



# DOE Advanced Gas Reactor Fuel Development and Qualification Program

November 2023

*Changing the World's Energy Future*

Paul A Demkowicz



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# **DOE Advanced Gas Reactor Fuel Development and Qualification Program**

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**November 2023**

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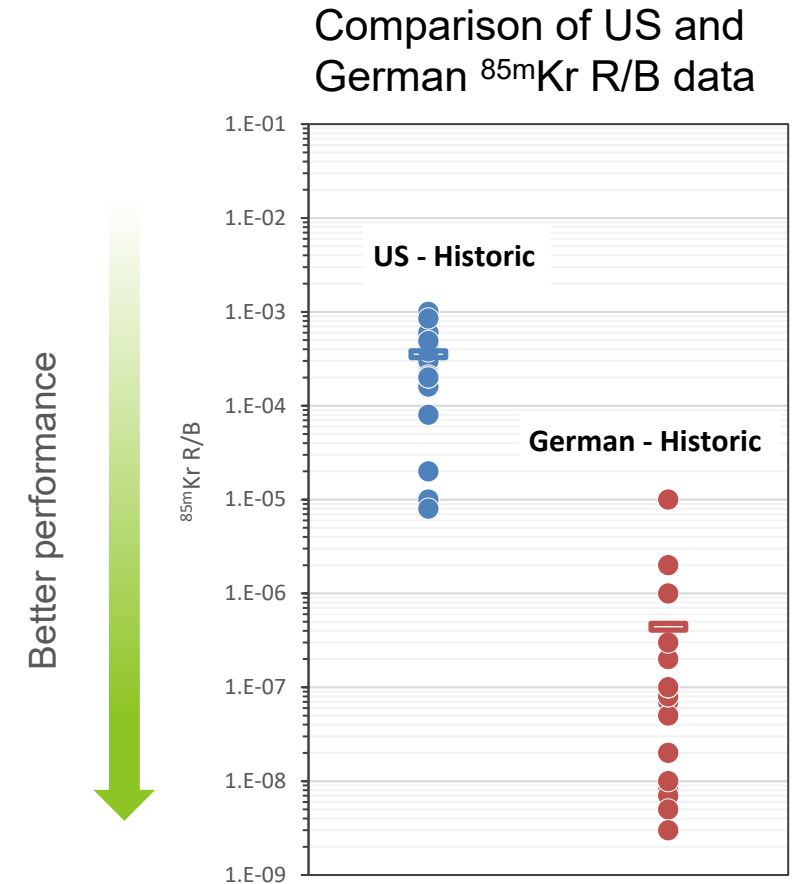
**Paul Demkowicz, Ph.D.**

AGR Program Technical Director

# DOE Advanced Gas Reactor Fuel Development and Qualification Program

# Background: Status of TRISO Technology Circa 2000

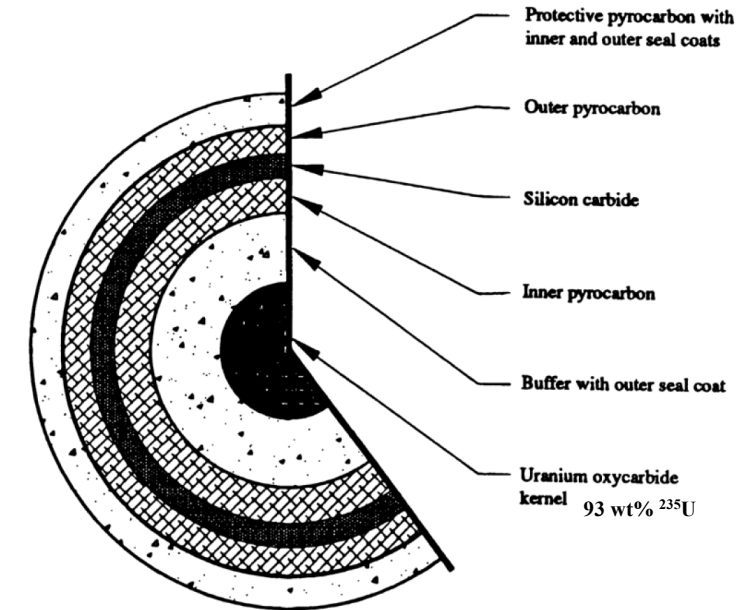
- Four decades of experience with coated particle fuel in numerous countries and operation of several demonstration reactors
- Successful demonstrations of TRISO fuel performance (German program in 1980s and 1990s)
- Major issues with US TRISO fuel performance including the NPR/MHTGR program irradiations in the early 1990s
- Generation IV International Forum included VHTR, but in the US and elsewhere more modest goals of an HTGR (outlet  $\leq 850^{\circ}\text{C}$ ) were established based primarily on lack of suitable high-temperature metals, not fuel performance shortcomings



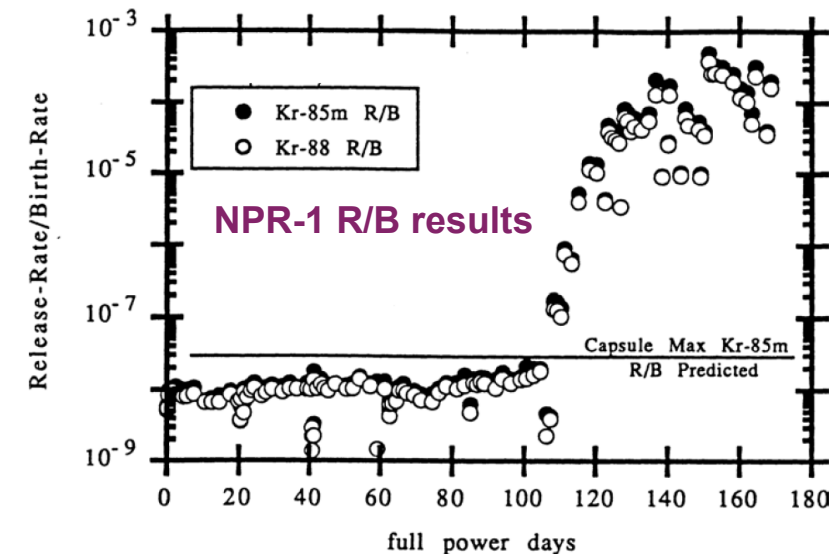
# New Production Reactor (NPR) Fuel Experience

- NPR program started 1988 to produce tritium in an MHTGR
- General Atomics implemented several changes to particle design including: PPyC, thicker IPyC, and thin PyC “seal coats”
  - Best as-manufactured fuel quality ever in the US
- Fuel performance models predicted no failures
- Three irradiations: NPR-1, NPR-2, NPR-1A
  - Failures occurred during all three irradiation tests at similar fast neutron fluence; total failed was  $\sim 700/230,000$  or  $3 \times 10^{-3}$
  - Pyrocarbon layers were implicated in high failure rates
- Sep 1992 – DOE announces termination of program
- Sep 1993 – Project closeout completed
- *“These results indicate that future particle fuel designs would benefit by considering the performance of the entire system of coating layers with respect to particle integrity under irradiation.”*  
(Maki et al., INEEL/EXT-02-01268, 2002)

## NPR fissile particle design



Maki et al., INEEL/EXT-02-01268, 2002



# Fuel Qualification

- “*Demonstration that a fuel product fabricated in accordance with a specification behaves as assumed or described in the applicable licensing safety case, and with the reliability necessary for economic operation of the reactor plant.*” (Crawford et al., J Nuc Mater 371 (2007) 232)
- Requires:
  - Specification for the fuel design, including relevant material properties and geometry
  - “A database of fuel properties and irradiation behavior to sufficiently reduce the safety and reliability uncertainty for use of the fuel design.”

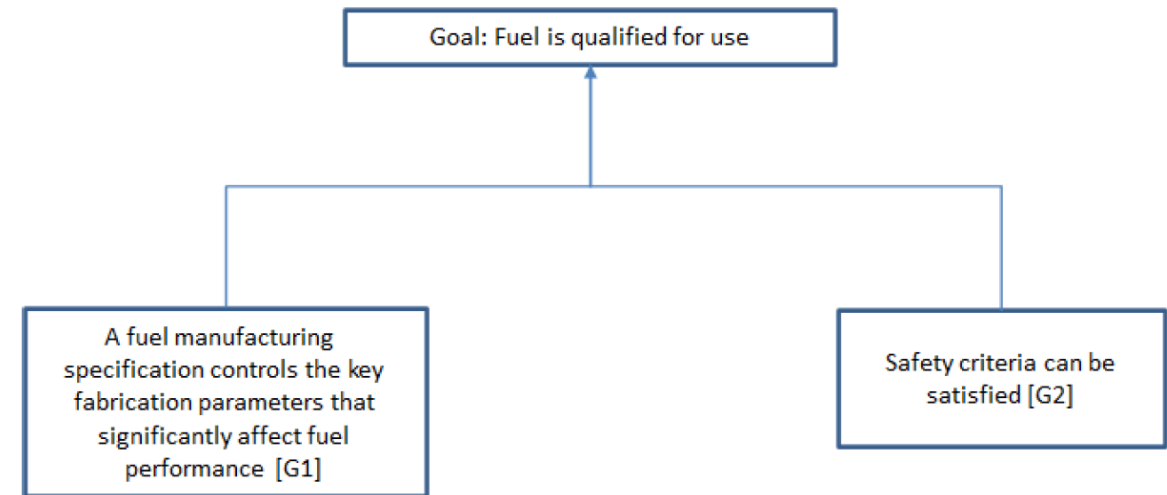


Figure 3-1 Decomposition of the Main Goal

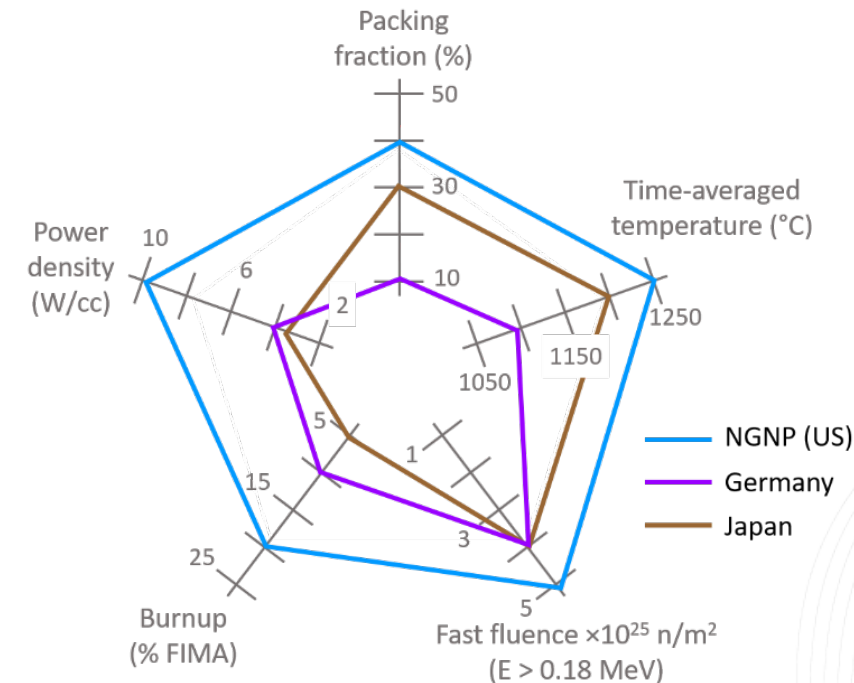
NUREG-2246, “Fuel Qualification for Advanced Reactors”  
<https://www.nrc.gov/reading-rm/doc-collections/nuregs/staff/sr2246/index.html>



# US DOE Advanced Gas Reactor (AGR) Fuel Development and Qualification Program

- Focus on LEU UCO TRISO fuel in cylindrical compacts, consistent with prismatic reactor designs that had been pursued in the US
- Pursued a more aggressive performance envelope compared to German and Japanese programs
- Objectives and Motivation:
  - Provide data for fuel qualification in support of reactor licensing
  - Establish a domestic commercial TRISO fuel fabrication capability

**Reduce  
market  
entry risk**





# Initial AGR Program Reference HTGR Design

- General Atomics *Modular High Temperature Gas Cooled Reactor* (MHTGR)
  - 350 MWt prismatic design
  - He-cooled, graphite moderated
  - 687 °C core outlet temperature
  - UCO TRISO fuel (15.5 wt%  $^{235}\text{U}$ ) in cylindrical compacts

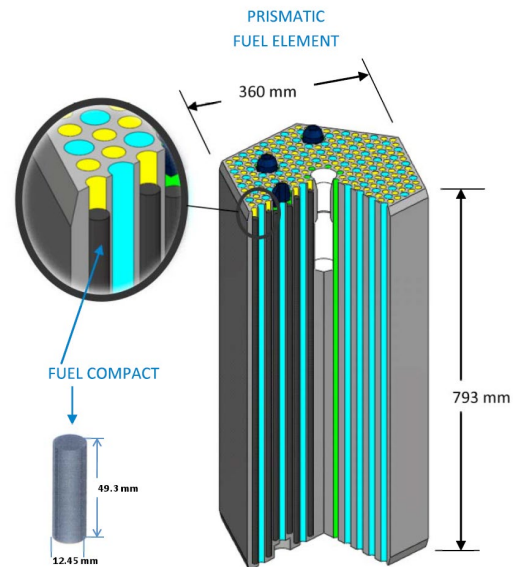
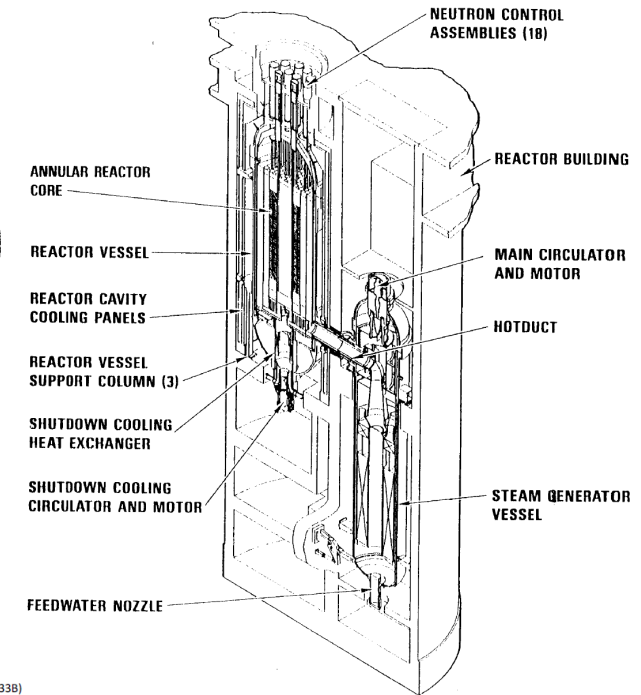


Fig. 5. Isometric view of fuel element containing fuel compacts.  
 Diagram reflects later GA SC-MHR design  
 (M. Richards et al., GA-A27283, 2012)

US-DOE MHTGR PROGRAM

350 MW(t)  
 MODULAR HTGR  
 ISOMETRIC

GENERAL ATOMICS



R.F. Turner and A.J. Neylan,  
 GA-A19391, 1988

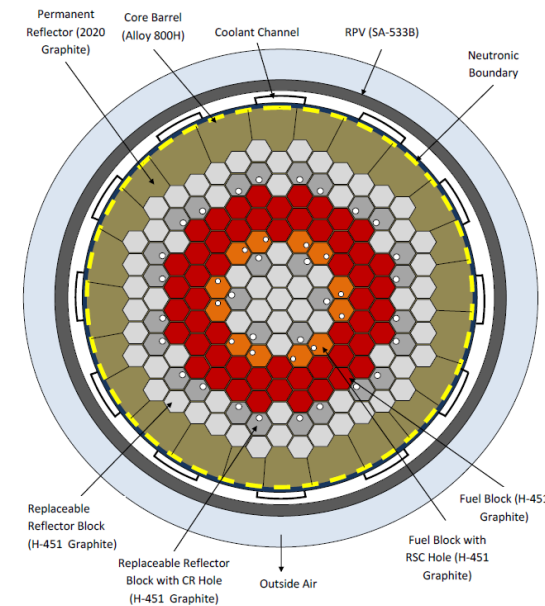
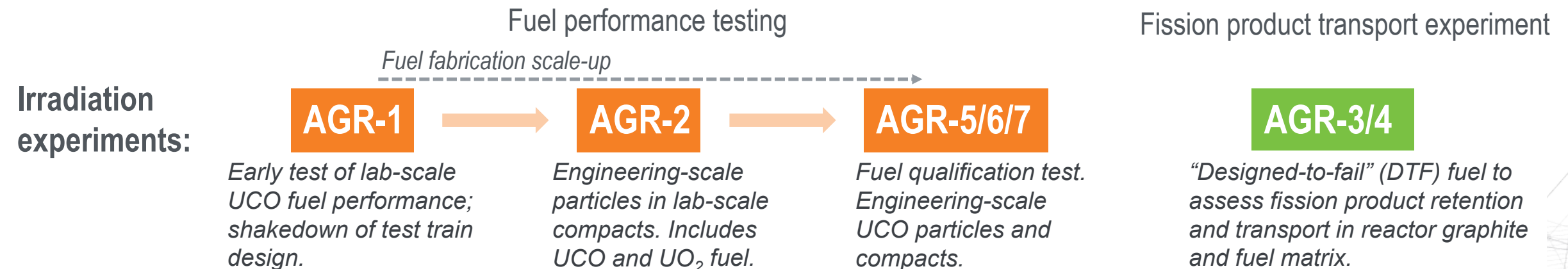


Figure I-3: MHTGR Reactor Unit Layout – Plane

# Fuel Qualification Approach

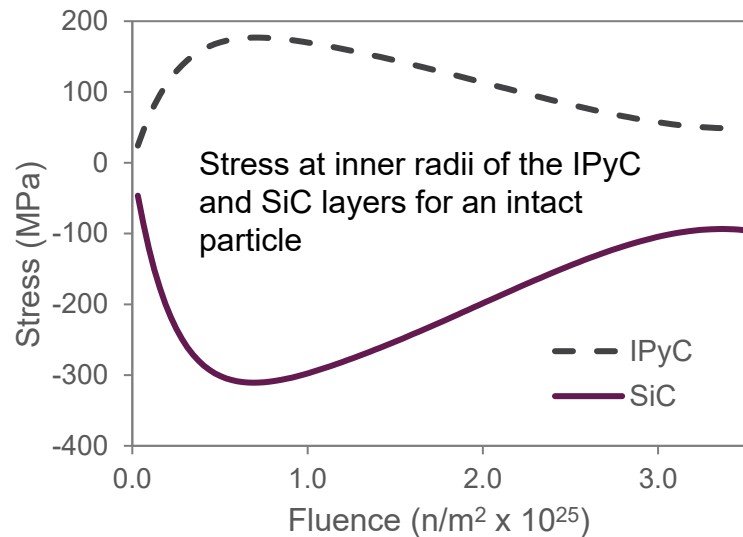
- Develop fuel performance models to describe particle behavior, explain past particle failures (NPR), and guide particle development
- Emulate successful German  $\text{UO}_2$  particle coating design and properties
  - Petti et al., Nucl. Eng. Des. 222 (2003) 281
- Retain UCO kernel from past US development work to accommodate burnup to 20% FIMA in prismatic reactor designs
  - Reduce/eliminate kernel migration (“amoeba effect”) and  $\text{CO(g)}$  corrosion of SiC
- Phased approach for fuel fabrication: demonstrate lab scale production of high-quality fuel with acceptable performance before committing to pilot scale fabrication



# Fuel Performance Modeling



1. Gas pressure is transmitted through IPyC
2. IPyC shrinks, pulling away from the SiC
3. OPyC shrinks, pushing on the SiC



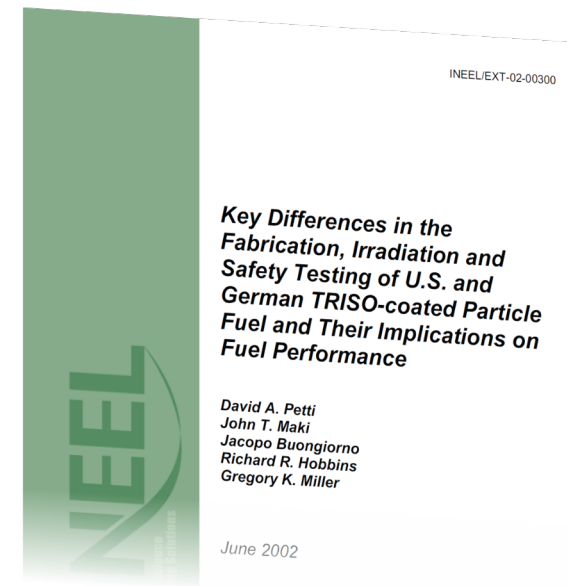
- Model thermomechanical behavior of coatings as a function of particle properties and irradiation conditions
- **Predict coating failure fractions**
- Predict fission product release
- Optimize particle design
- Help establish fuel product specifications
- Numerous codes developed in various countries dating to the 1960s
  - 2000s: Particle Fuel Performance Model (PARFUME)
  - 2010s: BISON Nuclear Fuel Performance Code

W. Jiang et al, *TRISO particle fuel performance and failure analysis with BISON*, JNM 548 (2021) 152795

# Fuel Fabrication

## Major effort to improve fuel fabrication capabilities

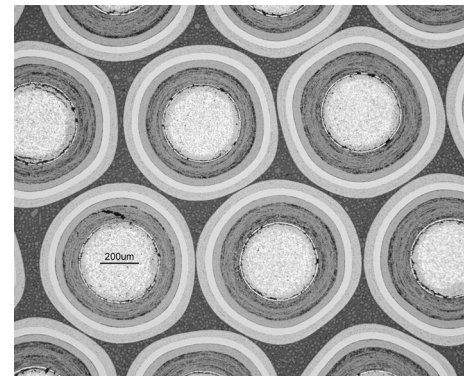
- Better understand coating layer properties that result in desirable fuel behavior
- Many improvements to fabrication methods
  - Minimize as-fabricated coating layer defects
  - Optimize kernel and coating properties
  - Narrow property distributions
- Improve measurement science for reliable fuel property characterization



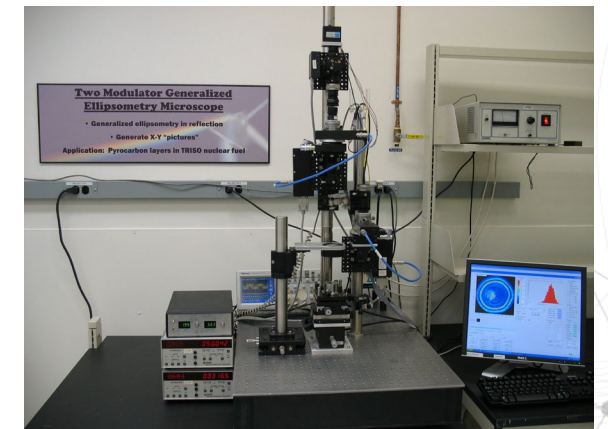
Coater  
chalice



Kernel formation

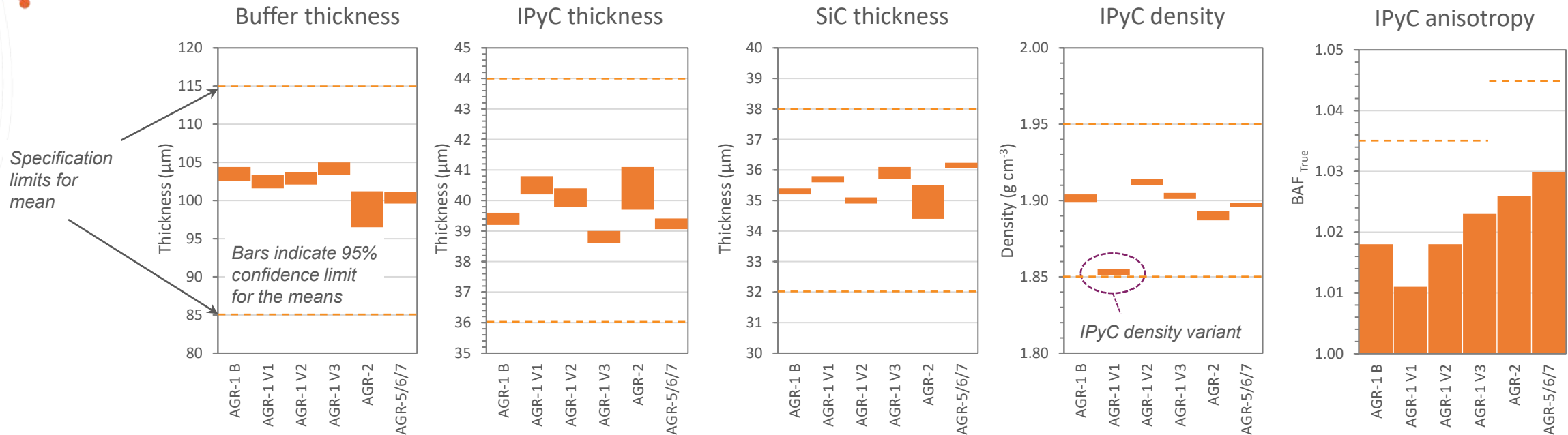


PyC anisotropy measurements





# Selected AGR-1, AGR-2, and AGR-5/6/7 Fuel Property Means

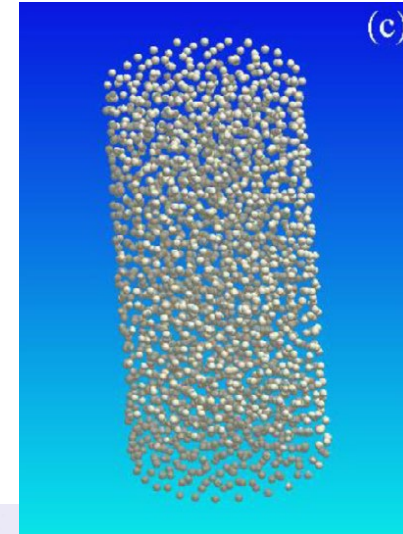
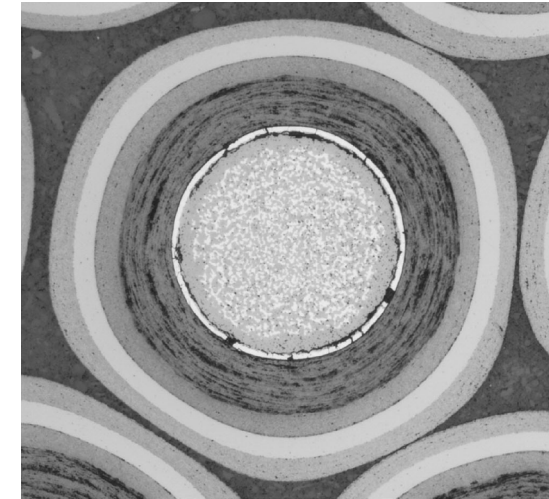


- Mean must be within the specification limits at 95% confidence
- Measured values typically lie well within the specification range
- Note that some specifications were changed following AGR-1, based on computational modeling results on fuel behavior

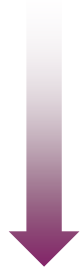
# AGR Program TRISO Fuel

AGR-5/6/7 fuel images

Experiment	Kernel (dia., $\mu\text{m}$ )	Enrichment (% $^{235}\text{U}$ )	Particles/ compact (packing fraction, %)	gU per compact
AGR-1	UCO (350)	19.7	4140 (37)	0.91
AGR-2	UCO (427)	14.0	3180 (37)	1.26
	UO <sub>2</sub> (508)	9.6	1540 (23)	0.99
AGR-5/6/7	UCO (426)	15.5	2240 (25)	0.89
			3430 (38)	1.36



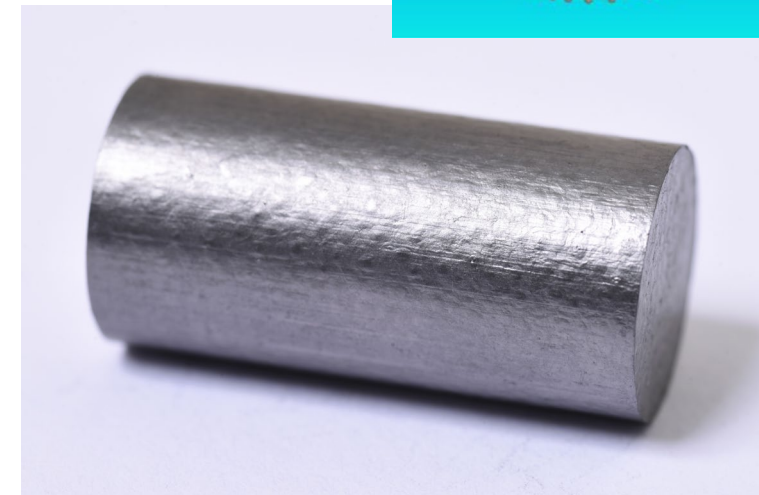
Fabrication  
scale up



	Kernels	Coatings	Compacts
AGR-1	Engineering scale	Lab Scale	Lab Scale
AGR-2	Engineering Scale	Engineering scale	Lab Scale
AGR-5/6/7	Engineering Scale	Engineering Scale	Engineering Scale

Lab Scale – ORNL

Engineering Scale – BWXT





# Key TRISO Fuel Performance Data

## During irradiation

- Fission gas release during irradiation: release-rate-to-birth-rate ratio (R/B)
- Coating layer failure statistics

## Post-irradiation examination

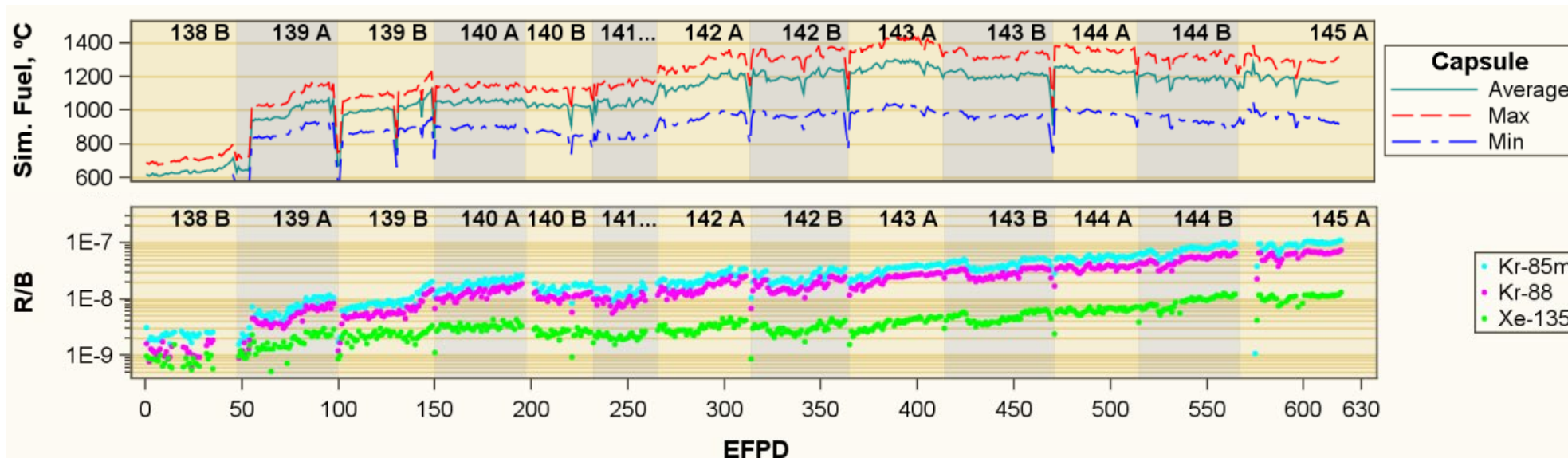
- Kernel and coating morphology evolution
- Condensable fission product release during irradiation (e.g., Cs, Ag, Sr)
- Fission product release during high-temperature accidents
- Coating layer failure statistics
- Oxidation behavior of fuel and fission products



# Irradiation Performance: Fission Gas R/B

- Sources of fission gas release:
  - Uranium contamination outside of intact SiC layers
  - Exposed kernel defects (as-fabricated)
  - Exposed kernels from in-service coating layer failure
- Fission gas release-rate-to-birth-rate ratio (R/B) provides information on the extent of coating failures during irradiation

*Allowable levels dictated by specifications*



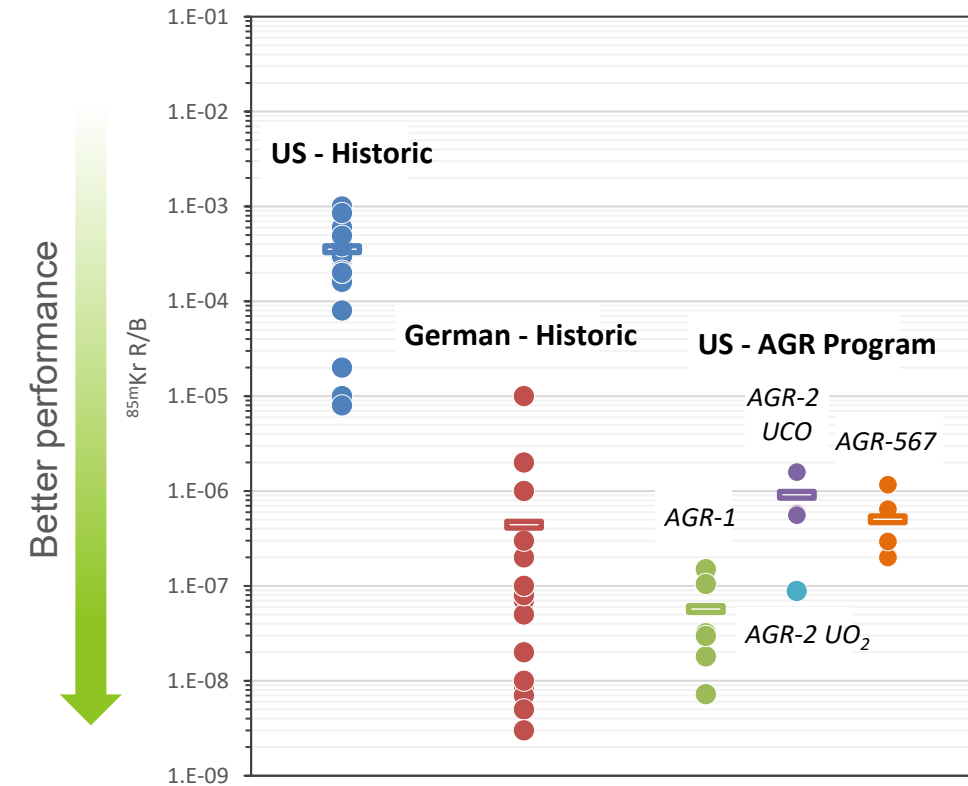
**AGR-1  
Capsule 6 Data**

→ **Data indicate zero as-fabricated exposed kernels or in-pile TRISO failures in this capsule**

# Irradiation Testing Results

- $\sim 10^6$  UCO particles in  $\sim 300$  fuel compacts irradiated under a broad range of HTGR conditions
- $^{85m}\text{Kr}$  R/B of  $\sim 10^{-8} - 10^{-6}$  at peak burnup of 19.6% FIMA
- Operational issues with AGR-2 and AGR-5/6/7 impaired R/B measurement during later cycles

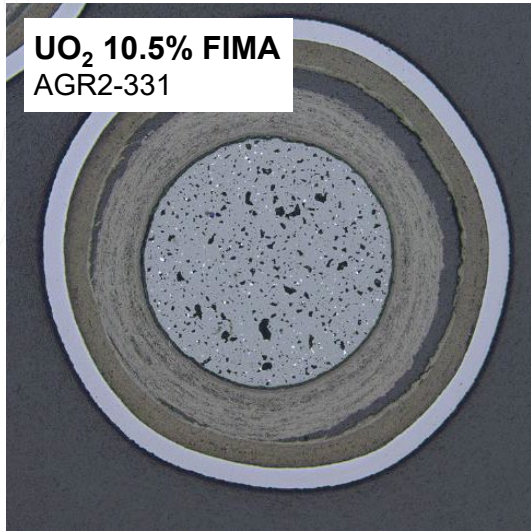
Comparison of US and German  $^{85}\text{Kr}$  R/B data



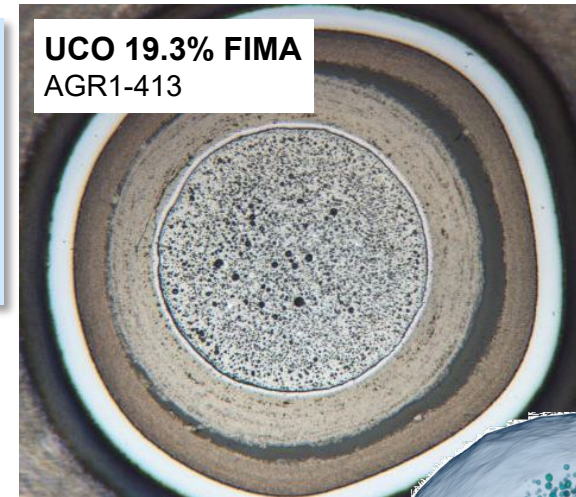
AGR-2 R/B values are through the first  $\sim 1/4$  of the irradiation (149 EFPD)

AGR-567 R/B values are through the first  $\sim 1/2$  of the irradiation (174 EFPD)

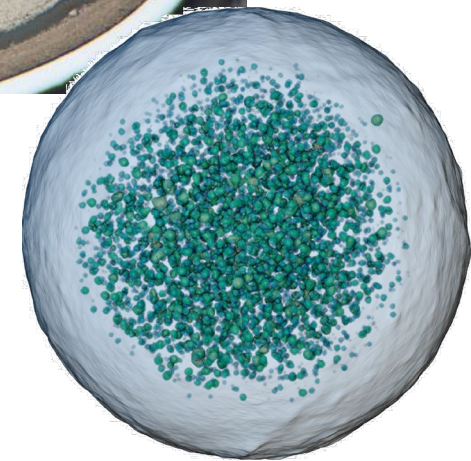
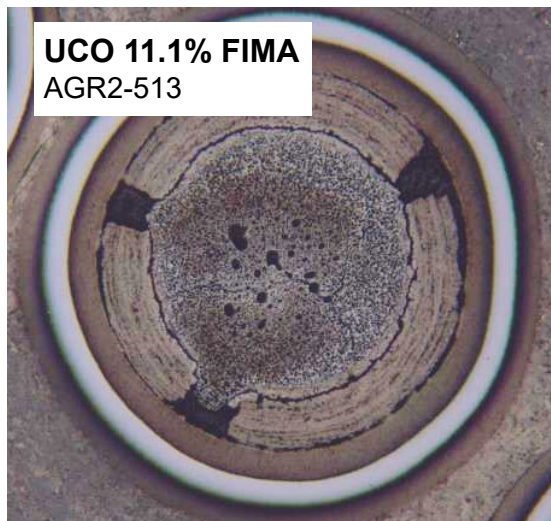
# Kernel and Coating Behavior During Irradiation



- Kernel swelling and pore formation
- Buffer densification and volume reduction
- Separation of buffer and IPyC layers



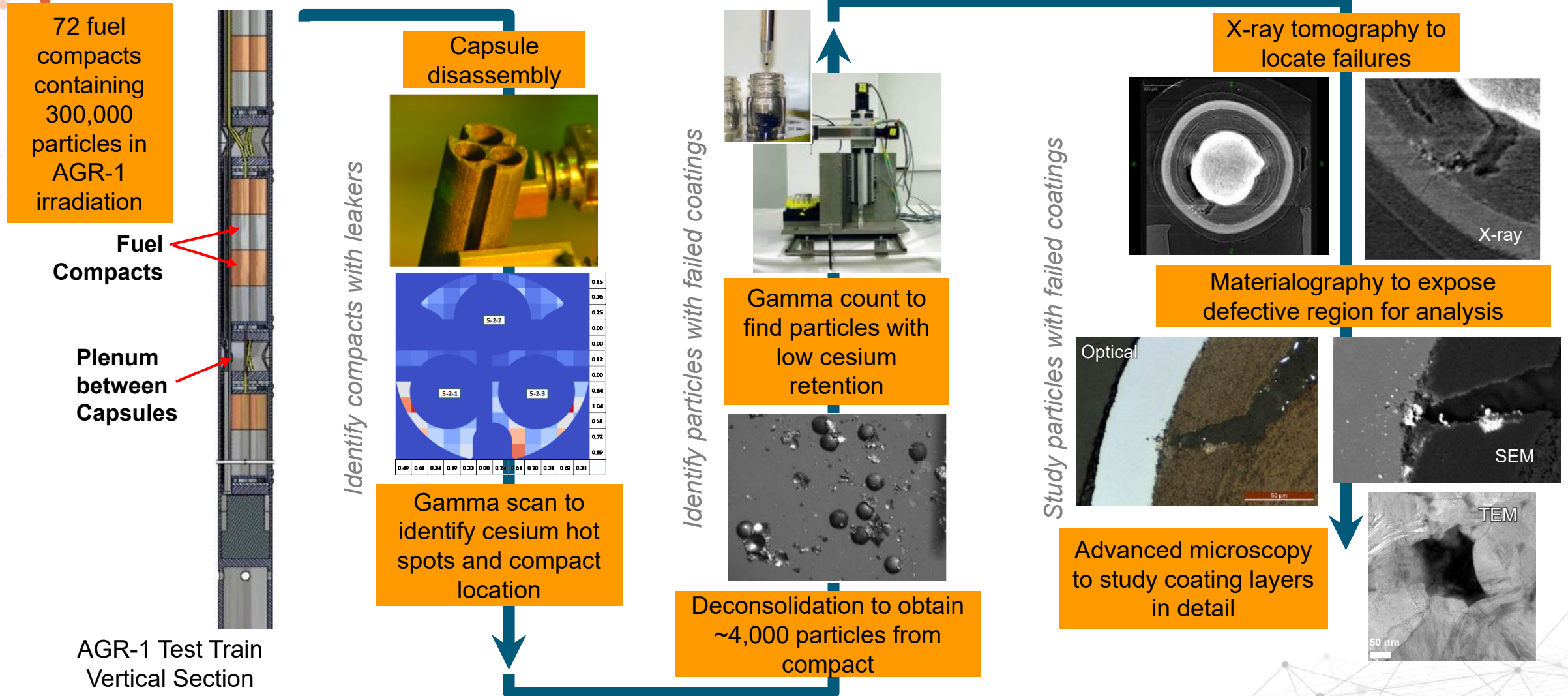
- Buffer fracture relatively common in UCO fuel particles
- Kernel can swell into gap
- Dependent on irradiation temperature and fast neutron fluence
- When buffer separates from IPyC, buffer fracture appears to have no detrimental effect on dense coating layers



3D rendering of irradiated AGR-2  
UCO kernel pore structure from  
x-ray computed tomography

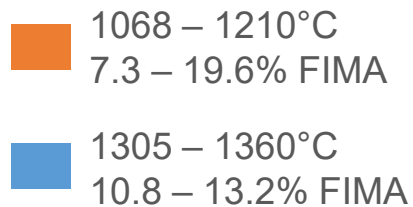
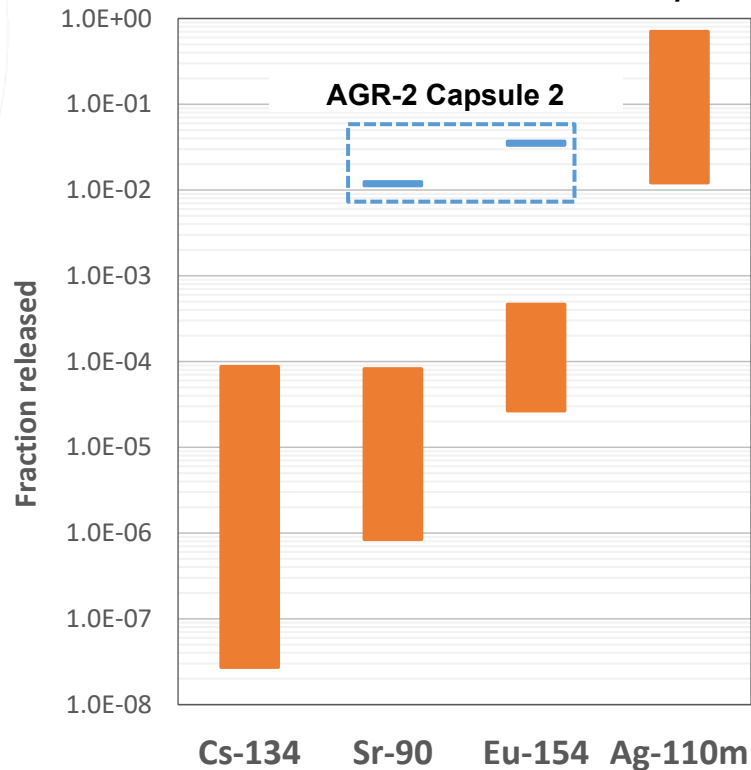


# Locating and Studying Failed Particles Greatly Improves Understanding of Fuel Performance



# Fission Product Release from UCO Fuel Compacts: AGR-1 and AGR-2 Examples

*Fission product release from AGR-1 and AGR-2 UCO fuel compacts*



Time-average peak temperatures

- Cs release is very low with intact SiC; higher releases are associated with a limited number of particles with failed SiC
- Sr and Eu can exhibit modest release; release is appreciably higher with high in-pile temperatures
- High Ag release
- Note these releases do not account for retention in core graphite

# HTGR Accident Safety Testing of TRISO Fuel

- Temperature transients are relatively slow (days)
- Peak fuel temperatures are limited to  $\sim 1600^{\circ}\text{C}$  in modular HTGR designs
- Fuel particles are designed to withstand accident conditions while still retaining key safety-significant fission products
- Total duration at peak temperatures is tens of hours, with a small fraction of the fuel in the core experiencing temperatures near the peak
- Extremely rapid reactivity insertion accidents (RIAs) are precluded by HTGR core design
- Assess fuel performance by post-irradiation heating tests while measuring fission product release at  $1600 - 1800^{\circ}\text{C}$

Core temperature during depressurized loss of forced cooling accident – HTR Module

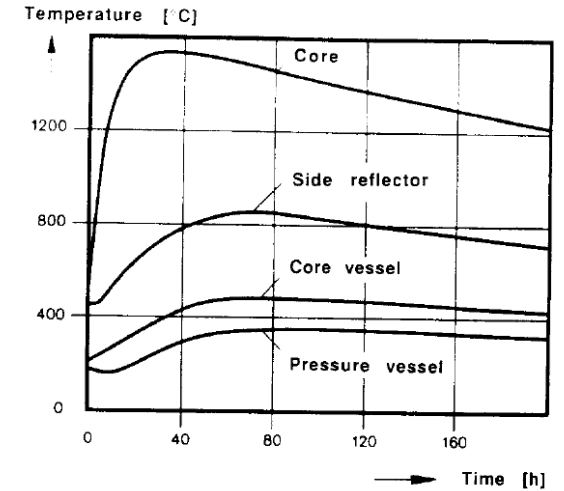


Fig. 11. Time-dependent component temperatures after depressurization accident.

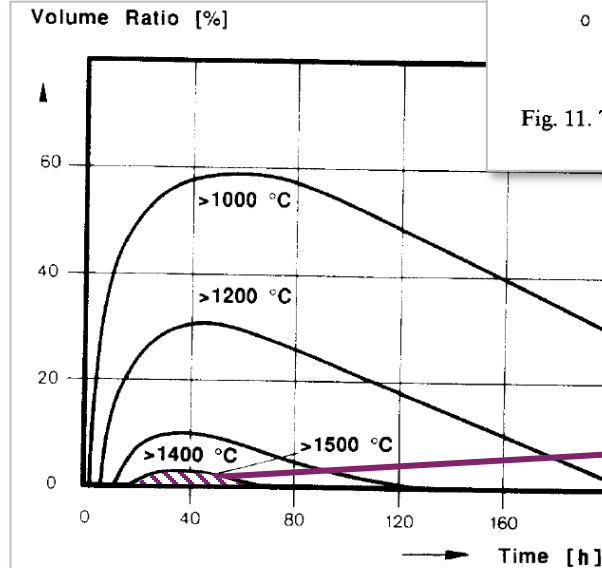
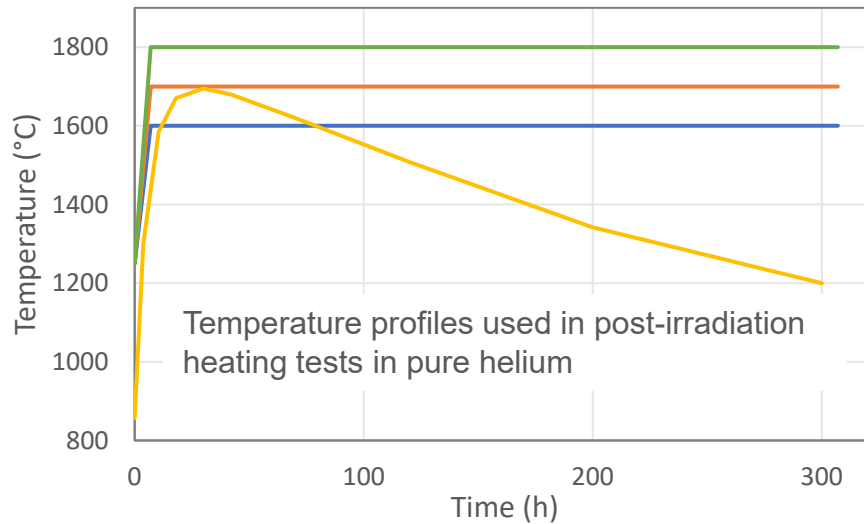


Fig 12. Time-dependent volume ratio of fuel element temperatures.

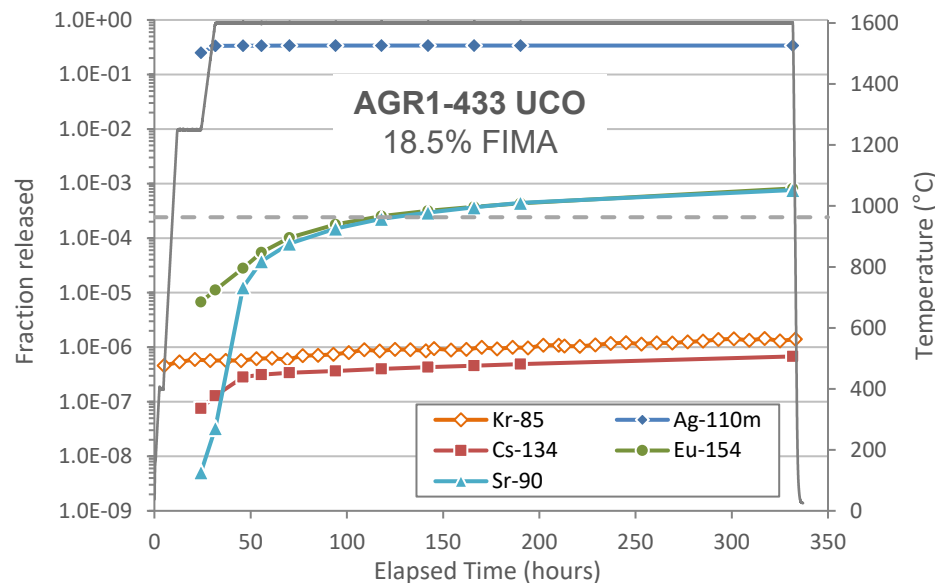
G. Lohnert, et al. Nuc. Eng. Des. 121 (1990) 259-275

~3% of fuel  $>1500^{\circ}\text{C}$

# Evaluating Behavior During D-LOFC Accidents



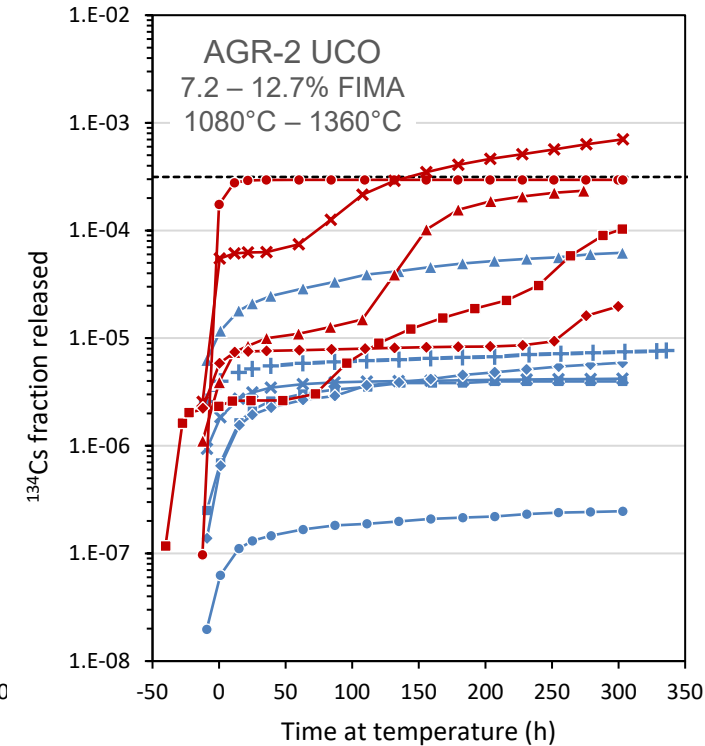
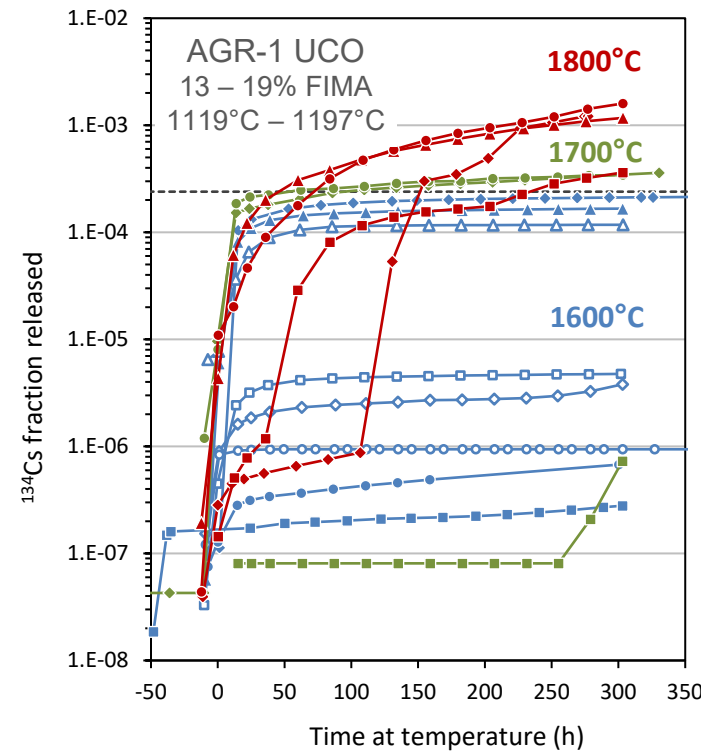
- Two types of heating profiles used:
  - Isothermal
  - Variable temperature mimicking peak fuel temperature during D-LOFC
- Hundreds of hours in pure helium
- Two test systems used:
  - Core Conduction Cooldown Test Facility (CCCTG) – ORNL
  - Fuel Accident Condition Simulator (FACS) – INL
- Kr release: indication of failed TRISO
- Cs release: indication of failed SiC (if PyC intact)





# Safety Test Results for US UCO Fuel

- Zero TRISO layer failures at 1600 – 1700°C (very low Kr release)
- Cs release through intact SiC is very low ( $<10^{-5}$ )
- Higher releases are dominated by a small number of particles with failure of the SiC layer
- Increasing test temperature increases the incidence of SiC failure

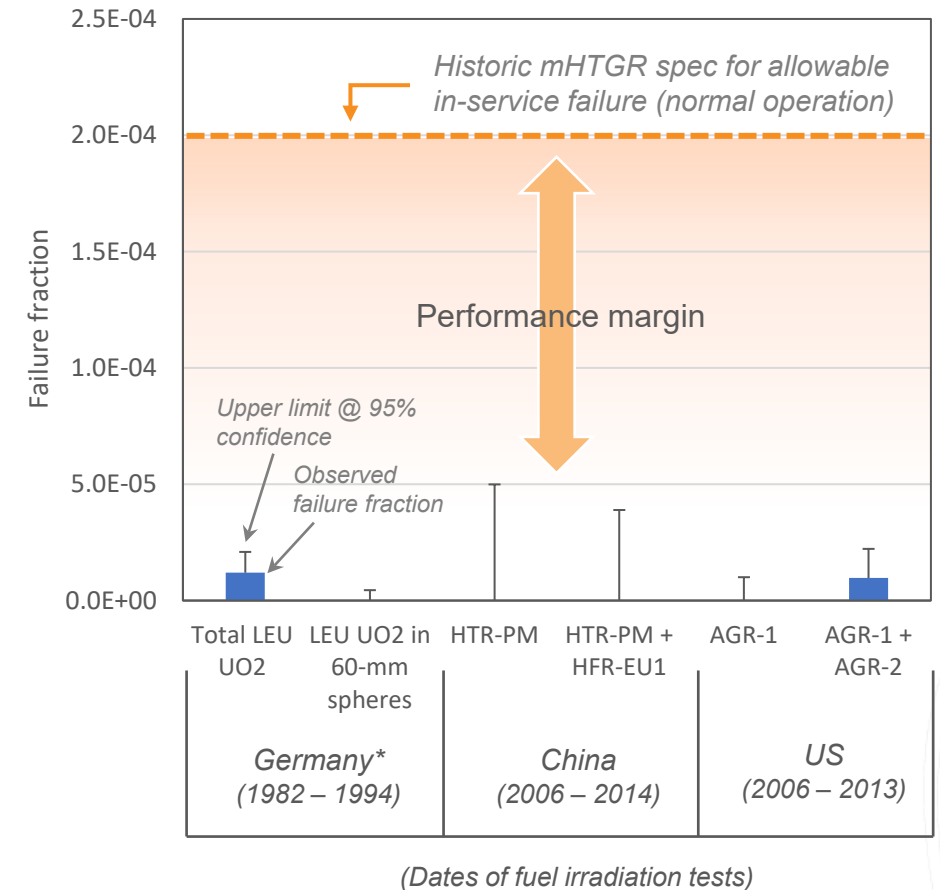
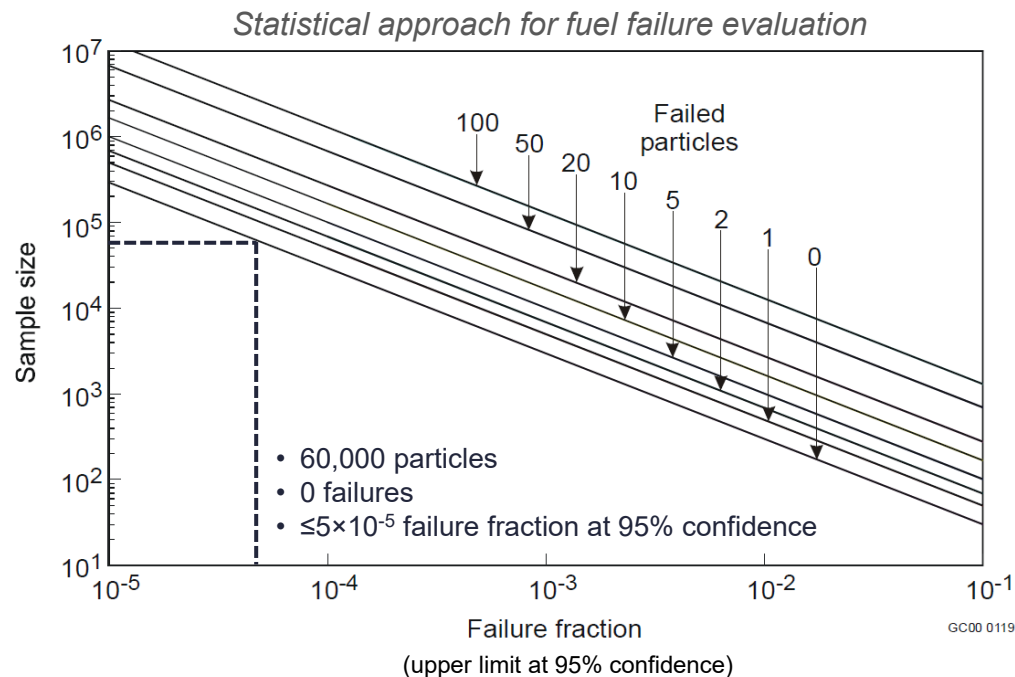


Temperatures are time-average peak irradiation temperature

Temperature (°C)	Avg $^{134}\text{Cs}$ release (300 h)
1600	$4 \times 10^{-5}$
1800	$6 \times 10^{-4}$

# Particle Failure Evaluation

- High-quality TRISO fuel demonstrates in-pile particle failure rates substantially below historic reactor design specifications
- Requires adequate particle population to demonstrate low failure fraction at the 95% confidence level

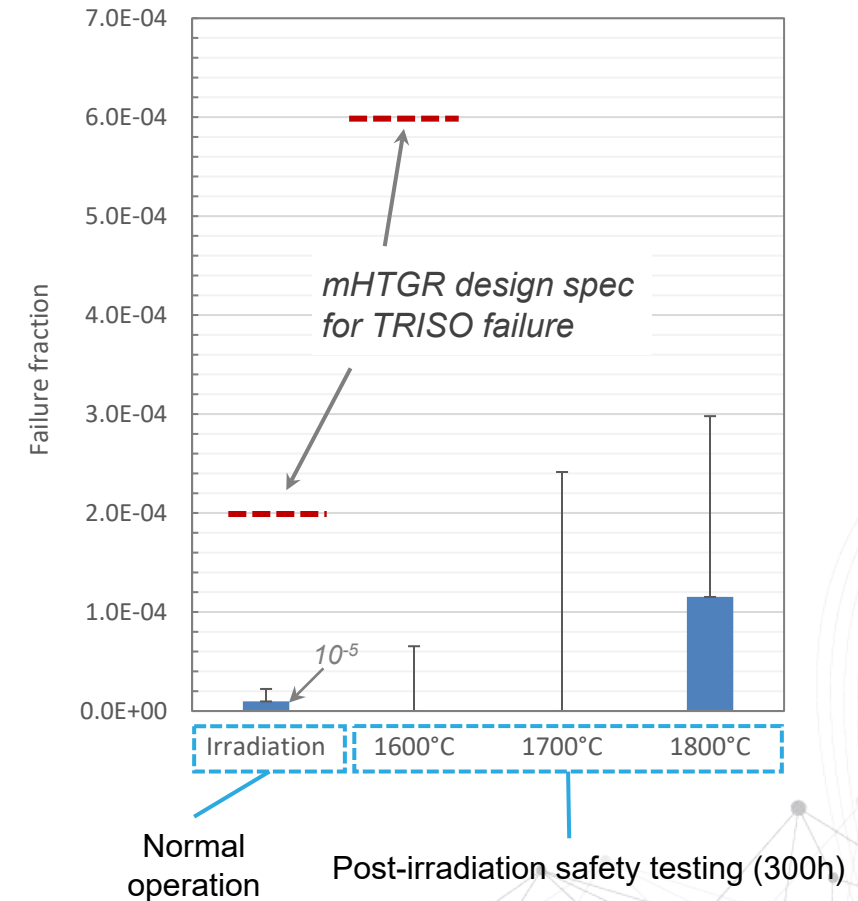


\* Kania et al., J. Nucl. Mater. 441 (2013) 545-562

# Fuel Performance Summary

- Very low in-pile particle failure rates
- Fuel withstands temperatures of 1600°C and beyond for 100s of hours without significant TRISO failure
- Release of condensable fission products is dominated by stored inventory in the matrix and gradual degradation of the SiC layer
- There is significant performance margin in terms of time at temperature

*Experimental TRISO failure fractions for AGR-1 + AGR-2*





# Ongoing Work and Outstanding Data Needs

- AGR-3/4 data analysis and reporting
- AGR-5/6/7 PIE and safety testing
  - Destructive fuel compact analysis
  - High temperature safety testing
- Fuel and fission product behavior in oxidizing environments
- Fuel performance and fission product transport modeling
  - Comparison of codes to empirical data; code refinement

# Core Oxidation

- Accident scenarios in steam-cycle gas-cooled reactors can include air or steam ingress into the core (design basis events or beyond design basis events)
- Core behavior under these conditions should be evaluated
  - Graphite and matrix oxidation
  - Fission product volatilization from matrix/graphite and exposed kernels
  - Oxidation of coated particles could impact particle integrity
- Previous work has included characterization of oxidation behavior of core materials:
  - Graphite oxidation data is available in literature
  - Limited data on matrix oxidation
  - Limited data on kernel and coated particle response to core oxidants

Fission gas release from irradiated UCO fuel kernel in response to water vapor injection (HRB-17 experiment)

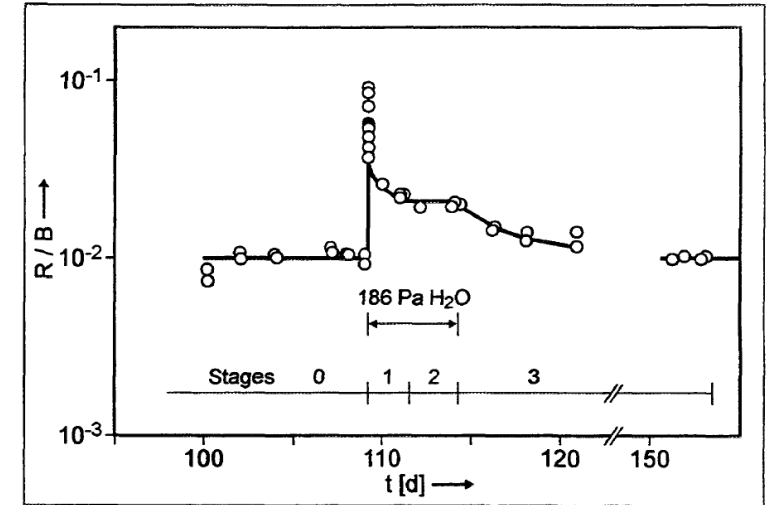


Fig. 5-1: R/B-time profile for Kr-85m before, during, and after a water vapor injection test with 186 Pa of water vapor at 755 °C

IAEA-TECDOC-978 (1997) is a good reference for earlier studies of fuel response to oxidants



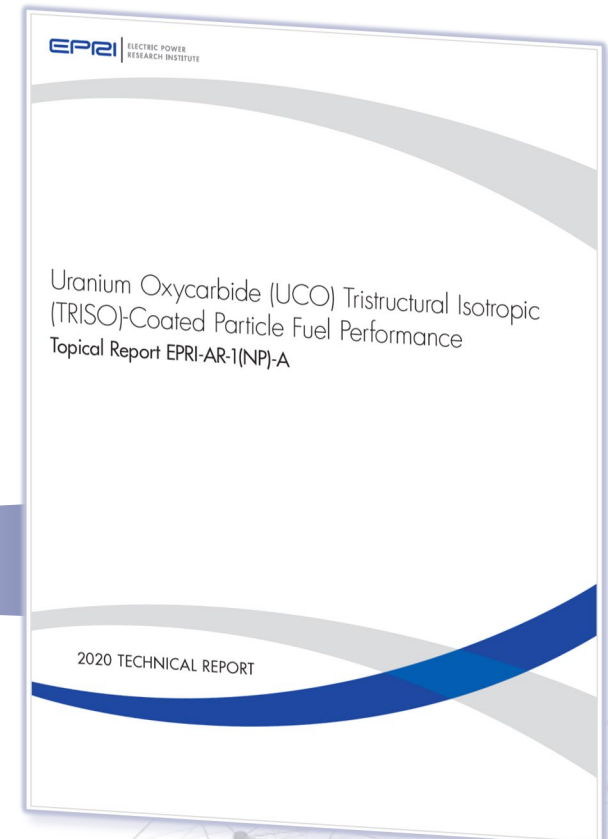
# Industry Engagement

- General Atomics supported early AGR program development
- BWXT fabricated AGR fuel
- NGNP Alliance
  - Active during NGNP program and subsequent years
- NEI High-Temperature Reactor Technology Working Group (HTR-TWG)
  - HTR developer's forum that addresses cross cutting issues
- EPRI TRISO topical report
- Ongoing industry engagement regarding AGR data interpretation, remaining program activities, and future licensing topical reports

The NGNP Industry Alliance  
Promoting the development and commercialization of High Temperature Gas-cooled Reactor (HTGR) technology



ConocoPhillips



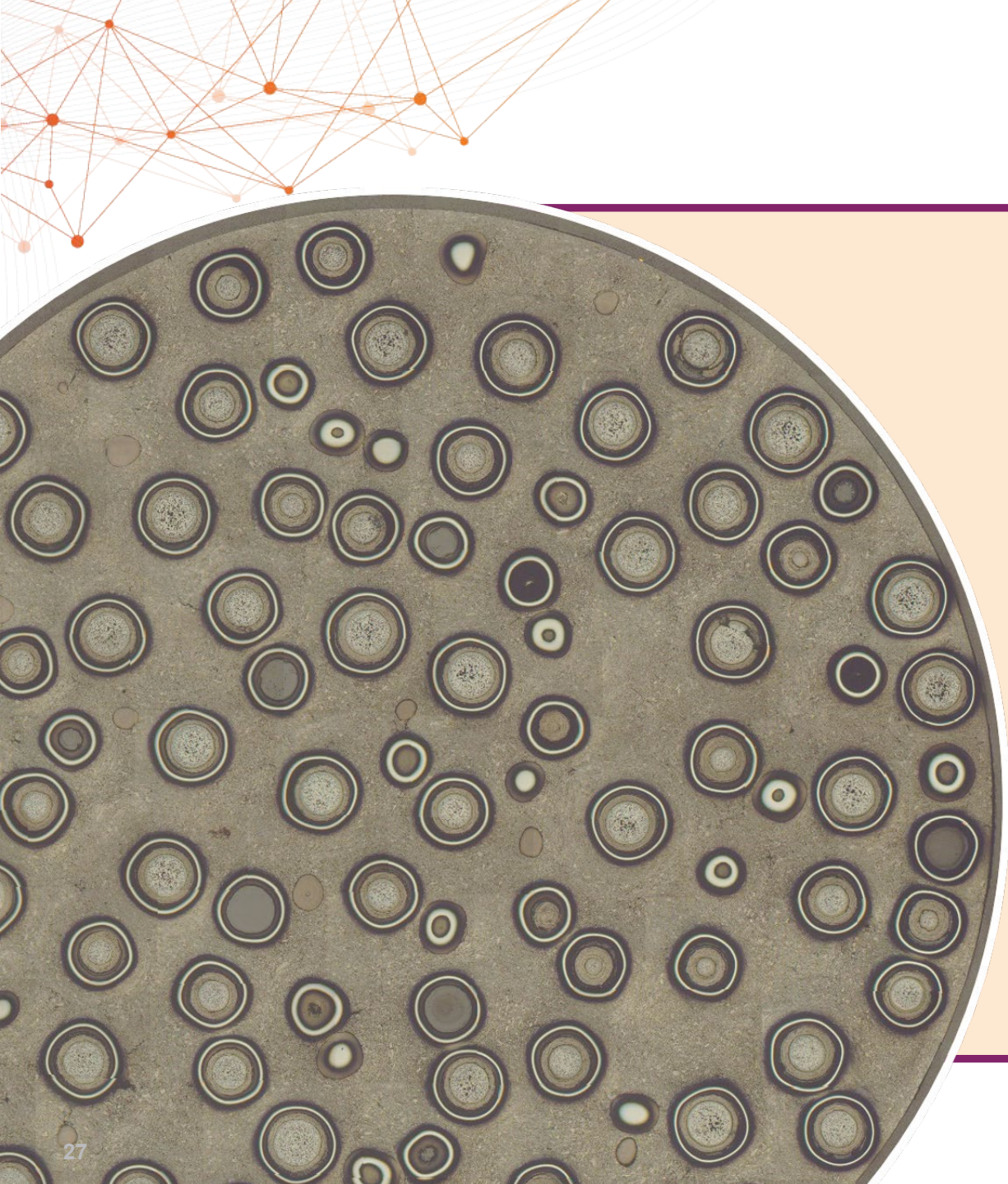
# Coated-Particle-Fueled Reactor Concepts and Fuel Designs

Developer	Description	Fuel design
X-energy	Xe-100 200 MWt PB HTGR Xe-Mobile 1 – 5 MWe microreactor	UCO TRISO pebbles, graphitic matrix UCO TRISO
Kairos Power	KP-FHR 140 MWe salt-cooled SMR Hermes 35 MWt test reactor	UCO TRISO pebbles, graphitic matrix UCO TRISO pebbles, graphitic matrix
BWXT	BANR 50 MWt microreactor Pele/MNPP 1 – 5 MWe transportable microreactor	UN TRISO in SiC matrix TRISO
Ultrasafe Nuclear	MMR 15 MWt microreactor	UCO TRISO in SiC matrix (“FCM”)
Westinghouse	eVinci 7-12 MWt microreactor	UCO TRISO compacts, graphitic matrix
Radiant Nuclear	Kaleidos >1 MWe transportable microreactor	UCO TRISO compacts, graphitic matrix
Framatome	SC-HTGR 625 MWt	UCO TRISO compacts, graphitic matrix
StarCore Power	10 MWe HTGR	TRISO
HolosGen	22 MWt scalable microreactor	TRISO fuel compacts
ORNL	Transformational Challenge Reactor	UN TRISO in SiC matrix
NASA	Nuclear thermal propulsion (NTP), nuclear electric propulsion (NEP)	Various

## Useful references:

- Advances in Small Modular Reactor Technology Developments. A Supplement to: IAEA Advanced Reactors Information System (ARIS), 2020 Edition, IAEA ([https://aris.iaea.org/Publications/SMR\\_Book\\_2020.pdf](https://aris.iaea.org/Publications/SMR_Book_2020.pdf))
- <https://www.world-nuclear.org/information-library/nuclear-fuel-cycle/nuclear-power-reactors/small-nuclear-power-reactors.aspx> (updated Jan 2023)





***Thank you for your attention***

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