

Electrorefiner Speciation and Phase Model for Prediction of Operation Lifetime

March 2024

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Electrorefiner Speciation and Phase Model for Prediction of Operation Lifetime

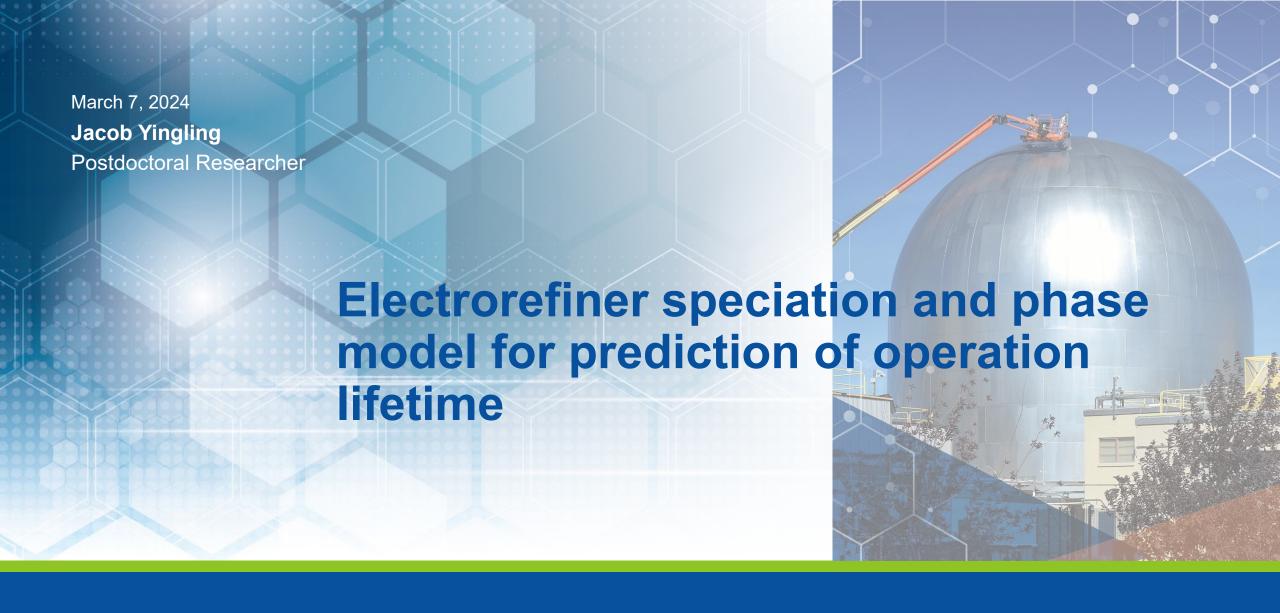
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About the Presenter

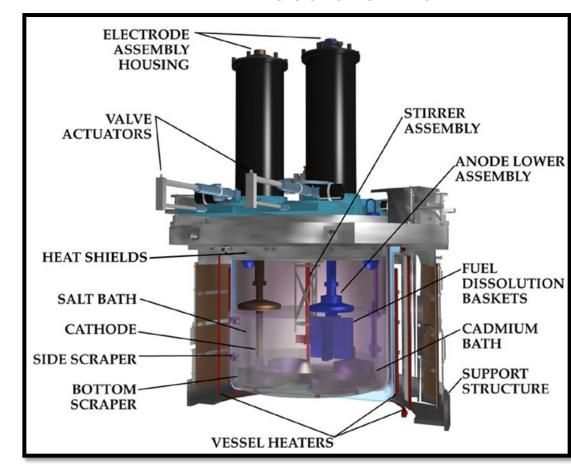
- Jacob A. Yingling, Postdoctoral research associate, Ph.D.
- Thermodynamics via computation of phase diagrams (CALPHAD)
- Veteran Naval Officer (Nuclear Power Training)
- Fuel salt synthesis for the Molten Chloride Reactor Experiment
- Thermodynamics in support of pyrochemical processing of used nuclear fuels
- Collaborators
 - Idaho National Laboratory: Toni Karlsson, Tae-Sic Yoo, Guy Fredrickson,
 - University of South Carolina: Juliano Schorne-Pinto, Jorge Palma, Clara Dixon
- Jacob.Yingling@inl.gov



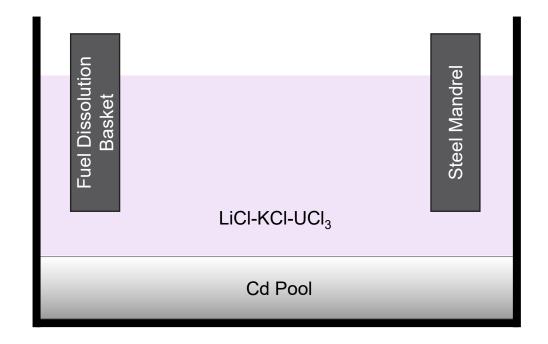
Historical context: EBR-II

- Na cooled fast breeder (1964-1994)
 - Stainless steel clad, Na bonded metallic fuel
 - Facility power and testing of fast reactor fuels
- Integral Fast Reactor prototype intended to demonstrate reprocessing
 - Changed to a Pu disposition strategy with recovery of U
 - Challenging since fission yield produces a wide distribution of elements
- IFR reprocessing equipment repurposed to processing of EBR-II driver fuel

Mk-IV Electrorefiner



Mark IV Electrorefiner



Modes of Operation

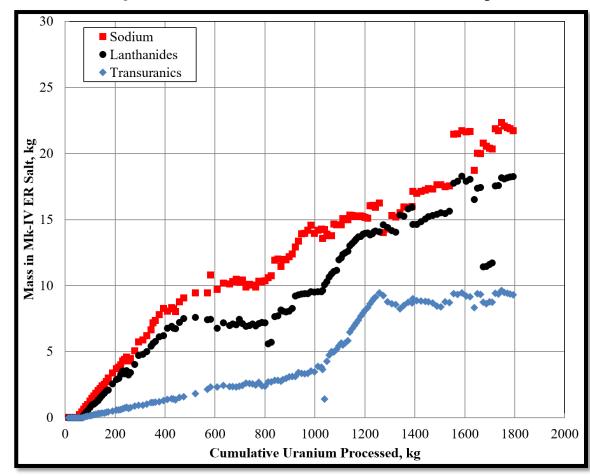
C 11	Anode						
Cell Configurations	FDBs	Cadmium Pool					
Cathode Steel mandrel Cadmium pool	Direct transport Anodic dissolution	Deposition Trivial					

- Used fuel can be transported to the steel mandrel directly or indirectly
 - Cd as secondary electrode
 - Cd as intermediate electrode
- Complex distribution of species present within electrolyte and Cd pool
 - Significant material balance challenge

Progressive accumulation of chlorides

- LiCl-KCl-UCl₃ electrolyte
- Oxidation of impure uranium and elements more electropositive
- Reduction of highly pure uranium
- Other elements remain in electrolyte
- 500°C max operating temperature
- Accumulation of NaCl steadily increases the melting point (801°C)

Species Accumulation in Electrolyte



Which Species Matter?

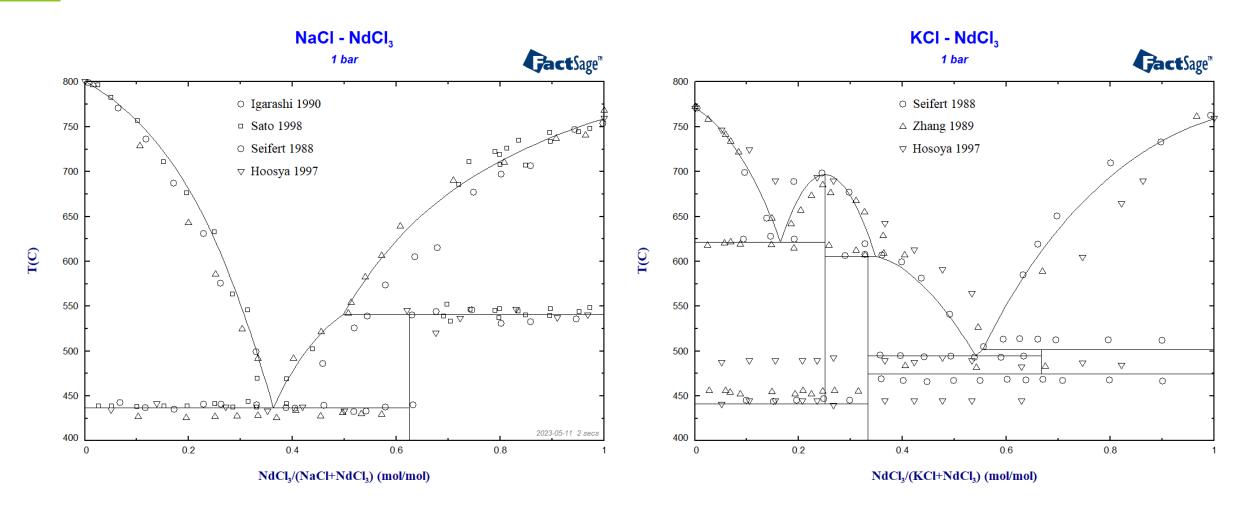
Compound	NaCl	UCI3	LiCl	NdCl3	PuCl3	CsCl	CeCl3	BaCl2	LaCl3	PrCl3	SmCl3	SrCl2	YCI3	RbCl	NpCl3	EuCl3	GdCl3
KCI	0.109	0.078	0.220	0.038	0.020	0.004	0.017	0.005	0.005	0.005	0.004	0.001	0.001	0.000	0.000	0.000	0.000
NaCl	0.000	0.040	0.083	0.023	0.014	0.004	0.012	0.004	0.004	0.004	0.003	0.001	0.001	0.000	0.000	0.000	0.000
UCI3		0.000	0.061	0.022	0.013	0.003	0.012	0.004	0.004	0.004	0.003	0.001	0.001	0.000	0.000	0.000	0.000
LiCI			0.000	0.032	0.017	0.004	0.015	0.004	0.005	0.004	0.003	0.001	0.001	0.000	0.000	0.000	0.000
NdCl3				0.000	0.009	0.003	0.009	0.003	0.003	0.003	0.003	0.001	0.001	0.000	0.000	0.000	0.000
PuCl3					0.000	0.002	0.006	0.003	0.003	0.003	0.002	0.001	0.001	0.000	0.000	0.000	0.000
CsCl						0.000	0.002	0.001	0.001	0.001	0.001	0.000	0.001	0.000	0.000	0.000	0.000
CeCl3							0.000	0.002	0.003	0.002	0.002	0.001	0.001	legli	gible	0.000	0.000
BaCl2								0.000	0.001	0.001	0.001	0.000	0.001	0.000	0.000	0.000	0.000
LaCl3									0.000	0.001	0.001	0.000	0.001	0.000	0.000	0.000	0.000
PrCl3										0.000	0.001	0.000	0.001	0.000	0.000	0.000	0.000
SmCl3											0.000	0.000	0.001	0.000	0.000	0.000	0.000
SrCl2					Dup	licat	650					ACI -	$-BCl_a$				0.000
YCI3					0.00d	0.000	0.000		E		- x'(1)			([']) a	~/][~ ·	_v 1	0.000
RbCl									Γ	contrib	=x'(1	. — x j	$ax_{\rm p}$	() + u	$X \mid [X_A]$	ι_B]	0.000
NpCl3												x' = -	ax_B				0.000
EuCl3												<u>a</u>	$x_B + x$	A			0.000
GdCl3	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

Contribution parameter calculated as the weighted average of binary Førland fractions → weighted asymmetric contributions

Thermochemical Modeling

- Models based on Molten Salt Thermal Properties Database Thermochemical (MSTDB-TC)
 - Modified quasi-chemical model in quadruplet approximation $(A-X-A)+(B-X-B)=2(A-X-B) o\Delta G_{AB/X}$
- Model developer chooses parameterization of $\Delta G_{AB/X}$ =A+BT+CTInT+D/T+...+
- Accounts for short-range ordering of non-ideal Gibbs energy contributions
- Order of importance: KCl, LiCl, NaCl, UCl₃, NdCl₃, PuCl₃ ...
 - NdCl₃ systems not included in MSTDB-TC v2.0 and earlier
- Assessed systems: ACI-NdCl₃ (A=Li,Na,K,Cs)
 - Model parameterization constrained based on available experimental data
 - Optimized using experimental weights for phase equilibria, and enthalpy of mixing

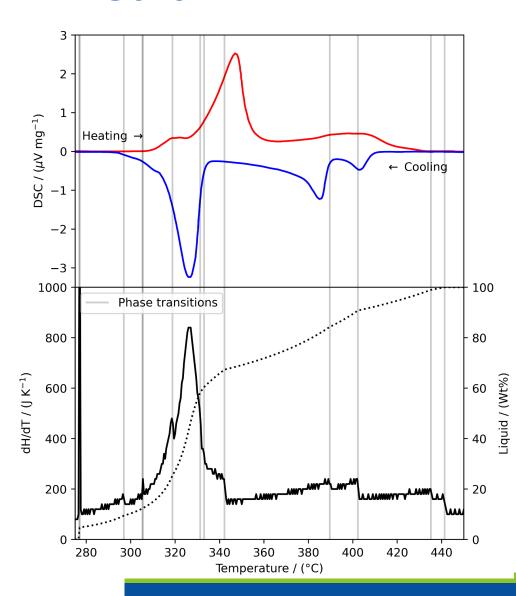
Selected calculated phase diagrams



Fitting data includes phase equilibria, $\Delta_{mix}H$, and ΔH_{298}^o $\Delta G_{AB/X}$ =A+BT+CTInT+D/T+...+ reduced to A+BT or less for each eutectic

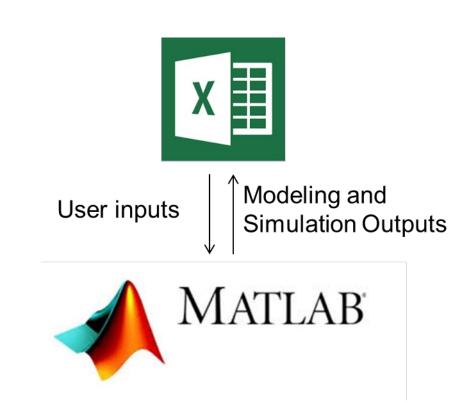
Thermal measurements of Mk-IV salt

- Differential Scanning Calorimetry heating and cooling at 5C/min
- MSTDB-TC v3.1 (pre-release)
 - Includes ACI-NdCl₃ models developed in this work
- Calculated equilibrium transitions and solution enthalpy
- DSC minus background compares well to calculated dH/dT
- Calculated transition temperatures appear to agree very well with thermal measurements.



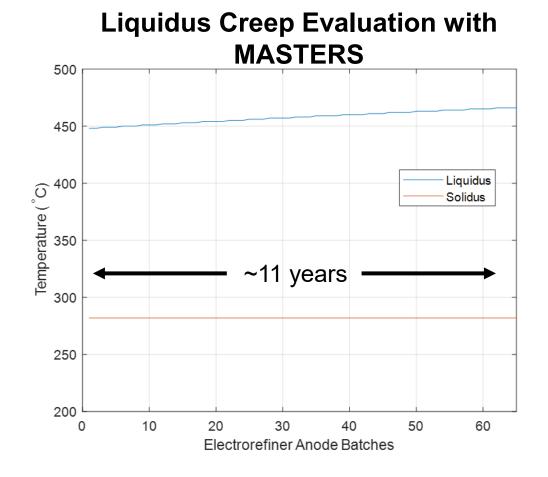
MASTERS (Modeling And Simulation Tool for Electrochemical Recycling Systems)

- MASTERS based on MatLab and Microsoft Excel
- Recent Python interface addition for Factsage/Chemapp
- Tracks over over 1000 isotopes
- Flexible code system to simulate various fuel processing scenarios



Strategies to minimize liquidus creep

- Dilute with LiCl-KCl
- Extract NaCl
- Extract TRU
- Extract Lanthanides
- ER operation in 2-phase region
- All options can be studied with MASTERS. A draft documenting selected strategy evaluation with MASTERS is underway



Conclusions

- MQMQA is a highly effective tool for evaluating many component salts
- Pseudo-binary models developed for the LiCl-NdCl₃, NaCl-NdCl₃, KCl-NdCl₃, CsCl-NdCl₃ salts
- Models contributed to MSTDB-TC
- Mk-IV ER operation may continue for several years without salt processing
- Missions beyond EBR-II driver fuel processing will require strategies for mitigating liquidus increase

Questions?



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