

Powder Metallurgy Hot Isostatic Pressing of 316H Stainless Steel

June 2023

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Powder Metallurgy – Hot Isostatic Pressing of 316H Stainless Steel

ASME Code Case Development in Support of Microreactors

Joint ART Materials/AMMT Program Review DOE Headquarters, Germantown, MD June 5-8, 2023

Tate Patterson
Idaho National Laboratory

Fiscal Year 2023 Work Package

AT-23IN0804094 – Structural Materials

Team

- Tate Patterson (INL)
- Ryann Bass (now at US NRC)
- Richard Wright (Structural Alloys, LLC)
- Sam Sham (INL)

Background

- Powder metallurgy hot isostatic pressing (PM-HIP) is a manufacturing technique to produce metallic components by consolidating metal powder
 - Minimizes additional fabrication steps
 - Eliminates directional grains and solidification structures







UK - Nuclear Advanced Manufacturing Research Center (NAMRC) System

PM-HIP Adoption for Microreactors

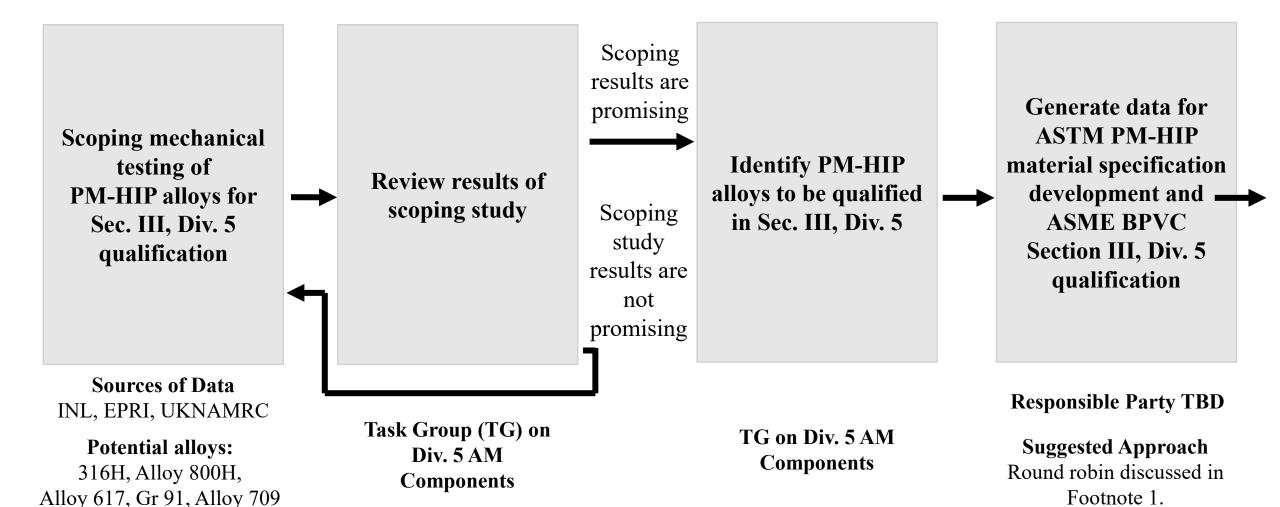
PM-HIP can benefit microreactor construction to optimize designs, reduce construction time, reduce waste, and improve component/material availability

Goals

- Demonstrate high temperature mechanical properties of PM-HIP materials compared to wrought materials
- First address PM-HIP 316H stainless steel to support multiple advanced reactors
- Develop specifications and acceptance criteria for PM-HIP components



PM-HIP Div. 5 Code Cases Roadmap



PM-HIP Div. 5 Code Cases Roadmap

Submit data package to ASTM for alloy(s) to be added to ASTM **PM-HIP**

(Note: This step is not required for Gr. 91)

Responsible Party TBD

TG on Div. 5 AM **Components**

Determine ASME BPVC qualification approach

Three options compared to wrought material:

- 1) Use the same design rules (shortest)
- 2) Use a knockdown factor
- 3) Develop different design rules (longest)

Ballot code case permitting PM-HIP for low temperature Sec. III, Div. 5

applications

permitting **PM-HIP for** elevated temperature Sec. III, Div. 5 applications

Ballot code case

TG on Div. 5 AM **Components**

Responsible Party TBD



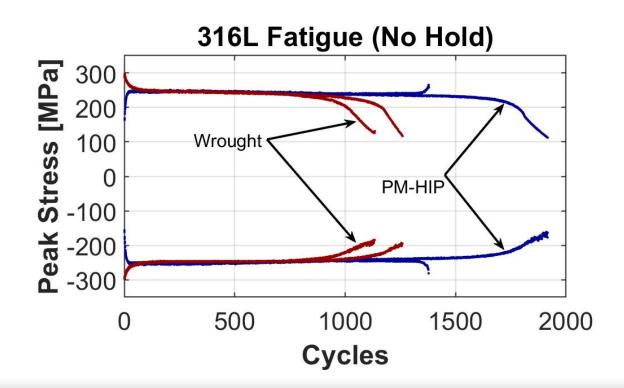
Major Milestones

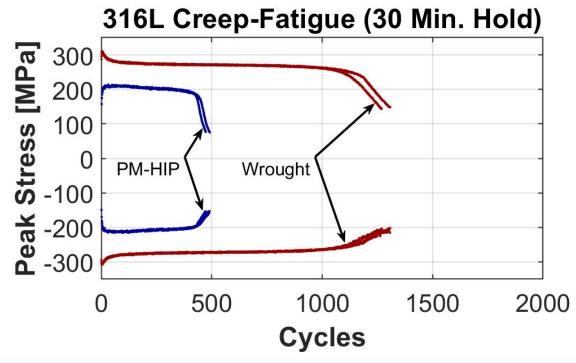
- Complete development of PM-HIP 316H code cases for the American Society of Mechanical Engineers (ASME) Section III, Division 5, Class A applications by 2025
 - Low temperature PM-HIP 316H code case (up to 371°C)
 - High temperature PM-HIP 316H code case (371°C<T<816°C)

Prior Results – 316L

Fatigue and creep-fatigue at 650°C

650°C,
$$\Delta \varepsilon = 1\%$$
, $R = -1$, $\dot{\varepsilon} = 0.001 \, s^{-1}$

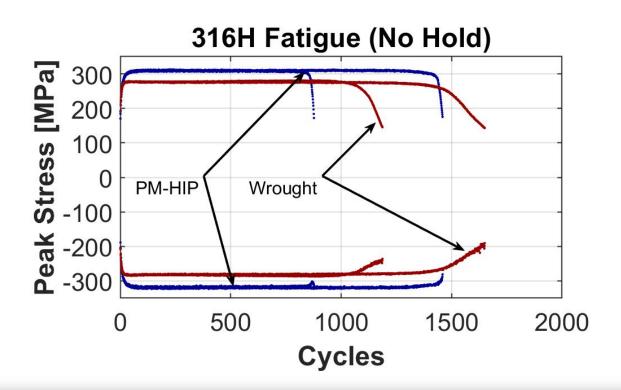


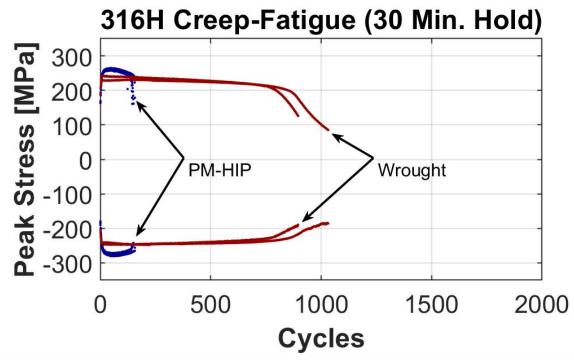


Prior Results – 316H

Fatigue and creep-fatigue at 650°C

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Properties and Process Optimization

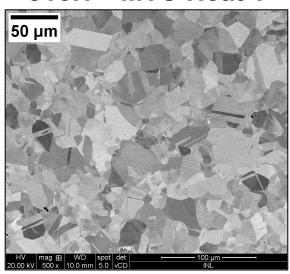
Why are fatigue and creep-fatigue results showing inferior performance compared to wrought 316 stainless steel?

- Need to better understand how the composition and microstructure influence PM-HIP mechanical properties
 - Overall oxygen concentration
 - Prior data has shown that >130 ppm oxygen content in PM-HIP SS may be deleterious to elevated temperature properties
 - Oxide size and distribution
 - Grain size and grain size distribution

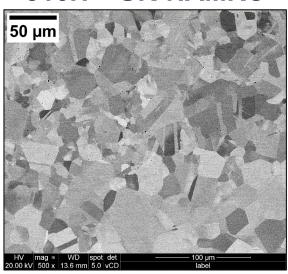
Current Material Investigation

Consolidated Product Chemical Compositions (wt%)										Hardness	
	Ni	Cr	Мо	С	Si	Mn	S	Р	0	N	(HV _{0.3})
316H – MTC Heat 1	12.0	16.2	2.53	0.05	0.17	0.21	0.01	0.003	0.0190	0.141	224
316H – UK-NAMRC	11.8	17.3	2.53	0.04	0.17	0.18	< 0.003	< 0.005	0.015	0.069	194
316L – UK-NAMRC	11.9	17.7	2.44	0.015	0.83	1.88	0.008	0.008	0.0117	0.06	173

316H - MTC Heat 1

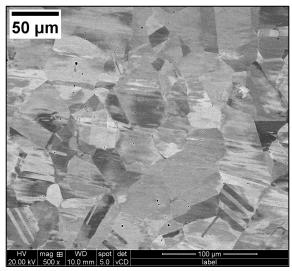


316H - UK-NAMRC





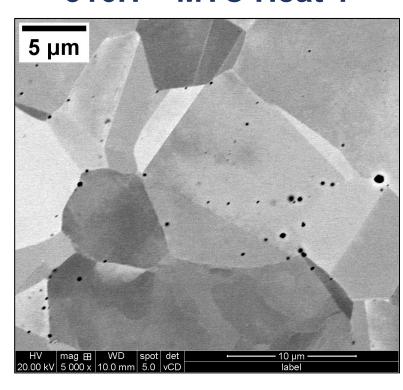
316L – UK-NAMRC

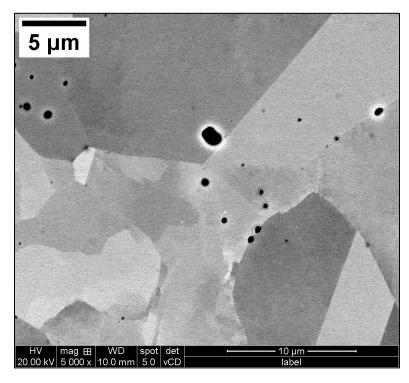


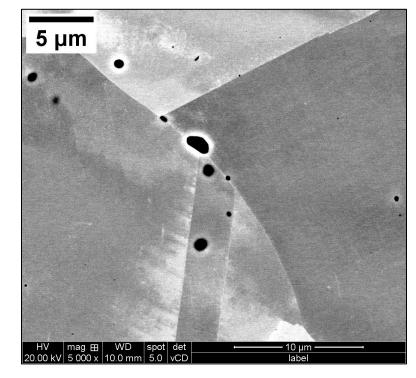
316H - MTC Heat 1



316L – UK-NAMRC







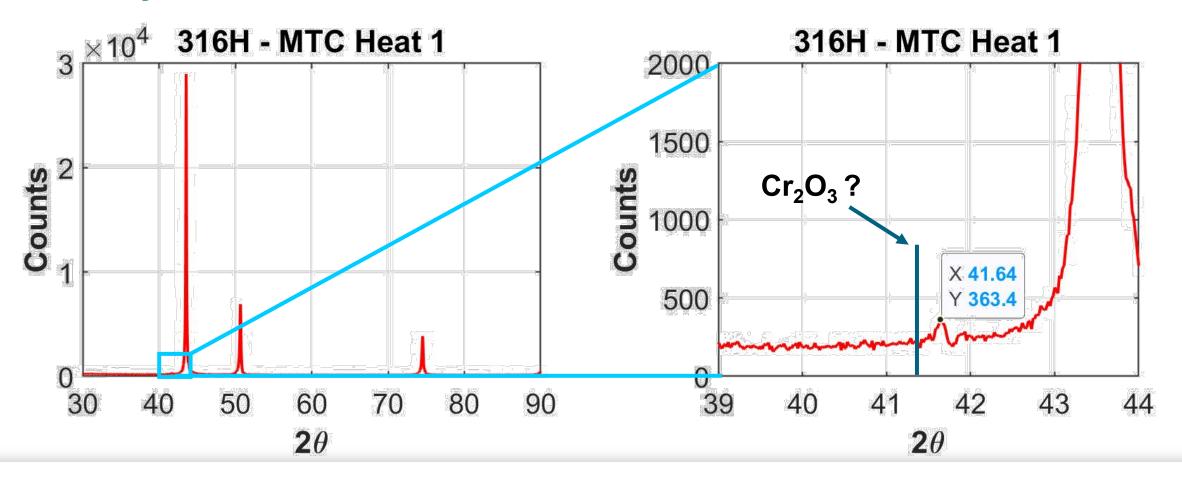
Oxide Area Fraction = 0.10%

Oxide Area Fraction = 0.18%

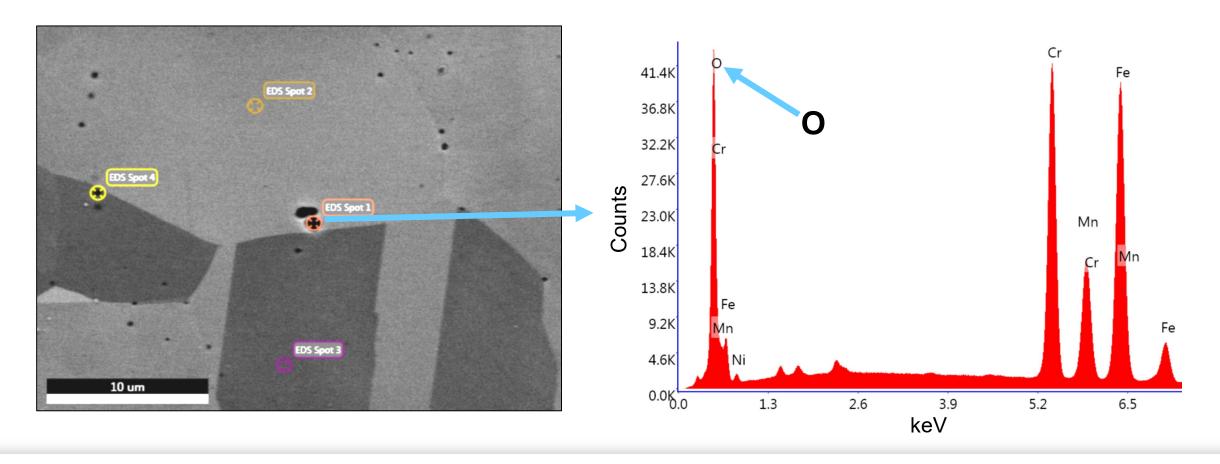
Oxide Area Fraction = 0.18%

^{*}Fraction averages are from five random images at an original magnification of 2500X captured at a 10 µm working distance

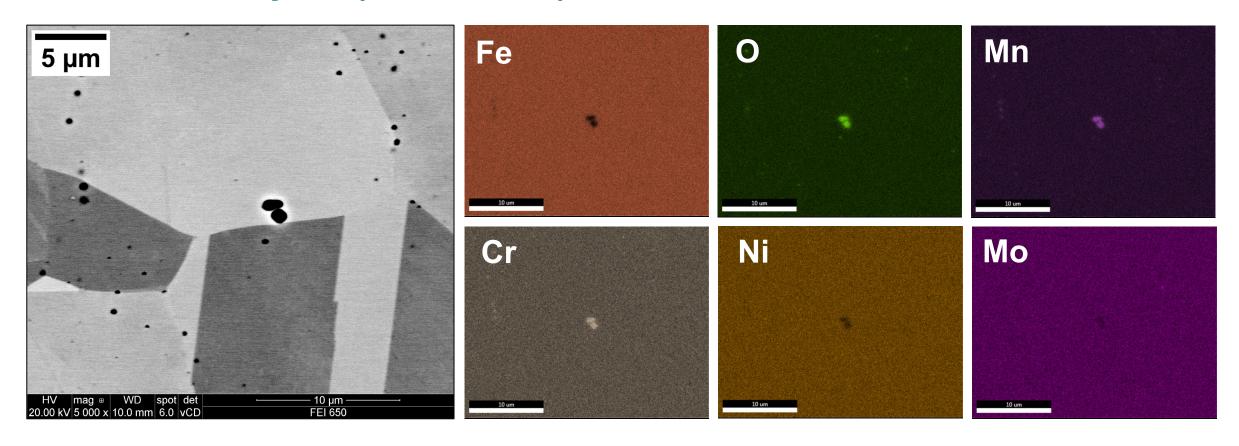
X-ray Diffraction Data



Are the precipitates oxides?

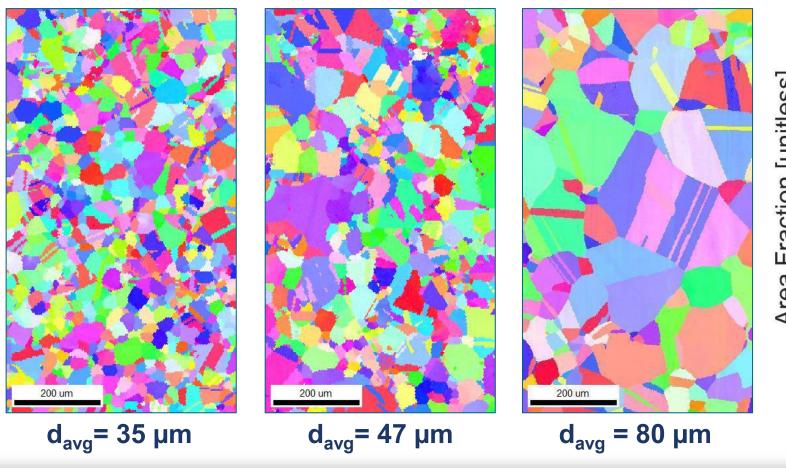


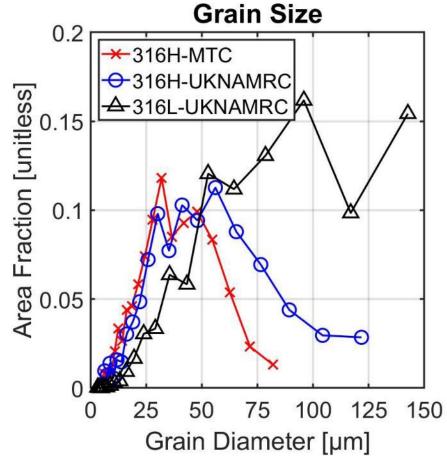
• EDS Analysis (Qualitative) – UKNAMRC 316H



Results - Grain Size

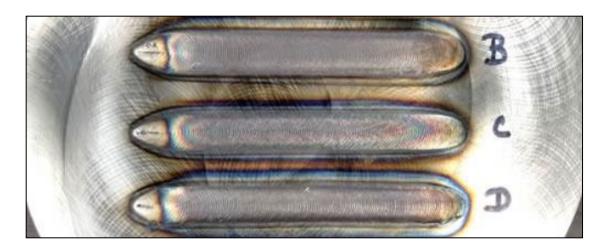
316H MTC Heat 1 316H UK-NAMRC 316L UK-NAMRC

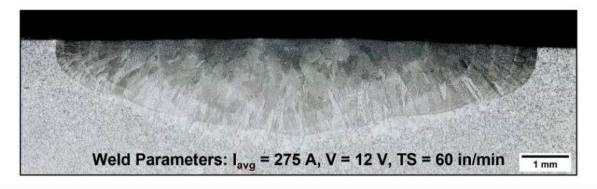


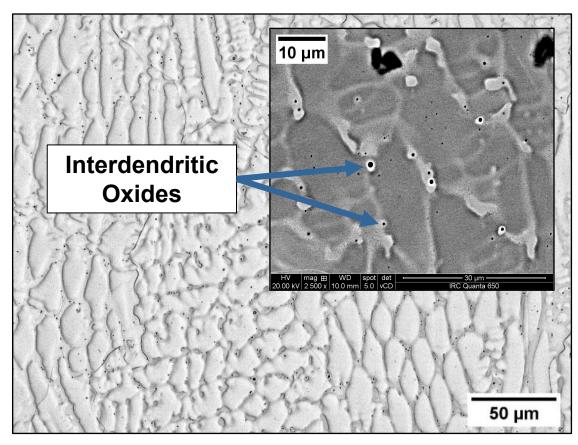


Results – Initial Weldability

Bead-on-plate welds on 316H – MTC Heat 1







316H Procurement Status

- MTC Heat 2 was procured with an oxygen concentration in the powder of 120 ppm
- One-third of the powder was hot isostatically pressed and underwent a heat treatment identical to MTC Heat 1
- Another third is being heat treated at different conditions to try to influence the oxide size/distribution





Conclusions

- Initial evaluation of 316L and 316H stainless steel showed poor creep-fatigue performance compared to wrought materials
- It is currently unknown as the exact mechanism resulting in the reduced creep-fatigue properties
- Evidence of oxide size and distribution may be attributing to the reduced properties regardless of the overall oxygen concentration
- Oxides remained in the gas tungsten arc weld metal

Future Work

- Conduct elevated temperature mechanical testing on the MTC Heat 2 alloy and UK-NAMRC 316 alloys
- Determine if a lower overall oxygen content improves the creep-fatigue properties
- Compare oxide size and distribution at lower oxygen content

Powder Chemical Composition (wt%)											D50 Powder
	Ni	Cr	Мо	C	Si	Mn	S	Р	0	N	Size (um)
316H – MTC Heat 2	12.0	17.0	2.53	0.05	0.20	0.21	0.003	0.004	0.0120	0.1010	52
316H – UK-NAMRC	11.9	17.1	2.52	0.05	0.17	0.18	0.002	0.004	0.0064	0.0755	100
316L – UK-NAMRC	11.9	17.7	2.44	0.015	0.83	1.88	0.008	0.008	0.0117	0.06	-

FY23 Milestone

M3AT-23IN0804091, 9/15/2023

 Complete an initial evaluation of the elevated-temperature cyclic properties of optimized Alloy 316H fabricated by powder metallurgy hot isostatic pressing

M4AT-23IN0804093, 9/29/2023

 Provide status of procurement of several heats of PM-HIP 316H stainless steel with optimized processing

Thank you

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