



GCR: Alloy 617 Notch Effect Testing Status

June 2022

Changing the World's Energy Future

Ryann Elizabeth Bass



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**Idaho National Laboratory
Idaho Falls, Idaho 83415**

<http://www.inl.gov>

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Ryann Bass
Idaho National Laboratory (INL)

Contributors

- Ryann Bass, Mike McMurtrey, Joseph Bass, and Sam Sham (INL)
- Richard Wright (Structural Alloys, LLC, formerly INL)
- Mark Messner (Argonne National Laboratory)

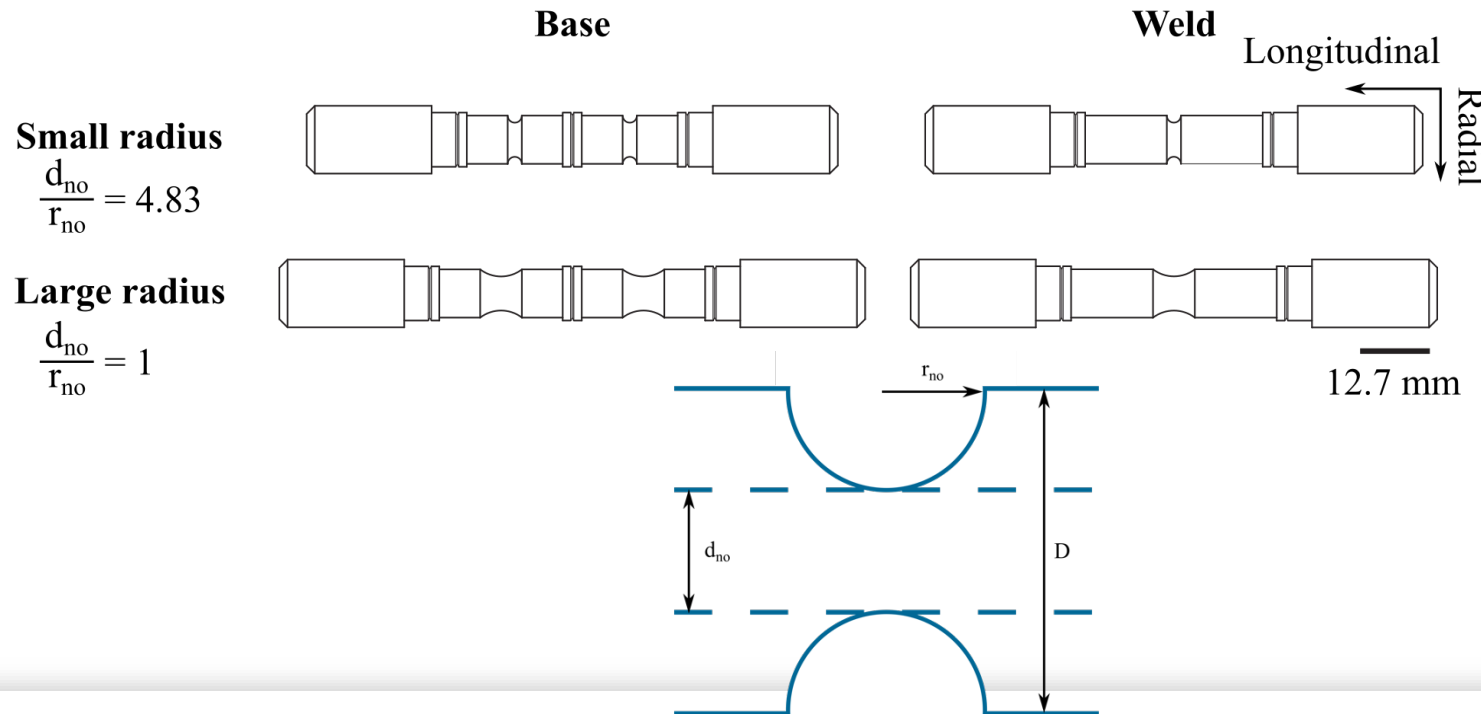
Fiscal Year 2022 (FY-22) Work Packages

- AT-22IN060405, Long-Term VHTR Material Qualification - INL

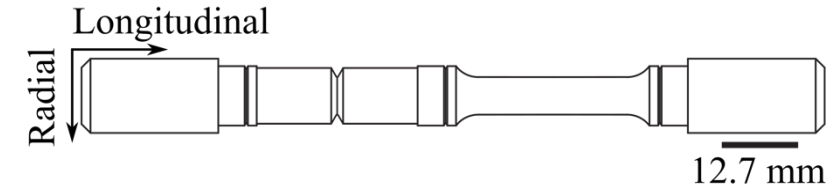
Introduction

A Nuclear Regulatory Commission (NRC)-sponsored assessment of a previous version of Section III, Division 5 of the American Society of Mechanical Engineers (ASME) Boiler and Pressure Vessel Code (BPVC) identified an inadequate understanding of the impact of a multiaxial stress, structural discontinuities, and notch effects.

U-notch (Bridgman notch)

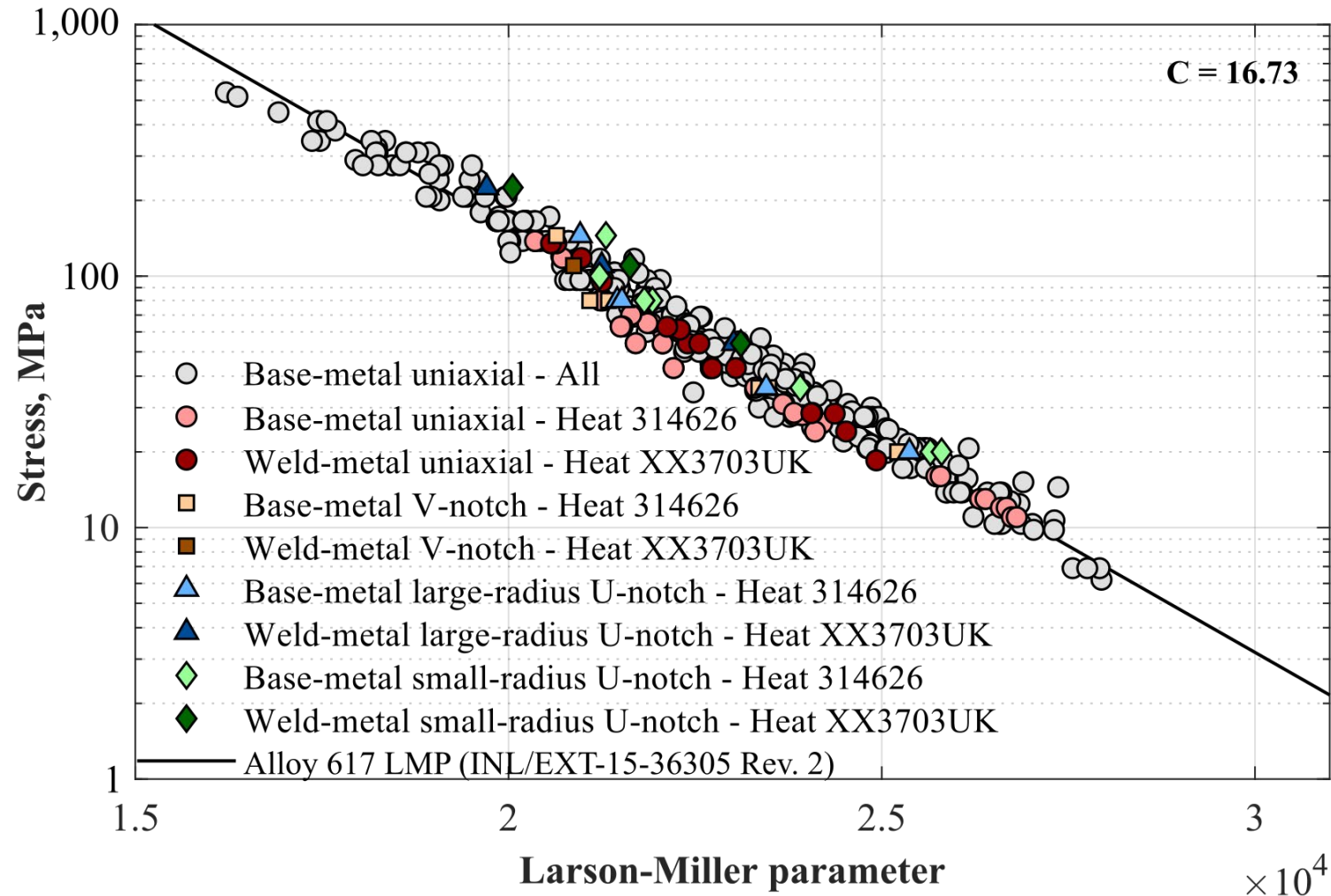


V-notch



Short term

Alloy 617 base- and weld-metal short-term (aim 1,000 to 2,000-hour rupture life) creep-rupture properties were not degraded by geometric discontinuities nor multiaxial-stress states.



Short term

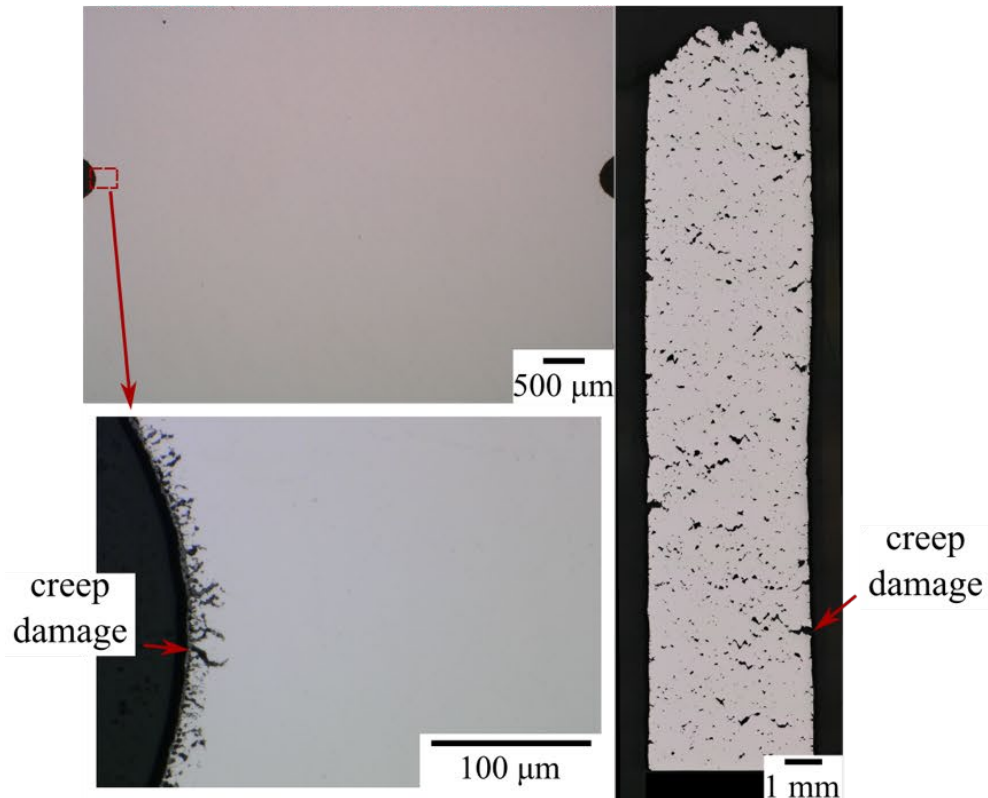
Alloy 617 was found to be notch strengthening.

Base

(800°C, 80 MPa)

V-notch

Straight gauge



Weld

(800°C, 110 MPa)

V-notch

Straight gauge

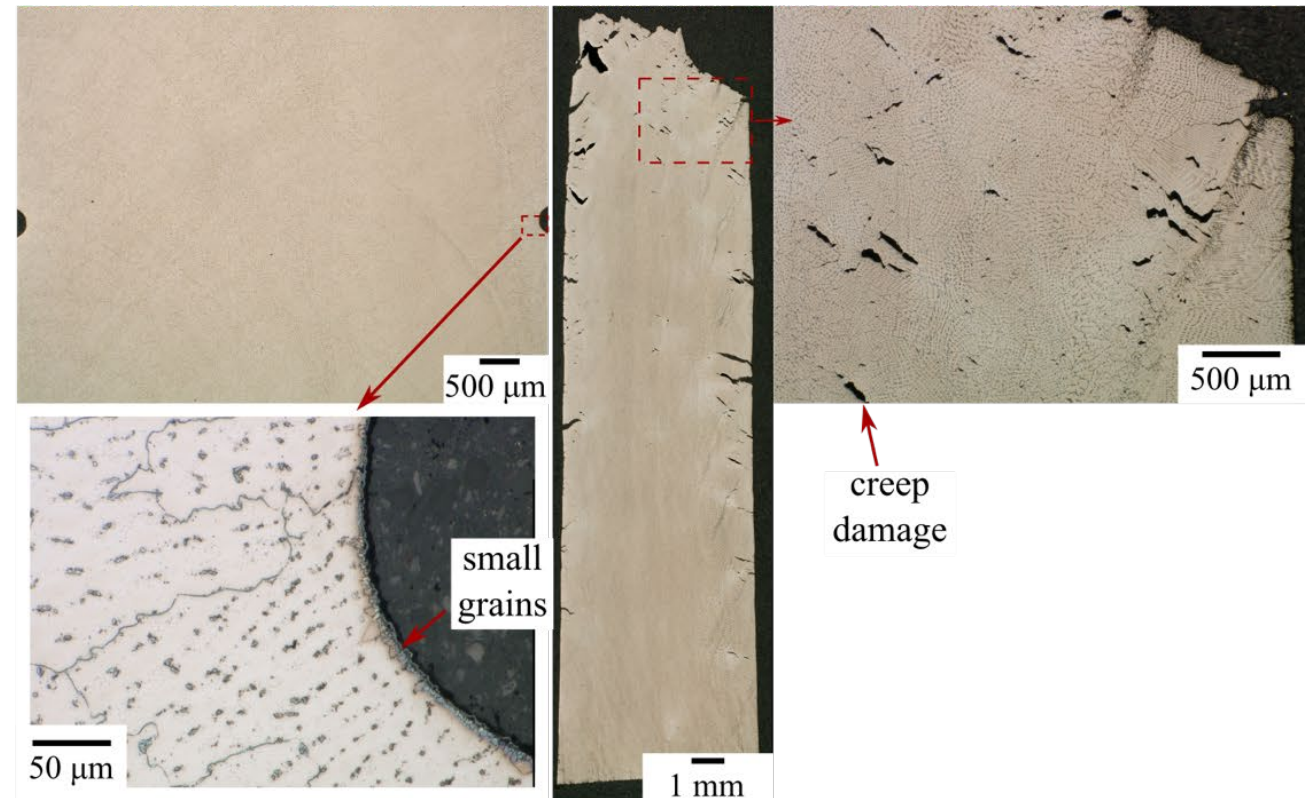
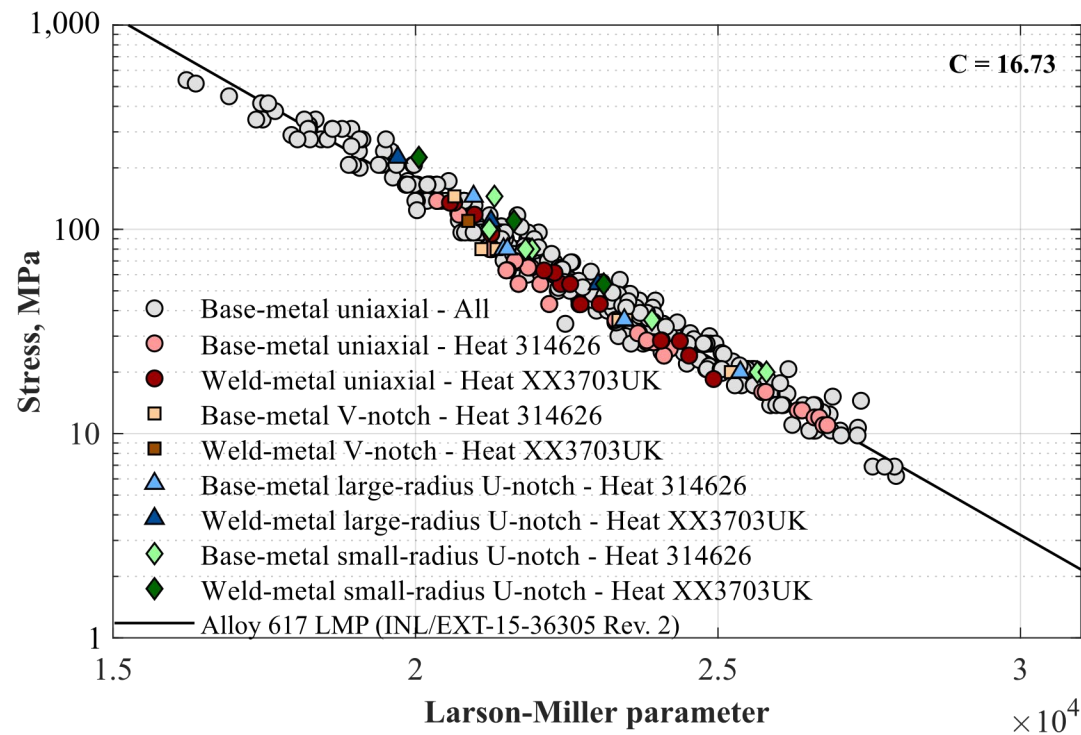


Figure modified from: Rupp, R.E., & McMurtrey, M.D. (2020). The Impact of Geometric Discontinuities on Alloy 617 Creep-Rupture Behavior (PVP2020-21587). In *Proceedings of the ASME 2020 Pressure Vessels & Piping Conference*. The American Society of Mechanical Engineers.

Short term

A stronger multiaxial stress increased the rupture life. This may be a consequence of the notch strengthening nature of the material.



1,000°C, 20 MPa

Small radius



Large radius

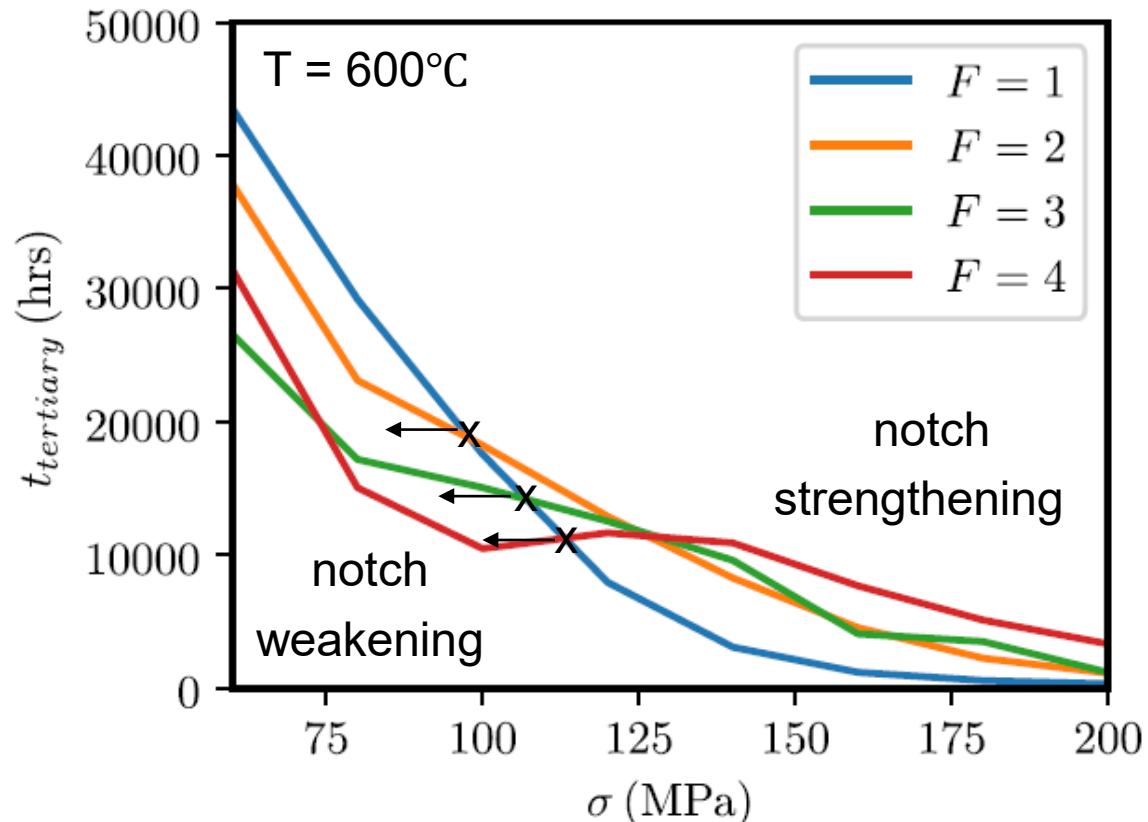


1 mm

Right figure from: Rupp, R.E., & McMurtrey, M.D. (2020). The Impact of Geometric Discontinuities on Alloy 617 Creep-Rupture Behavior (PVP2020-21587). In *Proceedings of the ASME 2020 Pressure Vessels & Piping Conference*. The American Society of Mechanical Engineers.

Intermediate length and long term

- Notch rupture behavior is sensitive to a variety of elements including temperature and stress. Consequently, there is a concern of notch weakening at temperature and stress combinations that result in a long rupture life.
- Intermediate-length (aim 8,000 to 12,000-hour rupture life) and long-term (aim 100,000-hour rupture life) creep-rupture testing of the base- and weld-metal are in progress.



$$F = 3 \frac{\sigma_m}{\sigma_e}$$

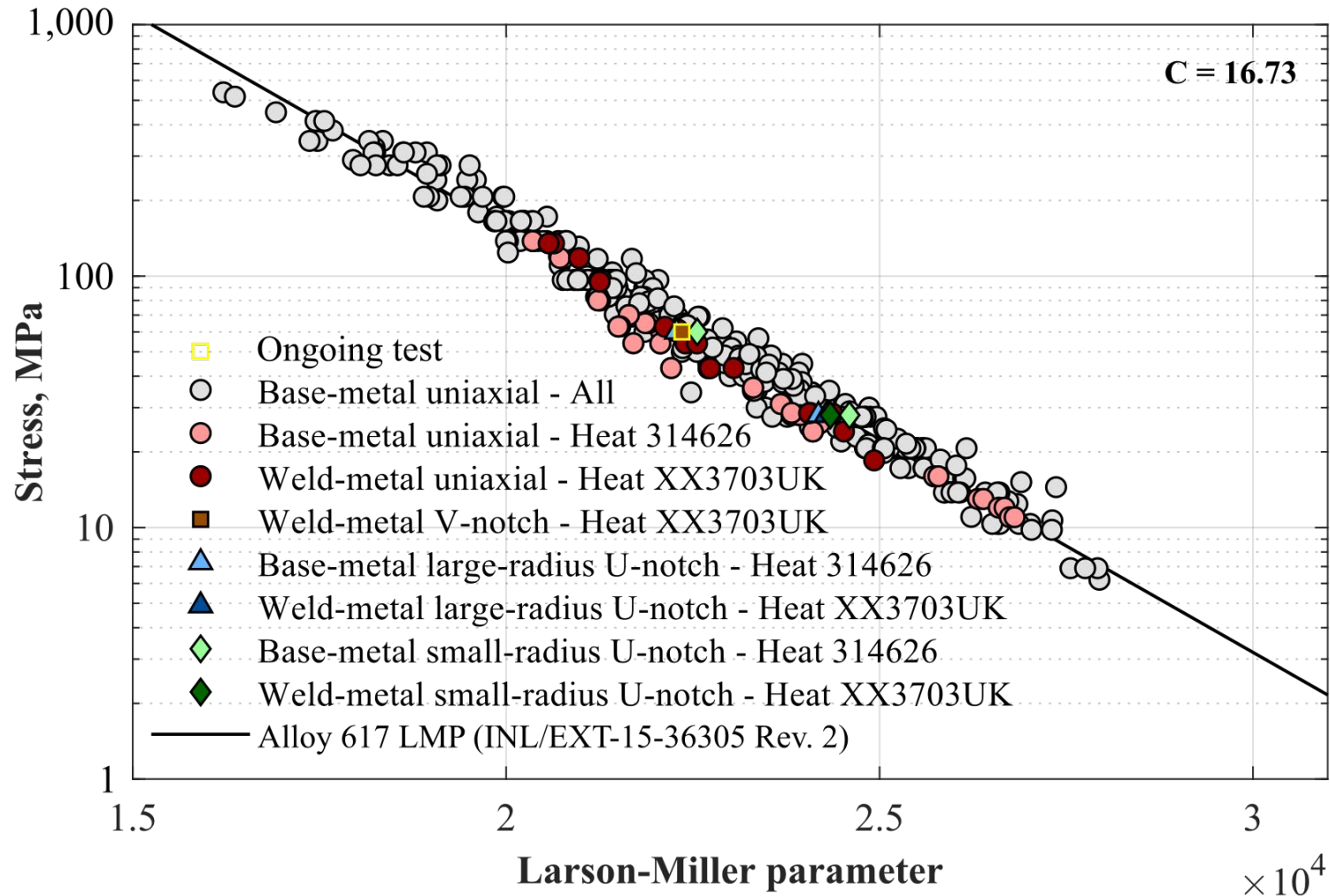
F = triaxiality ratio

σ_m = mean stress

σ_e = effective stress

Intermediate length

Alloy 617 base- and weld-metal intermediate-length (aim 8,000 to 12,000-hour rupture life) creep-rupture properties were not degraded by geometric discontinuities nor multiaxial-stress states. A stronger multiaxial stress increased the rupture life.



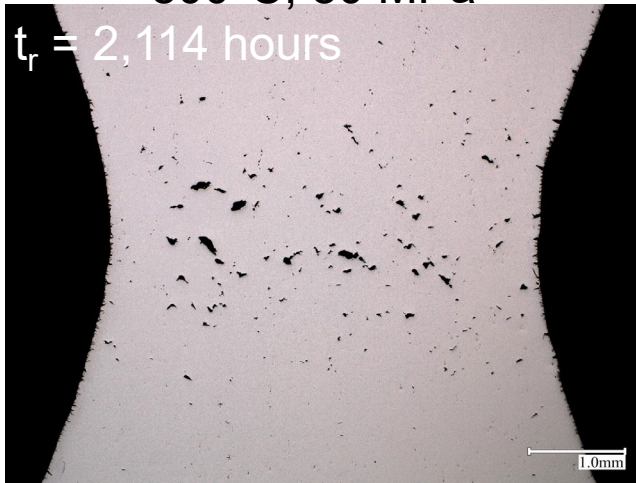
Intermediate length

The distribution of creep damage in the unruptured U-notch base-metal specimens after short-term and intermediate-length creep-rupture testing is similar.

Short term

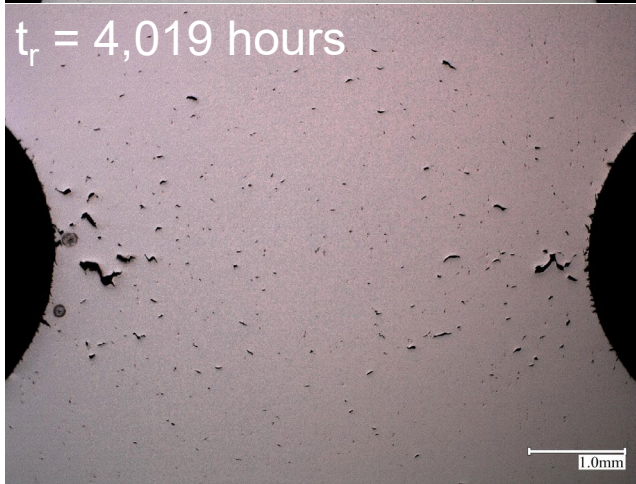
800°C, 80 MPa

$t_r = 2,114$ hours



Large-
radius
U-notch

$t_r = 4,019$ hours



Small-
radius
U-notch

Intermediate length

800°C, 60 MPa

$t_r = 10,873$ hours



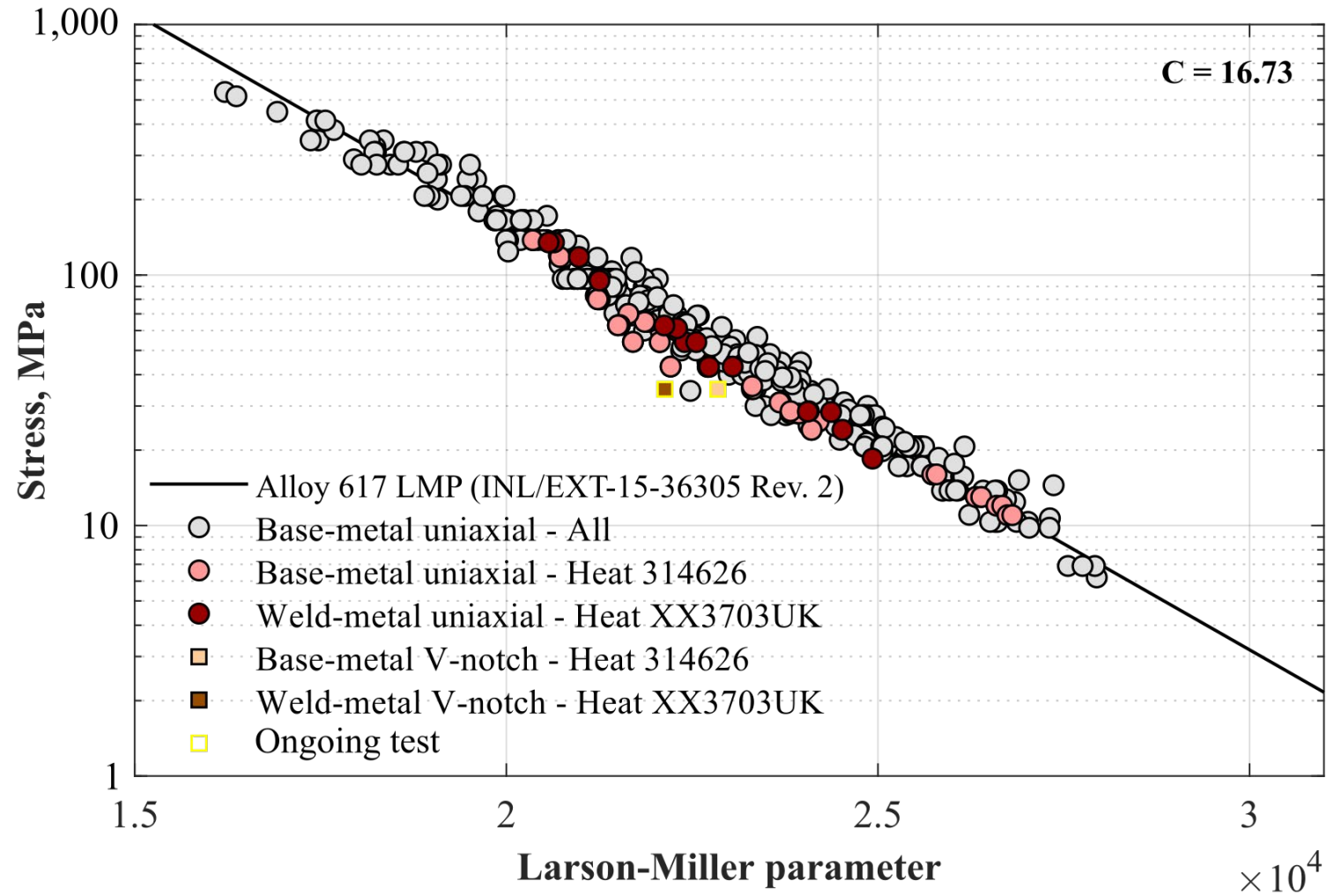
$t_r = 19,650$ hours



1.0 mm

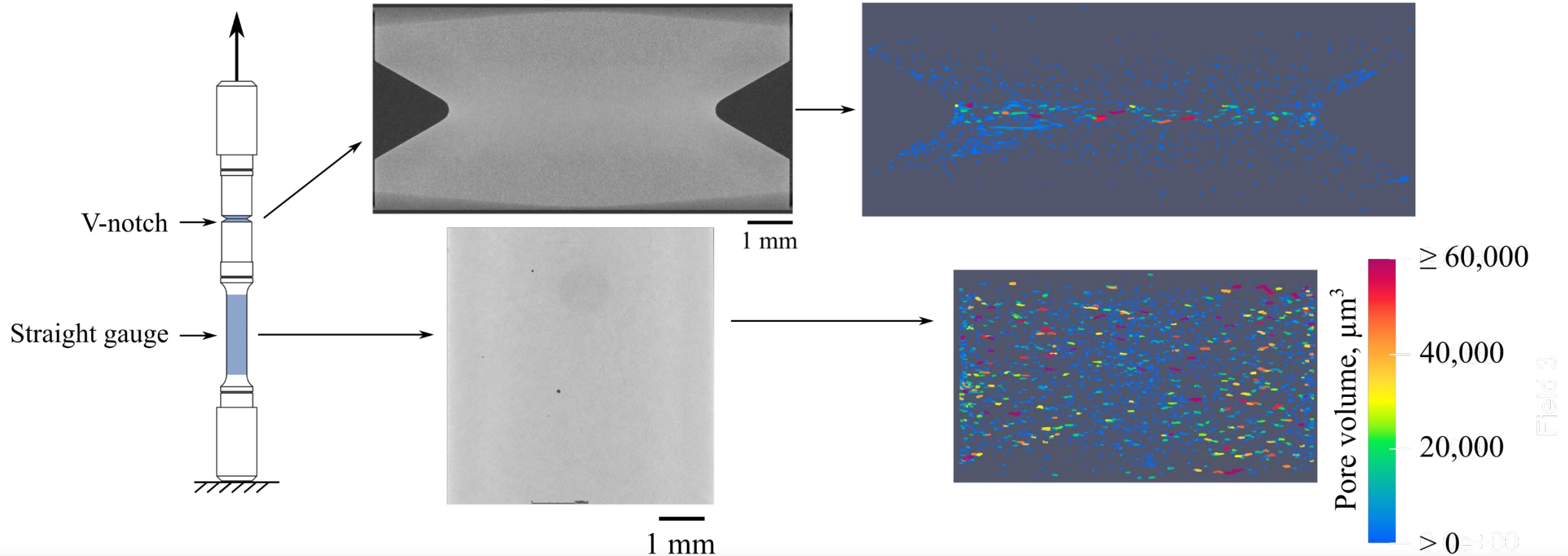
Long term

A base- and a weld-metal V-notch creep-rupture test with an estimated 100,000-hour rupture life are in progress.



X-ray CT characterization

A technique utilizing X-ray computed tomography (CT) was developed with the goal of being able to identify the failure location prior to rupture.



Baseline

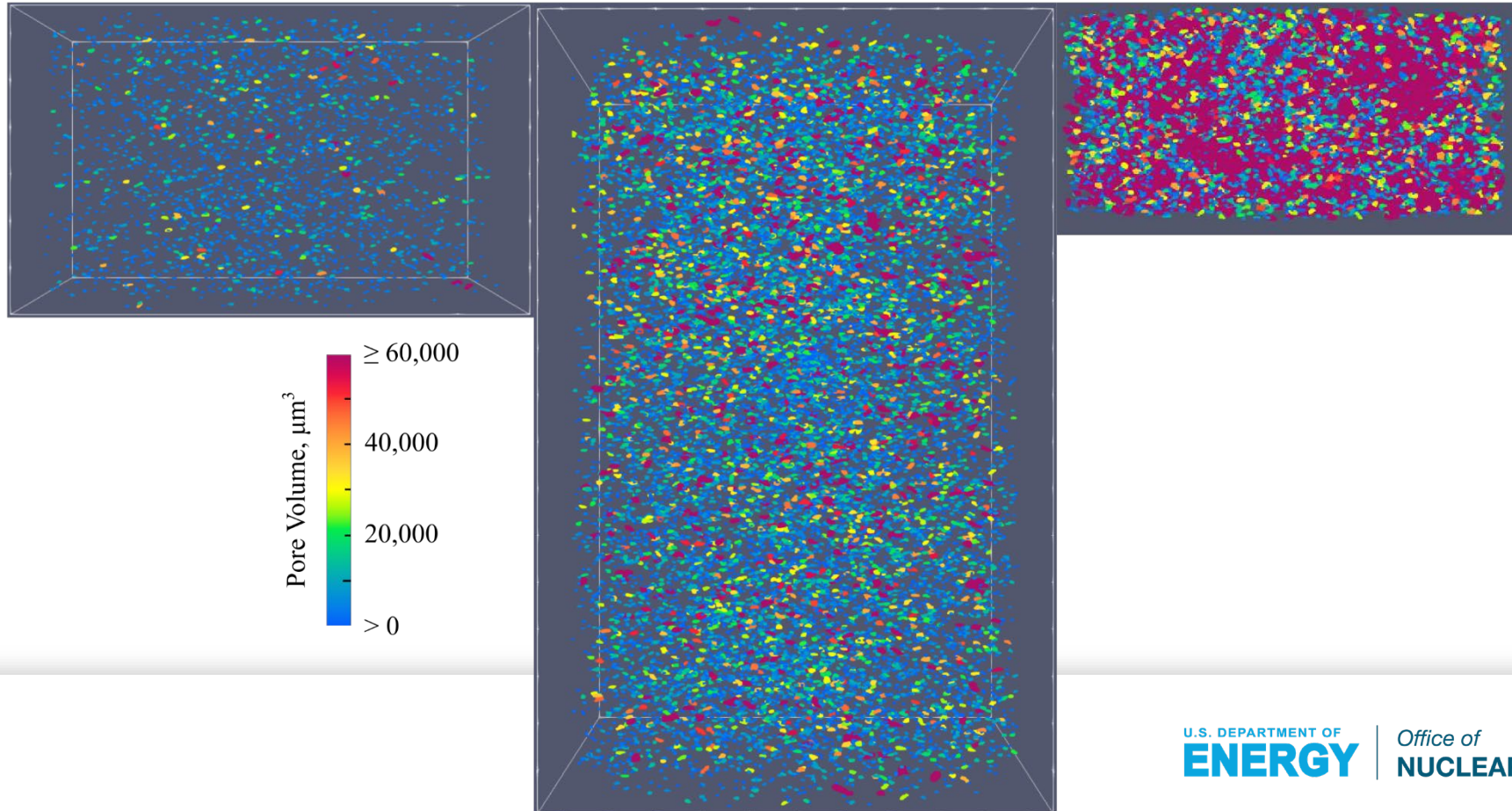
A base-metal V-notch specimen tested at 800°C and 65.3 MPa ruptured in the straight gauge. As the test progressed, the number and size of the cavities in the straight gauge increased.

2,005 hours (71% life)
0.02% porosity

2,500 hours (89% life)
0.1% porosity

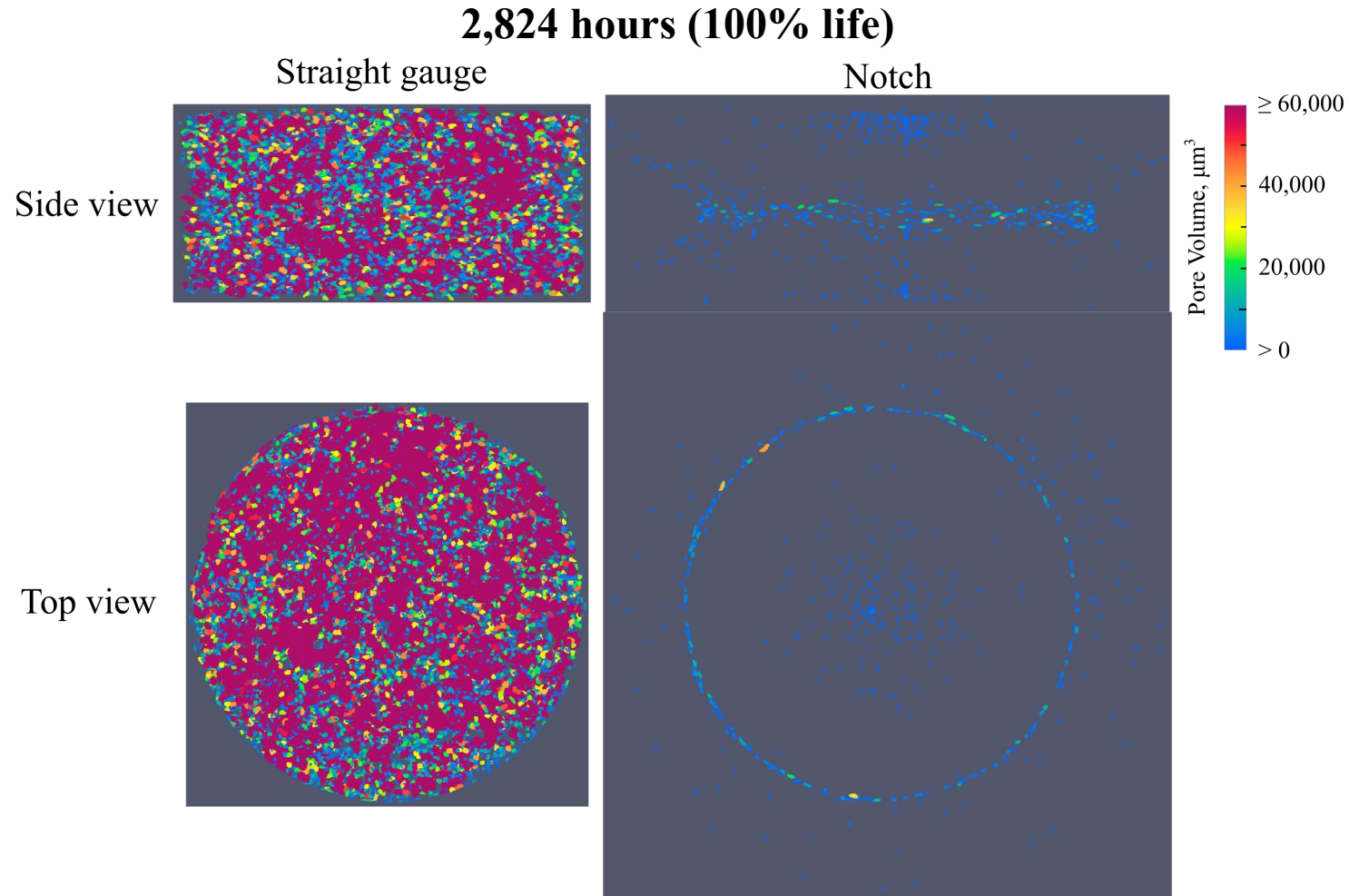
2,824 hours (100% life)
1.87% porosity

Straight gauge



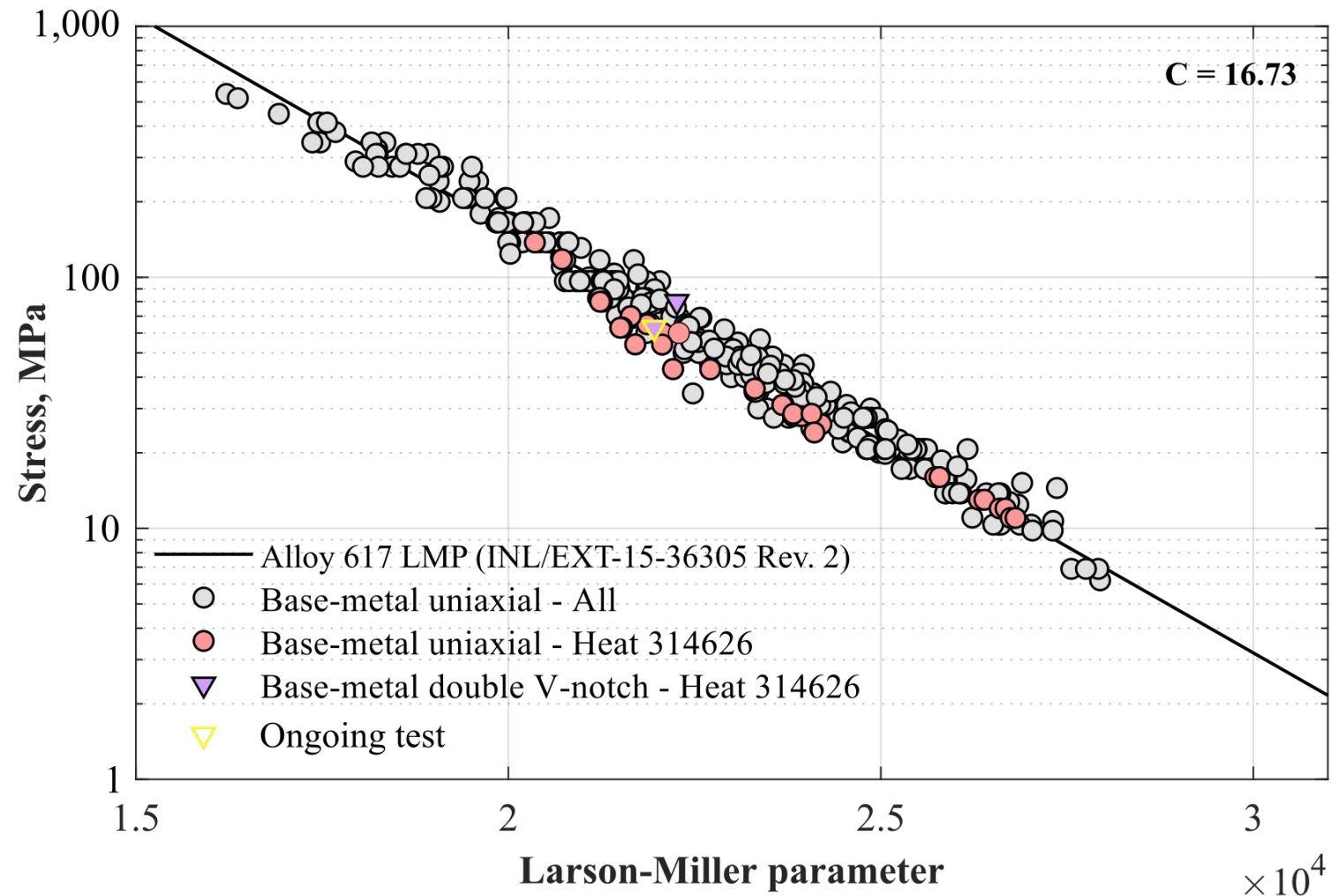
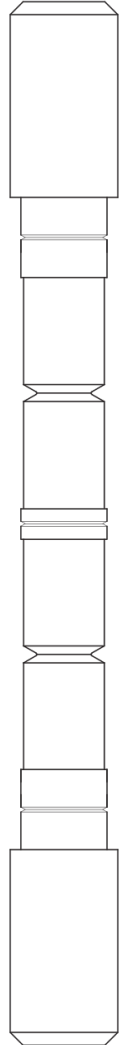
Baseline

No cavities larger than the resolution of the X-ray CT were detected in the notch for the base-metal specimen tested at 800°C and 65.3 MPa for the two scans collected prior to rupture. Damage in the notch was primarily limited to the surface at the notch tip.



V-notch characterization

All completed V-notch creep-rupture tests have failed in the straight gauge with little to no creep damage observed in the V-notch.

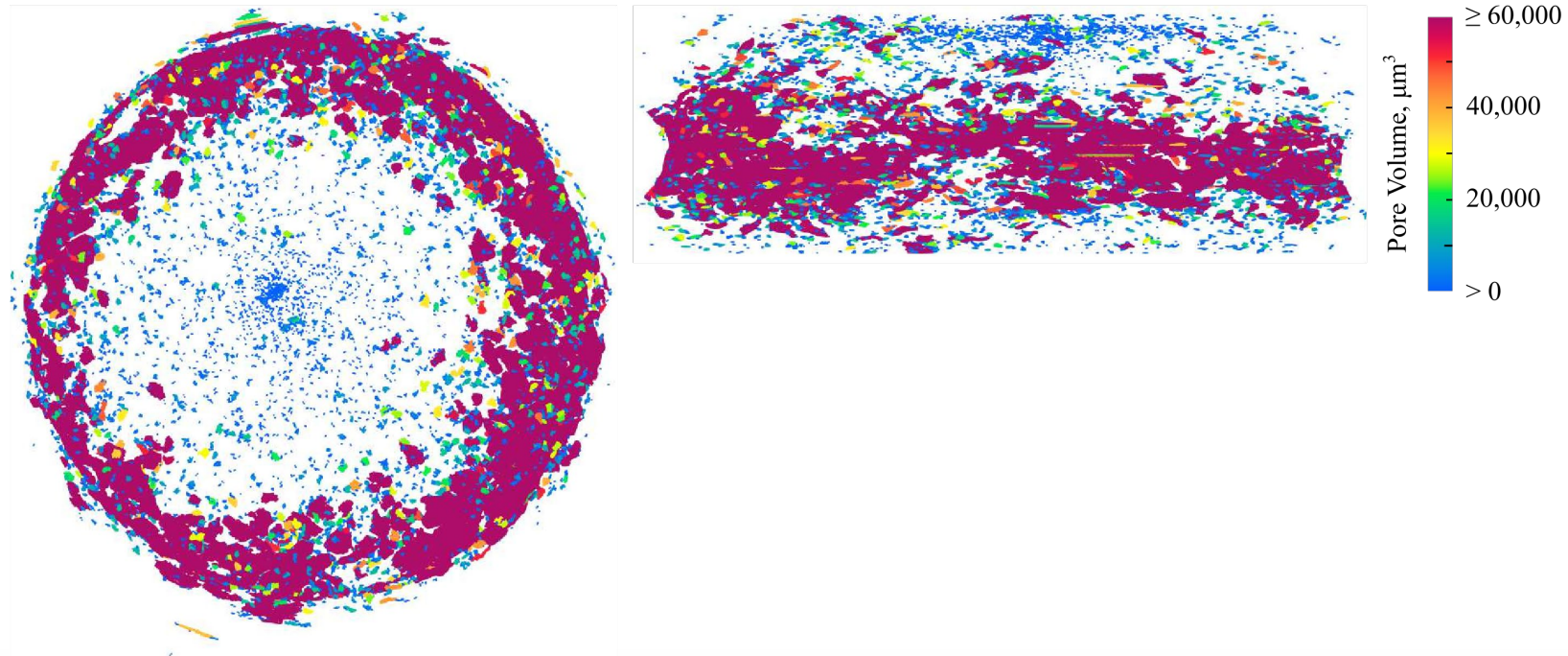


V-notch characterization

Work is in progress to characterize the distribution of creep damage in the V-notch and to correlate it with the percent of rupture life. Most of the creep damage in the non-ruptured V-notch for a base-metal double V-notch specimen tested at 800°C and 80 MPa to rupture was primarily limited to the surface of the specimen at the minimum diameter.

Top view

Side view



Summary

- Alloy 617 base- and weld-metal short-term (aim 1,000 to 2,000-hour rupture life) and intermediate length (aim 8,000 to 12,000-hour rupture life) creep-rupture properties were not degraded by geometric discontinuities nor multiaxial-stress states.
- Work is ongoing at INL to
 - Evaluate the various damage models by comparing creep damage predicted by finite element modeling with experimental observations.
 - Continue conducting long-term creep-rupture tests and periodically characterize these specimens with X-ray CT.
 - Continue conducting intermediate-length tests and characterize specimens of interest with light optical microscopy.
 - Continue conducting baseline testing with periodic X-ray CT characterization in order to correlate creep damage to rupture life.
 - Utilize the double V-notch specimen to characterize creep damage in the V-notch and quantify the notch strengthening effect.

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