 qcblkout sum 1.0 0.0 0
20513031 0.0 1.0 cntrlvar 1302 1.0 cntrlvar 1068
20513032 1.0 cntrlvar 1078 1.0 cntrlvar 1088
20513033 1.0 cntrlvar 1128 1.0 cntrlvar 1138
20513034 1.0 cntrlvar 1148
*
* net heat out of core and reflectors
*
20513040 qcortout sum 1.0 0.0 0
20513041 0.0 1.0 cntrlvar 1303 1.0 cntrlvar 1158
20513042 1.0 cntrlvar 1048
*
* net heat out of core, reflectors, and core barrel
*
20513050 qbarout sum 1.0 0.0 0
20513051 0.0 1.0 cntrlvar 1304 1.0 cntrlvar 1028
20513052 1.0 cntrlvar 1038
*
* net heat out of entire primary pressure vessel
*
20513060 qrvout sum 1.0 0.0 0
20513061 0.0 1.0 cntrlvar 1305 1.0 cntrlvar 1008
20513062 1.0 cntrlvar 1018 1.0 cntrlvar 1058
20513063 1.0 cntrlvar 1168 1.0 cntrlvar 1178
20513064 1.0 cntrlvar 2008
*
* environmental heat losses
*
20514010 hs200ehl sum 1.0 0.0 1
20514011 0.0 0.656 htrnr 200100101 0.656 htrnr 200100201
*
20514030 hs215ehl sum 1.0 0.0 1
20514031 0.0 0.723 htrnr 215000101
*
20514040 hs220ehl sum 1.0 0.0 1
20514041 0.0 0.889 htrnr 220000101
*
20514050 hs228ehl sum 1.0 0.0 1
20514051 0.0 0.756 htrnr 228000101

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*
20514060  hs230ehl  sum  1.0  0.0  1
20514061  0.0  2.303  htrnr  230000101
*
20514070  hs235ehl  sum  1.0  0.0  1
20514071  0.0  2.045  htrnr  235000101
*
20514080  hs240ehl  sum  1.0  0.0  1
20514081  0.0  1.305  htrnr  240000101
*
20514090  hs250ehl  sum  1.0  0.0  1
20514091  0.0  1.101  htrnr  250000101  0.364  htrnr  250000201
20514092  0.628  htrnr  250000301
*
20514110  hs260ehl  sum  1.0  0.0  1
20514111  0.0  0.369  htrnr  260000101
*
20514120  hs270ehl  sum  1.0  0.0  1
20514121  0.0  0.725  htrnr  270000101  0.725  htrnr  270000201
20514122  1.144  htrnr  270000301  0.759  htrnr  270000401
*
20514130  hs280ehl  sum  1.0  0.0  1
20514131  0.0  8.969  htrnr  280000101  29.852  htrnr  280000201
* replace the card above with the one below when using the single-volume RCST
*20514131  0.0  38.821  htrnr  280000101
*
20514140  hs340ehl  sum  1.0  0.0  1
20514141  0.0  0.315  htrnr  340000101  0.315  htrnr  340000201
20514142  0.318  htrnr  340000301  0.318  htrnr  340000401
20514143  0.318  htrnr  340000501  0.318  htrnr  340000601
20514144  0.318  htrnr  340000701  0.318  htrnr  340000801
20514145  0.318  htrnr  340000901  0.318  htrnr  340001001
20514146  1.416  htrnr  340001101  1.275  htrnr  340001201
20514147  1.249  htrnr  340001301
*
20514150  hs355ehl  sum  1.0  0.0  1
20514151  0.0  0.689  htrnr  355000101
*
* use the cards below for a CRD line break
*
*20514160  h10100  sum  1.0  0.0  1
*20514161  0.0  0.0149  htrnr  10000101  0.0149  htrnr  10000201
*20514162  0.0149  htrnr  10000301  0.0149  htrnr  10000401
*20514163  0.0149  htrnr  10000501  0.0149  htrnr  10000601
*20514164  0.0149  htrnr  10000701  0.0149  htrnr  10000801
*20514165  0.0149  htrnr  10000901  0.0149  htrnr  10001001
*20514166  0.0149  htrnr  10001101  0.0149  htrnr  10001201
*20514167  0.0149  htrnr  10001301  0.0149  htrnr  10001401
*20514168  0.0149  htrnr  10001501  0.0149  htrnr  10001601
*+  0.0149  htrnr  10001701  0.0149  htrnr  10001801
*+  0.0149  htrnr  10001901  0.0149  htrnr  10002001
*+  0.0149  htrnr  10002101  0.0149  htrnr  10002201
*+  0.0149  htrnr  10002301  0.0149  htrnr  10002401
*+  0.0149  htrnr  10002501
*
*20514170  h1020-1  sum  1.0  0.0  1
*20514171  0.0  0.0139  htrnr  20000101  0.0139  htrnr  20000201
*20514172  0.0139  htrnr  20000301  0.0139  htrnr  20000401
*20514173  0.0139  htrnr  20000501  0.0139  htrnr  20000601
*20514174  0.0139  htrnr  20000701  0.0139  htrnr  20000801
*20514175  0.0139  htrnr  20000901  0.0139  htrnr  20001001
*20514176  0.0139  htrnr  20001101  0.0139  htrnr  20001201
*20514177  0.0139  htrnr  20001301  0.0139  htrnr  20001401

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*20514178 0.0139 htrnr 20001501 0.0139 htrnr 20001601
*+ 0.0139 htrnr 20001701 0.0139 htrnr 20001801
*+ 0.0139 htrnr 20001901 0.0139 htrnr 20002001
*+ 0.0139 htrnr 20002101 0.0139 htrnr 20002201
*+ 0.0139 htrnr 20002301 0.0139 htrnr 20002401
*+ 0.0139 htrnr 20002501 0.0139 htrnr 20002601
*+ 0.0139 htrnr 20002701 0.0139 htrnr 20002801
*+ 0.0139 htrnr 20002901 0.0139 htrnr 20003001
*+ 0.0139 htrnr 20003101 0.0139 htrnr 20003201
*+ 0.0139 htrnr 20003301 0.0139 htrnr 20003401
*+ 0.0139 htrnr 20003501
*
*20514180 hl030-1 sum 1.0 0.0 1
*20514181 0.0 0.0136 htrnr 30000101 0.0136 htrnr 30000201
*20514182 0.0136 htrnr 30000301 0.0136 htrnr 30000401
*20514183 0.0136 htrnr 30000501 0.0136 htrnr 30000601
*20514184 0.0136 htrnr 30000701 0.0136 htrnr 30000801
*20514185 0.0136 htrnr 30000901 0.0136 htrnr 30001001
*20514186 0.0136 htrnr 30001101 0.0136 htrnr 30001201
*20514187 0.0136 htrnr 30001301 0.0136 htrnr 30001401
*20514188 0.0136 htrnr 30001501 0.0136 htrnr 30001601
*+ 0.0136 htrnr 30001701 0.0136 htrnr 30001801
*+ 0.0136 htrnr 30001901 0.0136 htrnr 30002001
*+ 0.0136 htrnr 30002101 0.0136 htrnr 30002201
*+ 0.0136 htrnr 30002301 0.0136 htrnr 30002401
*+ 0.0136 htrnr 30002501 0.0136 htrnr 30002601
*+ 0.0136 htrnr 30002701 0.0136 htrnr 30002801
*+ 0.0136 htrnr 30002901 0.0136 htrnr 30003001
*+ 0.0136 htrnr 30003101 0.0136 htrnr 30003201
*+ 0.0136 htrnr 30003301 0.0136 htrnr 30003401
*+ 0.0136 htrnr 30003501 0.0136 htrnr 30003601
*+ 0.0136 htrnr 30003701 0.0136 htrnr 30003801
*+ 0.0136 htrnr 30003901 0.0136 htrnr 30004001
*
*20514190 hl030-2 sum 1.0 0.0 1
*20514191 0.0 0.0136 htrnr 30004101 0.0136 htrnr 30004201
*20514192 0.0136 htrnr 30004301 0.0136 htrnr 30004401
*20514193 0.0136 htrnr 30004501 0.0136 htrnr 30004601
*20514194 0.0136 htrnr 30004701 0.0136 htrnr 30004801
*20514195 0.0136 htrnr 30004901 0.0136 htrnr 30005001
*20514196 0.0136 htrnr 30005101 0.0136 htrnr 30005201
*20514197 0.0136 htrnr 30005301 0.0136 htrnr 30005401
*20514198 0.0136 htrnr 30005501 0.0136 htrnr 30005601
*+ 0.0136 htrnr 30005701 0.0136 htrnr 30005801
*+ 0.0136 htrnr 30005901 0.0136 htrnr 30006001
*+ 0.0136 htrnr 30006101 0.0136 htrnr 30006201
*+ 0.0136 htrnr 30006301 0.0136 htrnr 30006401
*+ 0.0136 htrnr 30006501 0.0136 htrnr 30006601
*+ 0.0136 htrnr 30006701 0.0136 htrnr 30006801
*+ 0.0136 htrnr 30006901 0.0136 htrnr 30007001
*+ 0.0136 htrnr 30007101 0.0136 htrnr 30007201
*+ 0.0136 htrnr 30007301 0.0136 htrnr 30007401
*+ 0.0136 htrnr 30007501 0.0136 htrnr 30007601
*+ 0.0136 htrnr 30007701 0.0136 htrnr 30007801
*+ 0.0136 htrnr 30007901 0.0136 htrnr 30008001
*
*20514200 hl030-3 sum 1.0 0.0 1
*20514201 0.0 0.0136 htrnr 30008101 0.0136 htrnr 30008201
*20514202 0.0136 htrnr 30008301 0.0136 htrnr 30008401
*20514203 0.0136 htrnr 30008501 0.0136 htrnr 30008601
*20514204 0.0136 htrnr 30008701 0.0136 htrnr 30008801
*20514205 0.0136 htrnr 30008901 0.0136 htrnr 30009001
*20514206 0.0136 htrnr 30009101 0.0136 htrnr 30009201

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*
*20514210 hs030ehl sum 1.0 0.0 1
*20514211 0.0 1.0 cntrlvar 1418 1.0 cntrlvar 1419
*20514212 1.0 cntrlvar 1420
*
*20514220 hl032-1 sum 1.0 0.0 1
*20514221 0.0 0.0136 htrnr 32000101 0.0136 htrnr 32000201
*20514222 0.0136 htrnr 32000301 0.0136 htrnr 32000401
*20514223 0.0136 htrnr 32000501 0.0136 htrnr 32000601
*20514224 0.0136 htrnr 32000701 0.0136 htrnr 32000801
*20514225 0.0136 htrnr 32000901 0.0136 htrnr 32001001
*20514226 0.0136 htrnr 32001101 0.0136 htrnr 32001201
*20514227 0.0136 htrnr 32001301 0.0136 htrnr 32001401
*20514228 0.0136 htrnr 32001501 0.0136 htrnr 32001601
*+ 0.0136 htrnr 32001701 0.0136 htrnr 32001801
*+ 0.0136 htrnr 32001901 0.0136 htrnr 32002001
*+ 0.0136 htrnr 32002101 0.0136 htrnr 32002201
*+ 0.0136 htrnr 32002301 0.0136 htrnr 32002401
*+ 0.0136 htrnr 32002501 0.0136 htrnr 32002601
*+ 0.0136 htrnr 32002701 0.0136 htrnr 32002801
*+ 0.0136 htrnr 32002901 0.0136 htrnr 32003001
*+ 0.0136 htrnr 32003101 0.0136 htrnr 32003201
*+ 0.0136 htrnr 32003301 0.0136 htrnr 32003401
*+ 0.0136 htrnr 32003501 0.0136 htrnr 32003601
*+ 0.0136 htrnr 32003701 0.0136 htrnr 32003801
*+ 0.0136 htrnr 32003901 0.0136 htrnr 32004001
*
*20514230 hl032-2 sum 1.0 0.0 1
*20514231 0.0 0.0136 htrnr 32004101 0.0136 htrnr 32004201
*20514232 0.0136 htrnr 32004301 0.0136 htrnr 32004401
*20514233 0.0136 htrnr 32004501 0.0136 htrnr 32004601
*20514234 0.0136 htrnr 32004701 0.0136 htrnr 32004801
*20514235 0.0136 htrnr 32004901 0.0136 htrnr 32005001
*20514236 0.0136 htrnr 32005101 0.0136 htrnr 32005201
*20514237 0.0136 htrnr 32005301 0.0136 htrnr 32005401
*20514238 0.0136 htrnr 32005501 0.0136 htrnr 32005601
*+ 0.0136 htrnr 32005701 0.0136 htrnr 32005801
*+ 0.0136 htrnr 32005901 0.0136 htrnr 32006001
*+ 0.0136 htrnr 32006101 0.0136 htrnr 32006201
*+ 0.0136 htrnr 32006301 0.0136 htrnr 32006401
*+ 0.0136 htrnr 32006501 0.0136 htrnr 32006601
*+ 0.0136 htrnr 32006701 0.0136 htrnr 32006801
*+ 0.0136 htrnr 32006901 0.0136 htrnr 32007001
*+ 0.0136 htrnr 32007101 0.0136 htrnr 32007201
*+ 0.0136 htrnr 32007301 0.0136 htrnr 32007401
*+ 0.0136 htrnr 32007501 0.0136 htrnr 32007601
*+ 0.0136 htrnr 32007701 0.0136 htrnr 32007801
*+ 0.0136 htrnr 32007901 0.0136 htrnr 32008001
*
*20514240 hl032-3 sum 1.0 0.0 1
*20514241 0.0 0.0136 htrnr 32008101 0.0136 htrnr 32008201
*20514242 0.0136 htrnr 32008301 0.0136 htrnr 32008401
*20514243 0.0136 htrnr 32008501 0.0136 htrnr 32008601
*20514244 0.0136 htrnr 32008701 0.0136 htrnr 32008801
*20514245 0.0136 htrnr 32008901 0.0136 htrnr 32009001
*20514246 0.0136 htrnr 32009101 0.0136 htrnr 32009201
*
*20514250 hs032ehl sum 1.0 0.0 1
*20514251 0.0 1.0 cntrlvar 1422 1.0 cntrlvar 1423
*20514252 1.0 cntrlvar 1424
*
*20514260 hl034-1 sum 1.0 0.0 1
*20514261 0.0 0.0136 htrnr 34000101 0.0136 htrnr 34000201

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*20514262 0.0136 htrnr 34000301 0.0136 htrnr 34000401
*20514263 0.0136 htrnr 34000501 0.0136 htrnr 34000601
*20514264 0.0136 htrnr 34000701 0.0136 htrnr 34000801
*20514265 0.0136 htrnr 34000901 0.0136 htrnr 34001001
*20514266 0.0136 htrnr 34001101 0.0136 htrnr 34001201
*20514267 0.0136 htrnr 34001301 0.0136 htrnr 34001401
*20514268 0.0136 htrnr 34001501 0.0136 htrnr 34001601
*+ 0.0136 htrnr 34001701 0.0136 htrnr 34001801
*+ 0.0136 htrnr 34001901 0.0136 htrnr 34002001
*+ 0.0136 htrnr 34002101 0.0136 htrnr 34002201
*+ 0.0136 htrnr 34002301 0.0136 htrnr 34002401
*+ 0.0136 htrnr 34002501 0.0136 htrnr 34002601
*+ 0.0136 htrnr 34002701 0.0136 htrnr 34002801
*+ 0.0136 htrnr 34002901 0.0136 htrnr 34003001
*+ 0.0136 htrnr 34003101 0.0136 htrnr 34003201
*+ 0.0136 htrnr 34003301 0.0136 htrnr 34003401
*+ 0.0136 htrnr 34003501 0.0136 htrnr 34003601
*+ 0.0136 htrnr 34003701 0.0136 htrnr 34003801
*+ 0.0136 htrnr 34003901 0.0136 htrnr 34004001
*
*20514270 hl034-2 sum 1.0 0.0 1
*20514271 0.0 0.0136 htrnr 34004101 0.0136 htrnr 34004201
*20514272 0.0136 htrnr 34004301 0.0136 htrnr 34004401
*20514273 0.0136 htrnr 34004501 0.0136 htrnr 34004601
*20514274 0.0136 htrnr 34004701 0.0136 htrnr 34004801
*20514275 0.0136 htrnr 34004901 0.0136 htrnr 34005001
*20514276 0.0136 htrnr 34005101 0.0136 htrnr 34005201
*20514277 0.0136 htrnr 34005301 0.0136 htrnr 34005401
*20514278 0.0136 htrnr 34005501 0.0136 htrnr 34005601
*+ 0.0136 htrnr 34005701 0.0136 htrnr 34005801
*+ 0.0136 htrnr 34005901 0.0136 htrnr 34006001
*+ 0.0136 htrnr 34006101 0.0136 htrnr 34006201
*+ 0.0136 htrnr 34006301 0.0136 htrnr 34006401
*+ 0.0136 htrnr 34006501 0.0136 htrnr 34006601
*+ 0.0136 htrnr 34006701 0.0136 htrnr 34006801
*+ 0.0136 htrnr 34006901 0.0136 htrnr 34007001
*+ 0.0136 htrnr 34007101 0.0136 htrnr 34007201
*+ 0.0136 htrnr 34007301 0.0136 htrnr 34007401
*+ 0.0136 htrnr 34007501 0.0136 htrnr 34007601
*+ 0.0136 htrnr 34007701 0.0136 htrnr 34007801
*+ 0.0136 htrnr 34007901 0.0136 htrnr 34008001
*
*20514280 hl034-3 sum 1.0 0.0 1
*20514281 0.0 0.0136 htrnr 34008101 0.0136 htrnr 34008201
*20514282 0.0136 htrnr 34008301 0.0136 htrnr 34008401
*20514283 0.0136 htrnr 34008501 0.0136 htrnr 34008601
*20514284 0.0136 htrnr 34008701 0.0136 htrnr 34008801
*20514285 0.0136 htrnr 34008901 0.0136 htrnr 34009001
*20514286 0.0136 htrnr 34009101 0.0136 htrnr 34009201
*
*20514290 hs034ehl sum 1.0 0.0 1
*20514291 0.0 1.0 cntrlvar 1426 1.0 cntrlvar 1427
*20514292 1.0 cntrlvar 1428
*
*20514300 CRDbkehl sum 1.0 0.0 1
*20514301 0.0 1.0 cntrlvar 1416 1.0 cntrlvar 1417
*20514302 1.0 cntrlvar 1421 1.0 cntrlvar 1425
*20514303 1.0 cntrlvar 1429
*
* use the cards below for a vessel bottom break
*20514310 hl070-1 sum 1.0 0.0 1
*20514311 0.0 0.0137 htrnr 70000101 0.0137 htrnr 70000201
*20514312 0.0137 htrnr 70000301 0.0137 htrnr 70000401

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*20514313 0.0137 htrnr 70000501 0.0137 htrnr 70000601
*20514314 0.0137 htrnr 70000701 0.0137 htrnr 70000801
*20514315 0.0137 htrnr 70000901 0.0137 htrnr 70001001
*20514316 0.0137 htrnr 70001101 0.0137 htrnr 70001201
*20514317 0.0137 htrnr 70001301 0.0137 htrnr 70001401
*20514318 0.0137 htrnr 70001501 0.0137 htrnr 70001601
*+ 0.0137 htrnr 70001701 0.0137 htrnr 70001801
*+ 0.0137 htrnr 70001901 0.0137 htrnr 70002001
*+ 0.0137 htrnr 70002101 0.0137 htrnr 70002201
*+ 0.0137 htrnr 70002301 0.0137 htrnr 70002401
*+ 0.0137 htrnr 70002501 0.0137 htrnr 70002601
*+ 0.0137 htrnr 70002701 0.0137 htrnr 70002801
*+ 0.0137 htrnr 70002901 0.0137 htrnr 70003001
*+ 0.0137 htrnr 70003101 0.0137 htrnr 70003201
*+ 0.0137 htrnr 70003301 0.0137 htrnr 70003401
*+ 0.0137 htrnr 70003501 0.0137 htrnr 70003601
*+ 0.0137 htrnr 70003701 0.0137 htrnr 70003801
*+ 0.0137 htrnr 70003901 0.0137 htrnr 70004001
*
*20514320 hl070-2 sum 1.0 0.0 1
*20514321 0.0 0.0137 htrnr 70004101 0.0137 htrnr 70004201
*20514322 0.0137 htrnr 70004301 0.0137 htrnr 70004401
*20514323 0.0137 htrnr 70004501 0.0137 htrnr 70004601
*20514324 0.0137 htrnr 70004701 0.0137 htrnr 70004801
*20514325 0.0137 htrnr 70004901 0.0137 htrnr 70005001
*20514326 0.0137 htrnr 70005101 0.0137 htrnr 70005201
*20514327 0.0137 htrnr 70005301 0.0137 htrnr 70005401
*20514328 0.0137 htrnr 70005501 0.0137 htrnr 70005601
*+ 0.0137 htrnr 70005701 0.0137 htrnr 70005801
*+ 0.0137 htrnr 70005901 0.0137 htrnr 70006001
*+ 0.0137 htrnr 70006101 0.0137 htrnr 70006201
*+ 0.0137 htrnr 70006301 0.0137 htrnr 70006401
*+ 0.0137 htrnr 70006501 0.0137 htrnr 70006601
*+ 0.0137 htrnr 70006701 0.0137 htrnr 70006801
*+ 0.0137 htrnr 70006901 0.0137 htrnr 70007001
*+ 0.0137 htrnr 70007101 0.0137 htrnr 70007201
*+ 0.0137 htrnr 70007301
*
*20514330 hs070ehl sum 1.0 0.0 1
*20514331 0.0 1.0 cntrlvar 1431 1.0 cntrlvar 1432
*
*20514340 hl072-1 sum 1.0 0.0 1
*20514341 0.0 0.0137 htrnr 72000101 0.0137 htrnr 72000201
*20514342 0.0137 htrnr 72000301 0.0137 htrnr 72000401
*20514343 0.0137 htrnr 72000501 0.0137 htrnr 72000601
*20514344 0.0137 htrnr 72000701 0.0137 htrnr 72000801
*20514345 0.0137 htrnr 72000901 0.0137 htrnr 72001001
*20514346 0.0137 htrnr 72001101 0.0137 htrnr 72001201
*20514347 0.0137 htrnr 72001301 0.0137 htrnr 72001401
*20514348 0.0137 htrnr 72001501 0.0137 htrnr 72001601
*+ 0.0137 htrnr 72001701 0.0137 htrnr 72001801
*+ 0.0137 htrnr 72001901 0.0137 htrnr 72002001
*+ 0.0137 htrnr 72002101 0.0137 htrnr 72002201
*+ 0.0137 htrnr 72002301 0.0137 htrnr 72002401
*+ 0.0137 htrnr 72002501 0.0137 htrnr 72002601
*+ 0.0137 htrnr 72002701 0.0137 htrnr 72002801
*+ 0.0137 htrnr 72002901 0.0137 htrnr 72003001
*+ 0.0137 htrnr 72003101 0.0137 htrnr 72003201
*+ 0.0137 htrnr 72003301 0.0137 htrnr 72003401
*+ 0.0137 htrnr 72003501 0.0137 htrnr 72003601
*+ 0.0137 htrnr 72003701 0.0137 htrnr 72003801
*+ 0.0137 htrnr 72003901 0.0137 htrnr 72004001
*

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*20514350 hl072-2 sum 1.0 0.0 1
*20514351 0.0 0.0137 htrnr 72004101 0.0137 htrnr 72004201
*20514352 0.0137 htrnr 72004301 0.0137 htrnr 72004401
*20514353 0.0137 htrnr 72004501 0.0137 htrnr 72004601
*20514354 0.0137 htrnr 72004701 0.0137 htrnr 72004801
*20514355 0.0137 htrnr 72004901 0.0137 htrnr 72005001
*20514356 0.0137 htrnr 72005101 0.0137 htrnr 72005201
*20514357 0.0137 htrnr 72005301 0.0137 htrnr 72005401
*20514358 0.0137 htrnr 72005501 0.0137 htrnr 72005601
*+ 0.0137 htrnr 72005701 0.0137 htrnr 72005801
*+ 0.0137 htrnr 72005901 0.0137 htrnr 72006001
*+ 0.0137 htrnr 72006101 0.0137 htrnr 72006201
*+ 0.0137 htrnr 72006301 0.0137 htrnr 72006401
*+ 0.0137 htrnr 72006501 0.0137 htrnr 72006601
*+ 0.0137 htrnr 72006701 0.0137 htrnr 72006801
*+ 0.0137 htrnr 72006901 0.0137 htrnr 72007001
*+ 0.0137 htrnr 72007101 0.0137 htrnr 72007201
*+ 0.0137 htrnr 72007301
*
*20514360 hs072ehl sum 1.0 0.0 1
*20514361 0.0 1.0 cntrlvar 1434 1.0 cntrlvar 1435
*
*20514370 hl080-1 sum 1.0 0.0 1
*20514371 0.0 0.0136 htrnr 80000101 0.0136 htrnr 80000201
*20514372 0.0136 htrnr 80000301 0.0136 htrnr 80000401
*20514373 0.0136 htrnr 80000501 0.0136 htrnr 80000601
*20514374 0.0136 htrnr 80000701 0.0136 htrnr 80000801
*20514375 0.0136 htrnr 80000901 0.0136 htrnr 80001001
*20514376 0.0136 htrnr 80001101 0.0136 htrnr 80001201
*20514377 0.0136 htrnr 80001301 0.0136 htrnr 80001401
*20514378 0.0136 htrnr 80001501 0.0136 htrnr 80001601
*+ 0.0136 htrnr 80001701 0.0136 htrnr 80001801
*+ 0.0136 htrnr 80001901 0.0136 htrnr 80002001
*+ 0.0136 htrnr 80002101 0.0136 htrnr 80002201
*+ 0.0136 htrnr 80002301 0.0136 htrnr 80002401
*+ 0.0136 htrnr 80002501 0.0136 htrnr 80002601
*+ 0.0136 htrnr 80002701 0.0136 htrnr 80002801
*+ 0.0136 htrnr 80002901 0.0136 htrnr 80003001
*+ 0.0136 htrnr 80003101 0.0136 htrnr 80003201
*+ 0.0136 htrnr 80003301 0.0136 htrnr 80003401
*+ 0.0136 htrnr 80003501 0.0136 htrnr 80003601
*+ 0.0136 htrnr 80003701 0.0136 htrnr 80003801
*+ 0.0136 htrnr 80003901 0.0136 htrnr 80004001
*
*20514380 hl080-2 sum 1.0 0.0 1
*20514381 0.0 0.0136 htrnr 80004101 0.0136 htrnr 80004201
*20514382 0.0136 htrnr 80004301 0.0136 htrnr 80004401
*20514383 0.0136 htrnr 80004501 0.0136 htrnr 80004601
*20514384 0.0136 htrnr 80004701 0.0136 htrnr 80004801
*20514385 0.0136 htrnr 80004901 0.0136 htrnr 80005001
*20514386 0.0136 htrnr 80005101 0.0136 htrnr 80005201
*20514387 0.0136 htrnr 80005301 0.0136 htrnr 80005401
*20514388 0.0136 htrnr 80005501 0.0136 htrnr 80005601
*+ 0.0136 htrnr 80005701 0.0136 htrnr 80005801
*+ 0.0136 htrnr 80005901 0.0136 htrnr 80006001
*+ 0.0136 htrnr 80006101 0.0136 htrnr 80006201
*+ 0.0136 htrnr 80006301 0.0136 htrnr 80006401
*+ 0.0136 htrnr 80006501 0.0136 htrnr 80006601
*+ 0.0136 htrnr 80006701 0.0136 htrnr 80006801
*+ 0.0136 htrnr 80006901 0.0136 htrnr 80007001
*+ 0.0136 htrnr 80007101 0.0136 htrnr 80007201
*+ 0.0136 htrnr 80007301 0.0136 htrnr 80007401
*+ 0.0136 htrnr 80007501 0.0136 htrnr 80007601

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*+ 0.0136 htrnr 80007701 0.0136 htrnr 80007801
*+ 0.0136 htrnr 80007901 0.0136 htrnr 80008001
*
*20514390 hl080-3 sum 1.0 0.0 1
*20514391 0.0 0.0136 htrnr 80008101 0.0136 htrnr 80008201
*20514392 0.0136 htrnr 80008301 0.0136 htrnr 80008401
*20514393 0.0136 htrnr 80008501 0.0136 htrnr 80008601
*20514394 0.0136 htrnr 80008701 0.0136 htrnr 80008801
*20514395 0.0136 htrnr 80008901 0.0136 htrnr 80009001
*20514396 0.0136 htrnr 80009101 0.0136 htrnr 80009201
*20514397 0.0136 htrnr 80009301 0.0136 htrnr 80009401
*20514398 0.0136 htrnr 80009501 0.0136 htrnr 80009601
*
*20514400 hs080ehl sum 1.0 0.0 1
*20514401 0.0 1.0 cntrlvar 1437 1.0 cntrlvar 1438
*20514402 1.0 cntrlvar 1439
*
*20514410 vbtbkehl sum 1.0 0.0 1
*20514411 0.0 1.0 cntrlvar 1436 1.0 cntrlvar 1440
*
20514440 pipeehl sum 1.0 0.0 1
20514441 0.0 1.0 cntrlvar 1401 1.0 cntrlvar 1403
20514442 1.0 cntrlvar 1406 1.0 cntrlvar 1407
20514443 1.0 cntrlvar 1408 1.0 cntrlvar 1409
20514444 1.0 cntrlvar 1411 1.0 cntrlvar 1412
*
20514450 SGehl sum 1.0 0.0 1
20514451 0.0 1.0 cntrlvar 1404 1.0 cntrlvar 1405
20514452 1.0 cntrlvar 1414 1.0 cntrlvar 1415
*
20514460 PCSehl sum 1.0 0.0 1
20514461 0.0 1.0 cntrlvar 1444 1.0 cntrlvar 1404
20514462 1.0 cntrlvar 1405 1.0 cntrlvar 1413
* add the card below if the vessel CRD break line is included in the model
*20514463 1.0 cntrlvar 1430
* add the card below if the vessel bottom break line is included in the model
*20514463 1.0 cntrlvar 1441
* add the card below if both vessel break lines are included in the model
*20514463 1.0 cntrlvar 1430 1.0 cntrlvar 1441
*
20514470 SCSehl sum 1.0 0.0 1
20514471 0.0 1.0 cntrlvar 1414 1.0 cntrlvar 1415
*
20514490 totalehl sum 1.0 0.0 1
20514491 0.0 1.0 cntrlvar 1446 1.0 cntrlvar 1447
*
20514500 toflehlq integral 1.0 0.0 0
20514501 cntrlvar 1449
*
* system mass variables
*
20516010 mass140 sum 1.0 0.0 1
20516011 0.0 1.0 tmassv 140010000 1.0 tmassv 140020000
20516012 1.0 tmassv 140030000 1.0 tmassv 140040000
20516013 1.0 tmassv 140050000 1.0 tmassv 140060000
20516014 1.0 tmassv 140070000 1.0 tmassv 140080000
20516015 1.0 tmassv 140090000 1.0 tmassv 140100000
20516016 1.0 tmassv 140110000 1.0 tmassv 140120000
20516017 1.0 tmassv 140130000 1.0 tmassv 140140000
*
20516020 mass145 sum 1.0 0.0 1
20516021 0.0 1.0 tmassv 145010000 1.0 tmassv 145020000
20516022 1.0 tmassv 145030000 1.0 tmassv 145040000

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20516023 1.0 tmassv 145050000 1.0 tmassv 145060000
20516024 1.0 tmassv 145070000 1.0 tmassv 145080000
20516025 1.0 tmassv 145090000 1.0 tmassv 145100000
20516026 1.0 tmassv 145110000 1.0 tmassv 145120000
20516027 1.0 tmassv 145130000 1.0 tmassv 145140000
*
20516030 mass150 sum 1.0 0.0 1
20516031 0.0 1.0 tmassv 150010000 1.0 tmassv 150020000
20516032 1.0 tmassv 150030000 1.0 tmassv 150040000
20516033 1.0 tmassv 150050000 1.0 tmassv 150060000
20516034 1.0 tmassv 150070000 1.0 tmassv 150080000
20516035 1.0 tmassv 150090000 1.0 tmassv 150100000
20516036 1.0 tmassv 150110000 1.0 tmassv 150120000
20516037 1.0 tmassv 150130000 1.0 tmassv 150140000
*
20516040 mass132 sum 1.0 0.0 1
20516041 0.0 1.0 tmassv 132010000 1.0 tmassv 132020000
20516042 1.0 tmassv 132030000 1.0 tmassv 132040000
20516043 1.0 tmassv 132050000 1.0 tmassv 132060000
20516044 1.0 tmassv 132070000 1.0 tmassv 132080000
20516045 1.0 tmassv 132090000 1.0 tmassv 132100000
20516046 1.0 tmassv 132110000 1.0 tmassv 132120000
20516047 1.0 tmassv 132130000 1.0 tmassv 132140000
*
20516050 mass162 sum 1.0 0.0 1
20516051 0.0 1.0 tmassv 162010000 1.0 tmassv 162020000
20516052 1.0 tmassv 162030000 1.0 tmassv 162040000
20516053 1.0 tmassv 162050000 1.0 tmassv 162060000
20516054 1.0 tmassv 162070000 1.0 tmassv 162080000
20516055 1.0 tmassv 162090000 1.0 tmassv 162100000
20516056 1.0 tmassv 162110000 1.0 tmassv 162120000
20516057 1.0 tmassv 162130000 1.0 tmassv 162140000
*
20516060 mass164 sum 1.0 0.0 1
20516061 0.0 1.0 tmassv 164010000 1.0 tmassv 164020000
20516062 1.0 tmassv 164030000 1.0 tmassv 164040000
20516063 1.0 tmassv 164050000 1.0 tmassv 164060000
20516064 1.0 tmassv 164070000 1.0 tmassv 164080000
20516065 1.0 tmassv 164090000 1.0 tmassv 164100000
20516066 1.0 tmassv 164110000 1.0 tmassv 164120000
20516067 1.0 tmassv 164130000 1.0 tmassv 164140000
*
20516070 mass166 sum 1.0 0.0 1
20516071 0.0 1.0 tmassv 166010000 1.0 tmassv 166020000
20516072 1.0 tmassv 166030000 1.0 tmassv 166040000
20516073 1.0 tmassv 166050000 1.0 tmassv 166060000
20516074 1.0 tmassv 166070000 1.0 tmassv 166080000
20516075 1.0 tmassv 166090000 1.0 tmassv 166100000
20516076 1.0 tmassv 166110000 1.0 tmassv 166120000
20516077 1.0 tmassv 166130000 1.0 tmassv 166140000
*
20516080 masscore sum 1.0 0.0 1
20516081 0.0 1.0 cntrlvar 1601 1.0 cntrlvar 1602
20516082 1.0 cntrlvar 1603 1.0 cntrlvar 1604
20516083 1.0 cntrlvar 1605 1.0 cntrlvar 1606
20516084 1.0 cntrlvar 1607
*
20516090 mass115 sum 1.0 0.0 1
20516091 0.0 1.0 tmassv 115010000 1.0 tmassv 115020000
20516092 1.0 tmassv 115030000 1.0 tmassv 115040000
20516093 1.0 tmassv 115050000 1.0 tmassv 115060000
20516094 1.0 tmassv 115070000 1.0 tmassv 115080000
20516095 1.0 tmassv 115090000 1.0 tmassv 115100000

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20516096 1.0 tmassv 115110000 1.0 tmassv 115120000
20516097 1.0 tmassv 115130000 1.0 tmassv 115140000
20516098 1.0 tmassv 115150000
*
20516100 massrv1 sum 1.0 0.0 1
20516101 0.0 1.0 tmassv 100010000 1.0 tmassv 105010000
20516102 1.0 tmassv 105020000 1.0 tmassv 110010000
20516103 1.0 tmassv 120010000 1.0 tmassv 175010000
*
20516110 massRV sum 1.0 0.0 1
20516111 0.0 1.0 cntrlvar 1608 1.0 cntrlvar 1609
20516112 1.0 cntrlvar 1610
*
20516150 masshleg sum 1.0 0.0 1
20516151 0.0 1.0 tmassv 200010000 1.0 tmassv 200020000
20516152 1.0 tmassv 200030000 1.0 tmassv 200040000
20516153 1.0 tmassv 200050000 1.0 tmassv 200060000
20516154 1.0 tmassv 215010000
*
20516160 massSGp sum 1.0 0.0 1
20516161 0.0 1.0 tmassv 220010000 1.0 tmassv 228010000
20516162 1.0 tmassv 225010000 1.0 tmassv 225020000
20516163 1.0 tmassv 225030000 1.0 tmassv 225040000
20516164 1.0 tmassv 225050000 1.0 tmassv 225060000
20516165 1.0 tmassv 225070000 1.0 tmassv 225080000
20516166 1.0 tmassv 225090000 1.0 tmassv 225100000
20516167 1.0 tmassv 225110000 1.0 tmassv 225120000
20516168 1.0 tmassv 225130000 1.0 tmassv 225140000
+ 1.0 tmassv 225150000 1.0 tmassv 225160000
+ 1.0 tmassv 225170000 1.0 tmassv 225180000
+ 1.0 tmassv 225190000 1.0 tmassv 225200000
+ 1.0 tmassv 225210000 1.0 tmassv 225220000
*
20516170 masscleg sum 1.0 0.0 1
20516171 0.0 1.0 tmassv 230010000 1.0 tmassv 235010000
20516172 1.0 tmassv 240010000 1.0 tmassv 250010000
20516173 1.0 tmassv 250020000 1.0 tmassv 250030000
20516174 1.0 tmassv 260010000 1.0 tmassv 270010000
20516175 1.0 tmassv 270020000 1.0 tmassv 270030000
20516176 1.0 tmassv 270040000 1.0 tmassv 293010000
*
20516180 massloop sum 1.0 0.0 1
20516181 0.0 1.0 cntrlvar 1615 1.0 cntrlvar 1616
20516182 1.0 cntrlvar 1617
*
20516190 massPCS sum 1.0 0.0 1
20516191 0.0 1.0 cntrlvar 1611 1.0 cntrlvar 1618
*
20516210 massRCST sum 1.0 0.0 1
20516211 0.0 1.0 tmassv 210010000 1.0 tmassv 258010000
20516212 1.0 tmassv 280010000 1.0 tmassv 280020000
* replace the card above with the one below when using the single-volume RCST
*20516212 1.0 tmassv 280010000
*
20516260 massSGs sum 1.0 0.0 1
20516261 0.0 1.0 tmassv 340010000 1.0 tmassv 340020000
20516262 1.0 tmassv 340030000 1.0 tmassv 340040000
20516263 1.0 tmassv 340050000 1.0 tmassv 340060000
20516264 1.0 tmassv 340070000 1.0 tmassv 340080000
20516265 1.0 tmassv 340090000 1.0 tmassv 340100000
20516266 1.0 tmassv 340110000 1.0 tmassv 350010000
20516267 1.0 tmassv 350020000 1.0 tmassv 350030000
20516268 1.0 tmassv 350040000 1.0 tmassv 350050000

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+ 1.0 tmassv 350060000 1.0 tmassv 350070000
+ 1.0 tmassv 350080000 1.0 tmassv 350090000
+ 1.0 tmassv 350100000 1.0 tmassv 350110000
+ 1.0 tmassv 350120000 1.0 tmassv 350130000
+ 1.0 tmassv 355010000 1.0 tmassv 360010000
*
20516270 massSCS sum 1.0 0.0 1
20516271 0.0 1.0 cntrlvar 1626 1.0 tmassv 330010000
20516272 1.0 tmassv 365010000 1.0 tmassv 390010000
*
20516310 mass950 sum 1.0 0.0 1
20516311 0.0 1.0 tmassv 950010000 1.0 tmassv 950020000
20516312 1.0 tmassv 950030000 1.0 tmassv 950040000
20516313 1.0 tmassv 950050000 1.0 tmassv 950060000
20516314 1.0 tmassv 950070000 1.0 tmassv 950080000
20516315 1.0 tmassv 950090000 1.0 tmassv 950100000
20516316 1.0 tmassv 950110000 1.0 tmassv 950120000
20516317 1.0 tmassv 950130000 1.0 tmassv 950140000
20516318 1.0 tmassv 950150000 1.0 tmassv 950160000
+ 1.0 tmassv 950170000 1.0 tmassv 950180000
+ 1.0 tmassv 950190000
*
20516320 massRCCS sum 1.0 0.0 1
20516321 0.0 1.0 cntrlvar 1631 1.0 tmassv 930010000
20516322 1.0 tmassv 940010000 1.0 tmassv 945010000
20516323 1.0 tmassv 955010000 1.0 tmassv 960010000
*
20516360 mass450 sum 1.0 0.0 1
20516361 0.0 1.0 tmassv 450010000 1.0 tmassv 450020000
20516362 1.0 tmassv 450030000 1.0 tmassv 450040000
20516363 1.0 tmassv 450050000 1.0 tmassv 450060000
*
20516370 massPWS sum 1.0 0.0 1
20516371 0.0 1.0 cntrlvar 1636 1.0 tmassv 420010000
20516372 1.0 tmassv 460010000 1.0 tmassv 490010000
*
20516400 massWS sum 1.0 0.0 1
20516401 0.0 1.0 cntrlvar 1627 1.0 cntrlvar 1632
20516402 1.0 cntrlvar 1637
*
* variables for scaling assessments
*
20520010 ch115dp sum 1.0 0.0 1
20520011 0.0 1.0 p 115010000 -1.0 p 115140000
*
20520020 ch115pav sum 1.0 0.0 1
20520021 0.0 0.5 p 115010000 0.5 p 115140000
*
20520030 ch115dt sum 1.0 0.0 1
20520031 0.0 1.0 tempg 115140000 -1.0 tempg 115010000
*
20520040 ch115tav sum 1.0 0.0 1
20520041 0.0 0.5 tempg 115140000 0.5 tempg 115010000
*
20520050 ch115rhv sum 1.0 0.0 1
20520051 0.0 0.5 rhog 115140000 0.5 rhog 115010000
*
20520060 ch115Cpt mult 1.0 0.0 1
20520061 csubpg 115010000
*
20520070 ch115Cpb mult 1.0 0.0 1
20520071 csubpg 115140000
*

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```

20520080 ch115Cpa sum 1.0 0.0 1
20520081 0.0 0.5 csubpg 115140000 0.5 csubpg 115010000
*
20520090 ch115vsm mult 1.0 1.0E-05 1
20520091 viscg 115080000
*
20520100 ch115ivs div 1.0 1.0E+05 1
20520101 viscg 115080000
*
20520110 ch115Bm mult 1.0 0.0 1
20520111 betagg 115080000
*
20520120 ch115Cpm mult 1.0 0.0 1
20520121 csubpg 115080000
*
20520130 ch115tcm mult 1.0 0.0 1
20520131 thcong 115080000
*
20520140 ch115itc div 1.0 0.0 1
20520141 thcong 115080000
*
20520150 ch115dTw sum 1.0 0.0 1
20520151 0.0 1.0 httemp 115001005 -1.0 tempg 115100000
*
20520160 ch115Gm mult 1.0 0.0 1
20520161 rhog 115080000 velg 115080000
*
20520170 ch115Re mult 0.11430 0.0 1
20520171 cntrlvar 2016 cntrlvar 2010
*
20520180 ch115Nu mult 0.11430 0.0 1
20520181 hthtc 115001001 cntrlvar 2014
*
20520190 ch115Pr mult 1.0 0.0 1
20520191 csubpg 115080000 viscg 115080000 cntrlvar 2014
*
20520200 ch115Gr mult 394.55 0.0 1
20520201 betagg 115080000 cntrlvar 2015 rhog 115080000
20520202 rhog 115080000 cntrlvar 2010 cntrlvar 2010
*
20520210 ch115Fr poweri 0.8927 0.0 1
20520211 velg 115080000 2
*
20520220 ch115q-1 mult 1.0 0.0 1
20520221 betagg 115080000 htrnr 115001001
*
20520230 ch115q-2 mult 1.0 0.0 1
20520231 cntrlvar 2016 csubpg 115080000
*
20520240 ch115q+ div 1.0 0.0 1
20520241 cntrlvar 2023 cntrlvar 2022
*
20520250 ch115Kv div 4.0 0.0 1
20520251 cntrlvar 2017 cntrlvar 2024
*
20520260 ch115Re2 poweri 1.0 0.0 1
20520261 cntrlvar 2017 2
*
20520270 ch115Ri div 1.0 0.0 1
20520271 cntrlvar 2026 cntrlvar 2020
*
20520280 ch115B01 powerr 1.0 0.0 1
20520281 cntrlvar 2026 1.7125

```

```

*
20520290 ch115B02 powerr 1.0 0.0 1
20520291 cntrlvar 2019 0.8
*
20520300 ch115B03 mult 1.0 0.0 1
20520301 cntrlvar 2028 cntrlvar 2029
*
20520310 ch115Bo div 1.0 0.0 1
20520311 cntrlvar 2030 cntrlvar 2020
*
20520510 ch132dp sum 1.0 0.0 1
20520511 0.0 1.0 p 132020000 -1.0 p 132130000
*
20520520 ch132pav sum 1.0 0.0 1
20520521 0.0 0.5 p 132020000 0.5 p 132130000
*
20520530 ch132dt sum 1.0 0.0 1
20520531 0.0 1.0 tempg 132130000 -1.0 tempg 132020000
*
20520540 ch132tav sum 1.0 0.0 1
20520541 0.0 0.5 tempg 132130000 0.5 tempg 132020000
*
20520550 ch132rhv sum 1.0 0.0 1
20520551 0.0 0.5 rhog 132130000 0.5 rhog 132020000
*
20520560 ch132Cpt mult 1.0 0.0 1
20520561 csubpg 132020000
*
20520570 ch132Cpb mult 1.0 0.0 1
20520571 csubpg 132130000
*
20520580 ch132Cpa sum 1.0 0.0 1
20520581 0.0 0.5 csubpg 132130000 0.5 csubpg 132020000
*
20520590 ch132vsm mult 1.0 1.0E-05 1
20520591 viscg 132080000
*
20520600 ch132ivs div 1.0 1.0E+05 1
20520601 viscg 132080000
*
20520610 ch132Bm mult 1.0 0.0 1
20520611 betagg 132080000
*
20520620 ch132Cpm mult 1.0 0.0 1
20520621 csubpg 132080000
*
20520630 ch132tcm mult 1.0 0.0 1
20520631 thcong 132080000
*
20520640 ch132itc div 1.0 0.0 1
20520641 thcong 132080000
*
20520650 ch132dTw sum 1.0 0.0 1
20520651 0.0 1.0 httemp 132000801 -1.0 tempg 132080000
*
20520660 ch132Gm mult 1.0 0.0 1
20520661 rhog 132080000 velg 132080000
*
20520670 ch132Re mult 0.0191 0.0 1
20520671 cntrlvar 2066 cntrlvar 2060
*
20520680 ch132Nu mult 0.0191 0.0 1
20520681 hthtc 132000800 cntrlvar 2064

```

```

*
20520690 ch132Pr mult 1.0 0.0 1
20520691 csubpg 132080000 viscg 132080000 cntrlvar 2064
*
20520700 ch132Gr mult 76.21 0.0 1
20520701 betagg 132080000 cntrlvar 2065 rhog 132080000
20520702 rhog 132080000 cntrlvar 2060 cntrlvar 2060
*
20520710 ch132Fr poweri 5.3565 0.0 1
20520711 velg 132080000 2
*
20520720 ch132q-1 mult 1.0 0.0 1
20520721 betagg 132080000 htrnr 132000800
*
20520730 ch132q-2 mult 1.0 0.0 1
20520731 cntrlvar 2066 csubpg 132080000
*
20520740 ch132q+ div 1.0 0.0 1
20520741 cntrlvar 2073 cntrlvar 2072
*
20520750 ch132Kv div 4.0 0.0 1
20520751 cntrlvar 2067 cntrlvar 2074
*
20520760 ch132Re2 poweri 1.0 0.0 1
20520761 cntrlvar 2067 2
*
20520770 ch132Ri div 1.0 0.0 1
20520771 cntrlvar 2076 cntrlvar 2070
*
20520780 ch132B01 powerr 1.0 0.0 1
20520781 cntrlvar 2076 1.7125
*
20520790 ch132B02 powerr 1.0 0.0 1
20520791 cntrlvar 2069 0.8
*
20520800 ch132B03 mult 1.0 0.0 1
20520801 cntrlvar 2078 cntrlvar 2079
*
20520810 ch132Bo div 1.0 0.0 1
20520811 cntrlvar 2080 cntrlvar 2070
*
20521010 ch140dp sum 1.0 0.0 1
20521011 0.0 1.0 p 140020000 -1.0 p 140130000
*
20521020 ch140pav sum 1.0 0.0 1
20521021 0.0 0.5 p 140020000 0.5 p 140130000
*
20521030 ch140dt sum 1.0 0.0 1
20521031 0.0 1.0 tempg 140130000 -1.0 tempg 140020000
*
20521040 ch140tav sum 1.0 0.0 1
20521041 0.0 0.5 tempg 140130000 0.5 tempg 140020000
*
20521050 ch140rhv sum 1.0 0.0 1
20521051 0.0 0.5 rhog 140130000 0.5 rhog 140020000
*
20521060 ch140Cpt mult 1.0 0.0 1
20521061 csubpg 140020000
*
20521070 ch140Cpb mult 1.0 0.0 1
20521071 csubpg 140130000
*
20521080 ch140Cpa sum 1.0 0.0 1

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```

20521081  0.0  0.5  csubpg  140130000  0.5  csubpg  140020000
*
20521090  ch140vsm  mult  1.0  1.0E-05  1
20521091  viscg  140080000
*
20521100  ch140ivs  div  1.0  1.0E+05  1
20521101  viscg  140080000
*
20521110  ch140Bm  mult  1.0  0.0  1
20521111  betagg  140080000
*
20521120  ch140Cpm  mult  1.0  0.0  1
20521121  csubpg  140080000
*
20521130  ch140tcm  mult  1.0  0.0  1
20521131  thcong  140080000
*
20521140  ch140itc  div  1.0  0.0  1
20521141  thcong  140080000
*
20521150  ch140dTw  sum  1.0  0.0  1
20521151  0.0  1.0  httemp  140100601  -1.0  tempg  140080000
*
20521160  ch140Gm  mult  1.0  0.0  1
20521161  rhog  140080000  velg  140080000
*
20521170  ch140Re  mult  0.015  0.0  1
20521171  cntrlvar  2116  cntrlvar  2110
*
20521180  ch140Nu  mult  0.015  0.0  1
20521181  hthtc  140100600  cntrlvar  2114
*
20521190  ch140Pr  mult  1.0  0.0  1
20521191  csubpg  140080000  viscg  140080000  cntrlvar  2114
*
20521200  ch140Gr  mult  76.21  0.0  1
20521201  betagg  140080000  cntrlvar  2115  rhog  140080000
20521202  rhog  140080000  cntrlvar  2110  cntrlvar  2110
*
20521210  ch140Fr  poweri  6.8027  0.0  1
20521211  velg  140080000  2
*
20521220  ch140q-1  mult  1.0  0.0  1
20521221  betagg  140080000  htrnr  140100600
*
20521230  ch140q-2  mult  1.0  0.0  1
20521231  cntrlvar  2116  csubpg  140080000
*
20521240  ch140q+  div  1.0  0.0  1
20521241  cntrlvar  2123  cntrlvar  2122
*
20521250  ch140Kv  div  4.0  0.0  1
20521251  cntrlvar  2117  cntrlvar  2124
*
20521260  ch140Re2  poweri  1.0  0.0  1
20521261  cntrlvar  2117  2
*
20521270  ch140Ri  div  1.0  0.0  1
20521271  cntrlvar  2126  cntrlvar  2120
*
20521280  ch140B01  powerr  1.0  0.0  1
20521281  cntrlvar  2126  1.7125
*

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```

20521290 ch140B02 powerr 1.0 0.0 1
20521291 cntrlvar 2119 0.8
*
20521300 ch140B03 mult 1.0 0.0 1
20521301 cntrlvar 2128 cntrlvar 2129
*
20521310 ch140Bo div 1.0 0.0 1
20521311 cntrlvar 2130 cntrlvar 2120
*
20521510 ch145dp sum 1.0 0.0 1
20521511 0.0 1.0 p 145020000 -1.0 p 145130000
*
20521520 ch145pav sum 1.0 0.0 1
20521521 0.0 0.5 p 145020000 0.5 p 145130000
*
20521530 ch145dt sum 1.0 0.0 1
20521531 0.0 1.0 tempg 145130000 -1.0 tempg 145020000
*
20521540 ch145tav sum 1.0 0.0 1
20521541 0.0 0.5 tempg 145130000 0.5 tempg 145020000
*
20521550 ch145rhv sum 1.0 0.0 1
20521551 0.0 0.5 rhog 145130000 0.5 rhog 145020000
*
20521560 ch145Cpt mult 1.0 0.0 1
20521561 csubpg 145020000
*
20521570 ch145Cpb mult 1.0 0.0 1
20521571 csubpg 145130000
*
20521580 ch145Cpa sum 1.0 0.0 1
20521581 0.0 0.5 csubpg 145130000 0.5 csubpg 145020000
*
20521590 ch145vsm mult 1.0 1.0E-05 1
20521591 viscg 145080000
*
20521600 ch145ivs div 1.0 1.0E+05 1
20521601 viscg 145080000
*
20521610 ch145Bm mult 1.0 0.0 1
20521611 betagg 145080000
*
20521620 ch145Cpm mult 1.0 0.0 1
20521621 csubpg 145080000
*
20521630 ch145tcm mult 1.0 0.0 1
20521631 thcong 145080000
*
20521640 ch145itc div 1.0 0.0 1
20521641 thcong 145080000
*
20521650 ch145dTw sum 1.0 0.0 1
20521651 0.0 1.0 httemp 145100601 -1.0 tempg 145080000
*
20521660 ch145Gm mult 1.0 0.0 1
20521661 rhog 145080000 velg 145080000
*
20521670 ch145Re mult 0.016 0.0 1
20521671 cntrlvar 2166 cntrlvar 2160
*
20521680 ch145Nu mult 0.016 0.0 1
20521681 htthtc 145100600 cntrlvar 2164
*

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20521690 ch145Fr mult 1.0 0.0 1
20521691 csubpg 145080000 viscg 145080000 cntrlvar 2164
*
20521700 ch145Gr mult 76.21 0.0 1
20521701 betagg 145080000 cntrlvar 2165 rhog 145080000
20521702 rhog 145080000 cntrlvar 2160 cntrlvar 2160
*
20521710 ch145Fr poweri 6.4278 0.0 1
20521711 velg 145080000 2
*
20521720 ch145q-1 mult 1.0 0.0 1
20521721 betagg 145080000 htrnr 145100600
*
20521730 ch145q-2 mult 1.0 0.0 1
20521731 cntrlvar 2166 csubpg 145080000
*
20521740 ch145q+ div 1.0 0.0 1
20521741 cntrlvar 2173 cntrlvar 2172
*
20521750 ch145Kv div 4.0 0.0 1
20521751 cntrlvar 2167 cntrlvar 2174
*
20521760 ch145Re2 poweri 1.0 0.0 1
20521761 cntrlvar 2167 2
*
20521770 ch145Ri div 1.0 0.0 1
20521771 cntrlvar 2176 cntrlvar 2170
*
20521780 ch145B01 powerr 1.0 0.0 1
20521781 cntrlvar 2176 1.7125
*
20521790 ch145B02 powerr 1.0 0.0 1
20521791 cntrlvar 2169 0.8
*
20521800 ch145B03 mult 1.0 0.0 1
20521801 cntrlvar 2178 cntrlvar 2179
*
20521810 ch145Bo div 1.0 0.0 1
20521811 cntrlvar 2180 cntrlvar 2170
*
20522010 ch150dp sum 1.0 0.0 1
20522011 0.0 1.0 p 150020000 -1.0 p 150130000
*
20522020 ch150pav sum 1.0 0.0 1
20522021 0.0 0.5 p 150020000 0.5 p 150130000
*
20522030 ch150dt sum 1.0 0.0 1
20522031 0.0 1.0 tempg 150130000 -1.0 tempg 150020000
*
20522040 ch150tav sum 1.0 0.0 1
20522041 0.0 0.5 tempg 150130000 0.5 tempg 150020000
*
20522050 ch150rhv sum 1.0 0.0 1
20522051 0.0 0.5 rhog 150130000 0.5 rhog 150020000
*
20522060 ch150Cpt mult 1.0 0.0 1
20522061 csubpg 150020000
*
20522070 ch150Cpb mult 1.0 0.0 1
20522071 csubpg 150130000
*
20522080 ch150Cpa sum 1.0 0.0 1
20522081 0.0 0.5 csubpg 150130000 0.5 csubpg 150020000

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```

*
20522090 ch150vsm mult 1.0 1.0E-05 1
20522091 viscg 150080000
*
20522100 ch150ivs div 1.0 1.0E+05 1
20522101 viscg 150080000
*
20522110 ch150Bm mult 1.0 0.0 1
20522111 betagg 150080000
*
20522120 ch150Cpm mult 1.0 0.0 1
20522121 csubpg 150080000
*
20522130 ch150tcm mult 1.0 0.0 1
20522131 thcong 150080000
*
20522140 ch150itc div 1.0 0.0 1
20522141 thcong 150080000
*
20522150 ch150dTw sum 1.0 0.0 1
20522151 0.0 1.0 httemp 150100601 -1.0 tempg 150080000
*
20522160 ch150Gm mult 1.0 0.0 1
20522161 rhog 150080000 velg 150080000
*
20522170 ch150Re mult 0.0144 0.0 1
20522171 cntrlvar 2216 cntrlvar 2210
*
20522180 ch150Nu mult 0.0144 0.0 1
20522181 hthtc 150100600 cntrlvar 2214
*
20522190 ch150Pr mult 1.0 0.0 1
20522191 csubpg 150080000 viscg 150080000 cntrlvar 2214
*
20522200 ch150Gr mult 76.21 0.0 1
20522201 betagg 150080000 cntrlvar 2215 rhog 150080000
20522202 rhog 150080000 cntrlvar 2210 cntrlvar 2210
*
20522210 ch150Fr poweri 7.0862 0.0 1
20522211 velg 150080000 2
*
20522220 ch150q-1 mult 1.0 0.0 1
20522221 betagg 150080000 htrnr 150100600
*
20522230 ch150q-2 mult 1.0 0.0 1
20522231 cntrlvar 2216 csubpg 150080000
*
20522240 ch150q+ div 1.0 0.0 1
20522241 cntrlvar 2223 cntrlvar 2222
*
20522250 ch150Kv div 4.0 0.0 1
20522251 cntrlvar 2217 cntrlvar 2224
*
20522260 ch150Re2 poweri 1.0 0.0 1
20522261 cntrlvar 2217 2
*
20522270 ch150Ri div 1.0 0.0 1
20522271 cntrlvar 2226 cntrlvar 2220
*
20522280 ch150B01 powerr 1.0 0.0 1
20522281 cntrlvar 2226 1.7125
*
20522290 ch150B02 powerr 1.0 0.0 1

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```

20522291  cntrlvar  2219  0.8
*
20522300  ch150B03  mult  1.0  0.0  1
20522301  cntrlvar  2228  cntrlvar  2229
*
20522310  ch150Bo  div  1.0  0.0  1
20522311  cntrlvar  2230  cntrlvar  2220
*
20522510  ch162dp  sum  1.0  0.0  1
20522511  0.0  1.0  p  162020000  -1.0  p  162130000
*
20522520  ch162pav  sum  1.0  0.0  1
20522521  0.0  0.5  p  162020000  0.5  p  162130000
*
20522530  ch162dt  sum  1.0  0.0  1
20522531  0.0  1.0  tempg  162130000  -1.0  tempg  162020000
*
20522540  ch162tav  sum  1.0  0.0  1
20522541  0.0  0.5  tempg  162130000  0.5  tempg  162020000
*
20522550  ch162rhv  sum  1.0  0.0  1
20522551  0.0  0.5  rhog  162130000  0.5  rhog  162020000
*
20522560  ch162Cpt  mult  1.0  0.0  1
20522561  csubpg  162020000
*
20522570  ch162Cpb  mult  1.0  0.0  1
20522571  csubpg  162130000
*
20522580  ch162Cpa  sum  1.0  0.0  1
20522581  0.0  0.5  csubpg  162130000  0.5  csubpg  162020000
*
20522590  ch162vsm  mult  1.0  1.0E-05  1
20522591  viscg  162080000
*
20522600  ch162ivs  div  1.0  1.0E+05  1
20522601  viscg  162080000
*
20522610  ch162Bm  mult  1.0  0.0  1
20522611  betagg  162080000
*
20522620  ch162Cpm  mult  1.0  0.0  1
20522621  csubpg  162080000
*
20522630  ch162tcm  mult  1.0  0.0  1
20522631  thcong  162080000
*
20522640  ch162itc  div  1.0  0.0  1
20522641  thcong  162080000
*
20522650  ch162dTw  sum  1.0  0.0  1
20522651  0.0  1.0  httemp  162000801  -1.0  tempg  162080000
*
20522660  ch162Gm  mult  1.0  0.0  1
20522661  rhog  162080000  velg  162080000
*
20522670  ch162Re  mult  0.015875  0.0  1
20522671  cntrlvar  2266  cntrlvar  2260
*
20522680  ch162Nu  mult  0.015875  0.0  1
20522681  hthtc  162000800  cntrlvar  2264
*
20522690  ch162Pr  mult  1.0  0.0  1

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20522691  csubpg  162080000  viscg  162080000  cntrlvar  2264
*
20522700  ch162Gr  mult  76.21  0.0  1
20522701  betagg  162080000  cntrlvar  2265  rhog  162080000
20522702  rhog  162080000  cntrlvar  2260  cntrlvar  2260
*
20522710  ch162Fr  poweri  6.4278  0.0  1
20522711  velg  162080000  2
*
20522720  ch162q-1  mult  1.0  0.0  1
20522721  betagg  162080000  htrnr  162000800
*
20522730  ch162q-2  mult  1.0  0.0  1
20522731  cntrlvar  2266  csubpg  162080000
*
20522740  ch162q+  div  1.0  0.0  1
20522741  cntrlvar  2273  cntrlvar  2272
*
20522750  ch162Kv  div  4.0  0.0  1
20522751  cntrlvar  2267  cntrlvar  2274
*
20522760  ch162Re2  poweri  1.0  0.0  1
20522761  cntrlvar  2267  2
*
20522770  ch162Ri  div  1.0  0.0  1
20522771  cntrlvar  2276  cntrlvar  2270
*
20522780  ch162B01  powerr  1.0  0.0  1
20522781  cntrlvar  2276  1.7125
*
20522790  ch162B02  powerr  1.0  0.0  1
20522791  cntrlvar  2269  0.8
*
20522800  ch162B03  mult  1.0  0.0  1
20522801  cntrlvar  2278  cntrlvar  2279
*
20522810  ch162Bo  div  1.0  0.0  1
20522811  cntrlvar  2280  cntrlvar  2270
*
20523010  ch164dp  sum  1.0  0.0  1
20523011  0.0  1.0  p  164020000  -1.0  p  164130000
*
20523020  ch164pav  sum  1.0  0.0  1
20523021  0.0  0.5  p  164020000  0.5  p  164130000
*
20523030  ch164dt  sum  1.0  0.0  1
20523031  0.0  1.0  tempg  164130000  -1.0  tempg  164020000
*
20523040  ch164tav  sum  1.0  0.0  1
20523041  0.0  0.5  tempg  164130000  0.5  tempg  164020000
*
20523050  ch164rhv  sum  1.0  0.0  1
20523051  0.0  0.5  rhog  164130000  0.5  rhog  164020000
*
20523060  ch164Cpt  mult  1.0  0.0  1
20523061  csubpg  164020000
*
20523070  ch164Cpb  mult  1.0  0.0  1
20523071  csubpg  164130000
*
20523080  ch164Cpa  sum  1.0  0.0  1
20523081  0.0  0.5  csubpg  164130000  0.5  csubpg  164020000
*

```

```

20523090 ch164vsm mult 1.0 1.0E-05 1
20523091 viscg 164080000
*
20523100 ch164ivs div 1.0 1.0E+05 1
20523101 viscg 164080000
*
20523110 ch164Bm mult 1.0 0.0 1
20523111 betagg 164080000
*
20523120 ch164Cpm mult 1.0 0.0 1
20523121 csubpg 164080000
*
20523130 ch164tcm mult 1.0 0.0 1
20523131 thcong 164080000
*
20523140 ch164itc div 1.0 0.0 1
20523141 thcong 164080000
*
20523150 ch164dTw sum 1.0 0.0 1
20523151 0.0 1.0 httemp 164000807 -1.0 tempg 164080000
*
20523160 ch164Gm mult 1.0 0.0 1
20523161 rhog 164080000 velg 164080000
*
20523170 ch164Re mult 0.0146304 0.0 1
20523171 cntrlvar 2316 cntrlvar 2310
*
20523180 ch164Nu mult 0.0146304 0.0 1
20523181 hthtc 164000801 cntrlvar 2314
*
20523190 ch164Pr mult 1.0 0.0 1
20523191 csubpg 164080000 viscg 164080000 cntrlvar 2314
*
20523200 ch164Gr mult 76.21 0.0 1
20523201 betagg 164080000 cntrlvar 2315 rhog 164080000
20523202 rhog 164080000 cntrlvar 2310 cntrlvar 2310
*
20523210 ch164Fr poweri 6.9746 0.0 1
20523211 velg 164080000 2
*
20523220 ch164q-1 mult 1.0 0.0 1
20523221 betagg 164080000 htrnr 164000801
*
20523230 ch164q-2 mult 1.0 0.0 1
20523231 cntrlvar 2316 csubpg 164080000
*
20523240 ch164q+ div 1.0 0.0 1
20523241 cntrlvar 2323 cntrlvar 2322
*
20523250 ch164Kv div 4.0 0.0 1
20523251 cntrlvar 2317 cntrlvar 2324
*
20523260 ch164Re2 poweri 1.0 0.0 1
20523261 cntrlvar 2317 2
*
20523270 ch164Ri div 1.0 0.0 1
20523271 cntrlvar 2326 cntrlvar 2320
*
20523280 ch164B01 powerr 1.0 0.0 1
20523281 cntrlvar 2326 1.7125
*
20523290 ch164B02 powerr 1.0 0.0 1
20523291 cntrlvar 2319 0.8

```

```

*
20523300 ch164B03 mult 1.0 0.0 1
20523301 cntrlvar 2328 cntrlvar 2329
*
20523310 ch164Bo div 1.0 0.0 1
20523311 cntrlvar 2330 cntrlvar 2320
*
20523510 ch166dp sum 1.0 0.0 1
20523511 0.0 1.0 p 166020000 -1.0 p 166130000
*
20523520 ch166pav sum 1.0 0.0 1
20523521 0.0 0.5 p 166020000 0.5 p 166130000
*
20523530 ch166dt sum 1.0 0.0 1
20523531 0.0 1.0 tempg 166130000 -1.0 tempg 166020000
*
20523540 ch166tav sum 1.0 0.0 1
20523541 0.0 0.5 tempg 166130000 0.5 tempg 166020000
*
20523550 ch166rhv sum 1.0 0.0 1
20523551 0.0 0.5 rhog 166130000 0.5 rhog 166020000
*
20523560 ch166Cpt mult 1.0 0.0 1
20523561 csubpg 166020000
*
20523570 ch166Cpb mult 1.0 0.0 1
20523571 csubpg 166130000
*
20523580 ch166Cpa sum 1.0 0.0 1
20523581 0.0 0.5 csubpg 166130000 0.5 csubpg 166020000
*
20523590 ch166vsm mult 1.0 1.0E-05 1
20523591 viscg 166080000
*
20523600 ch166ivs div 1.0 1.0E+05 1
20523601 viscg 166080000
*
20523610 ch166Bm mult 1.0 0.0 1
20523611 betag 166080000
*
20523620 ch166Cpm mult 1.0 0.0 1
20523621 csubpg 166080000
*
20523630 ch166tcm mult 1.0 0.0 1
20523631 thcong 166080000
*
20523640 ch166itc div 1.0 0.0 1
20523641 thcong 166080000
*
20523650 ch166dTw sum 1.0 0.0 1
20523651 0.0 1.0 httemp 166000807 -1.0 tempg 166080000
*
20523660 ch166Gm mult 1.0 0.0 1
20523661 rhog 166080000 velg 166080000
*
20523670 ch166Re mult 0.013 0.0 1
20523671 cntrlvar 2366 cntrlvar 2360
*
20523680 ch166Nu mult 0.013 0.0 1
20523681 hthtc 166000801 cntrlvar 2364
*
20523690 ch166Pr mult 1.0 0.0 1
20523691 csubpg 166080000 viscg 166080000 cntrlvar 2364

```

```

*
20523700 ch166Gr mult 76.21 0.0 1
20523701 betagg 166080000 cntrlvar 2365 rhog 166080000
20523702 rhog 166080000 cntrlvar 2360 cntrlvar 2360
*
20523710 ch166Fr poweri 8.0187 0.0 1
20523711 velg 166080000 2
*
20523720 ch166q-1 mult 1.0 0.0 1
20523721 betagg 166080000 htrnr 166000801
*
20523730 ch166q-2 mult 1.0 0.0 1
20523731 cntrlvar 2366 csubpg 166080000
*
20523740 ch166q+ div 1.0 0.0 1
20523741 cntrlvar 2373 cntrlvar 2372
*
20523750 ch166Kv div 4.0 0.0 1
20523751 cntrlvar 2367 cntrlvar 2374
*
20523760 ch166Re2 poweri 1.0 0.0 1
20523761 cntrlvar 2367 2
*
20523770 ch166Ri div 1.0 0.0 1
20523771 cntrlvar 2376 cntrlvar 2370
*
20523780 ch166B01 powerr 1.0 0.0 1
20523781 cntrlvar 2376 1.7125
*
20523790 ch166B02 powerr 1.0 0.0 1
20523791 cntrlvar 2369 0.8
*
20523800 ch166B03 mult 1.0 0.0 1
20523801 cntrlvar 2378 cntrlvar 2379
*
20523810 ch166Bo div 1.0 0.0 1
20523811 cntrlvar 2380 cntrlvar 2370
*
20524010 ch950dp sum 1.0 0.0 1
20524011 0.0 1.0 p 950010000 -1.0 p 950190000
*
20524020 ch950pav sum 1.0 0.0 1
20524021 0.0 0.5 p 950010000 0.5 p 950190000
*
20524030 ch950dt sum 1.0 0.0 1
20524031 0.0 1.0 tempg 950190000 -1.0 tempg 950010000
*
20524040 ch950tav sum 1.0 0.0 1
20524041 0.0 0.5 tempg 950190000 0.5 tempg 950010000
*
20524050 ch950rhv sum 1.0 0.0 1
20524051 0.0 0.5 rhog 950190000 0.5 rhog 950010000
*
20524060 ch950Cpt mult 1.0 0.0 1
20524061 csubpg 950010000
*
20524070 ch950Cpb mult 1.0 0.0 1
20524071 csubpg 950190000
*
20524080 ch950Cpa sum 1.0 0.0 1
20524081 0.0 0.5 csubpg 950190000 0.5 csubpg 950010000
*
20524090 ch950vsm mult 1.0 1.0E-05 1

```

```

20524091  viscg  950100000
*
20524100  ch950ivs  div  1.0  1.0E+05  1
20524101  viscg  950100000
*
20524110  ch950Bm  mult  1.0  0.0  1
20524111  betagg  950100000
*
20524120  ch950Cpm  mult  1.0  0.0  1
20524121  csubpg  950100000
*
20524130  ch950tcm  mult  1.0  0.0  1
20524131  thcong  950100000
*
20524140  ch950itc  div  1.0  0.0  1
20524141  thcong  950100000
*
20524150  ch950dTw  sum  1.0  0.0  1
20524151  0.0  1.0  httemp  950001004  -1.0  tempg  950100000
*
20524160  ch950Gm  mult  1.0  0.0  1
20524161  rhog  950100000  velg  950100000
*
20524170  ch950Re  mult  0.0508  0.0  1
20524171  cntrlvar  2416  cntrlvar  2410
*
20524180  ch950Nu  mult  0.0508  0.0  1
20524181  hthtc  950001001  cntrlvar  2414
*
20524190  ch950Pr  mult  1.0  0.0  1
20524191  csubpg  950100000  viscg  950100000  cntrlvar  2414
*
20524200  ch950Gr  mult  1440.41  0.0  1
20524201  betagg  950100000  cntrlvar  2415  rhog  950100000
20524202  rhog  950100000  cntrlvar  2410  cntrlvar  2410
*
20524210  ch950Fr  poweri  2.0087  0.0  1
20524211  velg  950100000  2
*
20524220  ch950q-1  mult  1.0  0.0  1
20524221  betagg  950100000  htrnr  950001001
*
20524230  ch950q-2  mult  1.0  0.0  1
20524231  cntrlvar  2416  csubpg  950100000
*
20524240  ch950q+  div  1.0  0.0  1
20524241  cntrlvar  2423  cntrlvar  2422
*
20524250  ch950Kv  div  4.0  0.0  1
20524251  cntrlvar  2417  cntrlvar  2424
*
20524260  ch950Re2  poweri  1.0  0.0  1
20524261  cntrlvar  2417  2
*
20524270  ch950Ri  div  1.0  0.0  1
20524271  cntrlvar  2426  cntrlvar  2420
*
20524280  ch950B01  powerr  1.0  0.0  1
20524281  cntrlvar  2426  1.7125
*
20524290  ch950B02  powerr  1.0  0.0  1
20524291  cntrlvar  2419  0.8
*

```



```

20524300 ch950B03 mult 1.0 0.0 1
20524301 cntrlvar 2428 cntrlvar 2429
*
20524310 ch950Bo div 1.0 0.0 1
20524311 cntrlvar 2430 cntrlvar 2420
*
* structure energy storage
*
20530010 hc100001 function 1.0E-06 0.0 1
20530011 htvat 1000001 3
*
20530020 es100001 mult 0.02156 0.0 1
20530021 htvat 1000001 cntrlvar 3001
*
20530030 hc100002 function 1.0E-06 0.0 1
20530031 htvat 1000002 3
*
20530040 es100002 mult 0.01464 0.0 1
20530041 htvat 1000002 cntrlvar 3003
*
20530050 hc100003 function 1.0E-06 0.0 1
20530051 htvat 1000003 3
*
20530060 es100003 mult 0.01656 0.0 1
20530061 htvat 1000003 cntrlvar 3005
*
20530070 hc100004 function 1.0E-06 0.0 1
20530071 htvat 1000004 3
*
20530080 es100004 mult 0.01656 0.0 1
20530081 htvat 1000004 cntrlvar 3007
*
20530090 hc100005 function 1.0E-06 0.0 1
20530091 htvat 1000005 3
*
20530100 es100005 mult 0.01305 0.0 1
20530101 htvat 1000005 cntrlvar 3009
*
20530110 hc100006 function 1.0E-06 0.0 1
20530111 htvat 1000006 3
*
20530120 es100006 mult 0.01305 0.0 1
20530121 htvat 1000006 cntrlvar 3011
*
20530130 hc100007 function 1.0E-06 0.0 1
20530131 htvat 1000007 3
*
20530140 es100007 mult 0.01305 0.0 1
20530141 htvat 1000007 cntrlvar 3013
*
20530150 hc100008 function 1.0E-06 0.0 1
20530151 htvat 1000008 3
*
20530160 es100008 mult 0.01305 0.0 1
20530161 htvat 1000008 cntrlvar 3015
*
20530170 hc100009 function 1.0E-06 0.0 1
20530171 htvat 1000009 3
*
20530180 es100009 mult 0.01305 0.0 1
20530181 htvat 1000009 cntrlvar 3017
*
20530190 hc100010 function 1.0E-06 0.0 1

```

```

20530191  htvat  1000010  3
*
20530200  es100010  mult  0.01305  0.0  1
20530201  htvat  1000010  cntrlvar  3019
*
20530210  hc100011  function  1.0E-06  0.0  1
20530211  htvat  1000011  3
*
20530220  es100011  mult  0.01305  0.0  1
20530221  htvat  1000011  cntrlvar  3021
*
20530230  hc100012  function  1.0E-06  0.0  1
20530231  htvat  1000012  3
*
20530240  es100012  mult  0.01305  0.0  1
20530241  htvat  1000012  cntrlvar  3023
*
20530250  hc100013  function  1.0E-06  0.0  1
20530251  htvat  1000013  3
*
20530260  es100013  mult  0.01305  0.0  1
20530261  htvat  1000013  cntrlvar  3025
*
20530270  hc100014  function  1.0E-06  0.0  1
20530271  htvat  1000014  3
*
20530280  es100014  mult  0.01305  0.0  1
20530281  htvat  1000014  cntrlvar  3027
*
20530290  hc100015  function  1.0E-06  0.0  1
20530291  htvat  1000015  3
*
20530300  es100015  mult  0.01255  0.0  1
20530301  htvat  1000015  cntrlvar  3029
*
20530310  hc100016  function  1.0E-06  0.0  1
20530311  htvat  1000016  3
*
20530320  es100016  mult  0.01339  0.0  1
20530321  htvat  1000016  cntrlvar  3031
*
20530330  hc100017  function  1.0E-06  0.0  1
20530331  htvat  1000017  3
*
20530340  es100017  mult  0.01800  0.0  1
20530341  htvat  1000017  cntrlvar  3033
*
20530350  hc100101  function  1.0E-06  0.0  1
20530351  htvat  1001001  3
*
20530360  es100101  mult  0.05438  0.0  1
20530361  htvat  1001001  cntrlvar  3035
*
20530380  es-pv  sum  1.0  0.0  1
20530381  0.0  1.0  cntrlvar  3002  1.0  cntrlvar  3004
20530382  1.0  cntrlvar  3006  1.0  cntrlvar  3008
20530383  1.0  cntrlvar  3010  1.0  cntrlvar  3012
20530384  1.0  cntrlvar  3014  1.0  cntrlvar  3016
20530385  1.0  cntrlvar  3018  1.0  cntrlvar  3020
20530386  1.0  cntrlvar  3022  1.0  cntrlvar  3024
20530387  1.0  cntrlvar  3026  1.0  cntrlvar  3028
20530388  1.0  cntrlvar  3030  1.0  cntrlvar  3032
+ 1.0  cntrlvar  3034  1.0  cntrlvar  3036

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```

*
20530410 hc105001 function 1.0E-06 0.0 1
20530411 htvat 1050001 3
*
20530420 es105001 mult 0.02046 0.0 1
20530421 htvat 1050001 cntrlvar 3041
*
20530430 hc110001 function 1.0E-06 0.0 1
20530431 htvat 1100001 3
*
20530440 es110001 mult 0.00946 0.0 1
20530441 htvat 1100001 cntrlvar 3043
*
20530490 hc115001 function 1.0E-06 0.0 1
20530491 htvat 1150001 3
*
20530500 es115001 mult 0.00744 0.0 1
20530501 htvat 1150001 cntrlvar 3049
*
20530510 hc115002 function 1.0E-06 0.0 1
20530511 htvat 1150002 3
*
20530520 es115002 mult 0.00505 0.0 1
20530521 htvat 1150002 cntrlvar 3051
*
20530530 hc115003 function 1.0E-06 0.0 1
20530531 htvat 1150003 3
*
20530540 es115003 mult 0.00572 0.0 1
20530541 htvat 1150003 cntrlvar 3053
*
20530550 hc115004 function 1.0E-06 0.0 1
20530551 htvat 1150004 3
*
20530560 es115004 mult 0.00572 0.0 1
20530561 htvat 1150004 cntrlvar 3055
*
20530570 hc115005 function 1.0E-06 0.0 1
20530571 htvat 1150005 3
*
20530580 es115005 mult 0.00450 0.0 1
20530581 htvat 1150005 cntrlvar 3057
*
20530590 hc115006 function 1.0E-06 0.0 1
20530591 htvat 1150006 3
*
20530600 es115006 mult 0.00450 0.0 1
20530601 htvat 1150006 cntrlvar 3059
*
20530610 hc115007 function 1.0E-06 0.0 1
20530611 htvat 1150007 3
*
20530620 es115007 mult 0.00450 0.0 1
20530621 htvat 1150007 cntrlvar 3061
*
20530630 hc115008 function 1.0E-06 0.0 1
20530631 htvat 1150008 3
*
20530640 es115008 mult 0.00450 0.0 1
20530641 htvat 1150008 cntrlvar 3063
*
20530650 hc115009 function 1.0E-06 0.0 1
20530651 htvat 1150009 3

```

```

*
20530660 es115009 mult 0.00450 0.0 1
20530661 htvat 1150009 cntrlvar 3065
*
20530670 hc115010 function 1.0E-06 0.0 1
20530671 htvat 1150010 3
*
20530680 es115010 mult 0.00450 0.0 1
20530681 htvat 1150010 cntrlvar 3067
*
20530690 hc115011 function 1.0E-06 0.0 1
20530691 htvat 1150011 3
*
20530700 es115011 mult 0.00450 0.0 1
20530701 htvat 1150011 cntrlvar 3069
*
20530710 hc115012 function 1.0E-06 0.0 1
20530711 htvat 1150012 3
*
20530720 es115012 mult 0.00450 0.0 1
20530721 htvat 1150012 cntrlvar 3071
*
20530730 hc115013 function 1.0E-06 0.0 1
20530731 htvat 1150013 3
*
20530740 es115013 mult 0.00450 0.0 1
20530741 htvat 1150013 cntrlvar 3073
*
20530750 hc115014 function 1.0E-06 0.0 1
20530751 htvat 1150014 3
*
20530760 es115014 mult 0.00529 0.0 1
20530761 htvat 1150014 cntrlvar 3075
*
20530770 hc115015 function 1.0E-06 0.0 1
20530771 htvat 1150015 3
*
20530780 es115015 mult 0.00433 0.0 1
20530781 htvat 1150015 cntrlvar 3077
*
20530790 hc115016 function 1.0E-06 0.0 1
20530791 htvat 1150016 3
*
20530800 es115016 mult 0.00433 0.0 1
20530801 htvat 1150016 cntrlvar 3079
*
20530810 es-cbar1 sum 1.0 0.0 1
20530811 0.0 1.0 cntrlvar 3050 1.0 cntrlvar 3052
20530812 1.0 cntrlvar 3054 1.0 cntrlvar 3056
20530813 1.0 cntrlvar 3058 1.0 cntrlvar 3060
20530814 1.0 cntrlvar 3062 1.0 cntrlvar 3064
20530815 1.0 cntrlvar 3066 1.0 cntrlvar 3068
20530816 1.0 cntrlvar 3070 1.0 cntrlvar 3072
20530817 1.0 cntrlvar 3074 1.0 cntrlvar 3076
20530818 1.0 cntrlvar 3078 1.0 cntrlvar 3080
*
20530830 hc120001 function 1.0E-06 0.0 1
20530831 htvat 1200001 4
*
20530840 es120001 mult 0.00399 0.0 1
20530841 htvat 1200001 cntrlvar 3083
*
20530850 hc120101 function 1.0E-06 0.0 1

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```

20530851  htvat  1201001  2
*
20530860  es120101  mult  0.02125  0.0  1
20530861  htvat  1201001  cntrlvar  3085
*
20530870  hc120201  function  1.0E-06  0.0  1
20530871  htvat  1202001  3
*
20530880  es120201  mult  0.00529  0.0  1
20530881  htvat  1202001  cntrlvar  3087
*
20530910  hc130001  function  1.0E-06  0.0  1
20530911  htvat  1300001  1
*
20530920  es130001  mult  0.00338  0.0  1
20530921  htvat  1300001  cntrlvar  3091
*
20530930  hc130002  function  1.0E-06  0.0  1
20530931  htvat  1300002  1
*
20530940  es130002  mult  0.00338  0.0  1
20530941  htvat  1300002  cntrlvar  3093
*
20530950  hc130003  function  1.0E-06  0.0  1
20530951  htvat  1300003  1
*
20530960  es130003  mult  0.00351  0.0  1
20530961  htvat  1300003  cntrlvar  3095
*
20530970  hc130004  function  1.0E-06  0.0  1
20530971  htvat  1300004  1
*
20530980  es130004  mult  0.00351  0.0  1
20530981  htvat  1300004  cntrlvar  3097
*
20530990  hc130005  function  1.0E-06  0.0  1
20530991  htvat  1300005  1
*
20531000  es130005  mult  0.00351  0.0  1
20531001  htvat  1300005  cntrlvar  3099
*
20531010  hc130006  function  1.0E-06  0.0  1
20531011  htvat  1300006  1
*
20531020  es130006  mult  0.00351  0.0  1
20531021  htvat  1300006  cntrlvar  3101
*
20531030  hc130007  function  1.0E-06  0.0  1
20531031  htvat  1300007  1
*
20531040  es130007  mult  0.00351  0.0  1
20531041  htvat  1300007  cntrlvar  3103
*
20531050  hc130008  function  1.0E-06  0.0  1
20531051  htvat  1300008  1
*
20531060  es130008  mult  0.00351  0.0  1
20531061  htvat  1300008  cntrlvar  3105
*
20531070  hc130009  function  1.0E-06  0.0  1
20531071  htvat  1300009  1
*
20531080  es130009  mult  0.00351  0.0  1

```

```

20531081  htvat  1300009  cntrlvar  3107
*
20531090  hc130010  function  1.0E-06  0.0  1
20531091  htvat  1300010  1
*
20531100  es130010  mult  0.00351  0.0  1
20531101  htvat  1300010  cntrlvar  3109
*
20531110  hc130011  function  1.0E-06  0.0  1
20531111  htvat  1300011  1
*
20531120  es130011  mult  0.00351  0.0  1
20531121  htvat  1300011  cntrlvar  3111
*
20531130  hc130012  function  1.0E-06  0.0  1
20531131  htvat  1300012  1
*
20531140  es130012  mult  0.00351  0.0  1
20531141  htvat  1300012  cntrlvar  3113
*
20531150  hc130013  function  1.0E-06  0.0  1
20531151  htvat  1300013  1
*
20531160  es130013  mult  0.00446  0.0  1
20531161  htvat  1300013  cntrlvar  3115
*
20531170  hc130014  function  1.0E-06  0.0  1
20531171  htvat  1300014  1
*
20531180  es130014  mult  0.00446  0.0  1
20531181  htvat  1300014  cntrlvar  3117
*
20531210  hc132001  function  1.0E-06  0.0  1
20531211  htvat  1320001  1
*
20531220  es132001  mult  0.01265  0.0  1
20531221  htvat  1320001  cntrlvar  3121
*
20531230  hc132002  function  1.0E-06  0.0  1
20531231  htvat  1320002  1
*
20531240  es132002  mult  0.01265  0.0  1
20531241  htvat  1320002  cntrlvar  3123
*
20531250  hc132003  function  1.0E-06  0.0  1
20531251  htvat  1320003  1
*
20531260  es132003  mult  0.01315  0.0  1
20531261  htvat  1320003  cntrlvar  3125
*
20531270  hc132004  function  1.0E-06  0.0  1
20531271  htvat  1320004  1
*
20531280  es132004  mult  0.01315  0.0  1
20531281  htvat  1320004  cntrlvar  3127
*
20531290  hc132005  function  1.0E-06  0.0  1
20531291  htvat  1320005  1
*
20531300  es132005  mult  0.01315  0.0  1
20531301  htvat  1320005  cntrlvar  3129
*
20531310  hc132006  function  1.0E-06  0.0  1

```

```

20531311  htvat  1320006  1
*
20531320  es132006  mult  0.01315  0.0  1
20531321  htvat  1320006  cntrlvar  3131
*
20531330  hc132007  function  1.0E-06  0.0  1
20531331  htvat  1320007  1
*
20531340  es132007  mult  0.01315  0.0  1
20531341  htvat  1320007  cntrlvar  3133
*
20531350  hc132008  function  1.0E-06  0.0  1
20531351  htvat  1320008  1
*
20531360  es132008  mult  0.01315  0.0  1
20531361  htvat  1320008  cntrlvar  3135
*
20531370  hc132009  function  1.0E-06  0.0  1
20531371  htvat  1320009  1
*
20531380  es132009  mult  0.01315  0.0  1
20531381  htvat  1320009  cntrlvar  3137
*
20531390  hc132010  function  1.0E-06  0.0  1
20531391  htvat  1320010  1
*
20531400  es132010  mult  0.01315  0.0  1
20531401  htvat  1320010  cntrlvar  3139
*
20531410  hc132011  function  1.0E-06  0.0  1
20531411  htvat  1320011  1
*
20531420  es132011  mult  0.01315  0.0  1
20531421  htvat  1320011  cntrlvar  3141
*
20531430  hc132012  function  1.0E-06  0.0  1
20531431  htvat  1320012  1
*
20531440  es132012  mult  0.01315  0.0  1
20531441  htvat  1320012  cntrlvar  3143
*
20531450  hc132013  function  1.0E-06  0.0  1
20531451  htvat  1320013  1
*
20531460  es132013  mult  0.01670  0.0  1
20531461  htvat  1320013  cntrlvar  3145
*
20531470  hc132014  function  1.0E-06  0.0  1
20531471  htvat  1320014  1
*
20531480  es132014  mult  0.01670  0.0  1
20531481  htvat  1320014  cntrlvar  3147
*
20531510  hc134001  function  1.0E-06  0.0  1
20531511  htvat  1340001  1
*
20531520  es134001  mult  0.00243  0.0  1
20531521  htvat  1340001  cntrlvar  3151
*
20531530  hc134002  function  1.0E-06  0.0  1
20531531  htvat  1340002  1
*
20531540  es134002  mult  0.00243  0.0  1

```

```
20531541  htvat  1340002  cntrlvar  3153
*
20531550  hc134003  function  1.0E-06  0.0  1
20531551  htvat  1340003  1
*
20531560  es134003  mult  0.00252  0.0  1
20531561  htvat  1340003  cntrlvar  3155
*
20531570  hc134004  function  1.0E-06  0.0  1
20531571  htvat  1340004  1
*
20531580  es134004  mult  0.00252  0.0  1
20531581  htvat  1340004  cntrlvar  3157
*
20531590  hc134005  function  1.0E-06  0.0  1
20531591  htvat  1340005  1
*
20531600  es134005  mult  0.00252  0.0  1
20531601  htvat  1340005  cntrlvar  3159
*
20531610  hc134006  function  1.0E-06  0.0  1
20531611  htvat  1340006  1
*
20531620  es134006  mult  0.00252  0.0  1
20531621  htvat  1340006  cntrlvar  3161
*
20531630  hc134007  function  1.0E-06  0.0  1
20531631  htvat  1340007  1
*
20531640  es134007  mult  0.00252  0.0  1
20531641  htvat  1340007  cntrlvar  3163
*
20531650  hc134008  function  1.0E-06  0.0  1
20531651  htvat  1340008  1
*
20531660  es134008  mult  0.00252  0.0  1
20531661  htvat  1340008  cntrlvar  3165
*
20531670  hc134009  function  1.0E-06  0.0  1
20531671  htvat  1340009  1
*
20531680  es134009  mult  0.00252  0.0  1
20531681  htvat  1340009  cntrlvar  3167
*
20531690  hc134010  function  1.0E-06  0.0  1
20531691  htvat  1340010  1
*
20531700  es134010  mult  0.00252  0.0  1
20531701  htvat  1340010  cntrlvar  3169
*
20531710  hc134011  function  1.0E-06  0.0  1
20531711  htvat  1340011  1
*
20531720  es134011  mult  0.00252  0.0  1
20531721  htvat  1340011  cntrlvar  3171
*
20531730  hc134012  function  1.0E-06  0.0  1
20531731  htvat  1340012  1
*
20531740  es134012  mult  0.00252  0.0  1
20531741  htvat  1340012  cntrlvar  3173
*
20531750  hc134013  function  1.0E-06  0.0  1
```



```

20531751  htvat  1340013  1
*
20531760  es134013  mult  0.00320  0.0  1
20531761  htvat  1340013  cntrlvar  3175
*
20531770  hc134014  function  1.0E-06  0.0  1
20531771  htvat  1340014  1
*
20531780  es134014  mult  0.00320  0.0  1
20531781  htvat  1340014  cntrlvar  3177
*
20531790  es-crefl  sum  1.0  0.0  1
20531791  0.0  1.0  cntrlvar  3092  1.0  cntrlvar  3094
20531792  1.0  cntrlvar  3096  1.0  cntrlvar  3098
20531793  1.0  cntrlvar  3100  1.0  cntrlvar  3102
20531794  1.0  cntrlvar  3104  1.0  cntrlvar  3106
20531795  1.0  cntrlvar  3108  1.0  cntrlvar  3110
20531796  1.0  cntrlvar  3112  1.0  cntrlvar  3114
20531797  1.0  cntrlvar  3116  1.0  cntrlvar  3118
20531798  1.0  cntrlvar  3122  1.0  cntrlvar  3124
+  1.0  cntrlvar  3126  1.0  cntrlvar  3128
+  1.0  cntrlvar  3130  1.0  cntrlvar  3132
+  1.0  cntrlvar  3134  1.0  cntrlvar  3136
+  1.0  cntrlvar  3138  1.0  cntrlvar  3140
+  1.0  cntrlvar  3142  1.0  cntrlvar  3144
+  1.0  cntrlvar  3146  1.0  cntrlvar  3148
+  1.0  cntrlvar  3152  1.0  cntrlvar  3154
+  1.0  cntrlvar  3156  1.0  cntrlvar  3158
+  1.0  cntrlvar  3160  1.0  cntrlvar  3162
+  1.0  cntrlvar  3164  1.0  cntrlvar  3166
+  1.0  cntrlvar  3168  1.0  cntrlvar  3170
+  1.0  cntrlvar  3172  1.0  cntrlvar  3174
+  1.0  cntrlvar  3176  1.0  cntrlvar  3178
*
20531810  hc140001  function  1.0E-06  0.0  1
20531811  htvat  1400001  1
*
20531820  es140001  mult  0.02123  0.0  1
20531821  htvat  1400001  cntrlvar  3181
*
20531830  hc140002  function  1.0E-06  0.0  1
20531831  htvat  1400002  1
*
20531840  es140002  mult  0.02123  0.0  1
20531841  htvat  1400002  cntrlvar  3183
*
20531850  hc140101  function  1.0E-06  0.0  1
20531851  htvat  1401001  1
*
20531860  es140101  mult  0.02208  0.0  1
20531861  htvat  1401001  cntrlvar  3185
*
20531870  hc140102  function  1.0E-06  0.0  1
20531871  htvat  1401002  1
*
20531880  es140102  mult  0.02208  0.0  1
20531881  htvat  1401002  cntrlvar  3187
*
20531890  hc140103  function  1.0E-06  0.0  1
20531891  htvat  1401003  1
*
20531900  es140103  mult  0.02208  0.0  1
20531901  htvat  1401003  cntrlvar  3189

```

```

*
20531910 hc140104 function 1.0E-06 0.0 1
20531911 htvat 1401004 1
*
20531920 es140104 mult 0.02208 0.0 1
20531921 htvat 1401004 cntrlvar 3191
*
20531930 hc140105 function 1.0E-06 0.0 1
20531931 htvat 1401005 1
*
20531940 es140105 mult 0.02208 0.0 1
20531941 htvat 1401005 cntrlvar 3193
*
20531950 hc140106 function 1.0E-06 0.0 1
20531951 htvat 1401006 1
*
20531960 es140106 mult 0.02208 0.0 1
20531961 htvat 1401006 cntrlvar 3195
*
20531970 hc140107 function 1.0E-06 0.0 1
20531971 htvat 1401007 1
*
20531980 es140107 mult 0.02208 0.0 1
20531981 htvat 1401007 cntrlvar 3197
*
20531990 hc140108 function 1.0E-06 0.0 1
20531991 htvat 1401008 1
*
20532000 es140108 mult 0.02208 0.0 1
20532001 htvat 1401008 cntrlvar 3199
*
20532010 hc140109 function 1.0E-06 0.0 1
20532011 htvat 1401009 1
*
20532020 es140109 mult 0.02208 0.0 1
20532021 htvat 1401009 cntrlvar 3201
*
20532030 hc140110 function 1.0E-06 0.0 1
20532031 htvat 1401010 1
*
20532040 es140110 mult 0.02208 0.0 1
20532041 htvat 1401010 cntrlvar 3203
*
20532050 hc140201 function 1.0E-06 0.0 1
20532051 htvat 1402001 1
*
20532060 es140201 mult 0.02802 0.0 1
20532061 htvat 1402001 cntrlvar 3205
*
20532070 hc140202 function 1.0E-06 0.0 1
20532071 htvat 1402002 1
*
20532080 es140202 mult 0.02802 0.0 1
20532081 htvat 1402002 cntrlvar 3207
*
20532110 hc145001 function 1.0E-06 0.0 1
20532111 htvat 1450001 1
*
20532120 es145001 mult 0.01981 0.0 1
20532121 htvat 1450001 cntrlvar 3211
*
20532130 hc145002 function 1.0E-06 0.0 1
20532131 htvat 1450002 1

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```

*
20532140 es145002 mult 0.01981 0.0 1
20532141 htvat 1450002 cntrlvar 3213
*
20532150 hc145101 function 1.0E-06 0.0 1
20532151 htvat 1451001 1
*
20532160 es145101 mult 0.02061 0.0 1
20532161 htvat 1451001 cntrlvar 3215
*
20532170 hc145102 function 1.0E-06 0.0 1
20532171 htvat 1451002 1
*
20532180 es145102 mult 0.02061 0.0 1
20532181 htvat 1451002 cntrlvar 3217
*
20532190 hc145103 function 1.0E-06 0.0 1
20532191 htvat 1451003 1
*
20532200 es145103 mult 0.02061 0.0 1
20532201 htvat 1451003 cntrlvar 3219
*
20532210 hc145104 function 1.0E-06 0.0 1
20532211 htvat 1451004 1
*
20532220 es145104 mult 0.02061 0.0 1
20532221 htvat 1451004 cntrlvar 3221
*
20532230 hc145105 function 1.0E-06 0.0 1
20532231 htvat 1451005 1
*
20532240 es145105 mult 0.02061 0.0 1
20532241 htvat 1451005 cntrlvar 3223
*
20532250 hc145106 function 1.0E-06 0.0 1
20532251 htvat 1451006 1
*
20532260 es145106 mult 0.02061 0.0 1
20532261 htvat 1451006 cntrlvar 3225
*
20532270 hc145107 function 1.0E-06 0.0 1
20532271 htvat 1451007 1
*
20532280 es145107 mult 0.02061 0.0 1
20532281 htvat 1451007 cntrlvar 3227
*
20532290 hc145108 function 1.0E-06 0.0 1
20532291 htvat 1451008 1
*
20532300 es145108 mult 0.02061 0.0 1
20532301 htvat 1451008 cntrlvar 3229
*
20532310 hc145109 function 1.0E-06 0.0 1
20532311 htvat 1451009 1
*
20532320 es145109 mult 0.02061 0.0 1
20532321 htvat 1451009 cntrlvar 3231
*
20532330 hc145110 function 1.0E-06 0.0 1
20532331 htvat 1451010 1
*
20532340 es145110 mult 0.02061 0.0 1
20532341 htvat 1451010 cntrlvar 3233

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```

*
20532350 hc145201 function 1.0E-06 0.0 1
20532351 htvat 1452001 1
*
20532360 es145201 mult 0.02615 0.0 1
20532361 htvat 1452001 cntrlvar 3235
*
20532370 hc145202 function 1.0E-06 0.0 1
20532371 htvat 1452002 1
*
20532380 es145202 mult 0.02615 0.0 1
20532381 htvat 1452002 cntrlvar 3237
*
20532410 hc150001 function 1.0E-06 0.0 1
20532411 htvat 1500001 1
*
20532420 es150001 mult 0.03821 0.0 1
20532421 htvat 1500001 cntrlvar 3241
*
20532430 hc150002 function 1.0E-06 0.0 1
20532431 htvat 1500002 1
*
20532440 es150002 mult 0.03821 0.0 1
20532441 htvat 1500002 cntrlvar 3243
*
20532450 hc150101 function 1.0E-06 0.0 1
20532451 htvat 1501001 1
*
20532460 es150101 mult 0.03974 0.0 1
20532461 htvat 1501001 cntrlvar 3245
*
20532470 hc150102 function 1.0E-06 0.0 1
20532471 htvat 1501002 1
*
20532480 es150102 mult 0.03974 0.0 1
20532481 htvat 1501002 cntrlvar 3247
*
20532490 hc150103 function 1.0E-06 0.0 1
20532491 htvat 1501003 1
*
20532500 es150103 mult 0.03974 0.0 1
20532501 htvat 1501003 cntrlvar 3249
*
20532510 hc150104 function 1.0E-06 0.0 1
20532511 htvat 1501004 1
*
20532520 es150104 mult 0.03974 0.0 1
20532521 htvat 1501004 cntrlvar 3251
*
20532530 hc150105 function 1.0E-06 0.0 1
20532531 htvat 1501005 1
*
20532540 es150105 mult 0.03974 0.0 1
20532541 htvat 1501005 cntrlvar 3253
*
20532550 hc150106 function 1.0E-06 0.0 1
20532551 htvat 1501006 1
*
20532560 es150106 mult 0.03974 0.0 1
20532561 htvat 1501006 cntrlvar 3255
*
20532570 hc150107 function 1.0E-06 0.0 1
20532571 htvat 1501007 1

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```

*
20532580 es150107 mult 0.03974 0.0 1
20532581 htvat 1501007 cntrlvar 3257
*
20532590 hc150108 function 1.0E-06 0.0 1
20532591 htvat 1501008 1
*
20532600 es150108 mult 0.03974 0.0 1
20532601 htvat 1501008 cntrlvar 3259
*
20532610 hc150109 function 1.0E-06 0.0 1
20532611 htvat 1501009 1
*
20532620 es150109 mult 0.03974 0.0 1
20532621 htvat 1501009 cntrlvar 3261
*
20532630 hc150110 function 1.0E-06 0.0 1
20532631 htvat 1501010 1
*
20532640 es150110 mult 0.03974 0.0 1
20532641 htvat 1501010 cntrlvar 3263
*
20532650 hc150201 function 1.0E-06 0.0 1
20532651 htvat 1502001 1
*
20532660 es150201 mult 0.05044 0.0 1
20532661 htvat 1502001 cntrlvar 3265
*
20532670 hc150202 function 1.0E-06 0.0 1
20532671 htvat 1502002 1
*
20532680 es150202 mult 0.05044 0.0 1
20532681 htvat 1502002 cntrlvar 3267
*
20532690 es-corec sum 1.0 0.0 1
20532691 0.0 1.0 cntrlvar 3182 1.0 cntrlvar 3184
20532692 1.0 cntrlvar 3186 1.0 cntrlvar 3188
20532693 1.0 cntrlvar 3190 1.0 cntrlvar 3192
20532694 1.0 cntrlvar 3194 1.0 cntrlvar 3196
20532695 1.0 cntrlvar 3198 1.0 cntrlvar 3200
20532696 1.0 cntrlvar 3202 1.0 cntrlvar 3204
20532697 1.0 cntrlvar 3206 1.0 cntrlvar 3208
20532698 1.0 cntrlvar 3212 1.0 cntrlvar 3214
+ 1.0 cntrlvar 3216 1.0 cntrlvar 3218
+ 1.0 cntrlvar 3220 1.0 cntrlvar 3222
+ 1.0 cntrlvar 3224 1.0 cntrlvar 3226
+ 1.0 cntrlvar 3228 1.0 cntrlvar 3230
+ 1.0 cntrlvar 3232 1.0 cntrlvar 3234
+ 1.0 cntrlvar 3236 1.0 cntrlvar 3238
+ 1.0 cntrlvar 3242 1.0 cntrlvar 3244
+ 1.0 cntrlvar 3246 1.0 cntrlvar 3248
+ 1.0 cntrlvar 3250 1.0 cntrlvar 3252
+ 1.0 cntrlvar 3254 1.0 cntrlvar 3256
+ 1.0 cntrlvar 3258 1.0 cntrlvar 3260
+ 1.0 cntrlvar 3262 1.0 cntrlvar 3264
+ 1.0 cntrlvar 3266 1.0 cntrlvar 3268
*
20532710 hc140301 function 1.0E-06 0.0 1
20532711 htvat 1403001 2
*
20532720 es140301 mult 0.00184 0.0 1
20532721 htvat 1403001 cntrlvar 3271
*

```

```
20532730 hc140302 function 1.0E-06 0.0 1
20532731 htvat 1403002 2
*
20532740 es140302 mult 0.00184 0.0 1
20532741 htvat 1403002 cntrlvar 3273
*
20532750 hc140303 function 1.0E-06 0.0 1
20532751 htvat 1403003 2
*
20532760 es140303 mult 0.00184 0.0 1
20532761 htvat 1403003 cntrlvar 3275
*
20532770 hc140304 function 1.0E-06 0.0 1
20532771 htvat 1403004 2
*
20532780 es140304 mult 0.00184 0.0 1
20532781 htvat 1403004 cntrlvar 3277
*
20532790 hc140305 function 1.0E-06 0.0 1
20532791 htvat 1403005 2
*
20532800 es140305 mult 0.00184 0.0 1
20532801 htvat 1403005 cntrlvar 3279
*
20532810 hc140306 function 1.0E-06 0.0 1
20532811 htvat 1403006 2
*
20532820 es140306 mult 0.00184 0.0 1
20532821 htvat 1403006 cntrlvar 3281
*
20532830 hc140307 function 1.0E-06 0.0 1
20532831 htvat 1403007 2
*
20532840 es140307 mult 0.00184 0.0 1
20532841 htvat 1403007 cntrlvar 3283
*
20532850 hc140308 function 1.0E-06 0.0 1
20532851 htvat 1403008 2
*
20532860 es140308 mult 0.00184 0.0 1
20532861 htvat 1403008 cntrlvar 3285
*
20532870 hc140309 function 1.0E-06 0.0 1
20532871 htvat 1403009 2
*
20532880 es140309 mult 0.00184 0.0 1
20532881 htvat 1403009 cntrlvar 3287
*
20532890 hc140310 function 1.0E-06 0.0 1
20532891 htvat 1403010 2
*
20532900 es140310 mult 0.00184 0.0 1
20532901 htvat 1403010 cntrlvar 3289
*
20532910 hc145301 function 1.0E-06 0.0 1
20532911 htvat 1453001 2
*
20532920 es145301 mult 0.00236 0.0 1
20532921 htvat 1453001 cntrlvar 3291
*
20532930 hc145302 function 1.0E-06 0.0 1
20532931 htvat 1453002 2
*
```

```

20532940 es145302 mult 0.00236 0.0 1
20532941 htvat 1453002 cntrlvar 3293
*
20532950 hc145303 function 1.0E-06 0.0 1
20532951 htvat 1453003 2
*
20532960 es145303 mult 0.00236 0.0 1
20532961 htvat 1453003 cntrlvar 3295
*
20532970 hc145304 function 1.0E-06 0.0 1
20532971 htvat 1453004 2
*
20532980 es145304 mult 0.00236 0.0 1
20532981 htvat 1453004 cntrlvar 3297
*
20532990 hc145305 function 1.0E-06 0.0 1
20532991 htvat 1453005 2
*
20533000 es145305 mult 0.00236 0.0 1
20533001 htvat 1453005 cntrlvar 3299
*
20533010 hc145306 function 1.0E-06 0.0 1
20533011 htvat 1453006 2
*
20533020 es145306 mult 0.00236 0.0 1
20533021 htvat 1453006 cntrlvar 3301
*
20533030 hc145307 function 1.0E-06 0.0 1
20533031 htvat 1453007 2
*
20533040 es145307 mult 0.00236 0.0 1
20533041 htvat 1453007 cntrlvar 3303
*
20533050 hc145308 function 1.0E-06 0.0 1
20533051 htvat 1453008 2
*
20533060 es145308 mult 0.00236 0.0 1
20533061 htvat 1453008 cntrlvar 3305
*
20533070 hc145309 function 1.0E-06 0.0 1
20533071 htvat 1453009 2
*
20533080 es145309 mult 0.00236 0.0 1
20533081 htvat 1453009 cntrlvar 3307
*
20533090 hc145310 function 1.0E-06 0.0 1
20533091 htvat 1453010 2
*
20533100 es145310 mult 0.00236 0.0 1
20533101 htvat 1453010 cntrlvar 3309
*
20533110 hc150301 function 1.0E-06 0.0 1
20533111 htvat 1503001 2
*
20533120 es150301 mult 0.00269 0.0 1
20533121 htvat 1503001 cntrlvar 3311
*
20533130 hc150302 function 1.0E-06 0.0 1
20533131 htvat 1503002 2
*
20533140 es150302 mult 0.00269 0.0 1
20533141 htvat 1503002 cntrlvar 3313
*

```

```

20533150 hc150303 function 1.0E-06 0.0 1
20533151 htvat 1503003 2
*
20533160 es150303 mult 0.00269 0.0 1
20533161 htvat 1503003 cntrlvar 3315
*
20533170 hc150304 function 1.0E-06 0.0 1
20533171 htvat 1503004 2
*
20533180 es150304 mult 0.00269 0.0 1
20533181 htvat 1503004 cntrlvar 3317
*
20533190 hc150305 function 1.0E-06 0.0 1
20533191 htvat 1503005 2
*
20533200 es150305 mult 0.00269 0.0 1
20533201 htvat 1503005 cntrlvar 3319
*
20533210 hc150306 function 1.0E-06 0.0 1
20533211 htvat 1503006 2
*
20533220 es150306 mult 0.00269 0.0 1
20533221 htvat 1503006 cntrlvar 3321
*
20533230 hc150307 function 1.0E-06 0.0 1
20533231 htvat 1503007 2
*
20533240 es150307 mult 0.00269 0.0 1
20533241 htvat 1503007 cntrlvar 3323
*
20533250 hc150308 function 1.0E-06 0.0 1
20533251 htvat 1503008 2
*
20533260 es150308 mult 0.00269 0.0 1
20533261 htvat 1503008 cntrlvar 3325
*
20533270 hc150309 function 1.0E-06 0.0 1
20533271 htvat 1503009 2
*
20533280 es150309 mult 0.00269 0.0 1
20533281 htvat 1503009 cntrlvar 3327
*
20533290 hc150310 function 1.0E-06 0.0 1
20533291 htvat 1503010 2
*
20533300 es150310 mult 0.00269 0.0 1
20533301 htvat 1503010 cntrlvar 3329
*
20533310 es-htrod sum 1.0 0.0 1
20533311 0.0 1.0 cntrlvar 3272 1.0 cntrlvar 3274
20533312 1.0 cntrlvar 3276 1.0 cntrlvar 3278
20533313 1.0 cntrlvar 3280 1.0 cntrlvar 3282
20533314 1.0 cntrlvar 3284 1.0 cntrlvar 3286
20533315 1.0 cntrlvar 3288 1.0 cntrlvar 3290
20533316 1.0 cntrlvar 3292 1.0 cntrlvar 3294
20533317 1.0 cntrlvar 3296 1.0 cntrlvar 3298
20533318 1.0 cntrlvar 3300 1.0 cntrlvar 3302
+ 1.0 cntrlvar 3304 1.0 cntrlvar 3306
+ 1.0 cntrlvar 3308 1.0 cntrlvar 3310
+ 1.0 cntrlvar 3312 1.0 cntrlvar 3314
+ 1.0 cntrlvar 3316 1.0 cntrlvar 3318
+ 1.0 cntrlvar 3320 1.0 cntrlvar 3322
+ 1.0 cntrlvar 3324 1.0 cntrlvar 3326

```



```
+ 1.0 cntrlvar 3328 1.0 cntrlvar 3330
*
20533410 hc160001 function 1.0E-06 0.0 1
20533411 htvat 1600001 1
*
20533420 es160001 mult 0.02046 0.0 1
20533421 htvat 1600001 cntrlvar 3341
*
20533430 hc160002 function 1.0E-06 0.0 1
20533431 htvat 1600002 1
*
20533440 es160002 mult 0.02046 0.0 1
20533441 htvat 1600002 cntrlvar 3343
*
20533450 hc160003 function 1.0E-06 0.0 1
20533451 htvat 1600003 1
*
20533460 es160003 mult 0.02128 0.0 1
20533461 htvat 1600003 cntrlvar 3345
*
20533470 hc160004 function 1.0E-06 0.0 1
20533471 htvat 1600004 1
*
20533480 es160004 mult 0.02128 0.0 1
20533481 htvat 1600004 cntrlvar 3347
*
20533490 hc160005 function 1.0E-06 0.0 1
20533491 htvat 1600005 1
*
20533500 es160005 mult 0.02128 0.0 1
20533501 htvat 1600005 cntrlvar 3349
*
20533510 hc160006 function 1.0E-06 0.0 1
20533511 htvat 1600006 1
*
20533520 es160006 mult 0.02128 0.0 1
20533521 htvat 1600006 cntrlvar 3351
*
20533530 hc160007 function 1.0E-06 0.0 1
20533531 htvat 1600007 1
*
20533540 es160007 mult 0.02128 0.0 1
20533541 htvat 1600007 cntrlvar 3353
*
20533550 hc160008 function 1.0E-06 0.0 1
20533551 htvat 1600008 1
*
20533560 es160008 mult 0.02128 0.0 1
20533561 htvat 1600008 cntrlvar 3355
*
20533570 hc160009 function 1.0E-06 0.0 1
20533571 htvat 1600009 1
*
20533580 es160009 mult 0.02128 0.0 1
20533581 htvat 1600009 cntrlvar 3357
*
20533590 hc160010 function 1.0E-06 0.0 1
20533591 htvat 1600010 1
*
20533600 es160010 mult 0.02128 0.0 1
20533601 htvat 1600010 cntrlvar 3359
*
20533610 hc160011 function 1.0E-06 0.0 1
```

```

20533611  htvat  1600011  1
*
20533620  es160011  mult  0.02128  0.0  1
20533621  htvat  1600011  cntrlvar  3361
*
20533630  hc160012  function  1.0E-06  0.0  1
20533631  htvat  1600012  1
*
20533640  es160012  mult  0.02128  0.0  1
20533641  htvat  1600012  cntrlvar  3363
*
20533650  hc160013  function  1.0E-06  0.0  1
20533651  htvat  1600013  1
*
20533660  es160013  mult  0.02701  0.0  1
20533661  htvat  1600013  cntrlvar  3365
*
20533670  hc160014  function  1.0E-06  0.0  1
20533671  htvat  1600014  1
*
20533680  es160014  mult  0.02701  0.0  1
20533681  htvat  1600014  cntrlvar  3367
*
20533710  hc162001  function  1.0E-06  0.0  1
20533711  htvat  1620001  1
*
20533720  es162001  mult  0.04244  0.0  1
20533721  htvat  1620001  cntrlvar  3371
*
20533730  hc162002  function  1.0E-06  0.0  1
20533731  htvat  1620002  1
*
20533740  es162002  mult  0.04244  0.0  1
20533741  htvat  1620002  cntrlvar  3373
*
20533750  hc162003  function  1.0E-06  0.0  1
20533751  htvat  1620003  1
*
20533760  es162003  mult  0.04413  0.0  1
20533761  htvat  1620003  cntrlvar  3375
*
20533770  hc162004  function  1.0E-06  0.0  1
20533771  htvat  1620004  1
*
20533780  es162004  mult  0.04413  0.0  1
20533781  htvat  1620004  cntrlvar  3377
*
20533790  hc162005  function  1.0E-06  0.0  1
20533791  htvat  1620005  1
*
20533800  es162005  mult  0.04413  0.0  1
20533801  htvat  1620005  cntrlvar  3379
*
20533810  hc162006  function  1.0E-06  0.0  1
20533811  htvat  1620006  1
*
20533820  es162006  mult  0.04413  0.0  1
20533821  htvat  1620006  cntrlvar  3381
*
20533830  hc162007  function  1.0E-06  0.0  1
20533831  htvat  1620007  1
*
20533840  es162007  mult  0.04413  0.0  1

```

```

20533841  htvat  1620007  cntrlvar  3383
*
20533850  hc162008  function  1.0E-06  0.0  1
20533851  htvat  1620008  1
*
20533860  es162008  mult  0.04413  0.0  1
20533861  htvat  1620008  cntrlvar  3385
*
20533870  hc162009  function  1.0E-06  0.0  1
20533871  htvat  1620009  1
*
20533880  es162009  mult  0.04413  0.0  1
20533881  htvat  1620009  cntrlvar  3387
*
20533890  hc162010  function  1.0E-06  0.0  1
20533891  htvat  1620010  1
*
20533900  es162010  mult  0.04413  0.0  1
20533901  htvat  1620010  cntrlvar  3389
*
20533910  hc162011  function  1.0E-06  0.0  1
20533911  htvat  1620011  1
*
20533920  es162011  mult  0.04413  0.0  1
20533921  htvat  1620011  cntrlvar  3391
*
20533930  hc162012  function  1.0E-06  0.0  1
20533931  htvat  1620012  1
*
20533940  es162012  mult  0.04413  0.0  1
20533941  htvat  1620012  cntrlvar  3393
*
20533950  hc162013  function  1.0E-06  0.0  1
20533951  htvat  1620013  1
*
20533960  es162013  mult  0.05602  0.0  1
20533961  htvat  1620013  cntrlvar  3395
*
20533970  hc162014  function  1.0E-06  0.0  1
20533971  htvat  1620014  1
*
20533980  es162014  mult  0.05602  0.0  1
20533981  htvat  1620014  cntrlvar  3397
*
20534010  hc164001  function  1.0E-06  0.0  1
20534011  htvat  1640001  1
*
20534020  es164001  mult  0.02025  0.0  1
20534021  htvat  1640001  cntrlvar  3401
*
20534030  hc164002  function  1.0E-06  0.0  1
20534031  htvat  1640002  1
*
20534040  es164002  mult  0.02025  0.0  1
20534041  htvat  1640002  cntrlvar  3403
*
20534050  hc164003  function  1.0E-06  0.0  1
20534051  htvat  1640003  1
*
20534060  es164003  mult  0.02106  0.0  1
20534061  htvat  1640003  cntrlvar  3405
*
20534070  hc164004  function  1.0E-06  0.0  1

```

20534071 htvat 1640004 1
*
20534080 es164004 mult 0.02106 0.0 1
20534081 htvat 1640004 cntrlvar 3407
*
20534090 hc164005 function 1.0E-06 0.0 1
20534091 htvat 1640005 1
*
20534100 es164005 mult 0.02106 0.0 1
20534101 htvat 1640005 cntrlvar 3409
*
20534110 hc164006 function 1.0E-06 0.0 1
20534111 htvat 1640006 1
*
20534120 es164006 mult 0.02106 0.0 1
20534121 htvat 1640006 cntrlvar 3411
*
20534130 hc164007 function 1.0E-06 0.0 1
20534131 htvat 1640007 1
*
20534140 es164007 mult 0.02106 0.0 1
20534141 htvat 1640007 cntrlvar 3413
*
20534150 hc164008 function 1.0E-06 0.0 1
20534151 htvat 1640008 1
*
20534160 es164008 mult 0.02106 0.0 1
20534161 htvat 1640008 cntrlvar 3415
*
20534170 hc164009 function 1.0E-06 0.0 1
20534171 htvat 1640009 1
*
20534180 es164009 mult 0.02106 0.0 1
20534181 htvat 1640009 cntrlvar 3417
*
20534190 hc164010 function 1.0E-06 0.0 1
20534191 htvat 1640010 1
*
20534200 es164010 mult 0.02106 0.0 1
20534201 htvat 1640010 cntrlvar 3419
*
20534210 hc164011 function 1.0E-06 0.0 1
20534211 htvat 1640011 1
*
20534220 es164011 mult 0.02106 0.0 1
20534221 htvat 1640011 cntrlvar 3421
*
20534230 hc164012 function 1.0E-06 0.0 1
20534231 htvat 1640012 1
*
20534240 es164012 mult 0.02106 0.0 1
20534241 htvat 1640012 cntrlvar 3423
*
20534250 hc164013 function 1.0E-06 0.0 1
20534251 htvat 1640013 1
*
20534260 es164013 mult 0.02673 0.0 1
20534261 htvat 1640013 cntrlvar 3425
*
20534270 hc164014 function 1.0E-06 0.0 1
20534271 htvat 1640014 1
*
20534280 es164014 mult 0.02673 0.0 1

```

20534281  htvat  1640014  cntrlvar  3427
*
20534290  es-crefl  sum  1.0  0.0  1
20534291  0.0  1.0  cntrlvar  3342  1.0  cntrlvar  3344
20534292  1.0  cntrlvar  3346  1.0  cntrlvar  3348
20534293  1.0  cntrlvar  3350  1.0  cntrlvar  3352
20534294  1.0  cntrlvar  3354  1.0  cntrlvar  3356
20534295  1.0  cntrlvar  3358  1.0  cntrlvar  3360
20534296  1.0  cntrlvar  3362  1.0  cntrlvar  3364
20534297  1.0  cntrlvar  3366  1.0  cntrlvar  3368
20534298  1.0  cntrlvar  3372  1.0  cntrlvar  3374
+  1.0  cntrlvar  3376  1.0  cntrlvar  3378
+  1.0  cntrlvar  3380  1.0  cntrlvar  3382
+  1.0  cntrlvar  3384  1.0  cntrlvar  3386
+  1.0  cntrlvar  3388  1.0  cntrlvar  3390
+  1.0  cntrlvar  3392  1.0  cntrlvar  3394
+  1.0  cntrlvar  3396  1.0  cntrlvar  3398
+  1.0  cntrlvar  3402  1.0  cntrlvar  3404
+  1.0  cntrlvar  3406  1.0  cntrlvar  3408
+  1.0  cntrlvar  3410  1.0  cntrlvar  3412
+  1.0  cntrlvar  3414  1.0  cntrlvar  3416
+  1.0  cntrlvar  3418  1.0  cntrlvar  3420
+  1.0  cntrlvar  3422  1.0  cntrlvar  3424
+  1.0  cntrlvar  3426  1.0  cntrlvar  3428
*
20534310  hc166001  function  1.0E-06  0.0  1
20534311  htvat  1660001  5
*
20534320  es166001  mult  0.11225  0.0  1
20534321  htvat  1660001  cntrlvar  3431
*
20534330  hc166002  function  1.0E-06  0.0  1
20534331  htvat  1660002  5
*
20534340  es166002  mult  0.11225  0.0  1
20534341  htvat  1660002  cntrlvar  3433
*
20534350  hc166003  function  1.0E-06  0.0  1
20534351  htvat  1660003  5
*
20534360  es166003  mult  0.11674  0.0  1
20534361  htvat  1660003  cntrlvar  3435
*
20534370  hc166004  function  1.0E-06  0.0  1
20534371  htvat  1660004  5
*
20534380  es166004  mult  0.11674  0.0  1
20534381  htvat  1660004  cntrlvar  3437
*
20534390  hc166005  function  1.0E-06  0.0  1
20534391  htvat  1660005  5
*
20534400  es166005  mult  0.11674  0.0  1
20534401  htvat  1660005  cntrlvar  3439
*
20534410  hc166006  function  1.0E-06  0.0  1
20534411  htvat  1660006  5
*
20534420  es166006  mult  0.11674  0.0  1
20534421  htvat  1660006  cntrlvar  3441
*
20534430  hc166007  function  1.0E-06  0.0  1
20534431  htvat  1660007  5

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```

*
20534440 es166007 mult 0.11674 0.0 1
20534441 htvat 1660007 cntrlvar 3443
*
20534450 hc166008 function 1.0E-06 0.0 1
20534451 htvat 1660008 5
*
20534460 es166008 mult 0.11674 0.0 1
20534461 htvat 1660008 cntrlvar 3445
*
20534470 hc166009 function 1.0E-06 0.0 1
20534471 htvat 1660009 5
*
20534480 es166009 mult 0.11674 0.0 1
20534481 htvat 1660009 cntrlvar 3447
*
20534490 hc166010 function 1.0E-06 0.0 1
20534491 htvat 1660010 5
*
20534500 es166010 mult 0.11674 0.0 1
20534501 htvat 1660010 cntrlvar 3449
*
20534510 hc166011 function 1.0E-06 0.0 1
20534511 htvat 1660011 5
*
20534520 es166011 mult 0.11674 0.0 1
20534521 htvat 1660011 cntrlvar 3451
*
20534530 hc166012 function 1.0E-06 0.0 1
20534531 htvat 1660012 5
*
20534540 es166012 mult 0.11674 0.0 1
20534541 htvat 1660012 cntrlvar 3453
*
20534550 hc166013 function 1.0E-06 0.0 1
20534551 htvat 1660013 5
*
20534560 es166013 mult 0.14818 0.0 1
20534561 htvat 1660013 cntrlvar 3455
*
20534570 hc166014 function 1.0E-06 0.0 1
20534571 htvat 1660014 5
*
20534580 es166014 mult 0.14818 0.0 1
20534581 htvat 1660014 cntrlvar 3457
*
20534590 es-PSR sum 1.0 0.0 1
20534591 0.0 1.0 cntrlvar 3432 1.0 cntrlvar 3434
20534592 1.0 cntrlvar 3436 1.0 cntrlvar 3438
20534593 1.0 cntrlvar 3440 1.0 cntrlvar 3442
20534594 1.0 cntrlvar 3444 1.0 cntrlvar 3446
20534595 1.0 cntrlvar 3448 1.0 cntrlvar 3450
20534596 1.0 cntrlvar 3452 1.0 cntrlvar 3454
20534597 1.0 cntrlvar 3456 1.0 cntrlvar 3458
*
20534610 hc175001 function 1.0E-06 0.0 1
20534611 htvat 1750001 3
*
20534620 es175001 mult 0.04499 0.0 1
20534621 htvat 1750001 cntrlvar 3461
*
20534630 hc175101 function 1.0E-06 0.0 1
20534631 htvat 1751001 1

```

```

*
20534640 es175101 mult 0.09527 0.0 1
20534641 htvat 1751001 cntrlvar 3463
*
20534660 es-core sum 1.0 0.0 1
20534661 0.0 1.0 cntrlvar 3179 1.0 cntrlvar 3269
20534662 1.0 cntrlvar 3331 1.0 cntrlvar 3429
20534663 1.0 cntrlvar 3459
*
20534680 es-pves1 sum 1.0 0.0 1
20534681 0.0 1.0 cntrlvar 3038 1.0 cntrlvar 3042
20534682 1.0 cntrlvar 3044 1.0 cntrlvar 3081
20534683 1.0 cntrlvar 3084 1.0 cntrlvar 3086
20534684 1.0 cntrlvar 3088 1.0 cntrlvar 3462
20534685 1.0 cntrlvar 3464 1.0 cntrlvar 3466
*
20534710 hc200001 function 1.0E-06 0.0 1
20534711 htvat 2000001 3
*
20534720 es200001 mult 0.00291 0.0 1
20534721 htvat 2000001 cntrlvar 3471
*
20534730 hc200002 function 1.0E-06 0.0 1
20534731 htvat 2000002 3
*
20534740 es200002 mult 0.00439 0.0 1
20534741 htvat 2000002 cntrlvar 3473
*
20534750 hc200003 function 1.0E-06 0.0 1
20534751 htvat 2000003 3
*
20534760 es200003 mult 0.00278 0.0 1
20534761 htvat 2000003 cntrlvar 3475
*
20534770 hc200004 function 1.0E-06 0.0 1
20534771 htvat 2000004 3
*
20534780 es200004 mult 0.00278 0.0 1
20534781 htvat 2000004 cntrlvar 3477
*
20534790 hc200101 function 1.0E-06 0.0 1
20534791 htvat 2001001 3
*
20534800 es200101 mult 0.00609 0.0 1
20534801 htvat 2001001 cntrlvar 3479
*
20534810 hc200102 function 1.0E-06 0.0 1
20534811 htvat 2001002 3
*
20534820 es200102 mult 0.00609 0.0 1
20534821 htvat 2001002 cntrlvar 3481
*
20534830 hc210001 function 1.0E-06 0.0 1
20534831 htvat 2100001 3
*
20534840 es210001 mult 0.00820 0.0 1
20534841 htvat 2100001 cntrlvar 3483
*
20534850 hc215001 function 1.0E-06 0.0 1
20534851 htvat 2150001 3
*
20534860 es215001 mult 0.01715 0.0 1
20534861 htvat 2150001 cntrlvar 3485

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```

*
20534870 hc220001 function 1.0E-06 0.0 1
20534871 htvat 2200001 3
*
20534880 es220001 mult 0.01075 0.0 1
20534881 htvat 2200001 cntrlvar 3487
*
20534890 hc220101 function 1.0E-06 0.0 1
20534891 htvat 2201001 3
*
20534900 es220101 mult 0.00113 0.0 1
20534901 htvat 2201001 cntrlvar 3489
*
20535010 hc225001 function 1.0E-06 0.0 1
20535011 htvat 2250001 3
*
20535020 es225001 mult 0.00184 0.0 1
20535021 htvat 2250001 cntrlvar 3501
*
20535030 hc225002 function 1.0E-06 0.0 1
20535031 htvat 2250002 3
*
20535040 es225002 mult 0.00184 0.0 1
20535041 htvat 2250002 cntrlvar 3503
*
20535050 hc225003 function 1.0E-06 0.0 1
20535051 htvat 2250003 3
*
20535060 es225003 mult 0.00186 0.0 1
20535061 htvat 2250003 cntrlvar 3505
*
20535070 hc225004 function 1.0E-06 0.0 1
20535071 htvat 2250004 3
*
20535080 es225004 mult 0.00186 0.0 1
20535081 htvat 2250004 cntrlvar 3507
*
20535090 hc225005 function 1.0E-06 0.0 1
20535091 htvat 2250005 3
*
20535100 es225005 mult 0.00186 0.0 1
20535101 htvat 2250005 cntrlvar 3509
*
20535110 hc225006 function 1.0E-06 0.0 1
20535111 htvat 2250006 3
*
20535120 es225006 mult 0.00186 0.0 1
20535121 htvat 2250006 cntrlvar 3511
*
20535130 hc225007 function 1.0E-06 0.0 1
20535131 htvat 2250007 3
*
20535140 es225007 mult 0.00186 0.0 1
20535141 htvat 2250007 cntrlvar 3513
*
20535150 hc225008 function 1.0E-06 0.0 1
20535151 htvat 2250008 3
*
20535160 es225008 mult 0.00186 0.0 1
20535161 htvat 2250008 cntrlvar 3515
*
20535170 hc225009 function 1.0E-06 0.0 1
20535171 htvat 2250009 3

```



```

*
20535180 es225009 mult 0.00186 0.0 1
20535181 htvat 2250009 cntrlvar 3517
*
20535190 hc225010 function 1.0E-06 0.0 1
20535191 htvat 2250010 3
*
20535200 es225010 mult 0.00186 0.0 1
20535201 htvat 2250010 cntrlvar 3519
*
20535210 hc225011 function 1.0E-06 0.0 1
20535211 htvat 2250011 3
*
20535220 es225011 mult 0.00238 0.0 1
20535221 htvat 2250011 cntrlvar 3521
*
20535230 hc225012 function 1.0E-06 0.0 1
20535231 htvat 2250012 3
*
20535240 es225012 mult 0.00238 0.0 1
20535241 htvat 2250012 cntrlvar 3523
*
20535250 hc225013 function 1.0E-06 0.0 1
20535251 htvat 2250013 3
*
20535260 es225013 mult 0.00186 0.0 1
20535261 htvat 2250013 cntrlvar 3525
*
20535270 hc225014 function 1.0E-06 0.0 1
20535271 htvat 2250014 3
*
20535280 es225014 mult 0.00186 0.0 1
20535281 htvat 2250014 cntrlvar 3527
*
20535290 hc225015 function 1.0E-06 0.0 1
20535291 htvat 2250015 3
*
20535300 es225015 mult 0.00186 0.0 1
20535301 htvat 2250015 cntrlvar 3529
*
20535310 hc225016 function 1.0E-06 0.0 1
20535311 htvat 2250016 3
*
20535320 es225016 mult 0.00186 0.0 1
20535321 htvat 2250016 cntrlvar 3531
*
20535330 hc225017 function 1.0E-06 0.0 1
20535331 htvat 2250017 3
*
20535340 es225017 mult 0.00186 0.0 1
20535341 htvat 2250017 cntrlvar 3533
*
20535350 hc225018 function 1.0E-06 0.0 1
20535351 htvat 2250018 3
*
20535360 es225018 mult 0.00186 0.0 1
20535361 htvat 2250018 cntrlvar 3535
*
20535370 hc225019 function 1.0E-06 0.0 1
20535371 htvat 2250019 3
*
20535380 es225019 mult 0.00186 0.0 1
20535381 htvat 2250019 cntrlvar 3537

```

```

*
20535390 hc225020 function 1.0E-06 0.0 1
20535391 htvat 2250020 3
*
20535400 es225020 mult 0.00186 0.0 1
20535401 htvat 2250020 cntrlvar 3539
*
20535410 hc225021 function 1.0E-06 0.0 1
20535411 htvat 2250021 3
*
20535420 es225021 mult 0.00184 0.0 1
20535421 htvat 2250021 cntrlvar 3541
*
20535430 hc225022 function 1.0E-06 0.0 1
20535431 htvat 2250022 3
*
20535440 es225022 mult 0.00184 0.0 1
20535441 htvat 2250022 cntrlvar 3543
*
20535460 es-Sgtub sum 1.0 0.0 1
20535461 0.0 1.0 cntrlvar 3502 1.0 cntrlvar 3504
20535462 1.0 cntrlvar 3506 1.0 cntrlvar 3508
20535463 1.0 cntrlvar 3510 1.0 cntrlvar 3512
20535464 1.0 cntrlvar 3514 1.0 cntrlvar 3516
20535465 1.0 cntrlvar 3518 1.0 cntrlvar 3520
20535466 1.0 cntrlvar 3522 1.0 cntrlvar 3524
20535467 1.0 cntrlvar 3526 1.0 cntrlvar 3528
20535468 1.0 cntrlvar 3530 1.0 cntrlvar 3532
+ 1.0 cntrlvar 3534 1.0 cntrlvar 3536
+ 1.0 cntrlvar 3538 1.0 cntrlvar 3540
+ 1.0 cntrlvar 3542 1.0 cntrlvar 3544
*
20535470 hc225101 function 1.0E-06 0.0 1
20535471 htvat 2251001 3
*
20535480 es225101 mult 0.00870 0.0 1
20535481 htvat 2251001 cntrlvar 3547
*
20535490 hc225102 function 1.0E-06 0.0 1
20535491 htvat 2251002 3
*
20535500 es225102 mult 0.00870 0.0 1
20535501 htvat 2251002 cntrlvar 3549
*
20535510 hc228001 function 1.0E-06 0.0 1
20535511 htvat 2280001 3
*
20535520 es228001 mult 0.00909 0.0 1
20535521 htvat 2280001 cntrlvar 3551
*
20535530 hc230001 function 1.0E-06 0.0 1
20535531 htvat 2300001 3
*
20535540 es230001 mult 0.01237 0.0 1
20535541 htvat 2300001 cntrlvar 3553
*
20535550 hc235001 function 1.0E-06 0.0 1
20535551 htvat 2350001 3
*
20535560 es235001 mult 0.17279 0.0 1
20535561 htvat 2350001 cntrlvar 3555
*
20535570 hc240001 function 1.0E-06 0.0 1

```

```

20535571 htvat 2400001 3
*
20535580 es240001 mult 0.00701 0.0 1
20535581 htvat 2400001 cntrlvar 3557
*
20535590 hc250001 function 1.0E-06 0.0 1
20535591 htvat 2500001 3
*
20535600 es250001 mult 0.00592 0.0 1
20535601 htvat 2500001 cntrlvar 3559
*
20535610 hc250002 function 1.0E-06 0.0 1
20535611 htvat 2500002 3
*
20535620 es250002 mult 0.00196 0.0 1
20535621 htvat 2500002 cntrlvar 3561
*
20535630 hc250003 function 1.0E-06 0.0 1
20535631 htvat 2500003 3
*
20535640 es250003 mult 0.00337 0.0 1
20535641 htvat 2500003 cntrlvar 3563
*
20535650 hc258001 function 1.0E-06 0.0 1
20535651 htvat 2580001 3
*
20535660 es258001 mult 0.00544 0.0 1
20535661 htvat 2580001 cntrlvar 3565
*
20535670 hc260001 function 1.0E-06 0.0 1
20535671 htvat 2600001 3
*
20535680 es260001 mult 0.00198 0.0 1
20535681 htvat 2600001 cntrlvar 3567
*
20535690 hc270001 function 1.0E-06 0.0 1
20535691 htvat 2700001 3
*
20535700 es270001 mult 0.00553 0.0 1
20535701 htvat 2700001 cntrlvar 3569
*
20535710 hc270002 function 1.0E-06 0.0 1
20535711 htvat 2700002 3
*
20535720 es270002 mult 0.00553 0.0 1
20535721 htvat 2700002 cntrlvar 3571
*
20535730 hc270003 function 1.0E-06 0.0 1
20535731 htvat 2700003 3
*
20535740 es270003 mult 0.00872 0.0 1
20535741 htvat 2700003 cntrlvar 3573
*
20535750 hc270004 function 1.0E-06 0.0 1
20535751 htvat 2700004 3
*
20535760 es270004 mult 0.00578 0.0 1
20535761 htvat 2700004 cntrlvar 3575
*
20535770 es-PCpip sum 1.0 0.0 1
20535771 0.0 1.0 cntrlvar 3472 1.0 cntrlvar 3474
20535772 1.0 cntrlvar 3476 1.0 cntrlvar 3478
20535773 1.0 cntrlvar 3480 1.0 cntrlvar 3482

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```

20535774 1.0 cntrlvar 3484 1.0 cntrlvar 3486
20535775 1.0 cntrlvar 3488 1.0 cntrlvar 3490
20535776 1.0 cntrlvar 3546 1.0 cntrlvar 3548
20535777 1.0 cntrlvar 3550 1.0 cntrlvar 3552
20535778 1.0 cntrlvar 3554 1.0 cntrlvar 3556
+ 1.0 cntrlvar 3558 1.0 cntrlvar 3560
+ 1.0 cntrlvar 3562 1.0 cntrlvar 3564
+ 1.0 cntrlvar 3566 1.0 cntrlvar 3568
+ 1.0 cntrlvar 3570 1.0 cntrlvar 3572
+ 1.0 cntrlvar 3574 1.0 cntrlvar 3576
*
20535780 es-PCS sum 1.0 0.0 1
20535781 0.0 1.0 cntrlvar 3468 1.0 cntrlvar 3577
*
*****
*
*
*****
* split hot duct input model
*****
* Input for a split hot duct is provided below. In addition to the hot duct, the
outlet plenum
* and RCST nodalizations are changed.
*
* The hot duct is split into top and bottom halves, and is extended to include all of
the
* piping between the pressure vessel and the RCST.
*
* The upper volume in the RCST is modeled as a large, short volume so that both the
top
* half of the hot duct and the cold duct can be connected to it. This provides a
large, well-mixed
* volume of gas to be circulated back into the primary coolant system. A small
* component is added to make the connection from the large RCST volume to the
* bottom of the hot duct.
*
* The outlet plenum is divided into four components: a volume at the top that connects
* to all of the core channels, a volume between this upper volume and the top half of
the
* hot duct, a vertical pipe containing most of the plenum volume (connected at the top
* to the upper volume), and a volume between the bottom half of the hot duct and the
pipe.
*
* The hot duct heat structures are changed to reflect the new nodalization, and one
* structure in the vessel outlet plenum has its left volume connection changed.
*
* Control variables are added and updated to reflect the new nodalization.
*
* Delete replaced/unneeded components and structures if renodalizing on a restart. If
* this model is being used for a new problem, delete or comment out the full component
input.
*
2050000 V-313 delete
2100000 hot-RCST delete
12100000 delete
*
* PSR-to-barrel gap outlet junction
*
1680000 PSRoutlt snljun
1680101 166150002 185010002 0.00596 0.84 0.46 0
1680201 0 0.0 0.0 0.0
*
* core outlet plenum

```

```

*
1750000 outplenm branch
1750001 2 1
1750101 0.7296 0.02000 0.0
1750102 0.0 -90.0 -0.02000
1750103 0.000046 0.097 0
1750200 3 1.00E+05 960.15
1751101 175010000 185000000 0.0 0.0 0.0 0
1752101 183010000 175010000 0.0 0.0 0.0 0
1751110 0.0 0.0 1.0 1.0
1752110 0.0 0.0 1.0 1.0
1751201 0.0 0.0 0.0
1752201 0.0 0.0 0.0
*
* outlet plenum volume connected to hot duct bottom half
*
1800000 opbothd branch
1800001 2 1
1800101 0.0365 0.16898 0.0
1800102 0.0 -90.0 -0.16898
1800103 0.000046 0.097 0
1800200 3 1.00E+05 960.15
1801101 206010000 180010003 0.0 0.0 0.0 0
1802101 180010002 183000000 0.0 0.0 0.0 0
1801110 0.0 0.0 1.0 1.0
1802110 0.0 0.0 1.0 1.0
1801201 0.0 0.0 0.0
1802201 0.0 0.0 0.0
*
* outlet plenum pipe
*
1830000 oplenum pipe
1830001 5
1830101 0.6931 5
1830301 0.04045 5
1830401 0.0 5
1830601 90.0 5
1830801 0.000046 0.097 5
1830901 0.0 0.0 4
1831001 0 5
1831101 0 4
1831201 3 1.00E+05 960.15 0.0 0.0 0.0 5
1831300 1
1831301 0.0 0.0 0.0 4
1831401 0.0 0.0 1.0 1.0 4
*
* outlet plenum volume connected to hot duct top half
*
1850000 optophd branch
1850001 1 1
1850101 0.0365 0.03327 0.0
1850102 0.0 -90.0 -0.03327
1850103 0.000046 0.097 0
1850200 3 1.00E+05 960.15
1851101 185010004 200000000 0.0 0.0 0.0 0
1851110 0.0 0.0 1.0 1.0
1851201 0.0 0.0 0.0
*
* hot duct top
*
2000000 "duct top" pipe
2000001 7
2000101 0.0349 4

```

```

2000102 0.0350 6
2000103 0.0350 7
2000301 0.43180 1
2000302 0.65095 2
2000303 0.41270 3
2000304 0.41270 4
2000305 0.49058 5
2000306 0.49058 6
2000307 0.66040 7
2001901 0.14898 7
2000401 0.0 7
2000601 0.0 7
2000801 0.000046 0.29797 4
2000802 0.000046 0.29845 6
2000803 0.000046 0.29845 7
2002401 0.0 0.0 7
2000901 0.0 0.0 4
2000902 0.057 0.057 5
2000903 0.0 0.0 6
2001001 0 7
2001101 0 6
2001201 3 1.00E+05 960.15 0.0 0.0 0.0 1
2001202 3 1.00E+05 960.15 0.0 0.0 0.0 2
2001203 3 1.00E+05 960.15 0.0 0.0 0.0 3
2001204 3 1.00E+05 960.15 0.0 0.0 0.0 4
2001205 3 1.00E+05 960.15 0.0 0.0 0.0 5
2001206 3 1.00E+05 960.15 0.0 0.0 0.0 6
2001207 3 1.00E+05 960.15 0.0 0.0 0.0 7
2001300 1
2001301 0.0 0.0 0.0 6
2001401 0.0 0.0 1.0 1.0 6
*
* hot duct top connection to RCST
*
2010000 "top-RCST" sngljun
2010101 200010000 280020003 0.0350 1.0 0.5 0
2010201 1 0.0 0.0 0.0
*
* hot duct bottom
*
2060000 "duct bot" pipe
2060001 7
2060101 0.0350 1
2060102 0.0350 3
2060103 0.0349 7
2060301 0.66040 1
2060302 0.49058 2
2060303 0.49058 3
2060304 0.41270 4
2060305 0.41270 5
2060306 0.65095 6
2060307 0.43180 7
2061901 0.05327 7
2060401 0.0 7
2060601 0.0 7
2060801 0.000046 0.29845 1
2060802 0.000046 0.29845 3
2060803 0.000046 0.29797 7
2062401 0.0 0.0 7
2060901 0.0 0.0 1
2060902 0.06 0.06 2
2060903 0.0 0.0 6
2061001 0 7

```

```

2061101 0 6
2061201 3 1.00E+05 960.15 0.0 0.0 0.0 1
2061202 3 1.00E+05 960.15 0.0 0.0 0.0 2
2061203 3 1.00E+05 960.15 0.0 0.0 0.0 3
2061204 3 1.00E+05 960.15 0.0 0.0 0.0 4
2061205 3 1.00E+05 960.15 0.0 0.0 0.0 5
2061206 3 1.00E+05 960.15 0.0 0.0 0.0 6
2061207 3 1.00E+05 960.15 0.0 0.0 0.0 7
2061300 1
2061301 0.0 0.0 0.0 6
2061401 0.0 0.0 1.0 1.0 6
*
* connections between hot duct top and bottom volumes
*
2090000 hotduct mtpljun
2090001 7 1
* 0nnm from to area kfor krev efvcahs sub 2ph sup
2090011 206070006 200010005 0.12866 0.1 0.1 0 1.0 1.0 1.0
* inc-frm inc-to 0 limit
2090012 0 0 0 1
* 0nnm from to area kfor krev efvcahs sub 2ph sup
2090021 206060006 200020005 0.19396 0.1 0.1 0 1.0 1.0 1.0
* inc-frm inc-to 0 limit
2090022 0 0 0 2
* 0nnm from to area kfor krev efvcahs sub 2ph sup
2090031 206050006 200030005 0.12297 0.1 0.1 0 1.0 1.0 1.0
* inc-frm inc-to 0 limit
2090032 0 0 0 3
* 0nnm from to area kfor krev efvcahs sub 2ph sup
2090041 206040006 200040005 0.12297 0.1 0.1 0 1.0 1.0 1.0
* inc-frm inc-to 0 limit
2090042 0 0 0 4
* 0nnm from to area kfor krev efvcahs sub 2ph sup
2090051 206030006 200050005 0.14641 0.1 0.1 0 1.0 1.0 1.0
* inc-frm inc-to 0 limit
2090052 0 0 0 5
* 0nnm from to area kfor krev efvcahs sub 2ph sup
2090061 206020006 200060005 0.14641 0.1 0.1 0 1.0 1.0 1.0
* inc-frm inc-to 0 limit
2090062 0 0 0 6
* 0nnm from to area kfor krev efvcahs sub 2ph sup
2090071 206010006 200070005 0.19710 0.1 0.1 0 1.0 1.0 1.0
* inc-frm inc-to 0 limit
2090072 0 0 0 7
* lnnm mflowf mflowg #
2091011 0.0 0.0 1
2091021 0.0 0.0 2
2091031 0.0 0.0 3
2091041 0.0 0.0 4
2091051 0.0 0.0 5
2091061 0.0 0.0 6
2091071 0.0 0.0 7
* 2nnm Dhyd b c m #
2092011 0.0 0.0 1.0 1.0 1
2092021 0.0 0.0 1.0 1.0 2
2092031 0.0 0.0 1.0 1.0 3
2092041 0.0 0.0 1.0 1.0 4
2092051 0.0 0.0 1.0 1.0 5
2092061 0.0 0.0 1.0 1.0 6
2092071 0.0 0.0 1.0 1.0 7
*
* reactor cavity simulation tank (two-volume configuration)
*

```

```

2800000 RCST pipe
2800001 2
2800101 0.0 2
2800301 1.5240 1
2800302 0.14898 2
2800401 3.8 1
2800402 14.1 2
2800601 90.0 2
2800701 1.5240 1
2800702 0.14898 2
2800801 0.000046 2.0828 2
2800901 0.0 0.0 1
2801001 0 2
2801101 0 1
2801201 3 1.00E+05 300.00 0.0 0.0 0.0 2
2801300 1
2801301 0.0 0.0 0.0 1
*
* small RCST volume connected to hot duct bottom half
*
2820000 optophd branch
2820001 2 1
2820101 0.0340 0.02663 0.0
2820102 0.0 -90.0 -0.02663
2820103 0.000000 2.083 0
2820200 3 1.00E+05 300.00
2821101 280020001 282000000 0.0 0.0 0.0 0
2822101 282010000 206000000 0.0350 0.5 1.0 0
2821110 0.0 0.0 1.0 1.0
2822110 0.0 0.0 1.0 1.0
2821201 0.0 0.0 0.0
2822201 0.0 0.0 0.0
*
* outlet plenum lower plate - heat structure 1750
*
11750000 1 9 1 0 0.0 0
11750100 0 1
11750101 4 0.079375
11750102 2 0.111375
11750103 2 0.136775
11750201 -1 4
11750202 -1 6
11750203 3 8
11750301 0.0 8
11750400 -1
11750401 960.0 960.0 900.0 900.0 800.0 700.0 700.0 600.0 600.0
11750501 183010000 0 1 1 1.7713 1
11750601 105020000 0 1 1 1.7713 1
11750701 0 0.0 0.0 0.0 1
11750800 1
11750801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.14 1.1 1.0 1
11750900 1
11750901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.14 1.1 1.0 1
*
* hot duct top half, volumes 1-4 - heat structure 2000
*
12000000 4 9 2 0 0.148984 0
12000100 0 1
12000101 1 0.1524
12000102 4 0.161925
12000103 3 0.1653413
12000201 3 1 * 304 stainless steel
12000202 -8 5 * alumina silica insulation

```



```

12000203 3 8 * 304 stainless steel
12000301 0.0 8
12000400 -1
12000401 900.0 800.0 700.0 600.0 500.0 450.0 400.0 350.0 300.0
12000402 900.0 800.0 700.0 600.0 500.0 450.0 400.0 350.0 300.0
12000403 900.0 800.0 700.0 600.0 500.0 450.0 400.0 350.0 300.0
12000404 900.0 800.0 700.0 600.0 500.0 450.0 400.0 350.0 300.0
12000501 200010000 0 1 1 0.2159 1
12000502 200020000 0 1 1 0.3255 2
12000503 200030000 0 1 1 0.2064 3
12000504 200040000 0 1 1 0.2064 4
12000601 270040000 0 1 1 0.2159 1
12000602 270030000 0 1 1 0.3255 2
12000603 270020000 0 1 1 0.2064 3
12000604 270010000 0 1 1 0.2064 4
12000701 0 0.0 0.0 0.0 4
12000800 1
12000801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 4
12000900 1
12000901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.33 1.1 1.0 4
*
* hot duct top half, volumes 5 and 6 - heat structure 2001
*
12001000 2 7 2 0 0.149225 0
12001100 0 1
12001101 3 0.161925
12001102 3 0.212925
12001201 3 3 * 304 stainless steel
12001202 -9 6 * pipe insulation
12001301 0 6
12001400 -1
12001401 400.0 400.0 400.0 350.0 350.0 300.0 300.0
12001402 400.0 400.0 400.0 350.0 350.0 300.0 300.0
12001501 200050000 10000 1 1 0.2453 2
12001601 -950 0 3951 1 0.2453 2
12001701 0 0.0 0.0 0.0 2
12001800 1
12001801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 2
*
* hot duct top half, volume 7 - heat structure 2002
*
12002000 1 4 2 0 0.1492 0
12002100 0 1
12002101 3 0.161925
12002201 3 3 * 304 stainless steel
12002301 0.0 3
12002400 -1
12002401 400.0 400.0 350.0 300.0
12002501 200070000 0 1 1 0.3302 1
12002601 280020000 0 1 1 0.3302 1
12002701 0 0.0 0.0 0.0 1
12002800 1
12002801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 1
12002900 1
12002901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.32 1.1 1.0 1
*
* hot duct bottom half, volume 1 - heat structure 2060
*
12060000 1 4 2 0 0.1492 0
12060100 0 1
12060101 3 0.161925
12060201 3 3 * 304 stainless steel
12060301 0.0 3

```

```

12060400 -1
12060401 400.0 400.0 350.0 300.0
12060501 206010000 0 1 1 0.3302 1
12060601 280020000 0 1 1 0.3302 1
12060701 0 0.0 0.0 0.0 1
12060800 1
12060801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 1
12060900 1
12060901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.32 1.1 1.0 1
*
* hot duct bottom half, volumes 2 and 3 - heat structure 2061
*
12061000 2 7 2 0 0.149225 0
12061100 0 1
12061101 3 0.161925
12061102 3 0.212925
12061201 3 3 * 304 stainless steel
12061202 -9 6 * pipe insulation
12061301 0 6
12061400 -1
12061401 400.0 400.0 400.0 350.0 350.0 300.0 300.0
12061402 400.0 400.0 400.0 350.0 350.0 300.0 300.0
12061501 206020000 10000 1 1 0.2453 2
12061601 -950 0 3951 1 0.2453 2
12061701 0 0.0 0.0 0.0 2
12061800 1
12061801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 2
*
* hot duct bottom half, volumes 4-7 - heat structure 2062
*
12062000 4 9 2 0 0.148984 0
12062100 0 1
12062101 1 0.1524
12062102 4 0.161925
12062103 3 0.1653413
12062201 3 1 * 304 stainless steel
12062202 -8 5 * alumina silica insulation
12062203 3 8 * 304 stainless steel
12062301 0.0 8
12062400 -1
12062401 900.0 800.0 700.0 600.0 500.0 450.0 400.0 350.0 300.0
12062402 900.0 800.0 700.0 600.0 500.0 450.0 400.0 350.0 300.0
12062403 900.0 800.0 700.0 600.0 500.0 450.0 400.0 350.0 300.0
12062404 900.0 800.0 700.0 600.0 500.0 450.0 400.0 350.0 300.0
12062501 206040000 0 1 1 0.2064 1
12062502 206050000 0 1 1 0.2064 2
12062503 206060000 0 1 1 0.3255 3
12062504 206070000 0 1 1 0.2159 4
12062601 270010000 0 1 1 0.2064 1
12062602 270020000 0 1 1 0.2064 2
12062603 270030000 0 1 1 0.3255 3
12062604 270040000 0 1 1 0.2159 4
12062701 0 0.0 0.0 0.0 4
12062800 1
12062801 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.30 1.1 1.0 4
12062900 1
12062901 0.0 1.0 1.0 0.0 0.0 0.0 0.0 1.0 0.33 1.1 1.0 4
*
* control variables
*
* environmental heat loss calculations
*
20514010 hs200ehl sum 1.0 0.0 1

```

```

20514011  0.0  0.328  htrnr  200100101  0.328  htrnr  200100201
20514012  0.328  htrnr  206100101  0.328  htrnr  206100201
*
* coolant mass calculations
*
20516150  masshleg  sum  1.0  0.0  1
20516151  0.0  1.0  tmassv  200010000  1.0  tmassv  200020000
20516152  1.0  tmassv  200030000  1.0  tmassv  200040000
20516153  1.0  tmassv  200050000  1.0  tmassv  200060000
20516154  1.0  tmassv  200070000  1.0  tmassv  206010000
20516155  1.0  tmassv  206020000  1.0  tmassv  206030000
20516156  1.0  tmassv  206040000  1.0  tmassv  206050000
20516157  1.0  tmassv  206060000  1.0  tmassv  206070000
*
20516210  massRCST  sum  1.0  0.0  1
20516211  0.0  1.0  tmassv  282010000  1.0  tmassv  258010000
20516212  1.0  tmassv  280010000  1.0  tmassv  280020000
*
* structure energy storage calculations
*
20534720  es200001  mult  0.00146  0.0  1
20534721  htvat  2000001  cntrlvar  3471
*
20534740  es200002  mult  0.00220  0.0  1
20534741  htvat  2000002  cntrlvar  3473
*
20534760  es200003  mult  0.00139  0.0  1
20534761  htvat  2000003  cntrlvar  3475
*
20534780  es200004  mult  0.00139  0.0  1
20534781  htvat  2000004  cntrlvar  3477
*
20534800  es200101  mult  0.00305  0.0  1
20534801  htvat  2001001  cntrlvar  3479
*
20534820  es200102  mult  0.00305  0.0  1
20534821  htvat  2001002  cntrlvar  3481
*
20534830  hc200201  function  1.0E-06  0.0  1
20534831  htvat  2002001  3
*
20534840  es200201  mult  0.00410  0.0  1
20534841  htvat  2002001  cntrlvar  3483
*
20535770  es-PCpip  sum  1.0  0.0  1
20535771  0.0  1.0  cntrlvar  3472  1.0  cntrlvar  3474
20535772  1.0  cntrlvar  3476  1.0  cntrlvar  3478
20535773  1.0  cntrlvar  3480  1.0  cntrlvar  3482
20535774  1.0  cntrlvar  3484  1.0  cntrlvar  3486
20535775  1.0  cntrlvar  3488  1.0  cntrlvar  3490
20535776  1.0  cntrlvar  3546  1.0  cntrlvar  3548
20535777  1.0  cntrlvar  3550  1.0  cntrlvar  3552
20535778  1.0  cntrlvar  3554  1.0  cntrlvar  3556
+ 1.0  cntrlvar  3558  1.0  cntrlvar  3560
+ 1.0  cntrlvar  3562  1.0  cntrlvar  3564
+ 1.0  cntrlvar  3566  1.0  cntrlvar  3568
+ 1.0  cntrlvar  3570  1.0  cntrlvar  3572
+ 1.0  cntrlvar  3574  1.0  cntrlvar  3576
+ 1.0  cntrlvar  3582  1.0  cntrlvar  3584
+ 1.0  cntrlvar  3586  1.0  cntrlvar  3588
+ 1.0  cntrlvar  3590  1.0  cntrlvar  3592
+ 1.0  cntrlvar  3594
*

```

```
20535810 hc206001 function 1.0E-06 0.0 1
20535811 htvat 2060001 3
*
20535820 es206001 mult 0.00410 0.0 1
20535821 htvat 2060001 cntrlvar 3581
*
20535830 hc206101 function 1.0E-06 0.0 1
20535831 htvat 2061001 3
*
20535840 es206101 mult 0.00305 0.0 1
20535841 htvat 2061001 cntrlvar 3583
*
20535850 hc206102 function 1.0E-06 0.0 1
20535851 htvat 2061002 3
*
20535860 es206102 mult 0.00305 0.0 1
20535861 htvat 2061002 cntrlvar 3585
*
20535870 hc206201 function 1.0E-06 0.0 1
20535871 htvat 2062001 3
*
20535880 es206201 mult 0.00139 0.0 1
20535881 htvat 2062001 cntrlvar 3587
*
20535890 hc206202 function 1.0E-06 0.0 1
20535891 htvat 2062002 3
*
20535900 es206202 mult 0.00139 0.0 1
20535901 htvat 2062002 cntrlvar 3589
*
20535910 hc206203 function 1.0E-06 0.0 1
20535911 htvat 2062003 3
*
20535920 es206203 mult 0.00220 0.0 1
20535921 htvat 2062003 cntrlvar 3591
*
20535930 hc206204 function 1.0E-06 0.0 1
20535931 htvat 2062004 3
*
20535940 es206204 mult 0.00146 0.0 1
20535941 htvat 2062004 cntrlvar 3593
*
```