



2018 Conference on Advanced Power Systems for Deep Space Exploration presentation - eMMRTG Development and Infusion

October 2018

Changing the World's Energy Future

Joe Giglio, Chris Matthes



INL is a U.S. Department of Energy National Laboratory operated by Battelle Energy Alliance, LLC

DISCLAIMER

This information was prepared as an account of work sponsored by an agency of the U.S. Government. Neither the U.S. Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness, of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. References herein to any specific commercial product, process, or service by trade name, trade mark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the U.S. Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the U.S. Government or any agency thereof.

2018 Conference on Advanced Power Systems for Deep Space Exploration presentation - eMMRTG Development and Infusion

Joe Giglio, Chris Matthes

October 2018

**Idaho National Laboratory
Idaho Falls, Idaho 83415**

<http://www.inl.gov>

**Prepared for the
U.S. Department of Energy
Under DOE Idaho Operations Office
Contract DE-AC07-05ID14517**

eMMRTG Development and Infusion

October 22, 2018

Joe Giglio

joe.giglio@inl.gov

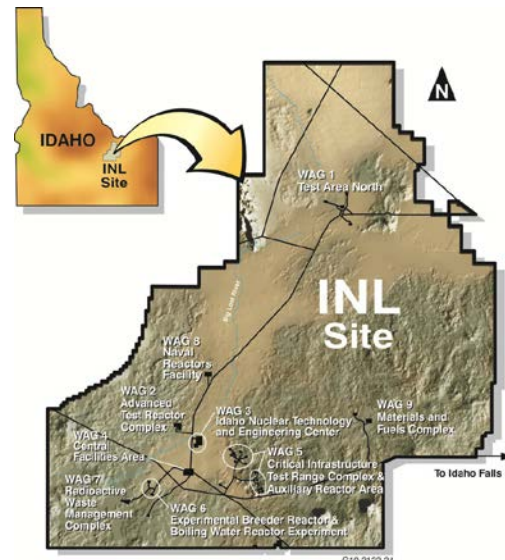
**Idaho National
Laboratory**

Chris Matthes

christopher.s.matthes@jpl.nasa.gov



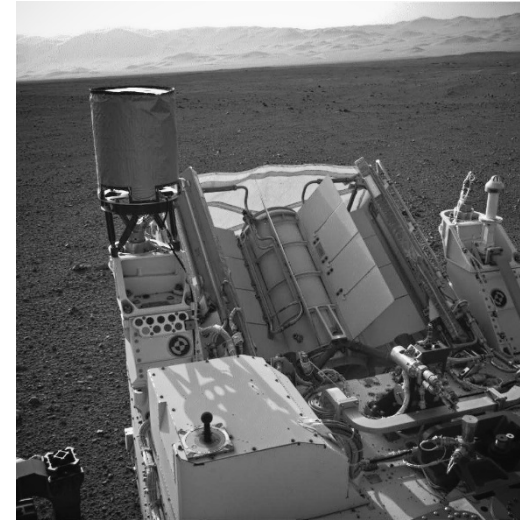
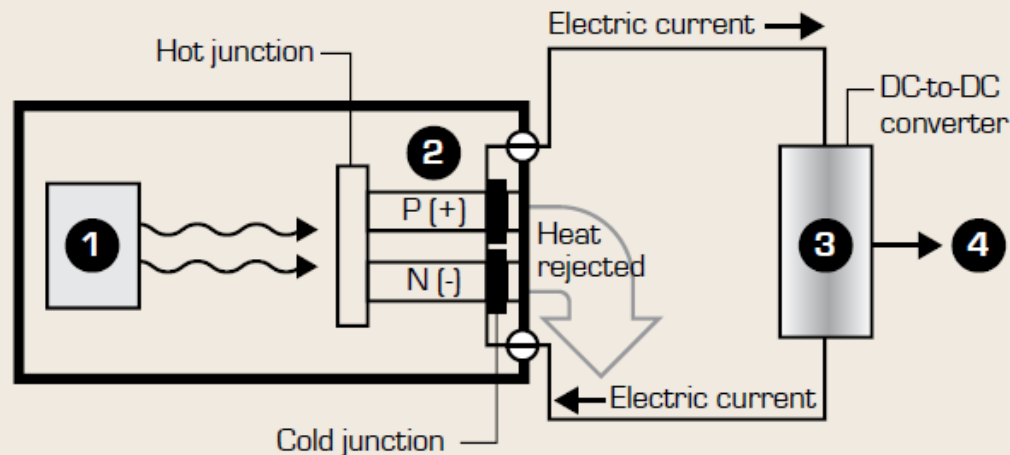
Jet Propulsion Laboratory
California Institute of Technology



Multi-Mission Radioisotope Thermoelectric Generator (MMRTG)

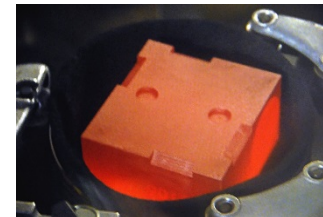
- The MMRTG converts heat generated from the natural decay of Pu-238 (alpha emitter) to electricity through the thermoelectric effect.

- 1 Nuclear fuel [e.g., plutonium-238] decays spontaneously producing heat
- 2 Thermocouples convert heat directly into electricity
- 3 Electricity is tapped from terminals connected to thermocouples
- 4 Power output



Missions
Mars Science Laboratory
Mars 2020
Potential Mission
Dragonfly

- Sealed thermoelectric cavity which allows planetary (atmosphere capable) and deep space use
- Based on 1970 era thermoelectric materials (PbTe/TAGS)
- Uses the General Purpose Heat Source (GPHS)
- Total power degradation is ~4.8%/year
 - Fuel decay ~1.1%



Terminology

BOL- Beginning of Life

BOM- Beginning of Mission

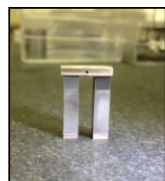
EODL – End of Design Life

Enhancing the MMRTG – Replacing the TE with State of the Art Technology

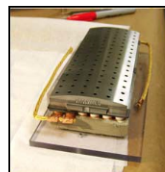
Technology Transfer & Maturation + MMRTG design mods = eMMRTG



Skutterudite (SKD) materials



SKD couples



Advanced SKD MMRTG modules

New SKD materials with higher performance and higher maximum operating temperature than MMRTG TE materials



10% increase in conversion efficiency over MMRTG couples

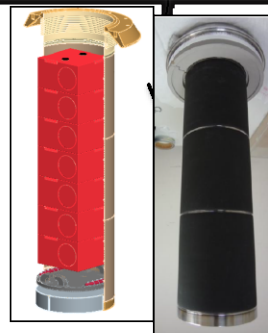
+

14% increase in conversion efficiency over MMRTG couples



• ≥ 24% increase in power over MMRTG at BOL
• ≥ 50% increase in power over MMRTG at 17 years

Operating Temperature rises from 800K to 873K



Liner changes boost operating temperature



enhanced MMRTG



Requirement:

Minimum EODL power of 77 W accounting for all degradation mechanisms when operated at nominal deep space conditions with minimum fuel load (1952 W BOL), fin root temperature of 157°C and load voltage of 34 V.

Minimize changes to a TRL-9 generator

- Replace the PbTe with SKD in the 48 couple module
 - Includes Aerogel insulation for sublimation suppression
- Need to increase the hot junction operating temperature to realize enough benefit for the change
- Increases the operating temperatures from the TE to the fuel
 - Duplicate the emissive coating on the outside of the liner on the inside surface to lower the fuel temperature
 - Requires the fuel support structure to operate hotter than the MMRTG

	MMRTG	eMMRTG
Power, launch, W	110	140 (goal)
Efficiency, BOL	5.5%	7.5%
Power, EODL, W	55	77
Degradation rate, avg	4.8%	2.5%
# GPHSs	8	8
Length, m	0.69	0.69
Mass, kg	45	44

RPS Technology Maturation Process

End User Goals & Requirements
(Surrogate Mission Team)

Industry Technology, know-how, and expertise

RPS Program Office Guidance and Review

DOE Guidance and Review

Technology Selections

Phase A Formulation

GATE 1

Phase B Maturation

GATE 2

Phase C Refinement

GATE 3

Qualification / Flight Development (DOE)

Technology Decision Gate 1

Assess: Materials, components, manufacturability, performance capabilities , development risk and schedule

Technology Decision Gate 2

Assess: Materials, components, production capability, performance vs requirements, remaining risk and schedule

Technology Decision Gate 3

Assess: Technology maturity, production readiness, performance vs requirements, readiness for Qualification Development

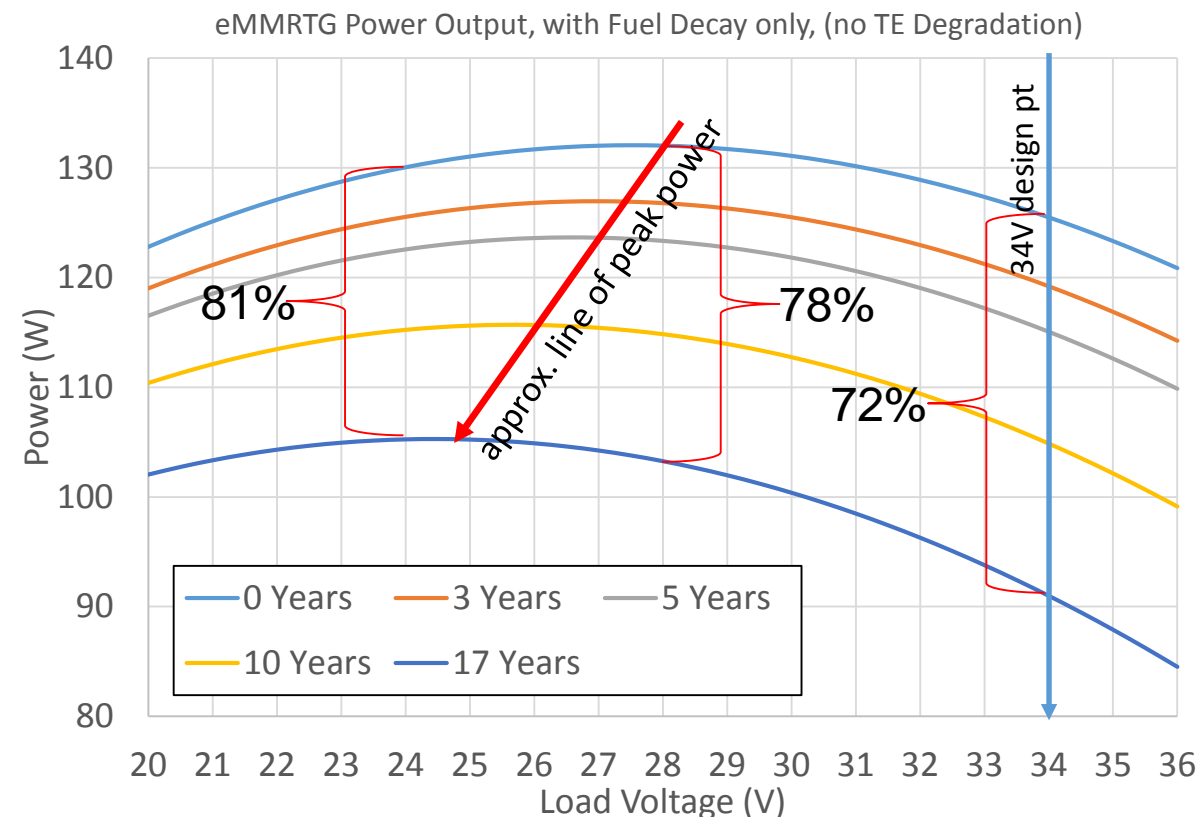
eMMRTG Status

- Approaching Gate 2 (January 2019) – Initial Life and Performance Assessment vs Requirements, Production Capabilities
 - SKD material fabrication transitioned from JPL to Teledyne Energy Systems (TESI).
 - 2 couple configurations (metallization layers) currently on test to characterize temperature dependent degradation rates.
 - Expect 3000+ hour test data in a variety conditions
 - Demonstrating manufacturability, performance and strength
- DOE through a contract administered by INL will assume the development after a successful Gate 2.
 - Tasked to develop and test a 48-couple eMMRTG module (Gate 3)
 - The current technology development team will remain in place.
 - NASA GRC – Project Management
 - JPL –Technology Formulation
 - TESI – Technology Manufacturer
 - Aerojet Rocketdyne (AR) – RTG System Engineering and Prime Contractor
 - INL – Contract Administrator, RTG Fueling and Flight Unit Supplier
 - eMMRTG electrically heated qualification unit build is expected after a successful Gate 3.
 - Maintain the option for an electrically heated eMMRTG or MMRTG flight delivery to INL in 2024 for 2026 launch.

How to Design an RTG Abbreviated Version

- Determine the power input level
- Set thermoelectric operating temperature limits
- Calculate the area/length ratio of the thermoelectrics to achieve the temperature limits
- Determine the peak power voltage output (28 V for MMRTG)
- Determine the number of couples by dividing V_{out} by V_{couple}
- Estimate the weight
- Iterate design until optimized

Choosing an operating voltage beyond the peak power point yields a higher fuel only degradation rate



eMMRTG Design Process

The eMMRTG is not optimized

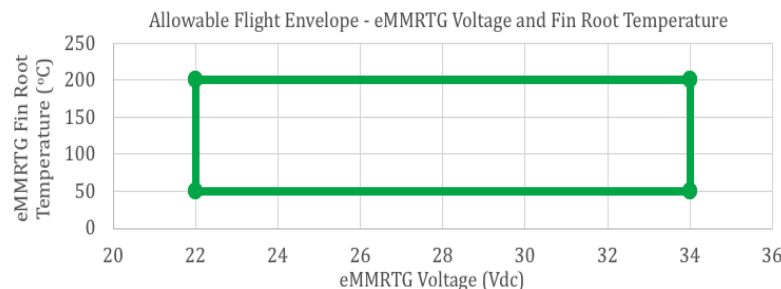
- Input power is the same as the MMRTG
- Structure is the same as an MMRTG
- T_c set by MMRTG design
- Couple length is set by the MMRTG envelope
- Design output voltage set at 34V
- Number of couples equals MMRTG
- Choose a hot junction temperature
- Calculate the cross sectional area of the couple

Characterizing and Selecting the Thermoelectric Performance

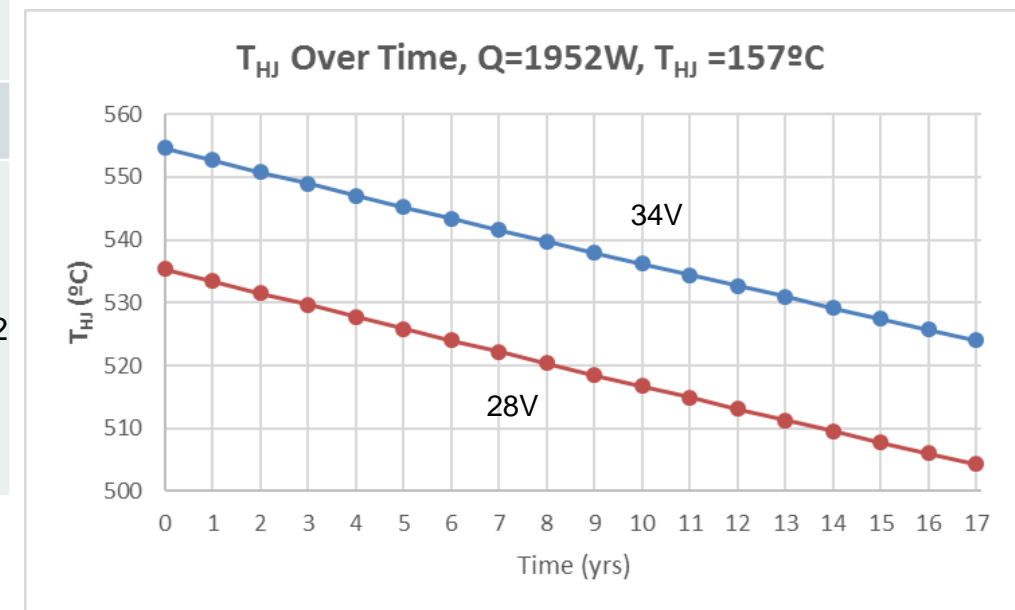
- eMMRTG design case requirement is a deep space environment
- Requirement to operate within the allowable flight envelope
- Final operating temperatures have not been determined
 - Higher T_h equals high power for a given T_c
 - TE degradation is temperature dependent
 - Requires couple leg sizing adjustments
 - Open variable through QU
 - Current predicted changes are within the tolerance band

Couple BOL Power Derived Requirement Adjusted for Current Couple Sizing		
T_h (°C) approx	600	550
T_c (°C) approx	216	175
Environment	Mars Hot	Deep Space
Comments	Conditions: <ul style="list-style-type: none"> • 157°C • $Q = 1952$ Wth • $V = 34$ V 	

The allowable flight envelope (AFE) of the eMMRTG from BOM to EODL is defined to be within the box.



- Preliminary testing above the design case T_h and analysis supports the EODL life requirement
- T_h is dependent on operating voltage
 - Lower operating voltage requires more current flow which increases Peltier cooling
 - ~20°C lower T_{hj} from operating at 28V vs 34V



Conclusion

- The eMMRTG design will solidify over the next 15 months
 - Gate 2 in January 2019
 - Select TE couple and insulation configuration design for module testing
 - Publish first iteration of life prediction modeling results
 - Gate 3 in December 2019
 - Thermoelectric module performance predictions
 - Test data from full-scale 48 couple module
- The end user will have a significant impact to the long term performance of the eMMRTG
 - Operating voltage impacts degradation
 - Primarily through natural decay of the fuel
 - Secondary through potential temperature dependent thermoelectric degradation
 - Operating voltage impacts the performance
 - Average of 5 watts, less than the difference between 28V and 34V power, over 14 years is $>0.5 \text{ MW}_e\text{-hrs}$
 - Recommend choosing an operating voltage based on the timeframe that peak science is performed

Acknowledgements

NASA Glenn Research Center

- John Hamley - RPS Program Manager
- Monica Hoffmann - eMMRTG/MMRTG Project Manager

Jet Propulsion Laboratory

- Thierry Caillat - eMMRTG Principal Investigator
- Jean-Pierre Fleurial - eMMRTG Interim Principal Technologist
- Stan Pinkowski - SKD Technology Development Manager
- Dave Woerner - RPS Principal Engineer
- Chris Matthes - eMMRTG / MMRTG Lead Engineer

Teledyne Energy Systems

- Russ Bennett –Chief Engineer
- Tom Hammel – Engineering Manager
- Steve Keyser –Program Manager
- Joe Vanderveer –System Engineer

Aerojet Rocketdyne

- Bill Otting –Program Manager

