



Temperature-Dependent Mechanical Anisotropy in Textured Zircaloy Cladding

March 2024

Changing the World's Energy Future

Malachi Michael Nelson, David W Kamerman



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**Prepared for the
U.S. Department of Energy
Under DOE Idaho Operations Office
Contract DE-AC07-05ID14517**

March 7, 2024

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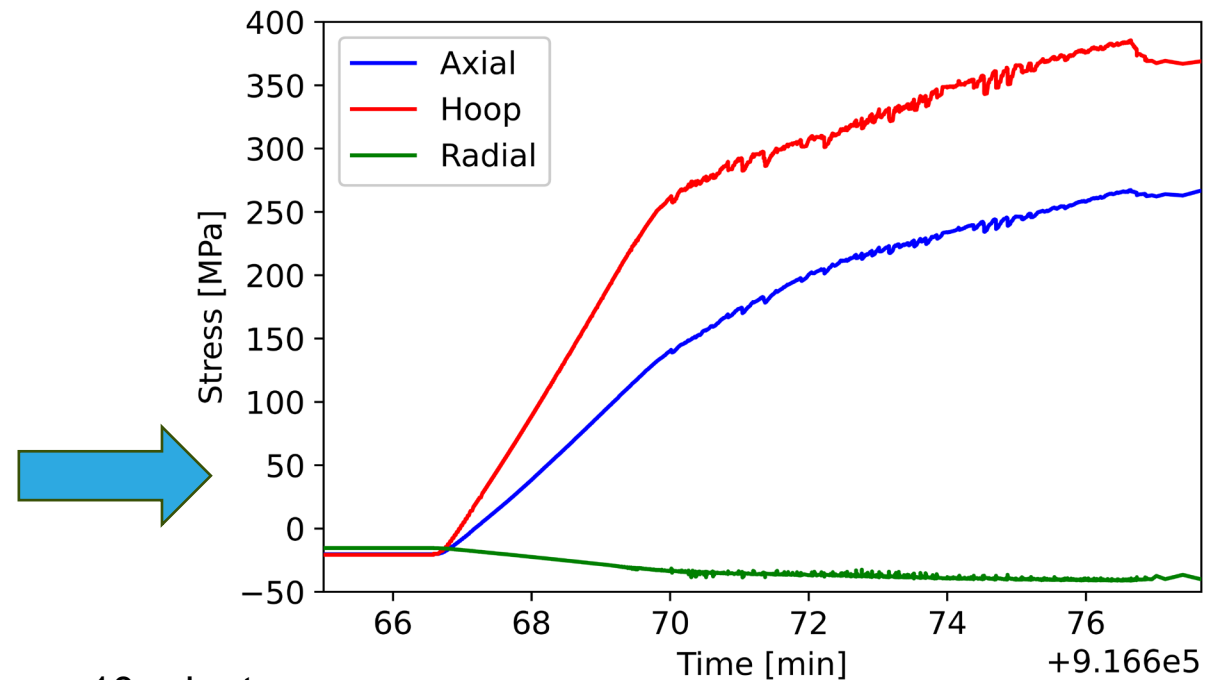
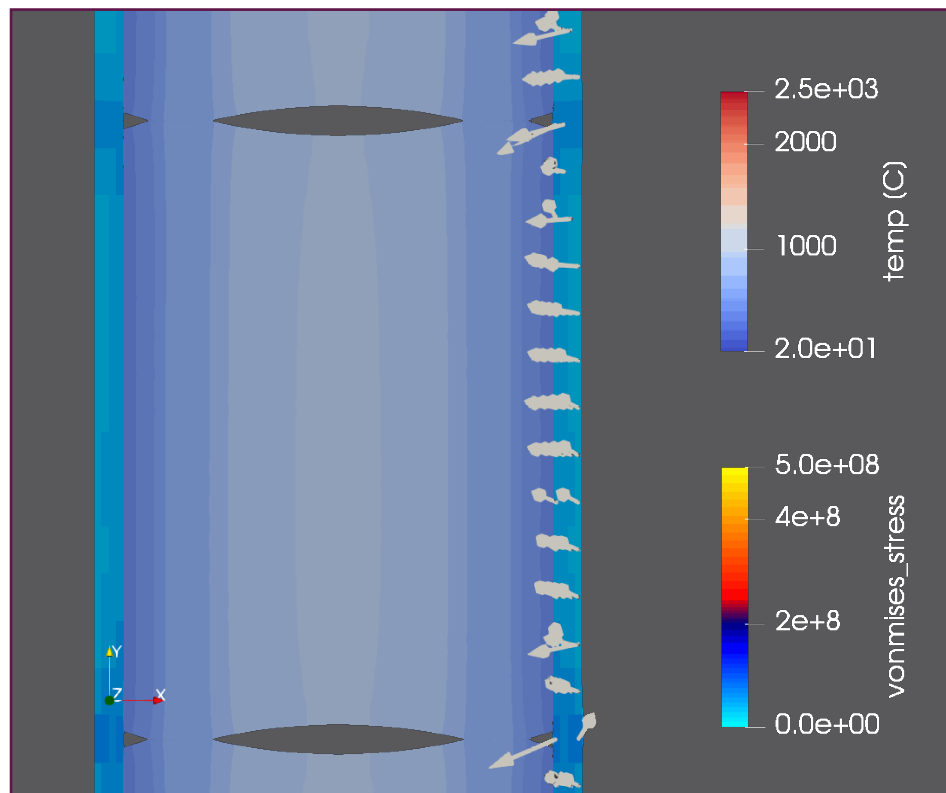
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Research Team

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 - Ph.D. Nuclear Engineering – UC Berkeley Exp. 2024
 - Idaho National Laboratory Graduate Fellow
- **Coauthors**
 - David Kamerman – Idaho National Laboratory
 - Peter Hosemann – UC Berkeley
 - Shmuel Samuha – UC Berkeley, NCRN
- **Funding**
 - This work was supported through the U.S. Department of Energy (DOE) Advanced Fuels Campaign under DOE Idaho Operations Office contract DE-AC07-05ID14517.

Pellet-Cladding Mechanical Interactions

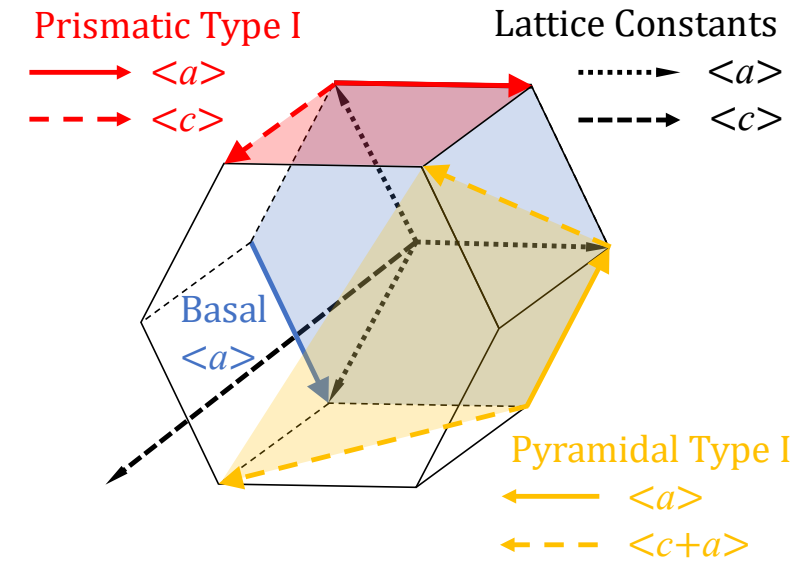
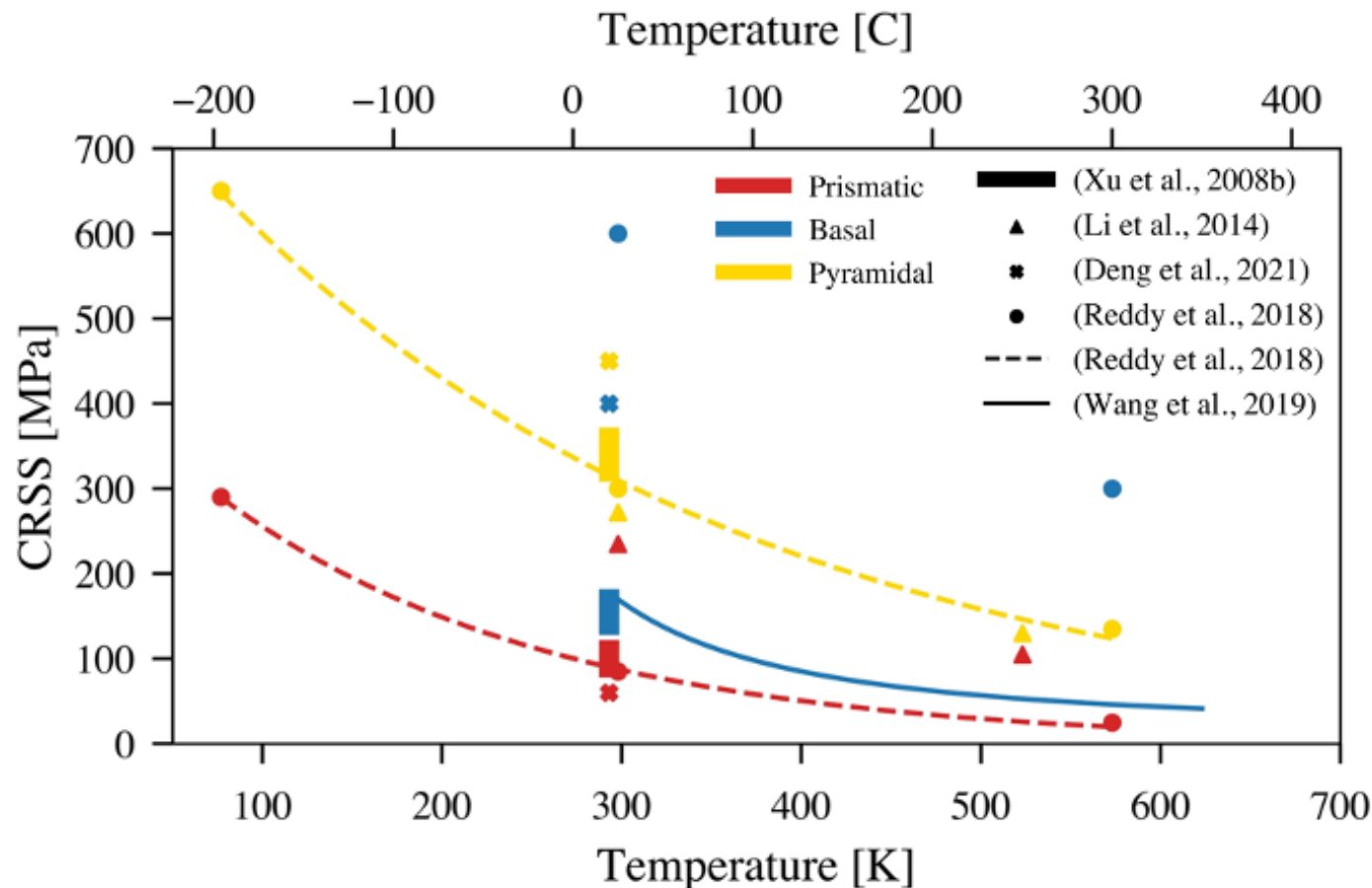
- Reactor power increases cause fuel pellet expansion
- Can generate stress in cladding, especially at burnup above ~20 GW/MTU
- Stress is near biaxial*: $(\sigma_z, \sigma_\theta, \sigma_r) \cong (0.75, 1, 0)$ *(Udagawa, et al., 2013), (Suzuki et al., 2006)



10-minute power ramp
simulated using BISON
fuel performance code.

Textured Zircaloy-4 Cladding

- Hexagonal close-packed (HCP) structure



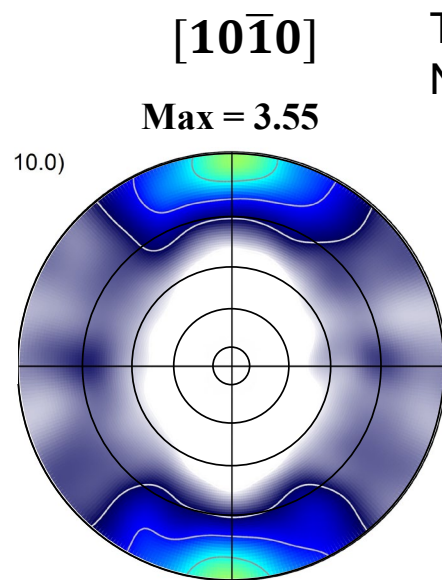
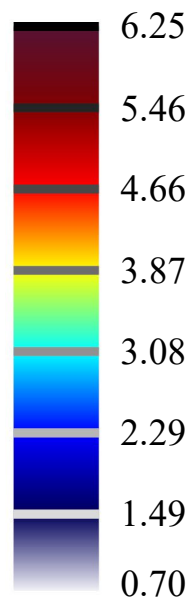
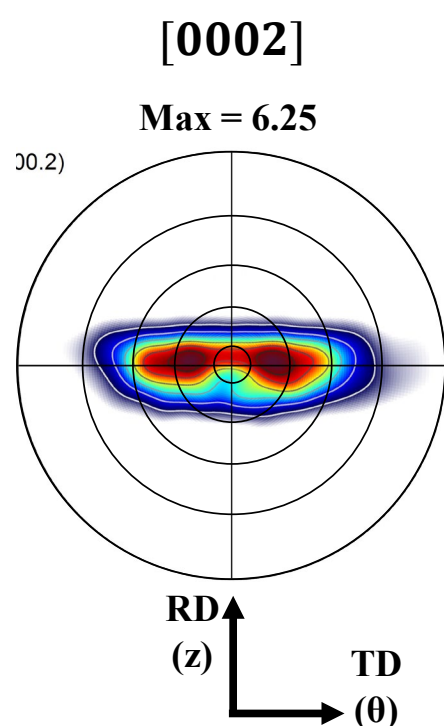
$$CRSS_{\text{prismatic } \langle a \rangle} = 439 \cdot \exp\left(-\frac{T}{185}\right)$$

$$CRSS_{\text{basal } \langle a \rangle} = 11.3 \cdot \exp\left(\frac{807.7}{T}\right)$$

$$CRSS_{\text{pyramidal } \langle c+a \rangle} = 837 \cdot \exp\left(-\frac{T}{300}\right)$$

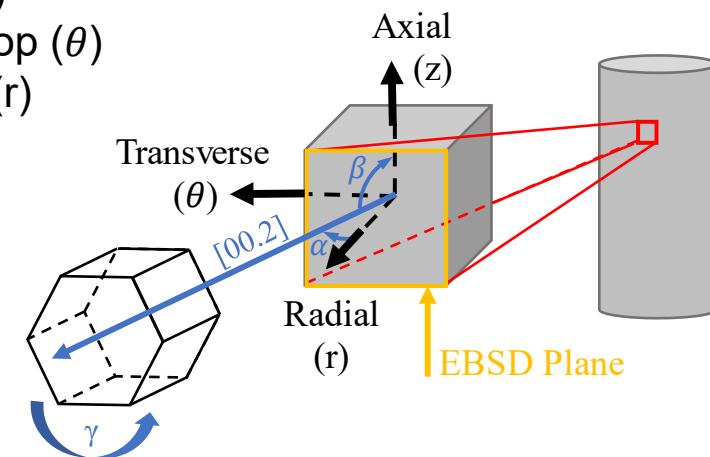
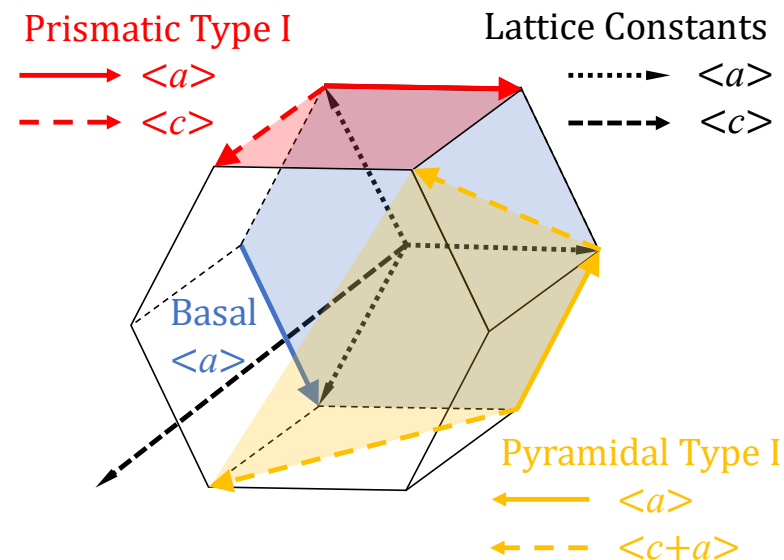
Textured Zircaloy-4 Cladding

- Hexagonal close-packed (HCP) structure
- Pilgering and rolling results in similar texture
- Texture retained to resist cladding thinning
- Multiscale anisotropy



Measured texture of Zry-4 cladding used in this study

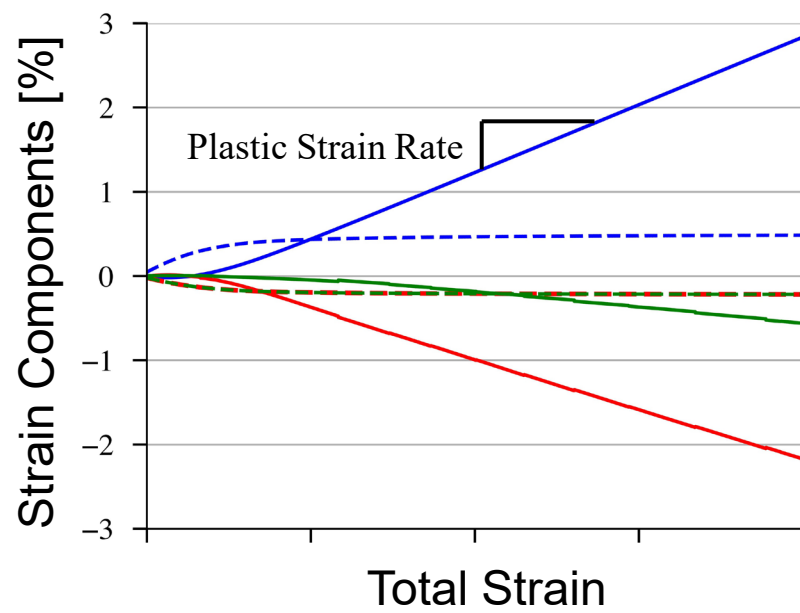
Rolled direction (RD) = axial (z)
Transverse direction (TD) = hoop (θ)
Normal direction (ND) = radial (r)



Hexagonal unit cell	Orthogonal unit cell	Engineering geometry
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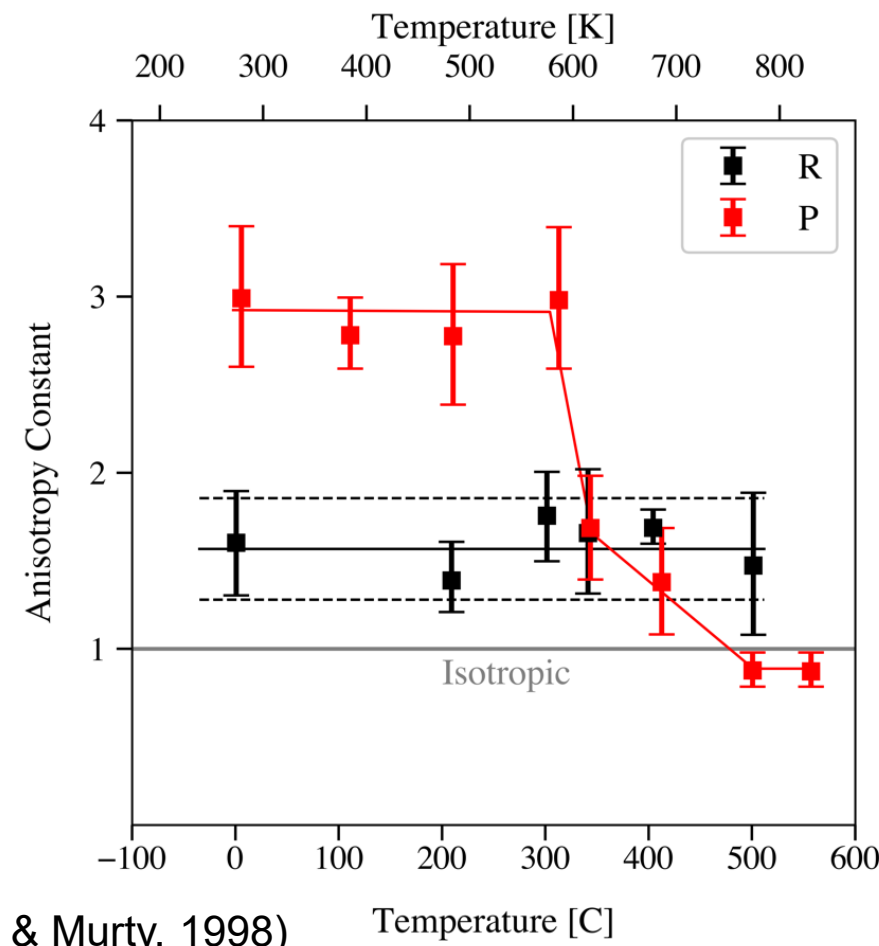
Mechanical Anisotropy in Textured Zircaloy-4

- Anisotropy defined by plastic strain ratios
- Unloaded plastic strains equal for isotropic
- Temperature independent anisotropy for RD
- Temperature dependent anisotropy for TD



$$R = \left(\frac{\dot{\epsilon}_{TD}}{\dot{\epsilon}_{ND}} \right) \sigma_{RD}$$

$$P = \left(\frac{\dot{\epsilon}_{RD}}{\dot{\epsilon}_{ND}} \right) \sigma_{TD}$$

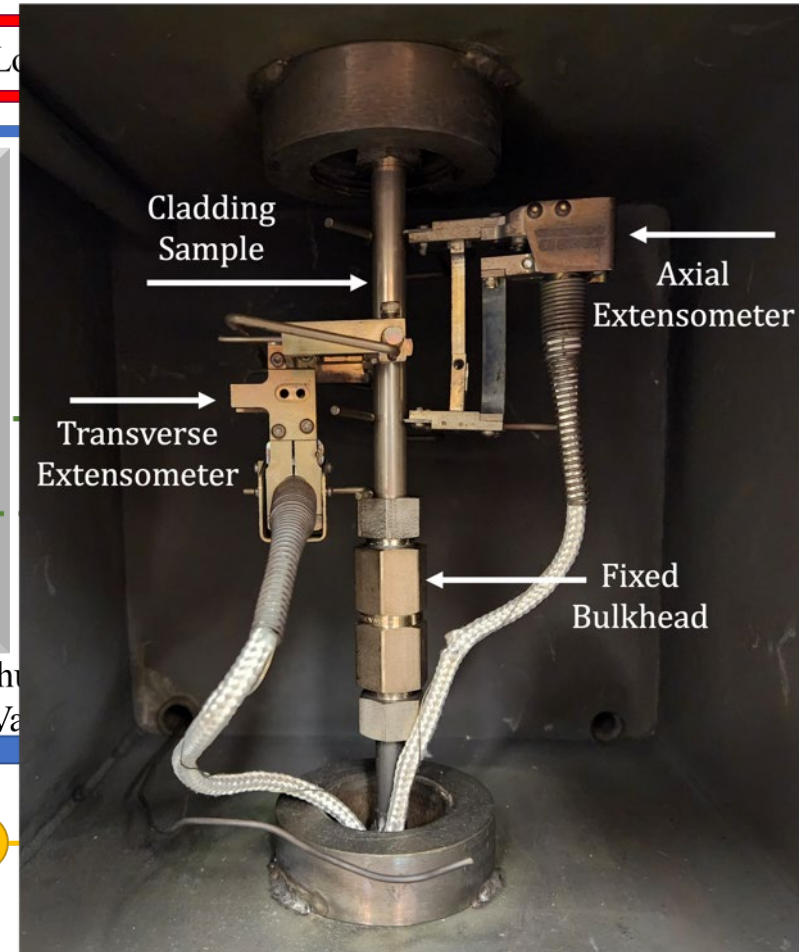
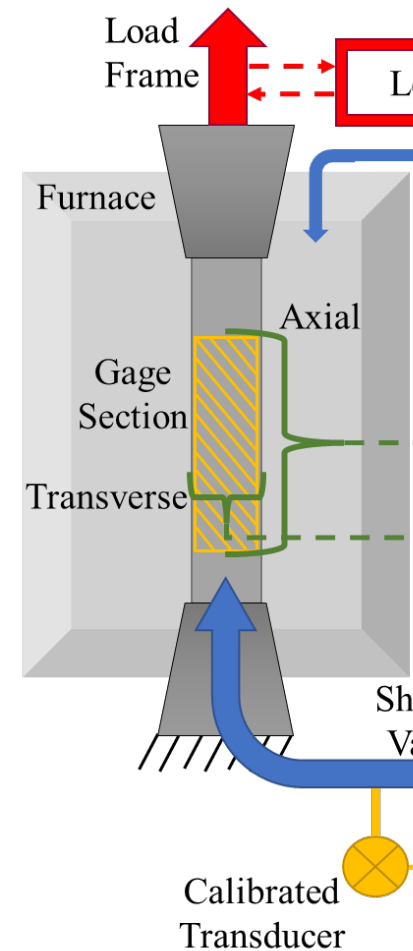


(Wang & Murty, 1998)

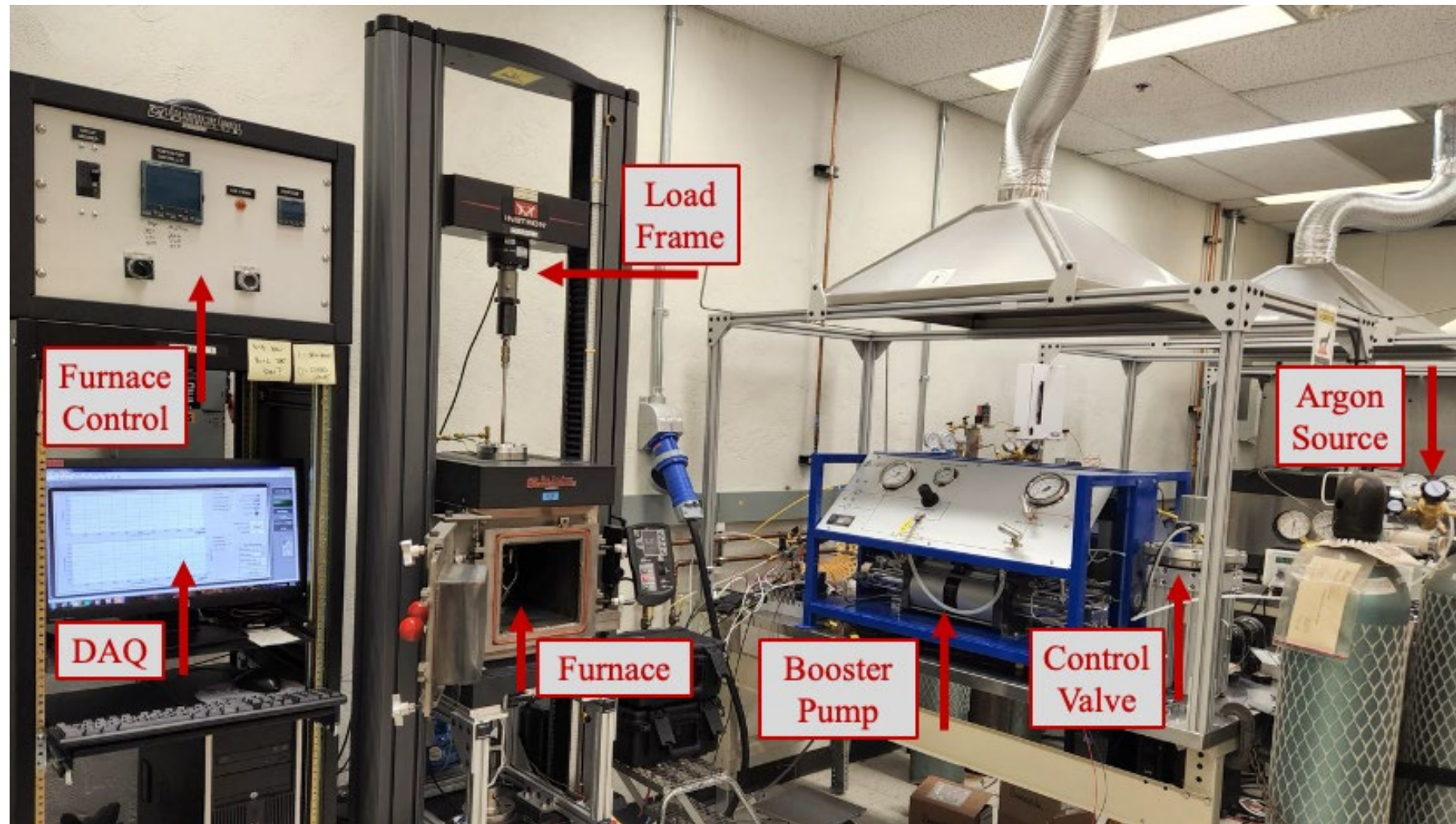


Mechanical Testing

- **Loading system**
 - Full tube axial tension
 - Internal pressure
- **Strain decomposition**
 - Axial and transverse extensometers
 - Plastic flow volume conservation

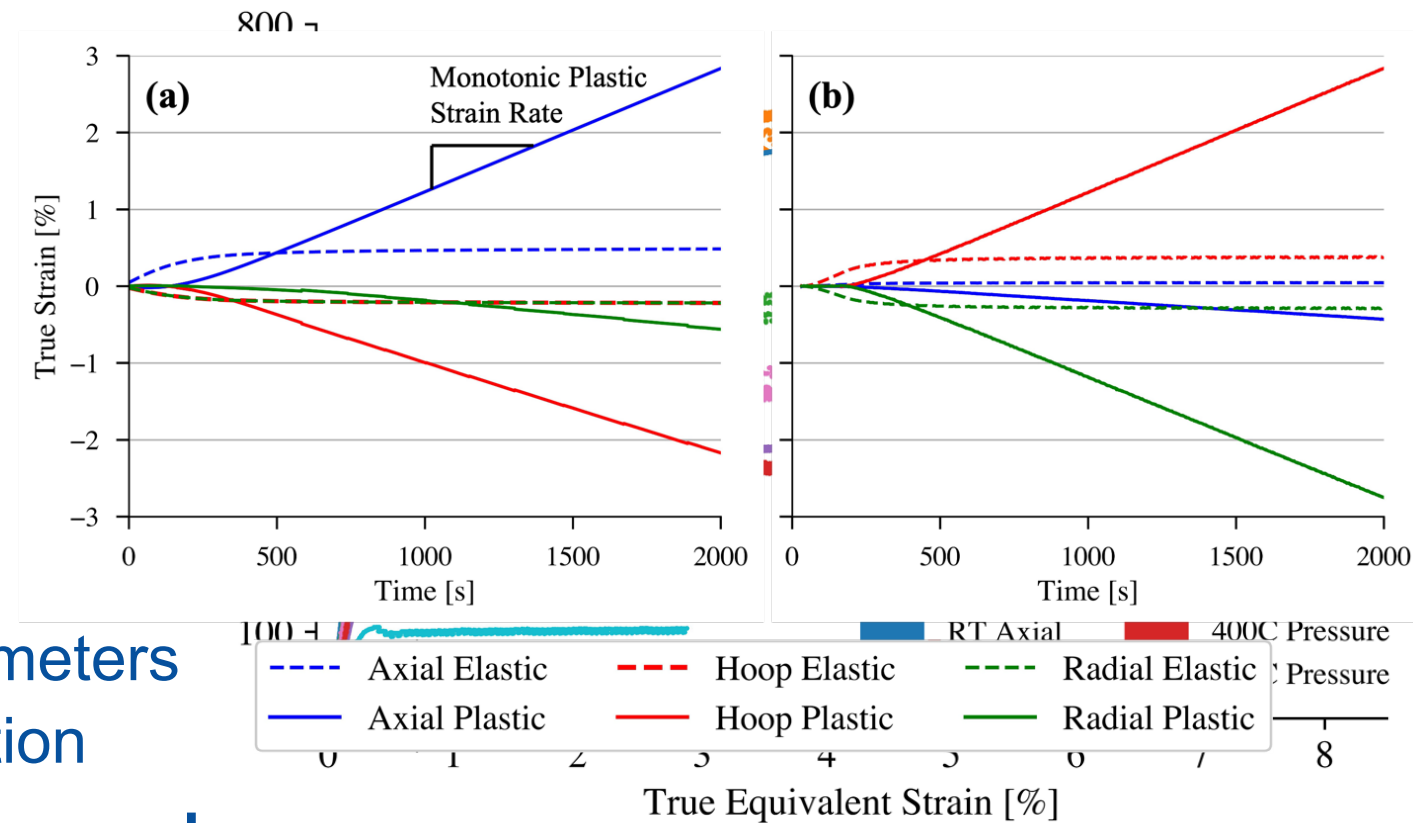


Mechanical Testing



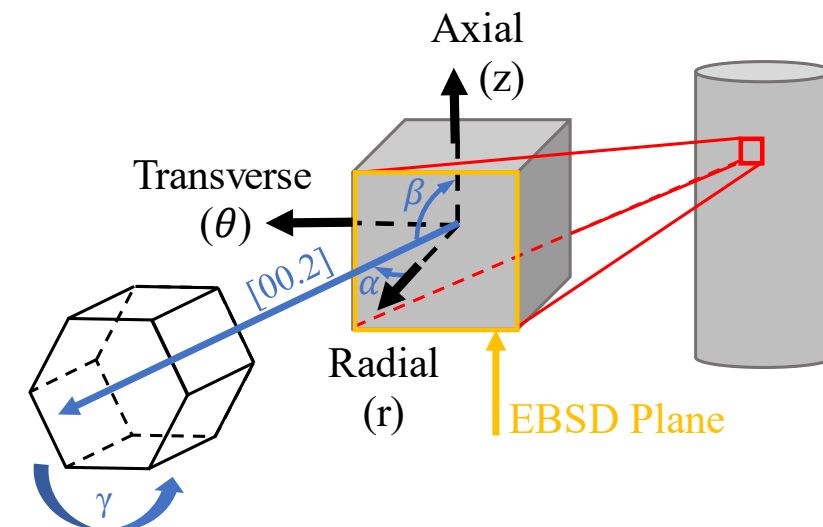
Mechanical Testing

- **Loading system**
 - Full tube axial tension
 - Internal pressure
- **Strain decomposition**
 - Axial and transverse extensometers
 - Plastic flow volume conservation
- **Found internal pressure anisotropy decreases significantly between 275 and 400 °C**



Resolved Shear Stress (RSS) Analysis

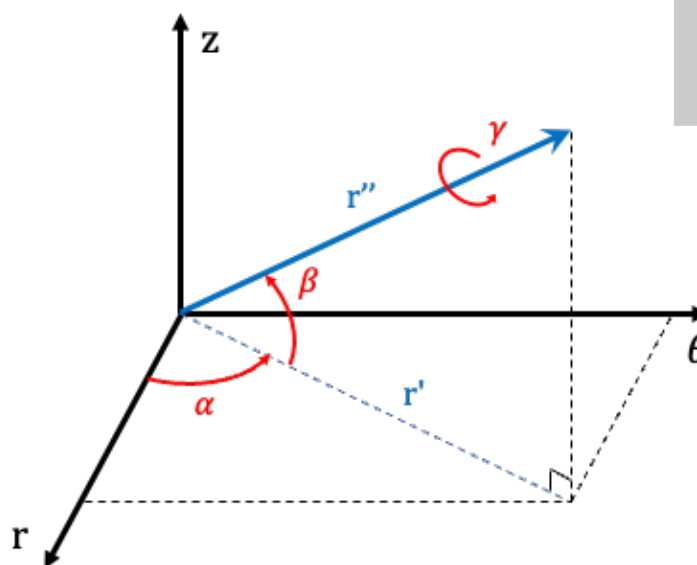
- **Use generalized Schmid factor (GSF)**
 - Normalized for any stress magnitude
 - Generalized to multiaxial stresses
- **Calculate SF on primary glide planes**
- **Evaluate SF for different orientations**
- **Project using basal $\langle a \rangle$ pole figures**



Rotation matrix

$$\text{GSF} = \hat{\mathbf{b}} \cdot \mathbf{g} \cdot \boldsymbol{\sigma} \cdot \mathbf{g}^T \cdot \hat{\mathbf{n}}$$

Slip direction Applied stress Glide plane normal



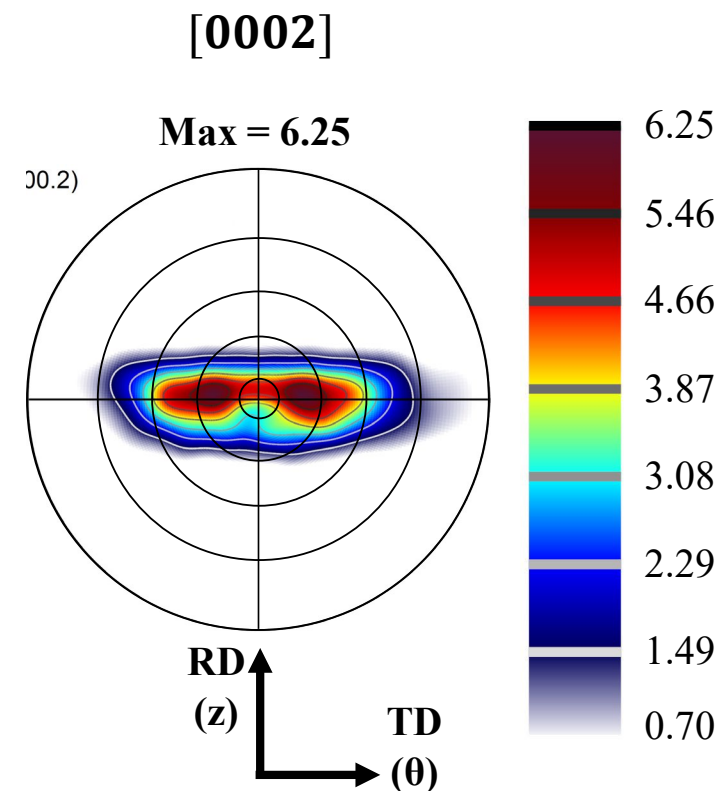
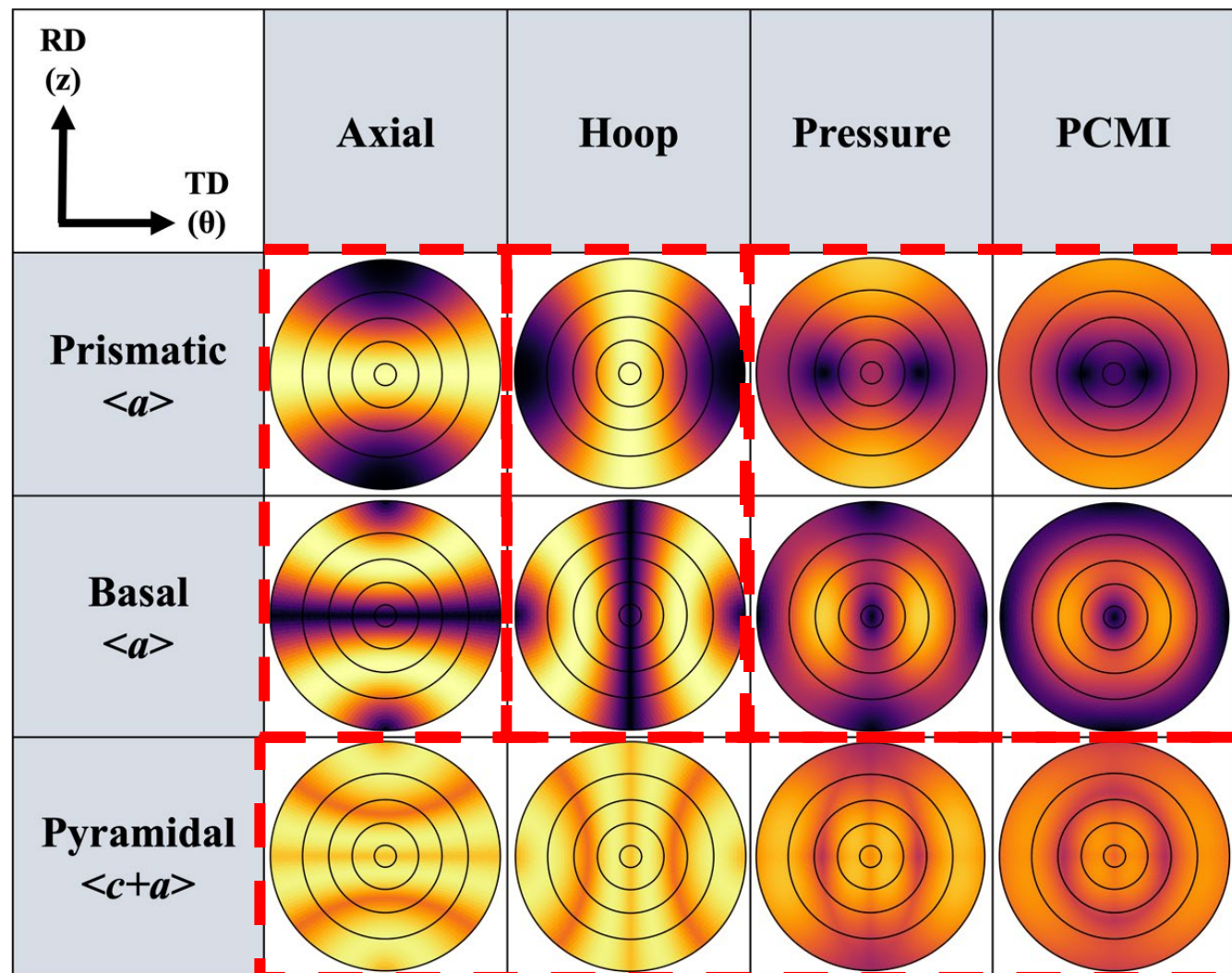
Hexagonal
unit cell

Orthogonal
unit cell

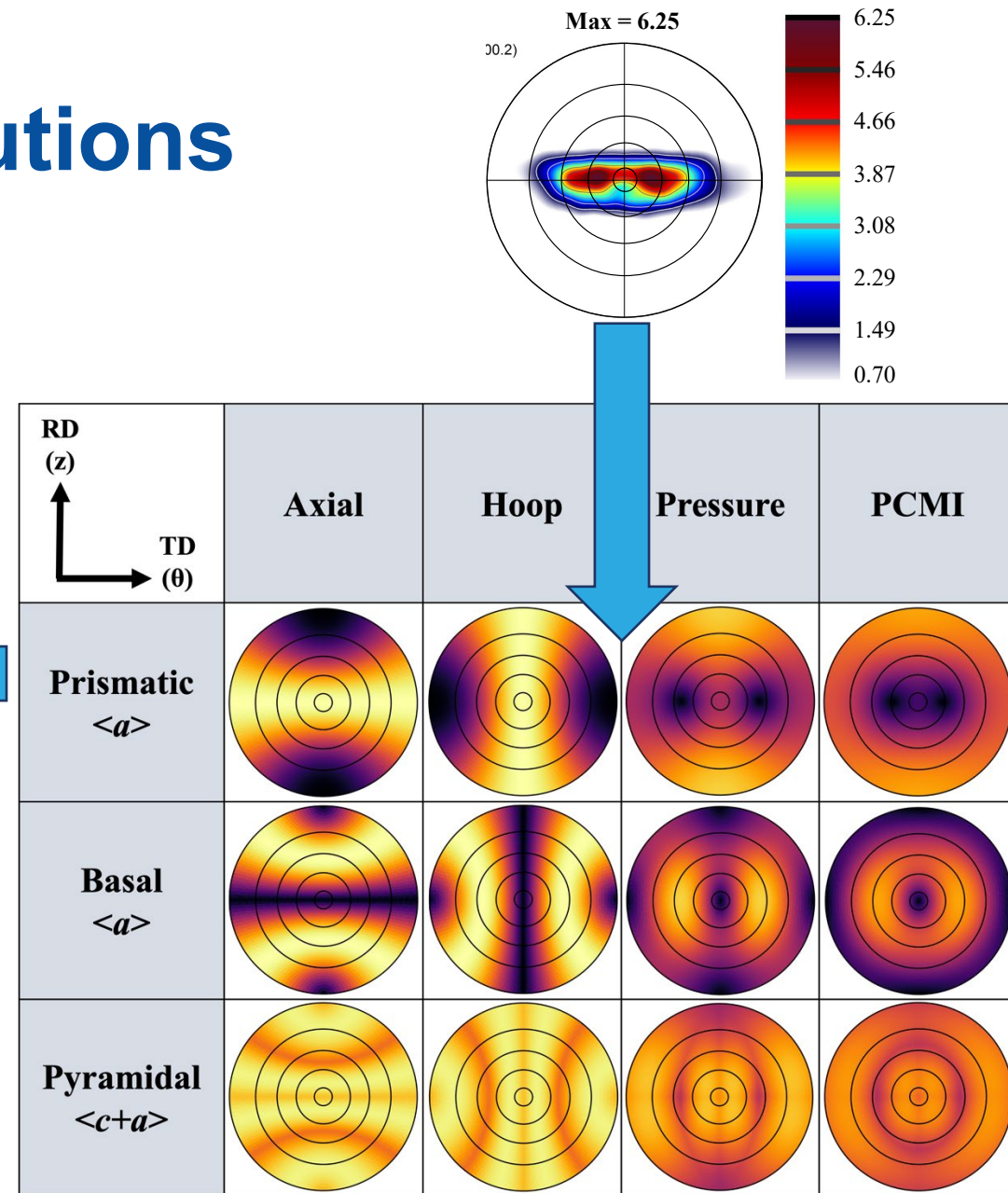
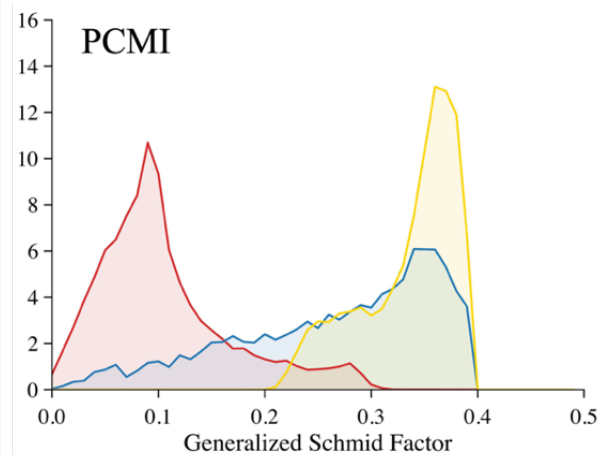
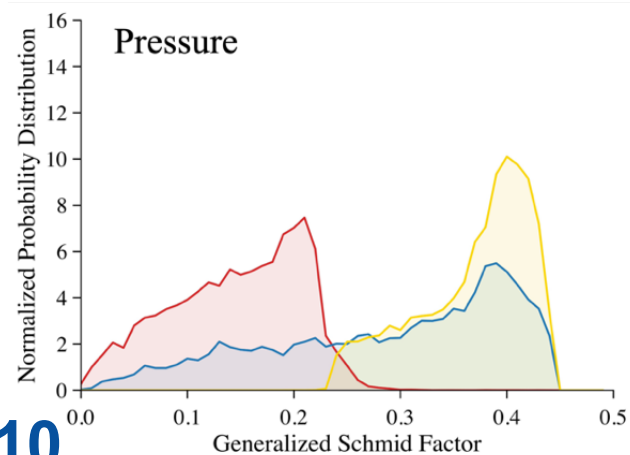
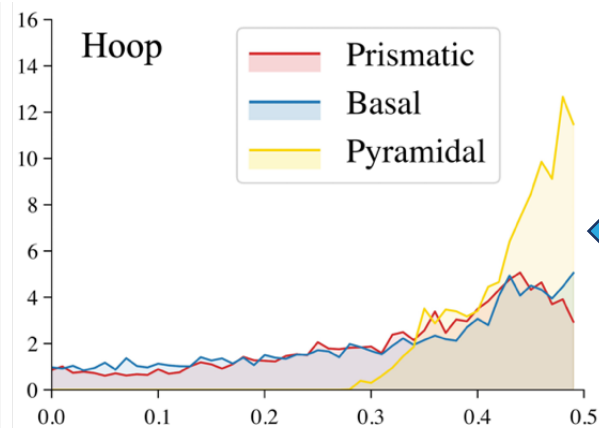
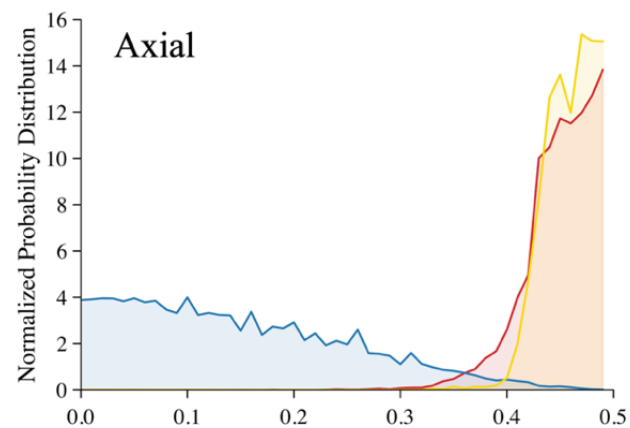
Engineering
geometry

RSS Analysis Results

- Max RSS for slip directions displayed



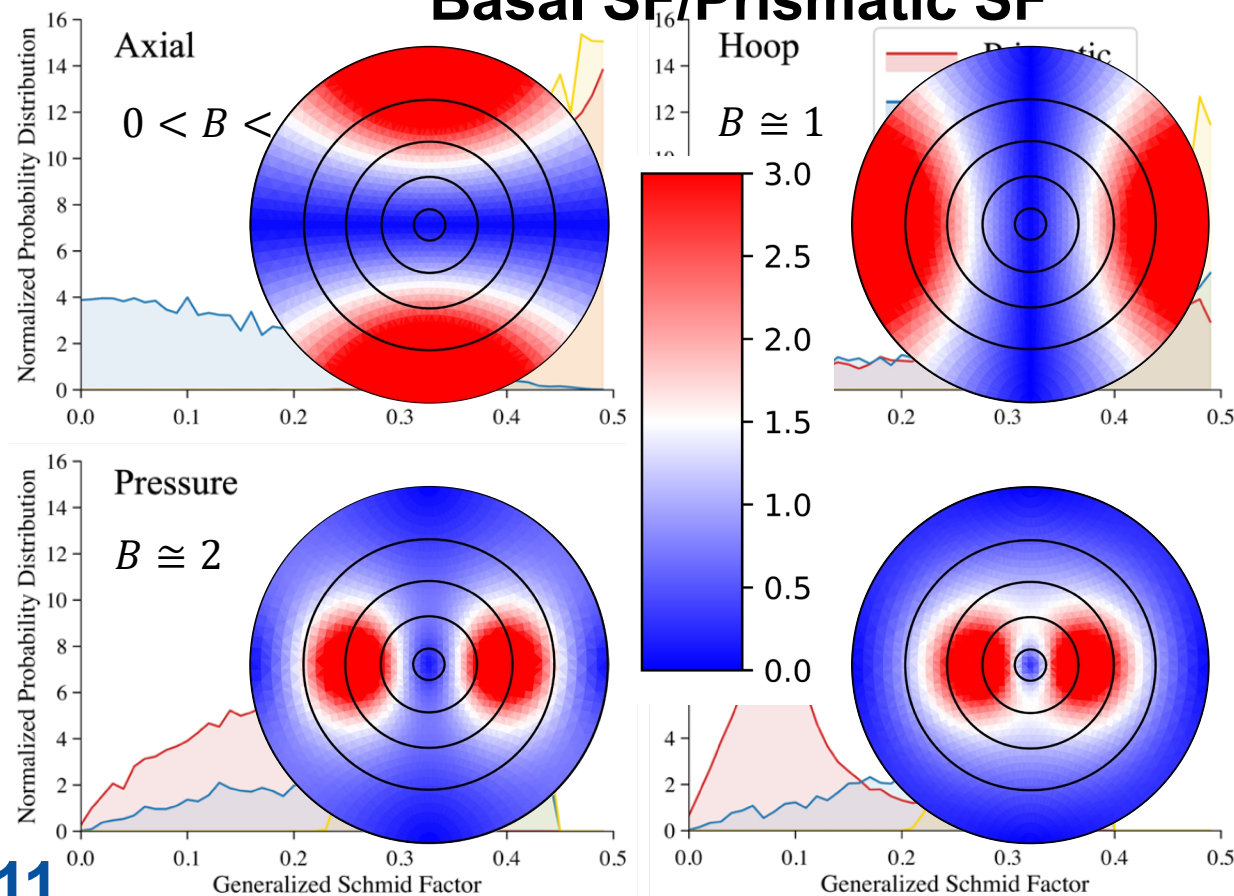
Microstructure RSS Distributions



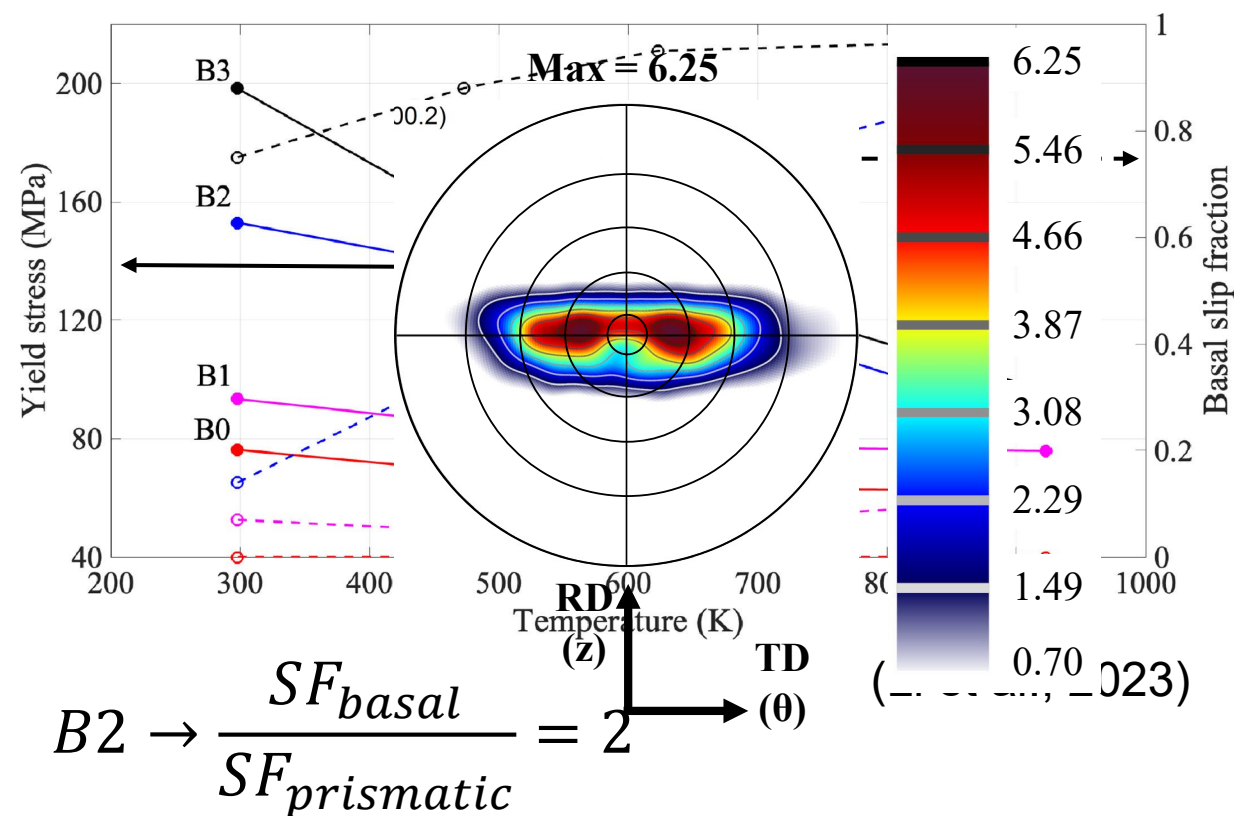
Schmid Factor Ratios

- Basal $\langle a \rangle$ activity increases temperature dependence

Basal SF/Prismatic SF



Discrete dislocation dynamics simulations of single crystal Zr

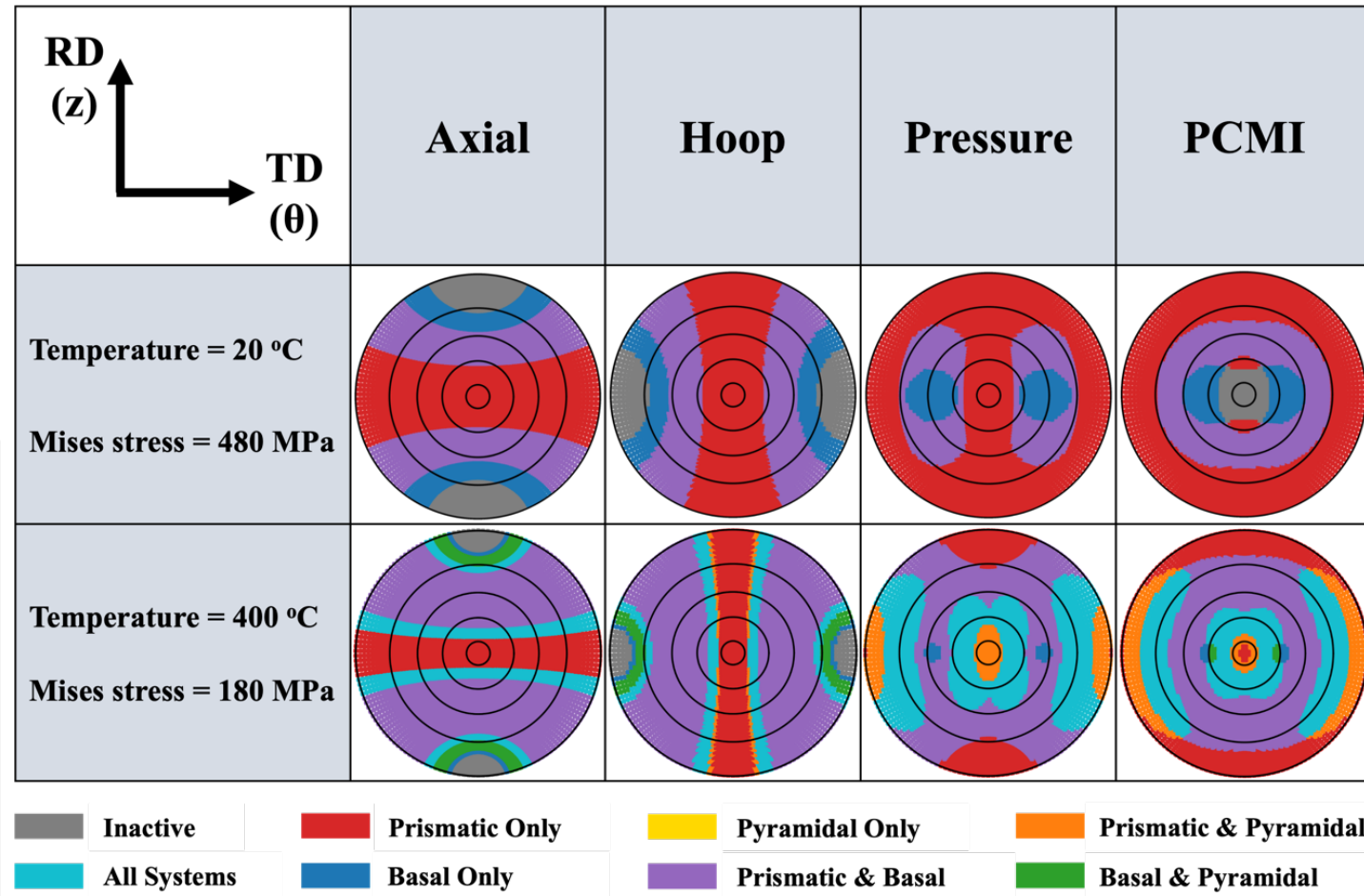
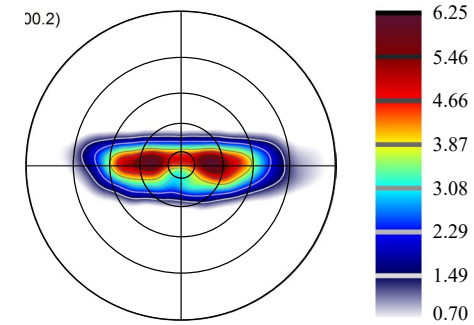
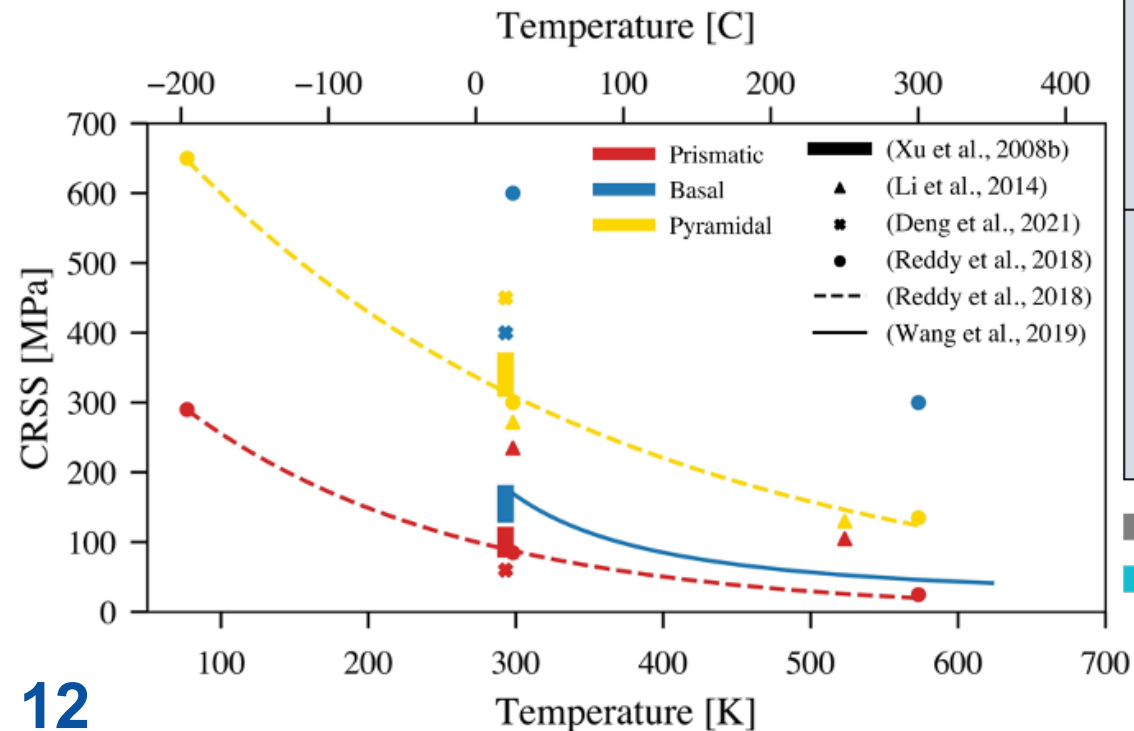


$$B2 \rightarrow \frac{SF_{basal}}{SF_{prismatic}} = 2 \rightarrow \text{TD} (\theta)$$

Temperature Dependent Activation

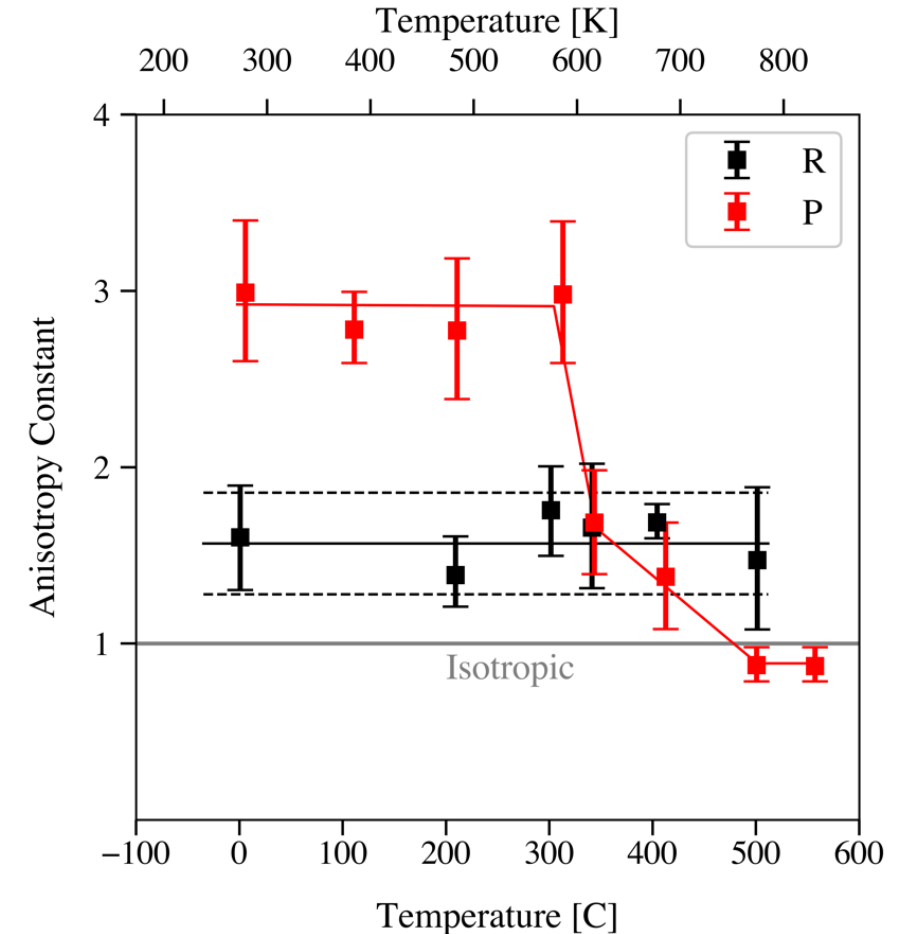
- Critical-RSS (CRSS) ratio decreases with temperature

$$RSS - CRSS(T) = \begin{matrix} + \text{ active} \\ - \text{ inactive} \end{matrix}$$



Conclusions

- **Axial stress produces:**
 - High SF on prismatic $\langle a \rangle$ systems
 - Low SF on basal $\langle a \rangle$ systems
 - Dominant prismatic $\langle a \rangle$ slip activity
 - Temperature independent mechanical anisotropy
- **Hoop stress produces:**
 - Mixed SF on prismatic $\langle a \rangle$ systems
 - Mixed SF on basal $\langle a \rangle$ systems
 - Competitive basal $\langle a \rangle$ and prismatic $\langle a \rangle$ slip activity
 - Temperature dependent mechanical anisotropy
- **Biaxial stress states produce:**
 - Low SF on prismatic $\langle a \rangle$ systems
 - High SF on basal $\langle a \rangle$ systems
 - Competitive basal $\langle a \rangle$ and prismatic $\langle a \rangle$ slip activity
 - Temperature dependent mechanical anisotropy



(Wang & Murty, 1998)

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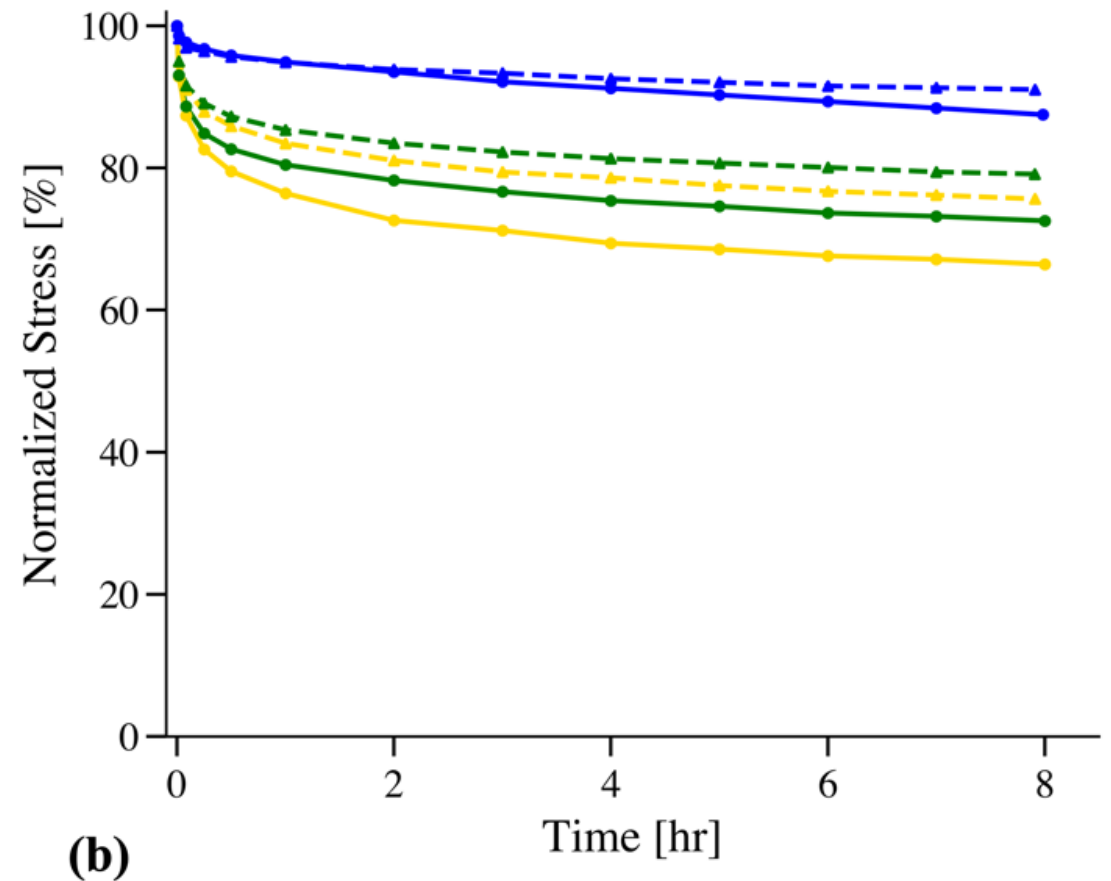
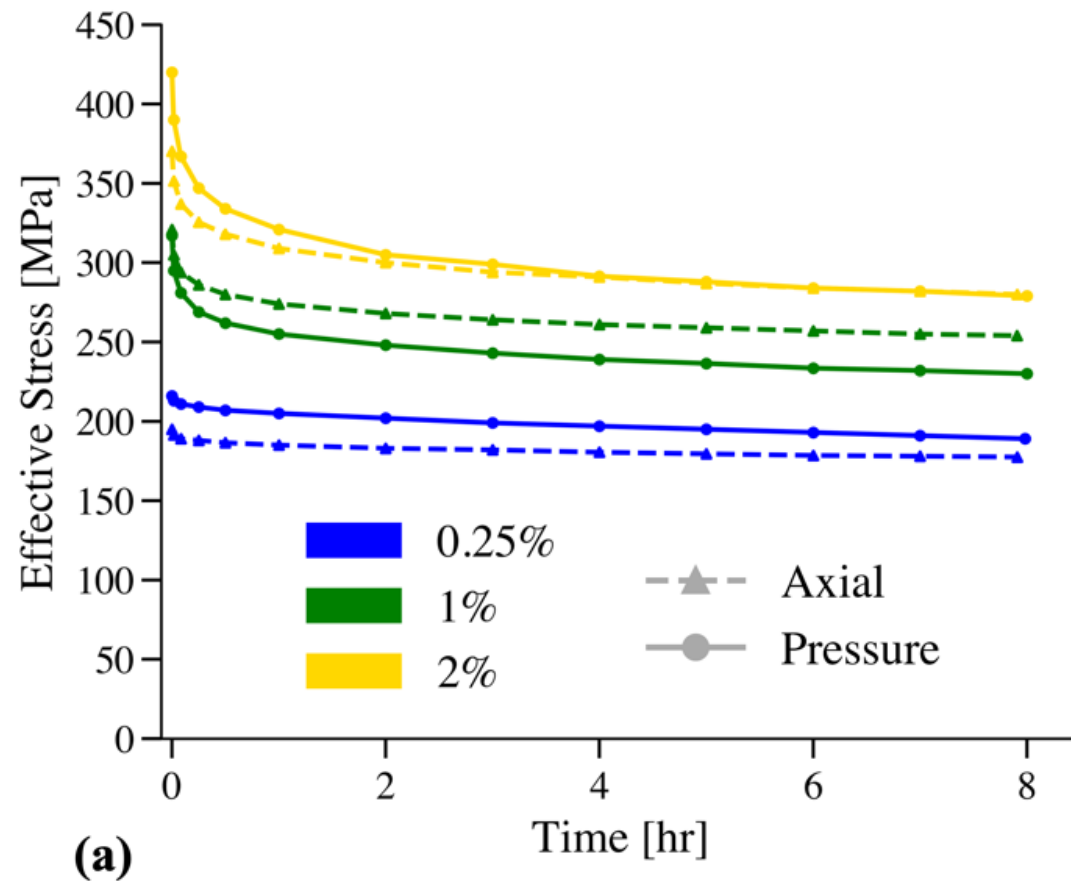


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Future Work – Effect on Stress Relaxation



Activation Volume Analysis

Preliminary Results

