



# Transient Physical Modelling for the Coupling of a High Temperature Gas Reactor with Thermal Energy Storage

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*Changing the World's Energy Future*

Aidan Christopher George Rigby, Vaclav Novotny, Daniel Mark Mikkelsen,  
Rami M Saeed



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**Idaho National Laboratory  
Idaho Falls, Idaho 83415**

**<http://www.inl.gov>**

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# Transient Physical Modelling for the Coupling of a High Temperature Gas Reactor with Thermal Energy Storage

Aidan Rigby\*, Vaclav Novotny†, Daniel Mikkelsen†, Rami Saeed†

\*University of Wisconsin-Madison, † Integrated Energy Systems, Idaho National Laboratory

## Introduction

Improving the **flexibility** of nuclear reactors to meet fluctuating demand on grids with high renewable energy generation penetration is key to improving reactor economics. **Economic optimization** using the code **HERON** gives maximum profit of coupling high temperature gas reactors (**HTGRs**) to thermal energy storage (**TES**) systems in the configuration shown in Figure 1 when following the demand in Figure 3 [1][2]. We look to **model the physics** of operation for a HTGR-TES using the **HYBRID** library in the code **Modelica**.

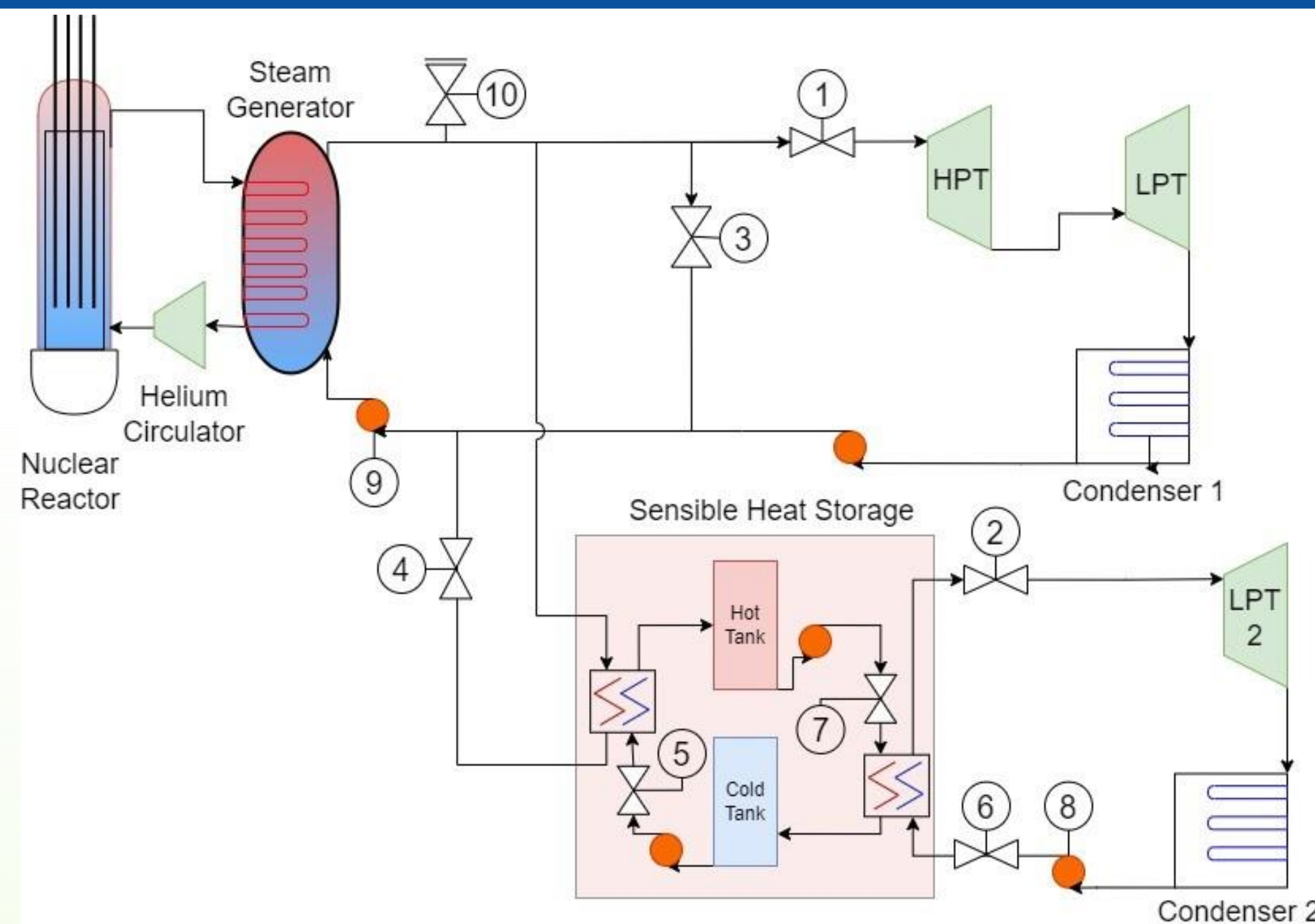


Figure 1: HTGR-TES layout with independent TES balance of plant

## Motivation

The physics Modelica model aims to answer:

- How the system could be **controlled over time**.
- How the **efficiency** of the system changes when operating the balance of plant (**BOP**) at **off-design**.
- If there are **fundamental physical limits** breached during switching states.

## Methodology

Figure 2 shows the state control decision logic with setpoints and actuators described in Table 2.

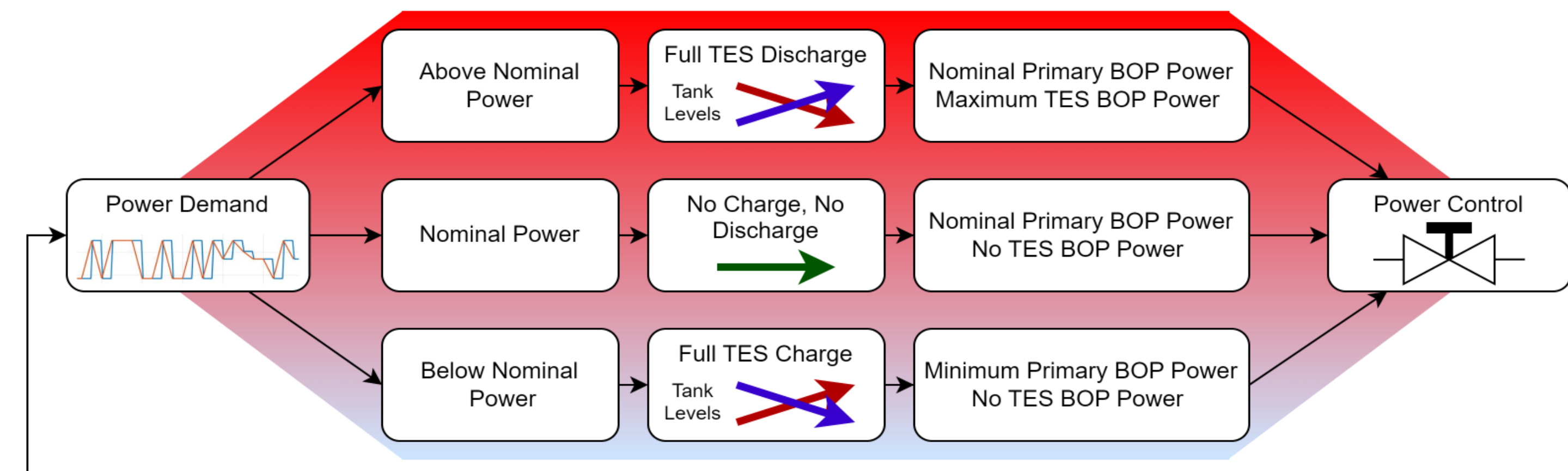


Figure 2: Power control as affected by the thermal energy storage

Table 1: Control Strategy for transient control:  $Q_{dem}$  is demanded power,  $Q_{nom}$  is nominal power of primary balance of plant = 83.16MW. Labels correspond to Figure 1.

Label	Name	Controlling	Setpoint
1	Turbine Control	Steam Inlet Pressure	34 bar
2	Discharge Turbine Control	Power	If $Q_{dem} > Q_{nom} = Q_{dem} - Q_{nom}$ else is 0.
3	Feedwater Heating	Feedwater Temperature	148°C
4	Turbine Bypass	Power	If $Q_{dem} > Q_{nom} = Q_{nom}$ else is $Q_{dem}$ .
5	Charging Control	TES Hot Tank Temperature	240°C
6	Discharging Feedwater Control	Power	If $Q_{dem} > Q_{nom} = Q_{dem} - Q_{nom}$ else is 0.
7	Discharging Control	TES Cold Tank Entry Temp.	180°C
8	Discharging Feedwater Control	Steam Inlet Pressure	12 bar
9	Feedwater Control	Secondary Mass Flow	67 kg/s
10	Pressure Relief	Pressure Overloads	Release at 150 bar

## Results and Conclusions

- **Efficiencies** for the primary BOP are: **39.49%** in full charge and **41.79%** at nominal power and for the TES BOP are **39.33%** at full discharge.
- Control system meets **power demand** with **10min ramp rates** between setpoints seen in Figure 3 keeping **reactor power constant at 203MW ± 0.1%**.
- Figure 4 shows the tank **charging level is periodic** and returns to original charge state.
- Some controlled parameters exhibit **large deviations** during transient operation including feedwater temperature shown in Figure 5.

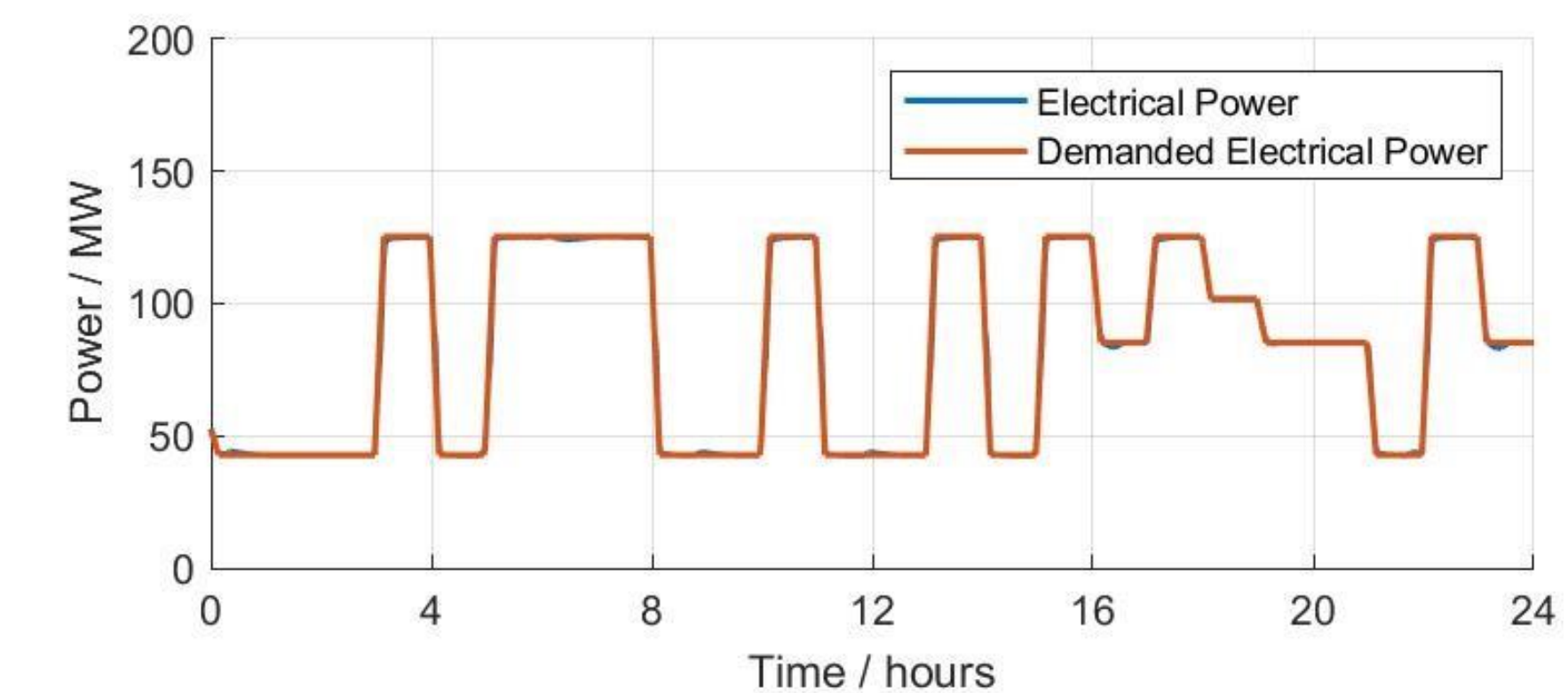


Figure 3: System ability to meet power demand

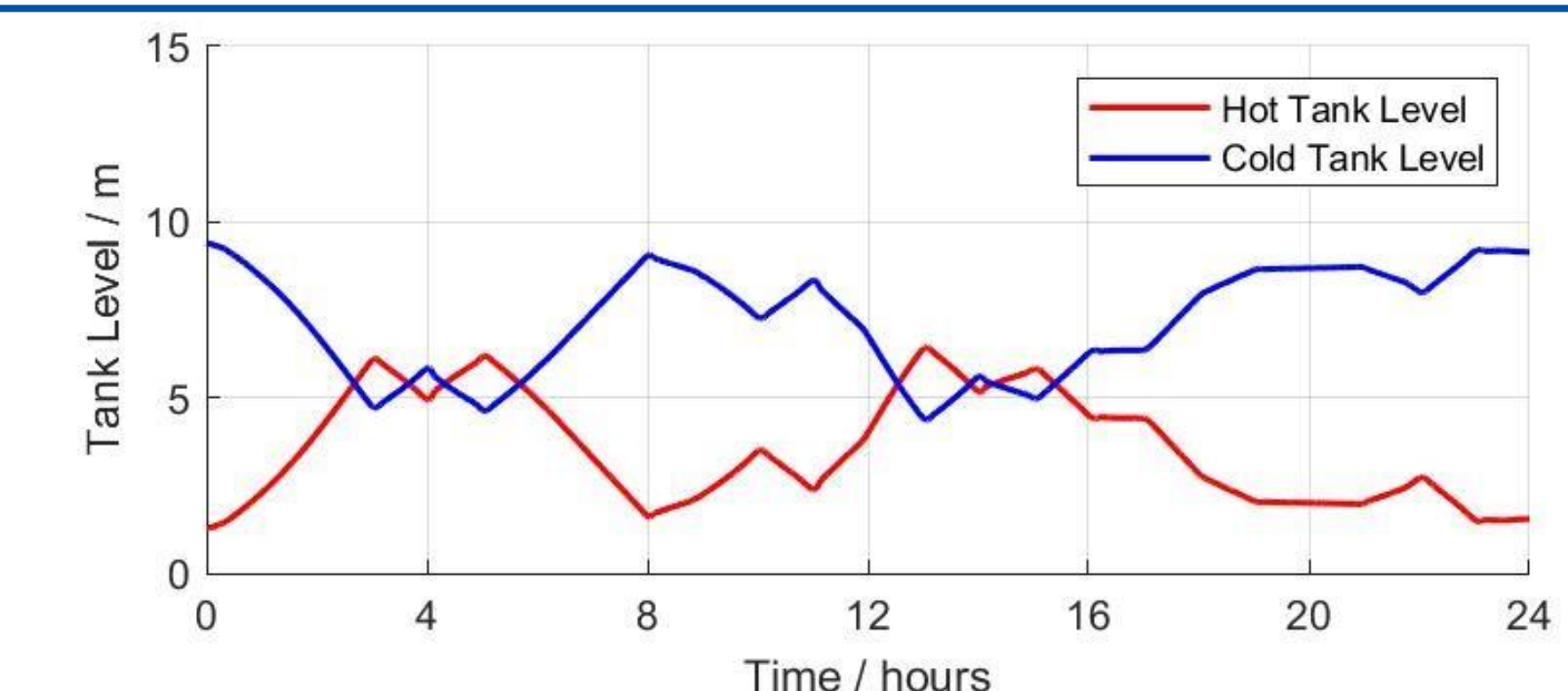


Figure 4: Charge Level of TES Tanks

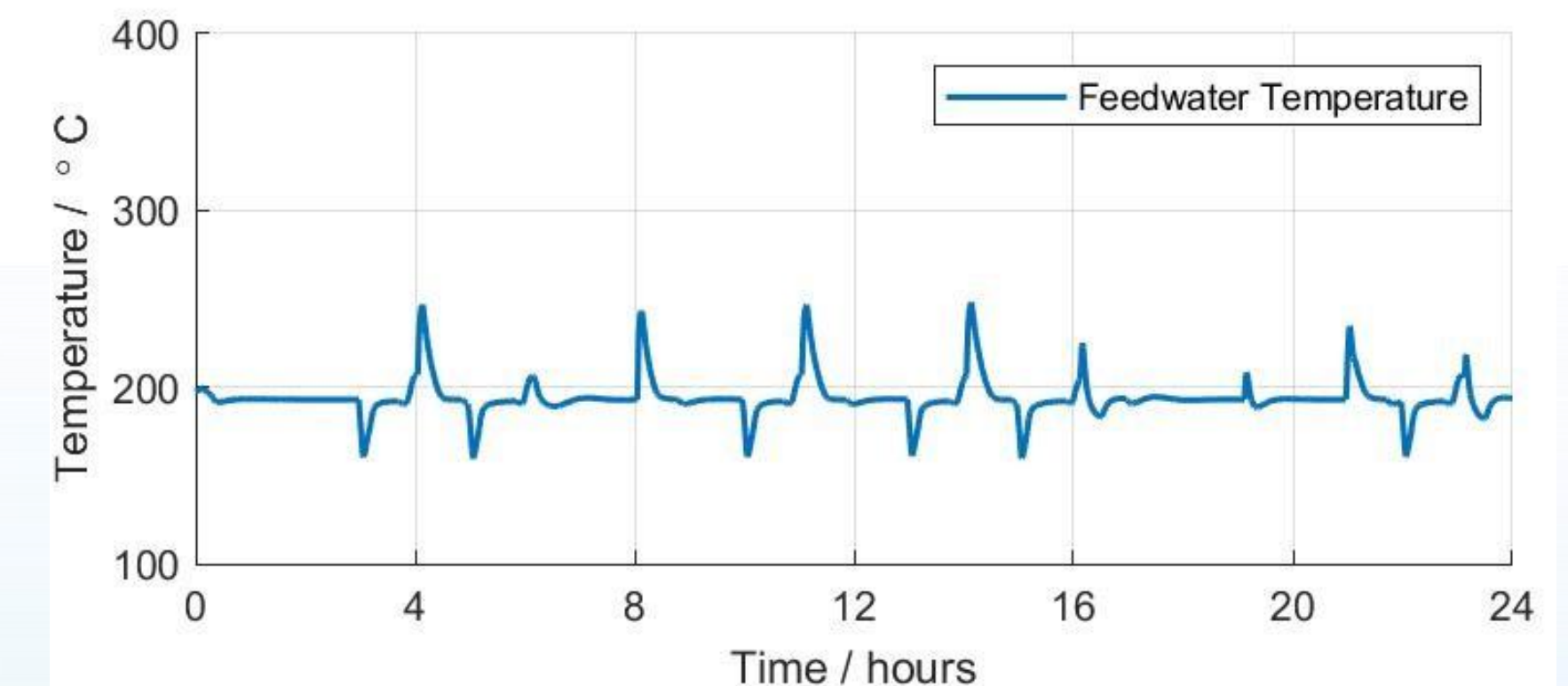


Figure 5: Feedwater Temperature during state switching

## Significance and Future Work

- **Control system is sufficient** to maintain desired ramp rates and nominal operation.
- Fundamental limit to minimum power observed due to **feedwater overheating**.
- Future work to examine **control of the high volatility** in variables like feedwater temperature that results from low valve operating margins and feedback from returning steam bypassed to the TES.

1. Saeed, Rami M., Shigrekar, Amey, Mikkelsen, Daniel Mark, George Rigby, Aidan Christopher, Yang Hui Otani, Courtney MarikGarrouste, Marisol, Frick, Konor L., and Bragg-Sitton, Shannon M. Multilevel Analysis, Design, and Modeling of Coupling Advanced Nuclear Reactors and Thermal Energy Storage in an Integrated Energy System. United States: N. p., 2022. Web. doi:10.2172/1890160.
2. Shigrekar, Amey, Toman, Jakub, and Saeed, Rami M. Synthetic Electricity Market Data Generation and HERON Use Case Setup of Advanced Nuclear Reactors Coupled with Thermal Energy Storage Systems. United States: N. p., 2023. Web. doi:10.2172/1960133.

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