

### Comparison of FAST Experiments to BISON Simulations

November 2023

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Prepared for the U.S. Department of Energy Under DOE Idaho Operations Office Contract DE-AC07-05ID14517

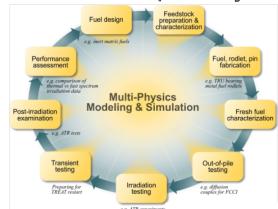
# Comparison of FAST Experiments to BISON Simulations

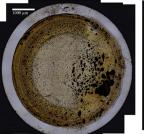
November 28 – 30, 2023 MMSNF Workshop 2023 Alexander Swearingen, Geoffrey L. Beausoleil II, Kyle Paaren, and Luca Capriotti

#### **FAST Motivation**

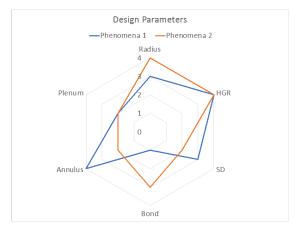
- Fuel testing takes too long
  - Slow iteration around the wheel
- Conventional fuel tests within ATR is high risk
  - Highly sensitive to fabrication tolerances
  - Execution failures are unknown for extended periods of time
- Model based design and true multi-physics performance codes require deeper, more diverse data sets
  - 13,000 data points of one design is not useful
  - Increased variation in experimental designs allows for more robust assessment and V&V

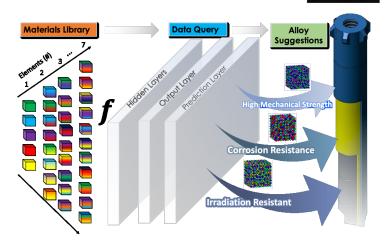








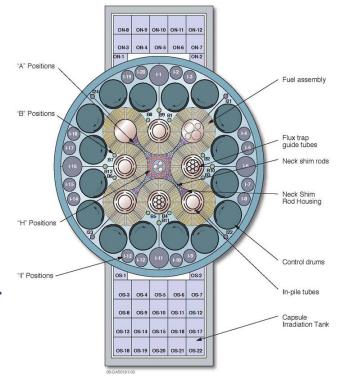


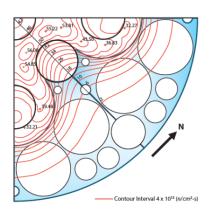




#### **Advanced Test Reactor (ATR)**

- Serpentine driver core creates nine flux traps and numerous other test positions
- 77 test volumes up to 48 inches long and <5.25 inches in diameter</li>
- 60-day cycles with ~3 cycles per year
- High neutron flux enables accelerated testing for fuel and materials development
  - Fast/thermal flux ratios ranging from 0.1
    1.0
  - Thermal flux in the range of 1E13-1E14 n/cm2/s
  - Fast flux in the range of 1E12-1E14 n/cm2/s
- Collocated with world class suite of properties testing and characterization equipment in shielded hot cells





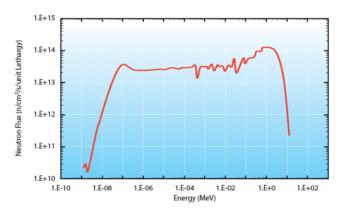


Table 2. Approximate peak flux values for various ATR capsule positions for a reactor power of 110 MW. (22 MW. in each labe)

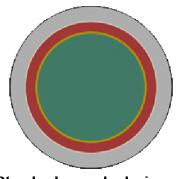
for a reactor power of 110 MW<sub>th</sub> (22 MW<sub>th</sub> in each lobe).

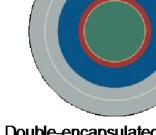
Position	Diameter (cm/in) <sup>a</sup>	Thermal Flux (n/cm²-s) <sup>b</sup>	Fast Flux (E>1 MeV) (n/cm²-s)	Typical Gamma Heating W/g (SS) <sup>c</sup>
Northwest and Northeast Flux Traps Other Flux Traps	13.3/5.250 7.62/3.000 <sup>d</sup>		2.2 x 10 <sup>14</sup> 9.7 x 10 <sup>13</sup>	
A-Positions (A-1 - A-8) (A-9 - A-16)	1.59 1.59/0.625	1.9 x 10 <sup>14</sup> 2.0 x 10 <sup>14</sup>	1.7 x 10 <sup>14</sup> 2.3 x 10 <sup>14</sup>	8.8
B-Positions (B-1 - B-8) (B-9 - B-12)	2.22/0.875 3.81/1.500	2.5 x 10 <sup>14</sup> 1.1 x 10 <sup>14</sup>	8.1 x 10 <sup>13</sup> 1.6 x 10 <sup>13</sup>	6.4 5.5
H-Positions (14)	1.59/0.625	1.9 x 10 <sup>14</sup>	1.7 x 10 <sup>14</sup>	8.4
I-Positions Large (4) Medium (16) Small (4)	12.7/5.000 8.26/3.500 3.81/1.500	1.7 x 10 <sup>13</sup> 3.4 x 10 <sup>13</sup> 8.4 x 10 <sup>13</sup>	1.3 x 10 <sup>12</sup> 1.3 x 10 <sup>12</sup> 3.2 x 10 <sup>12</sup>	0.66



#### A Revised Capsule Design

- Rekindling a small test performed in the 1960's, a FASTer approach to testing was developed
- The Fission Accelerated Steady-state Test (FAST) utilizes a reduced diameter fuel pin to achieve two objectives:



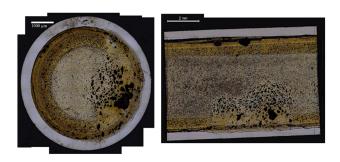


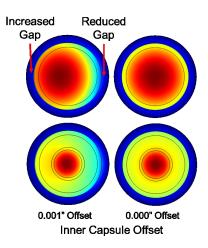
Standard capsule design Prototypic rodlet diameter

Double-encapsulated design ~1/2 standard rodlet diameter

1. Improve experiment reliability: reduced sensitivity to fabrication tolerances and capsule/pin eccentricity







2. Increase burnup rate for fuel experiments: reduce time to achieve high burnup

Given

$$Q_0 = \frac{LHGR_0}{\pi r_0^2}$$

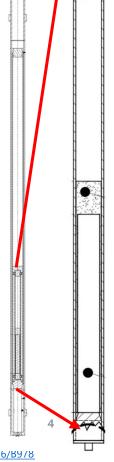
if  $r = \alpha r_0$  and LHGR=LHGR<sub>0</sub>, then

$$Q = \frac{Q_0}{\alpha^2}$$

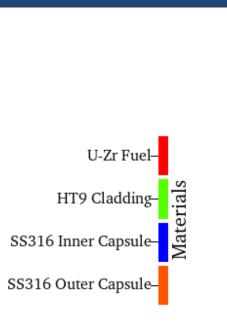
For 
$$\alpha=\frac{1}{2}$$
,

$$Q = 4Q_0$$
$$t \sim Q^{-1} :: t \sim \frac{t_0}{4}$$





#### **BISON Simulated FAST Conditions**



- Outside outer capsule wall is ATR coolant
- Helium inside outer capsule
- Sodium inside inner capsule
- Thermal bond between fuel and cladding
- Top of fuel pin assumed to be equal to Peak Inner Cladding Temperature (PICT)



# **FAST Metal Fuel Test Matrix (U-10Zr)**

Capsule	Rodlet ID	Fuel Comp	Geometry	Bond	Liner	Target BU
AFC-FAST-016=	FAST-035	U-10Zr	Solid	Na	-	2.0%
AFC-FAST-010—	FAST-036	U-10Zr	Solid	Na	-	2.0%
AEC EACT 005	FAST-007	U-10 <b>Z</b> r	Annular	Не	-	4%
AFC-FAST-005=	FAST-008	U-10Zr	Solid	Na	-	4%
AEC EAST 000—	FAST-025	U-10Zr	Solid	Na	Zr	8%
AFC-FAST-009=	FAST-051	U-10Zr	Solid	Na	-	8%
AEC EAST OOG	FAST-015	U-10Zr	Annular	Не	-	8%
AFC-FAST-006=	FAST-016	U-10Zr	Solid	Na	-	8%
AEC EAST 014	FAST-039	U-10Zr	Solid	Na	-	10%
AFC-FAST-014=	FAST-040	U-3Pd-10Zr	Solid	Na	-	10%
AEC EACT 012—	FAST-031	U-10 <b>Z</b> r	Solid	Na	-	10%
AFC-FAST-013=	FAST-032	U-3Sn-10Zr	Solid	Na	-	10%
AEC EACT 015—	FAST-045	U-10 <b>Z</b> r	Solid	Na	-	10%
AFC-FAST-015=	FAST-046	U-3Sb-10Zr	Solid	Na	-	10%
AFC-FAST-003 F	'AST-003 (OA)	U-10 <b>Z</b> r	Solid	Na	-	12%
AFC-FAST-010	FAST-026	U-10Zr	Solid	Na	Zr	12%
Arc-rasi-010—	FAST-052	U-10Zr	Solid	Na	-	12%
AFC-FAST-007	FAST-047	U-10Zr	Annular	Не	-	12%
AFC-FAST-00/	FAST-048	U-10Zr	Solid	Na	-	12%
AFC-FAST-011	FAST-027	U-10Zr	Solid	Na	Zr	16%
ΑΓC-ΓΑS1-011	FAST-053	U-10Zr	Solid	Na	-	16%
AFC-FAST-008	FAST-049	U-10Zr	Annular	Не	-	16%
Arc-ras1-006	FAST-050	U-10Zr	Solid	Na	-	16%



•	<b>Each capsule in the small-l positions</b>
	contains a novel experiment and
	control experiment

- Controls are solid, 75% SD U-10Zr in HT9
- Experiments include
  - He-bonded annular fuel
  - Additives: Pd, Sb, & Sn
  - Zr liners
- PIE underway for all low burnup pins (green)
- Recently removed from the reactor and awaiting transport (yellow)

AEC EAST 012—	FAST-028	U-10 <b>Z</b> r	Solid	Na	Zr	20%
AFC-FAS1-012	FAST-054	U-10Zr	Solid	Na	-	20%

#### **FAST Metal Fuel Test Matrix (U-Mo)**

- Experiments include
  - Solid and annular fuel geometries
  - Different wt % Mo
  - Zr liners
  - Unique fuel loading (yellow)
    - Depleted UNbZr slug sandwhiched between two U-10Mo slugs
- PIE underway for all U-Mo pins

Capsule	Rodlet ID	Fuel Comp	Geometry	Bond	Liner	Target LHGR (W/cm)
aLEU-	FAST-055	U-10Mo	Solid	Na	-	200
FAST-001	FAST-056	U-10Mo	Solid	Na	-	275
aLEU-	FAST-057	U-10Mo	Solid	Na	_	225
FAST-002	FAST-058	U-10Mo	Solid	Na	_	287
aLEU- FAST-003	FAST-059	U-7Mo	Solid	Na	<u>-</u>	225
aLEU-	FAST-061	U-10Mo/UNbZr	Annular	Na	-	425
FAST-004	FAST-069	U-10Mo	Annular	Na	Zr	275
aLEU-	FAST-062	U-10Mo/UNbZr	Annular	Na	-	425
FAST-005	FAST-070	U-10Mo	Annular	Na	Zr	275

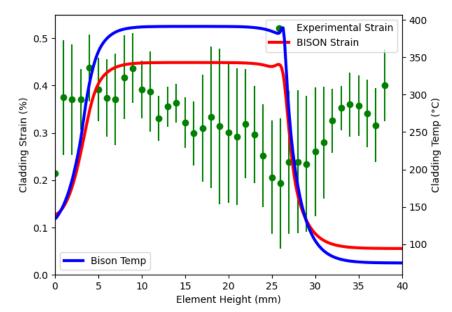


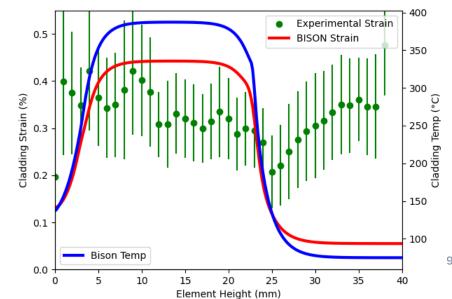
# **FAST U-10Zr Results Comparison**

**FAST-007** 

Pins	Burnup (% FIMA)	CLT (°C)	PICT (°C)	Max Cladding Strain (%)
FAST-007	4.02	539.12	486.24	0.449
FAST-008	3.32	580.65	437.14	0.442

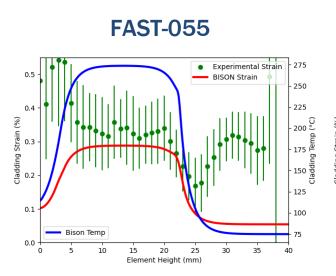
**FAST-008** 

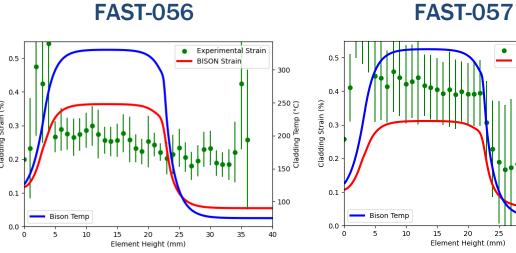


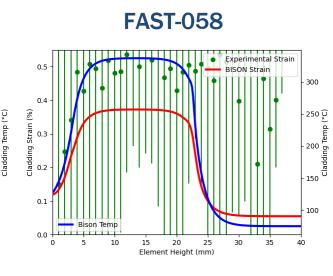




# FAST U-10Mo Solid Pin Results Comparison







Experimental Strain

Pins	Burnup (% FIMA)	CLT (°C)	PICT (°C)	Max Cladding Strain (%)
FAST-055	1.68	372.78	317.24	0.288
FAST-056	2.34	465.52	383.20	0.364
FAST-057	1.88	400.83	338.26	0.311
FAST-058	2.42	476.18	391.24	0.372

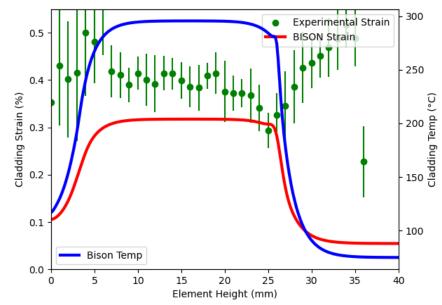


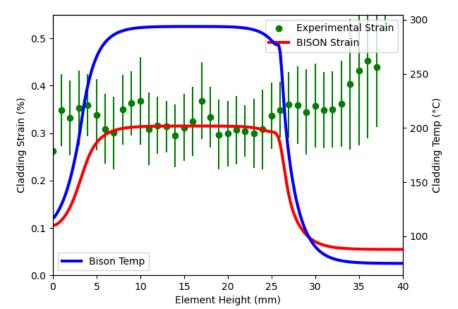
# FAST U-10Mo Annular Pin Results Comparison

**FAST-069** 

Pins	Burnup (% FIMA)	CLT (°C)	PICT (°C)	Max Cladding Strain (%)
FAST-069	2.30	394.13	364.07	0.317
FAST-070	2.28	391.92	362.09	0.315

**FAST-070** 

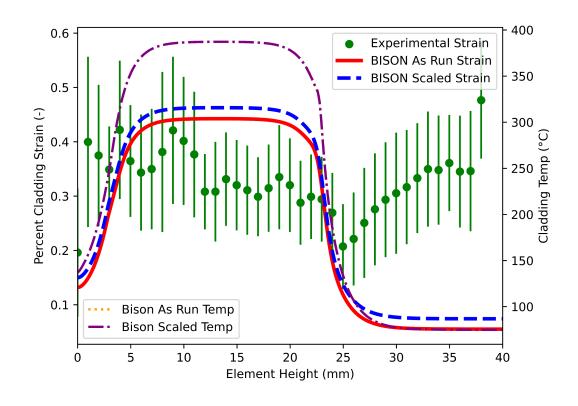






## **BISON HT9 Comparisons**

- HT9 cladding is not scaled like fuel
- Running comparison case
  - Scaled flux of EBR-II X425 to FAST-008 timescale
  - Applied flux to cladding only
  - Compare cladding strains
- Hoping to assess the impact of irradiation creep model on overall performance.

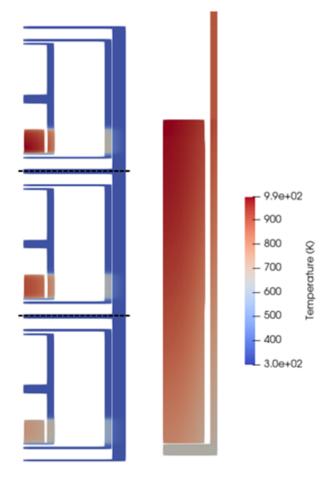




### FAST (U-10Zr) to EBR-II

- Control pins are used in each capsule; U-10Zr, 75%SD solid pin, Na-bonded, HT9 clad
- FIPD provides extensive datasets of burnup history and PIE data from EBR-II data as well as supporting Bison input file setup
- X425 and sub-assemblies have a burnup range that matches well with all control pins of the FAST tests
  - Pin T423
  - Pin T424
- Assessments of X425 are being used to compare cladding irradiation behavior with burnup levels

Experiment	Burnup (%FIMA)	Cladding Fluence (	PICT (°C)	Claddin g DPA
FAST-008	3.9%		410	1.61
FAST-016	8.5%		470	2.89
FAST-031	9.54%		510	2.66
FAST-048*	14.6%		543	4.16
FAST-052*	13.2%		475	4.33
FAST-050*	18.9%		500	5.40
FAST-053*	17.8%		476	5.78
X425A-T423 (142B-0.15)	3.9%		411	16.43
X425A-T423 (146A-0.583)	8.03%		468	39.82
X425A-T423 (146B-0.55)	9.55%		512	47.96
X425A-T424 (144A-0.117)	3.83%		435	17.3
X425A-T424 (150A-0.717)	8.57%		477	42.2
X425B-T424 (149A-0.517)	9.48%		504	47.85
X425C-T424 (158A-0.783)	14.6%		526	73.52
X425B-T424 (153A-0.417)	13.78%		477	71.65
X425C-T424 (158A-0.517)	17%		489	90.49

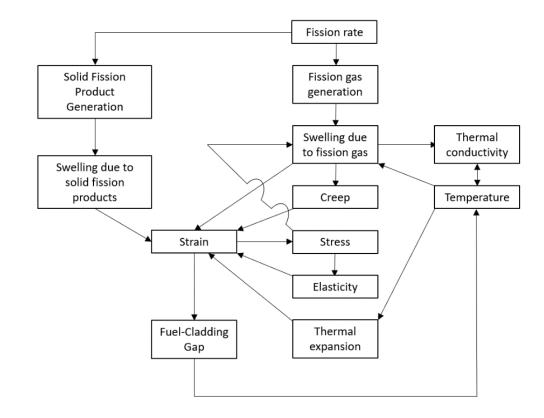




X425C-T424 (158A-0.517) 489 90.49

# **Conclusions/Look Ahead**

- FAST experiments useful for accelerating burnup in fuels
- BISON simulations have varying performance for scaled simulations
  - U-10Zr have so far overpredicted experimental profilometry data
  - U-Mo tend to underpredict experimental profilometry data
- BISON simulations show significant increase in HT9 strain under X425 irradiation conditions
- Complete comparison of U-10Zr pins
- Compare FAST simulations to EBR-II Simulations
- Evaluate BISON sensitivity to scaling



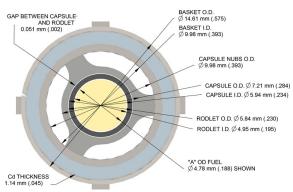


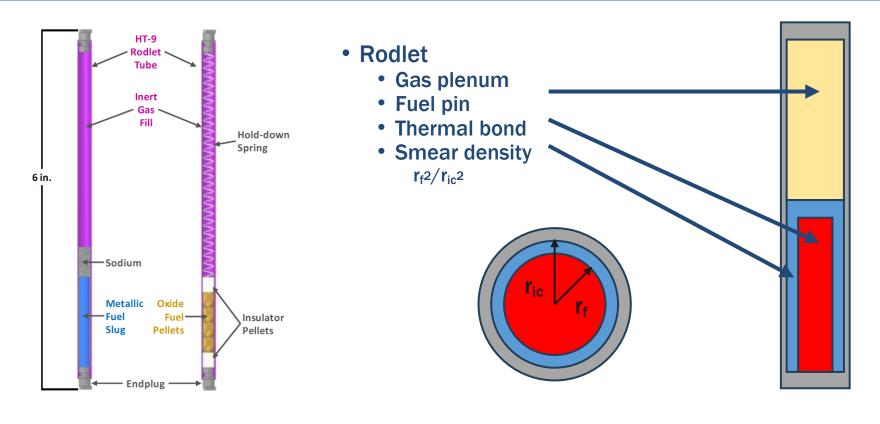


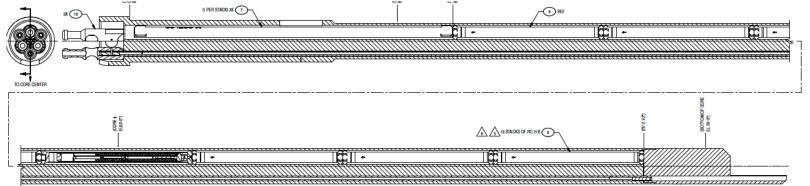


#### **Fuel Testing Capsule Basics**

- Irradiation Experiment
  - Basket
  - Capsule
  - Rodlet









#### **Burnup Acceleration**

Case	Burnup (at%) per 55 day ATR cycle	Time to Achieve 30 at.% Burnup (years)
Full Diameter Small B, 365 W/cm	0.7	11.7
One-Half Diameter Small I, 300 W/cm	3.6	2.3
One-Third Diameter Small I, 180 W/cm	5.1	1.6

Initial Condition	Burnup Condition	Burnup (GWd/t <sub>u</sub> ) per 55 day ATR cycle	Time to Achieve 60 GWd/t <sub>u</sub>
Full Diameter UO <sub>2</sub> 595.4 W/cm, 4.95% Enrichment	28.6 GWd/t <sub>U</sub> 321 W/cm 300 EFPD	~5 GWd/t <sub>U</sub>	12 cycles (3 years)
One-Half Diameter UO <sub>2</sub> 336.4 W/cm, 9.9% Enrichment	41.4 GWd/t <sub>U</sub> 212 W/cm 180 EFPD	~12 GWd/t <sub>U</sub>	5 cycles (1.25 years)



